

Generalized Linear Phase

A filter with generalized linear phase has the following form

$$H(e^{j\omega}) = A(e^{j\omega})e^{-j\alpha\omega}e^{j\beta}$$

$A(e^{j\omega})$ is a real function of frequency

Theorem: A linear phase Real, Causal, Stable, Rational (RCSR) filter is necessarily FIR. The group delay of such a filter is half its order and satisfies either the symmetry or antisymmetric relation ($h[n] = \pm h[M-n]$).

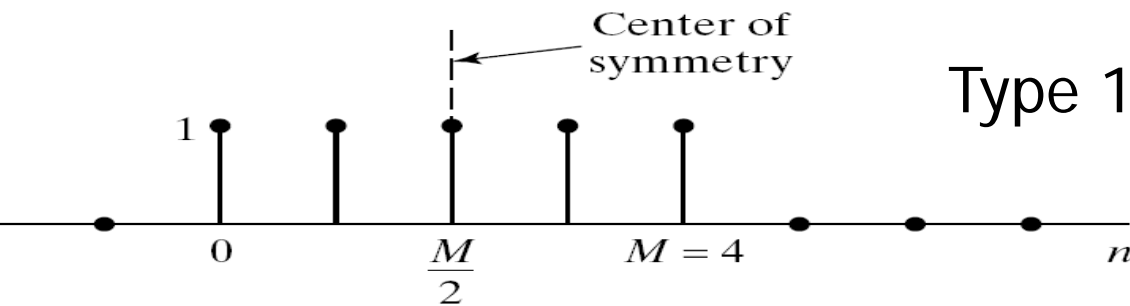
Generalized Linear Phase Filters

We will consider the design of Finite Impulse Response (FIR) filters with real impulse response

$$H(z) = \sum_{n=0}^M h[n]z^{-n}$$

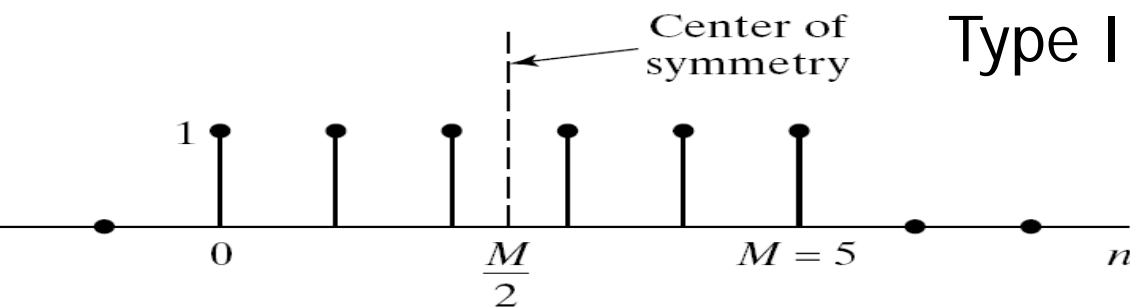
Four types of linear phase FIR filters.

- Type I $h[n] = h[M - n]$, M even
- Type II $h[n] = h[M - n]$, M odd
- Type III $h[n] = -h[M - n]$, M even
- Type IV $h[n] = -h[M - n]$, M odd



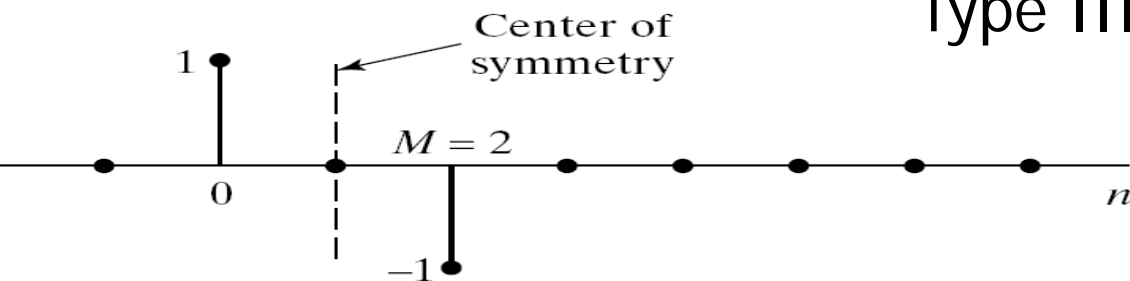
(a)

