# CH4010 Assignment-1: Targetting

#### Given stream data:

Stream No.	Туре	Heat Capacity* Flow Rate	Supply Temperature	Target Temperature	
		kW / K	°C	°C	
1	Hot	2.1	180	40	
2	Hot	4	150	40	
3	Cold	3	60	180	
4	Cold	2.6	30	130	

Since  $(\Delta T)_{min} = 9$  degrees C (even roll number), we can shift the hot stream below by 9/2 = 4.5 degrees and the cold stream above by 4.5 degrees. This results in:

#### Modified stream data:

Stream No.	Туре	Heat Capacity* Flow Rate kW / K	Supply Temperature	Target Temperature °C	
		-	_		
1	Hot	2.1	175.5	35.5	
2	Hot	4	145.5	35.5	
3	Cold	3	64.5	184.5	
4	Cold	2.6	34.5	134.5	

## Part-1: Pinch-point, $Q_c$ , $Q_H$ and composite curves

Using the problem table algorithm, one can arrive at the following table:

	2.1	4	3	2.6	$\Sigma$ (FC <sub>p, hot</sub> ) (in kW/C)	$\Sigma(FC_{p, cold})$ (in kW/C)	ΔT (in C)	ΔH (in kW)	q <sub>transfer</sub> (in kW)
184.5	0	0	1	0	0	3	9	27	0
175.5	1	0	1	0	2.1	3	30	27	-27
145.5	1	1	1	0	6.1	3	11	-34.1	-54
134.5	1	1	1	1	6.1	5.6	70	-35	-19.9
64.5	1	1	0	1	6.1	2.6	29	-101.5	15.1

35.5	0	0	0	1	0	2.6	1	2.6	116.6
34.5	0	0	0	0	0	0			114

We can see the lowest  $q_{transfer}$  is -54 kW. So if we provide a heating of 54 kW, all heat transfers will be non-negative (and hence heat won't flow from lower temperature to higher temperature).

	2.1	4	3	2.6	Σ (FC <sub>p, hot</sub> )	$\Sigma(FC_{p, cold})$	ΔΤ	ΔΗ	q <sub>transfer</sub> (in kW)
					(in kW/C)	(in kW/C)	(in C)	(in kW)	
184.5	0	0	1	0	0	3	9	27	54
175.5	1	0	1	0	2.1	3	30	27	27
145.5	1	1	1	0	6.1	3	11	-34.1	0
134.5	1	1	1	1	6.1	5.6	70	-35	34.1
64.5	1	1	0	1	6.1	2.6	29	-101.5	69.1
35.5	0	0	0	1	0	2.6	1	2.6	170.6
34.5	0	0	0	0	0	0			168

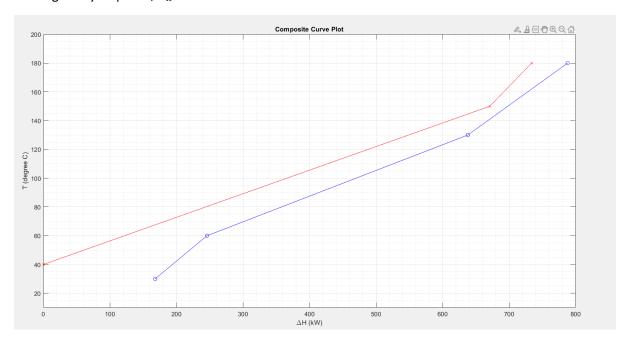
Hence from the above Problem Table we obtain the following:

**Pinch point:** i) cold stream pinch =  $145.5^{\circ}$  C -  $4.5^{\circ}$  C =  $141^{\circ}$  C

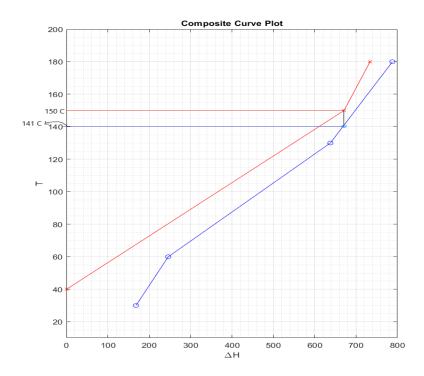
ii) hot stream pinch =  $145.5^{\circ} \text{C} + 4.5^{\circ} \text{C} = 150^{\circ} \text{C}$ 