Type 1, M even, $h[n] = h[M-n]$



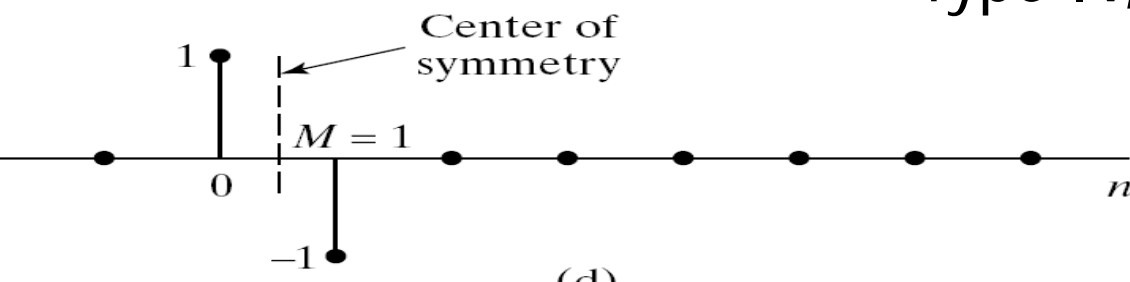
(b)

Type II, M odd, $h[n] = h[M-n]$



(c)

Type III, M even, $h[n] = -h[M-n]$



(d)

Type IV, M odd, $h[n] = -h[M-n]$

Zeros of Linear Phase FIR Filters

For Type I and II FIR Filters $H(z) = z^{-M} H(z^{-1})$

- Type II: M odd (Proof)

$$\begin{aligned} H(z) &= \sum_{n=0}^M h[n]z^{-n} = \sum_{n=0}^{\frac{M-1}{2}} h[n]z^{-n} + \sum_{n=\frac{M+1}{2}}^M h[n]z^{-n} \\ &= \sum_{n=0}^{\frac{M-1}{2}} h[n]z^{-n} + \sum_{n=0}^{\frac{M-1}{2}} h[M-n]z^{-(M-n)} \\ &= \sum_{n=0}^{\frac{M-1}{2}} h[n](z^{-n} + z^{-M+n}) = z^{-M} H(z^{-1}) \end{aligned}$$

- Type I: M even can be shown similarly

$$H(z) = \sum_{n=0}^L h[n](z^{-n} + z^{-(M-n)}), L = \frac{M-1}{2}$$

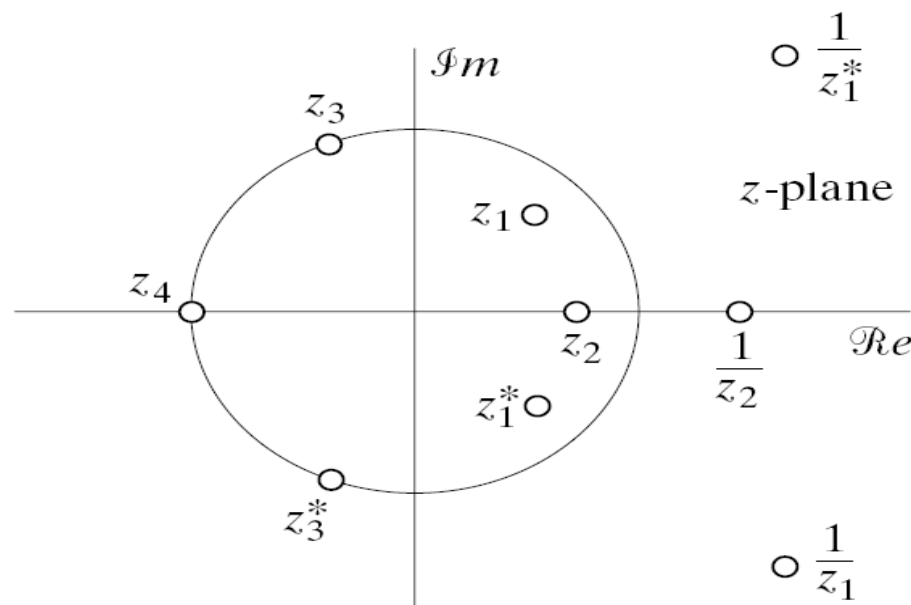
$$z^{-M}H(z^{-1}) = z^{-M} \sum_{n=0}^L h[n](z^n + z^{M-n}) = \sum_{n=0}^L h[n](z^{-(M-n)} + z^{-n}) = H(z)$$

Zeros of Linear Phase FIR Filters Cont'd

- For Type III and Type IV filters

$$H(z) = -z^{-M} H(z^{-1})$$

- NOTE: if z_i , is a zero of system $H(z)$, then $1/z_i$ is a zero of $H(z)$. True for all four types.