Heating utility required, Q<sub>h</sub> = **54 kW** 

Cooling utility required,  $Q_c = 168 \text{ kW}$ 

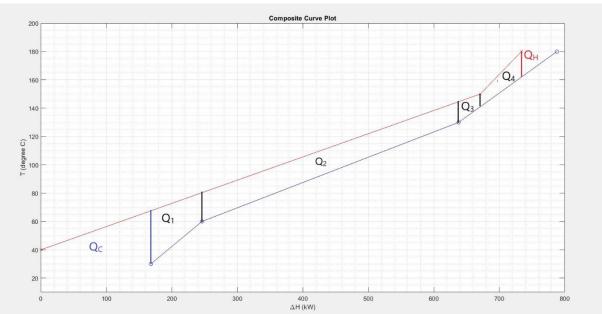


Plot 1a): Composite curves. Red: hot curve; blue: cold curve



Plot 1b): Composite curves with the pinch point marked. Red: hot curve; blue: cold curve





**Plot 2:** Showing different parts of the system where heat exchangers have to be used.

34:5-48/14 CH4010 ASSIGNMENT - 1 CH18B025 2. AREA TARGETTING control. First, let's start from finding out and a requirement of cooler. Assume that the arrange het travelue coefficient 1 U= 0.001 knowlike = | kW|m2 Q = AULMTD ⇒ A = Q Griner that Ux LMTD. part - 1: Assume the cooling water heats up from a temperature of 15°C to 30°; That entry = That least + T= 67.541 Hot stream (#1+ Hz) A1 = 67.74 17341 (F9 = Z-1+4 KW/K) 63 X 0.00 (X LMT) 15 Water LMTD = (67.541-30)  $ln\left(\frac{67.541-30}{40-15}\right)$ => LMTD = 30.8468° 0.001×10 × 30.84 +8 = 5.446 m² · . A 1 = 168 part - 2: Framplemons step From Lane 2.1 xWIK | C | (t-67.541) 6.1 = (60-30) (2-6) me (t-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31) (+-67.541)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = (60-31)6.1 = From grayh

$$Q = 2.6 (60 - 30) = 78 \text{ kW/K}$$

$$LMTQ = (80.328-60) - 167.541-30)$$

$$= 28.06°C$$

$$A = 78$$

$$0.001 \times 10^{3} \times 28.06 = 2.78 \text{ m}^{2}$$

$$T = 1000 \text{ for } 1000$$

ı

$$\frac{150}{140} = \frac{144.59}{140} = \frac{162}{140} = \frac{162}{140}$$

We can ourse that the see heating utility is Efeam and that it runs condenses at 300°C (only later theat) of Of = 54 kW i cold stream heated from 162 - 1803 LMTD = (180-300) X-(162-300) \_ 128.79.  $ln\left(\frac{300-180}{300-162}\right)$ 0.4193 A6= ~ 0.42 m2 Total dreaz E Ax 5.454 2.78 + 22.66 + 2.85 +4.85 +0.42 39.0073 m² Area target = 39.01 m² Above pinch, S = 1 hot + 1 old - 1 whiley .: No J herchangers = 3 Al 5-1 2 enelogy

Blow pinh 1 no of streams, 3 = 2 hot +2 cold + 1 whility of 45 Hears No of enchanges = \$-1 = 5-1 = 4 enchangery Minimum musker of heat entrages = 2 akers topale wints him 3 Min no. Junits = [6] heat entropys Steam Wt = \(\frac{7}{20000}\times \times \h = 120000 \times 54\times 10^{-3} Cost Target 6 480 rupers/year Water cot = 10000 x Qc = 10 + 168 x 10 Capital cost = 6x (4000 of 500 forget are) = 6x (40000 + 800x 39.0073) = = 259503.7 Annalystian factor = 0.25

+ Steel Cost = Annulaisatus faut x Capital Cast

+ Utillity Costs

- 0.25 x (259803.7)

+ 1680 + 6480

= 273035.917 / year

= 273036./year

1

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```

clear; close all;

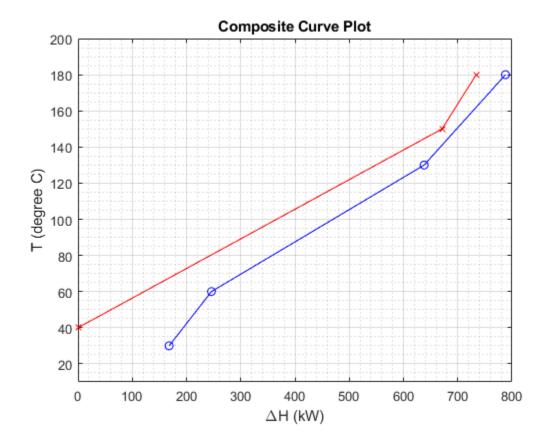
### Initialise values

```
Tpinch_hot = 150;
FCphot = [6.1,2.1];
hot_slopes = 1./FCphot;
ThotChange = [40,150,180];
FCpCold = [2.6,5.6,3];
cold_slopes = 1./FCpCold;
TcoldChange = [30,60,130,180];
Qc = 168;
Qh = 54;
```

## Plot the graphs

```
x1 = 0;
xhot = x1;
yhot = [];
for i = 1:length(ThotChange)-1
    m = hot_slopes(i);
    y1 = ThotChange(i);
    yhot = [yhot y1];
    y2 = ThotChange(i+1);
    x2 = (y2-y1)/m + x1;
    plot([x1 x2],[y1 y2],'r',[x1 x2],[y1 y2],'rx')
    hold on;
    x1 = x2;
    xhot = [xhot x2];
end
yhot = [yhot y2];
grid on;
grid minor;
x1 = Qc;
xcold = [x1];
ycold = [];
for i = 1:length(TcoldChange)-1
    m = cold_slopes(i);
    y1 = TcoldChange(i);
    ycold = [ycold y1];
    y2 = TcoldChange(i+1);
```

```
x2 = (y2-y1)/m + x1;
plot([x1 x2],[y1 y2],'b',[x1 x2],[y1 y2],'bo')
hold on;
x1 = x2;
xcold = [xcold x2];
end
ycold = [ycold y2];
title("Composite Curve Plot");
xlabel("\DeltaH (kW)");
ylabel("T (degree C)");
%legend("hot stream","","cold stream","");
ylim([10,200]);
%hold off;
```



# **Calculating Qs**

```
X = [xhot xcold];
chngs = length(X);
X = sort(X);
Q = zeros(chngs-1,1);
LMTDs = Q;
Thexit = ThotChange(2);
Tcentry = TcoldChange(1);
U = 0.001;
Thentry = 40;
Tcexit = 30;
```

```
lmtd = @(Th1, Th2, Tc1, Tc2)(((Th2-Tc1) - (Th1-Tc2))/log((Th2-Tc1)/(Th1-Tc2))/log((Th2-Tc1)/(Th1-Tc2))/log((Th2-Tc1)/(Th1-Tc2))/log((Th2-Tc1)/(Th1-Tc2))/log((Th2-Tc1)/(Th1-Tc2))/log((Th2-Tc1)/(Th1-Tc2))/log((Th2-Tc1)/(Th1-Tc2))/log((Th2-Tc1)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Th1-Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(Tc2)/(T
Tc2)));
Ths = [];
Tcs = [];
for i = 1:chngs-1
               Q(i) = X(i+1)-X(i);
                if i ~= 1 && i~= chngs-1
                               Thexit = interp1(xhot,yhot,X(i));
                               Thentry = interp1(xhot,yhot,X(i+1));
                               Tcentry = interp1(xcold,ycold,X(i));
                               Tcexit = interp1(xcold,ycold,X(i+1));
                               LMTDs(i) = lmtd(Thentry, Thexit, Tcentry, Tcexit);
                               disp(LMTDs(i));
                                % Areas(i) = Q(i)/(LMTDs(i)*U);
                               Ths = [Ths Thexit];
                               Tcs = [Tcs Tcentry];
                end
               Thexit = Thentry;
               Tcentry = Tcexit;
end
LMTDs(1) = Imtd(Ths(1), ThotChange(1), 15, 30);
LMTDs(chngs-1) = lmtd(300,300,Tcexit,TcoldChange(4));
Areas = Q./(LMTDs*U)/10^3; % since Q is in kW; converting to MW
Area_target = sum(Areas);
            28.0600
            17.3007
            11.5709
            12.9843
```

### Costs

```
n_hex = length(Areas);
Capital = n_hex*(40000 + 500*Area_target/n_hex);
Steam = Qh*120000/10^3;% Qh is in kW; converting to MW
Water = Qc*10000/10^3; % Qc is in kW; converting to MW
Annul = 0.25;
cost_target = Capital*Annul + Steam + Water;
```

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