More on the Zeros

- Type I and Type II: Since $H(z) = z^{-M} H(z^{-1})$

$$H(-1) = (-1)^{-M} H(-1)$$

- For Type II filters, M odd and hence $H(-1)=0$. Therefore, for Type II systems, $z=-1$ (or $\omega = \pi$) is a zero of $H(z)$.

More on the Zeros (cont.)

Type III and IV: Since $H(z) = -z^{-M} H(z^{-1})$

$$H(1) = -(1)^{-M} H(1)$$

and

$$H(-1) = -(-1)^{-M} H(-1)$$

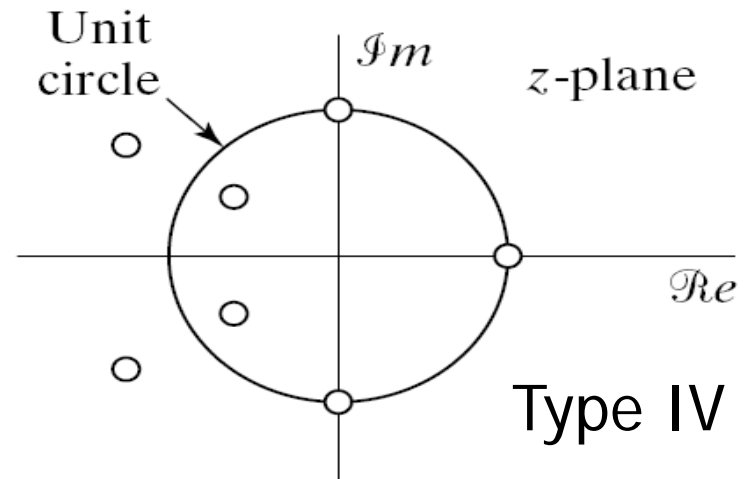
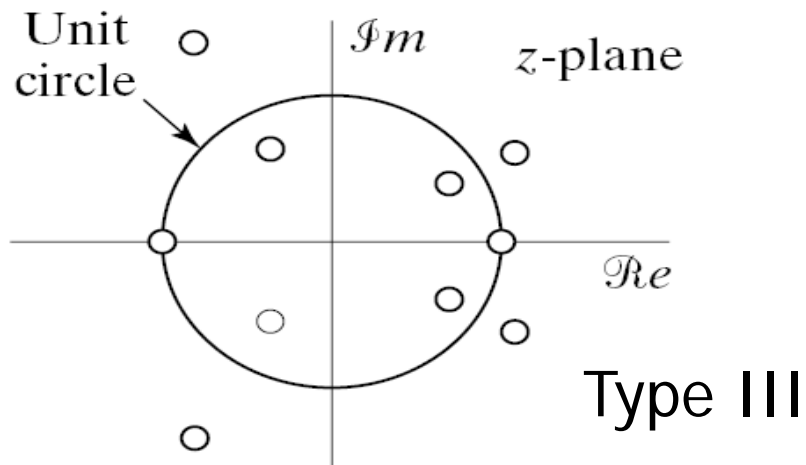
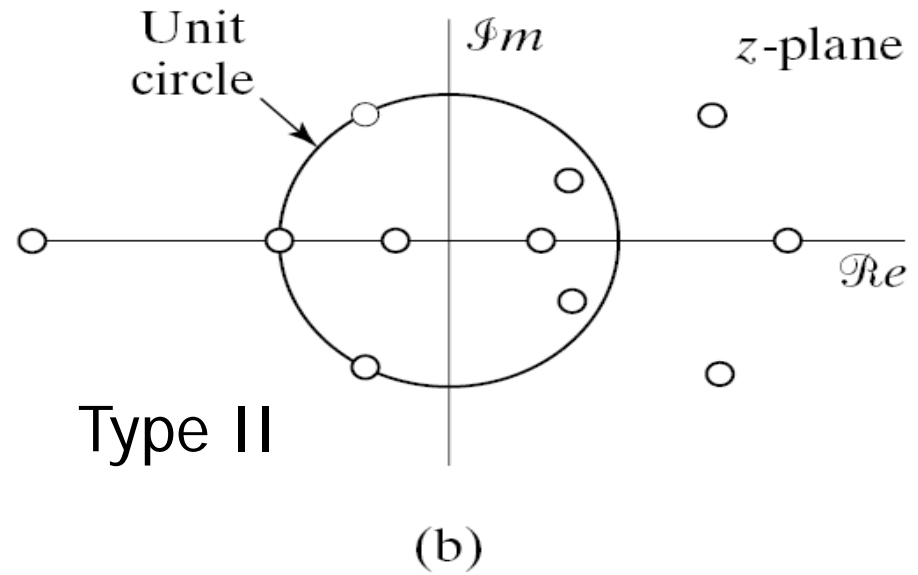
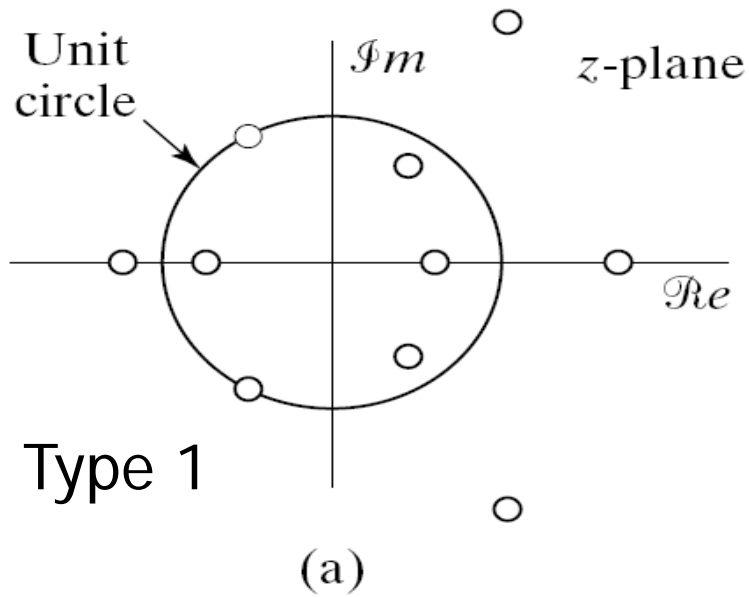
$z=1$ is a zero of both Type III and Type IV systems

$z=-1$ is a zero of Type III system

Summary on the Zeros

- For both Type III, and IV systems,
 $H(1)=0$ and hence $z=1$ (or $\omega = 0$) is a zero of $H(z)$
- For Type II and III systems
 $H(-1)=0$ and hence $z=-1$ (or $\omega = \pi$) is also a zero of the $H(z)$

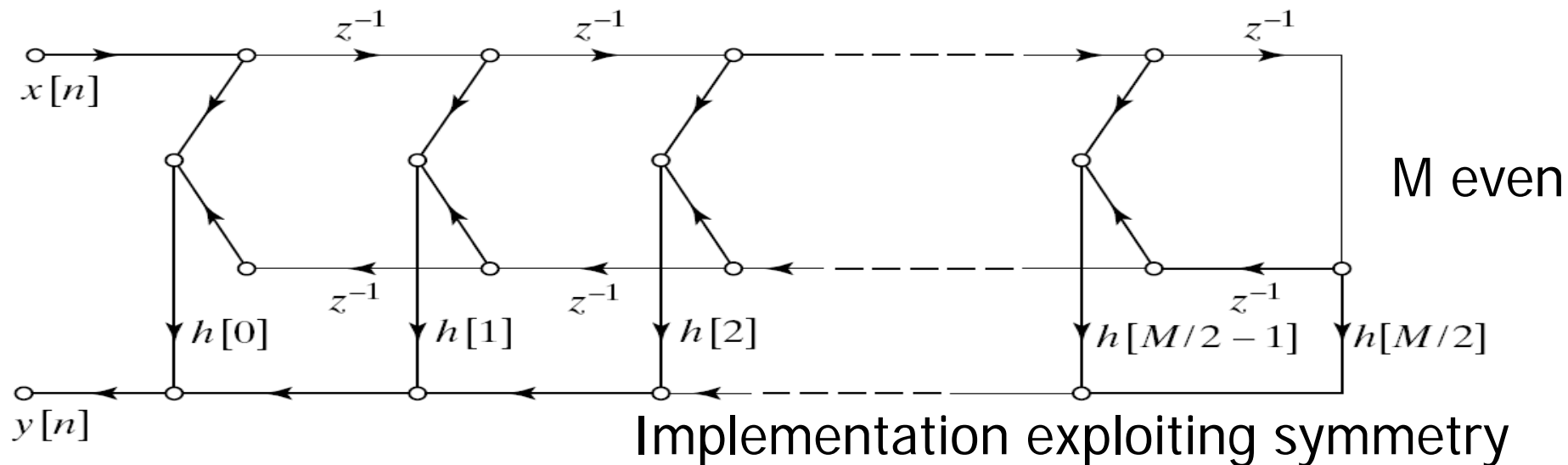
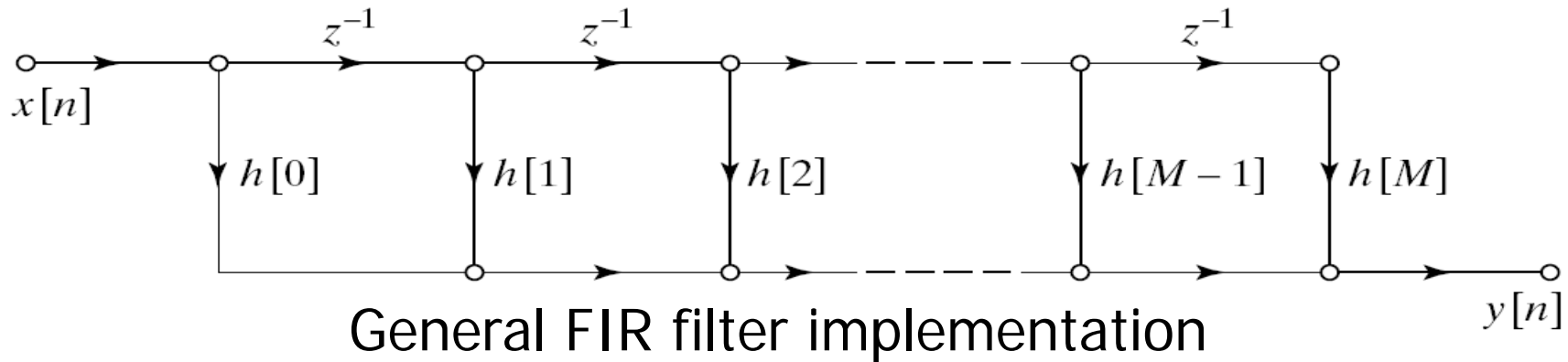
Typical Zero Plots for Linear Phase Systems

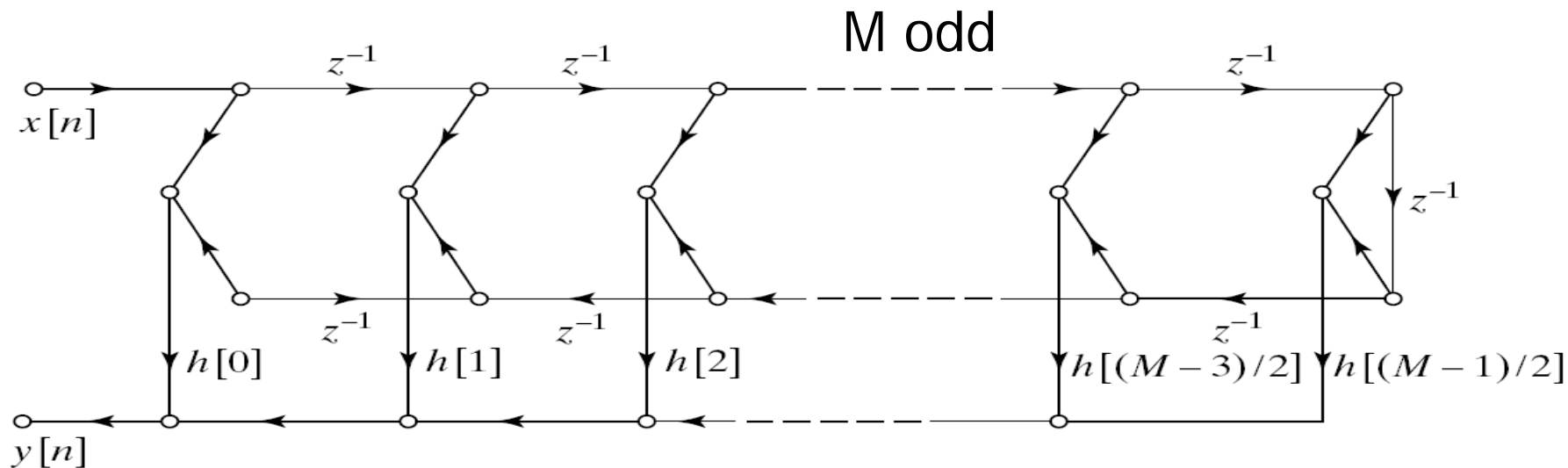


TYPE	1	2	3	4
Symmetry	$h(n) = h(M - n)$	$h(n) = h(M - n)$	$h(n) = -h(M - n)$	$h(n) = -h(M - n)$
Parity of M	M even	M odd	M even	M odd
Expression for frequency response	$e^{-j\omega M/2} H_R(\omega)$	$e^{-j\omega M/2} H_R(\omega)$	$je^{-j\omega M/2} H_R(\omega)$	$je^{-j\omega M/2} H_R(\omega)$
Amplitude response or zero-phases response	$\sum_{k=0}^{M_1} a[k] \cos(\omega k)$ $M_1 = M / 2$	$\sum_{k=1}^{M_1} b[k] \cos(\omega(k - 1/2))$ $M_1 = (M + 1) / 2$	$\sum_{k=1}^{M_1} c[k] \sin(\omega k)$ $M_1 = M / 2$	$\sum_{k=1}^{M_1} d[k] \sin(\omega(k - 1/2))$ $M_1 = (M + 1) / 2$
Special Features		Zero at $\omega = \pi$	Zero at $\omega = 0$ and π	Zero at $\omega = 0$

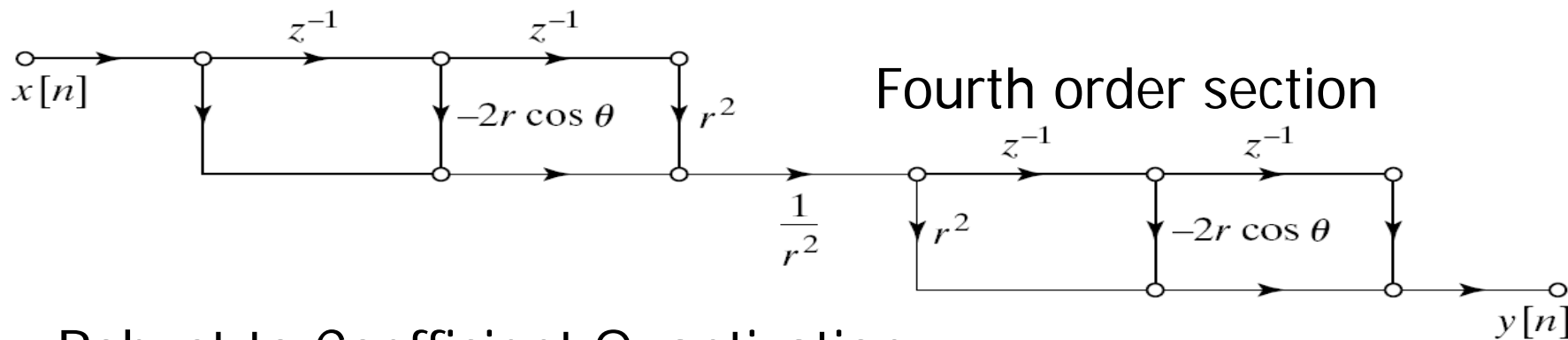
Filter Implementation

$$H(z) = \sum_{n=0}^M h[n]z^{-n}$$





$$H(z) = (1 - 2r \cos \theta \ z^{-1} + r^2 z^{-2}) \frac{1}{r^2} (r^2 - 2r \cos \theta \ z^{-1} + z^{-2})$$



Robust to Coefficient Quantization