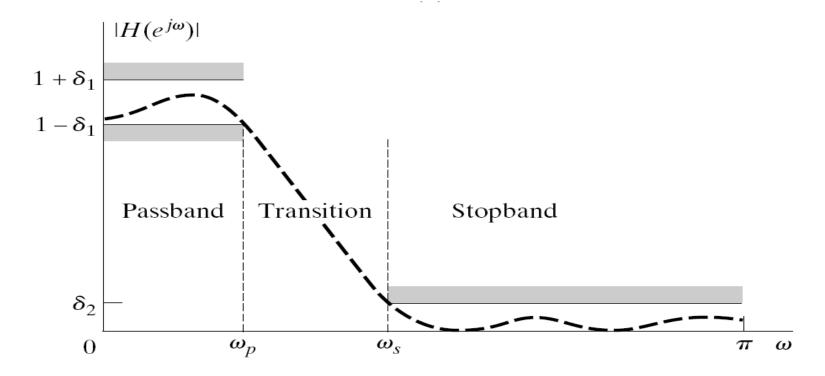
Windows and FIR Filter Design

Lecture By Prof. Meyer

ECE 161A

Filter Design: Low Pass Filter Design



Problem: Given $\delta_1, \delta_2, \omega_p$ and ω_s , find the lowest complexity filter that meets specification

Two Choices

- 1. IIR Filters (Infinite Impulse Response, $H(z) = \frac{B(z)}{A(z)}$
- 2. FIR Filters (Finite Impulse Response, H(z) = B(z)

FIR Filter Design

Approaches:

- 1. FIR Filters by Windowing
- Optimal Approximation (Parks and McClellan)

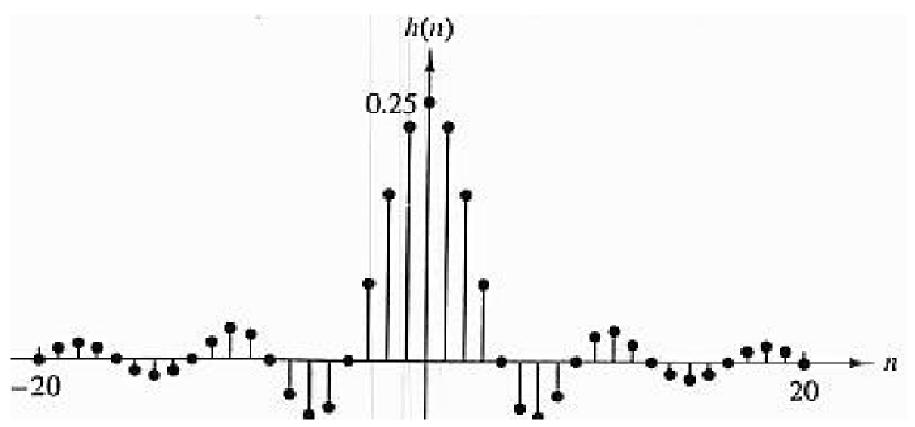
Ideal Low Pass Filter

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\alpha\omega}, |\omega| \le \omega_c \\ 0, \omega_c \le |\omega| \le \pi \end{cases}$$

$$h_d[n] = \frac{\sin(\omega_c(n-\alpha))}{\pi(n-\alpha)}, \alpha = \frac{M}{2}$$

FIR Filter Design (Cont.)

For Linear Phase
$$\alpha = \frac{M}{2}$$



Unit sample response of an ideal lowpass filter

Rectangular Windowing

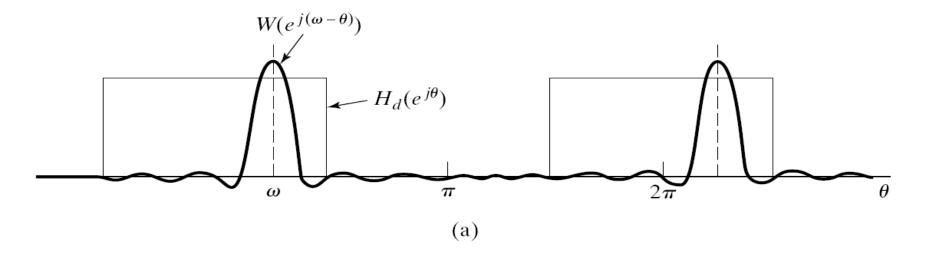
$$h[n] = h_d[n]w_r[n]$$

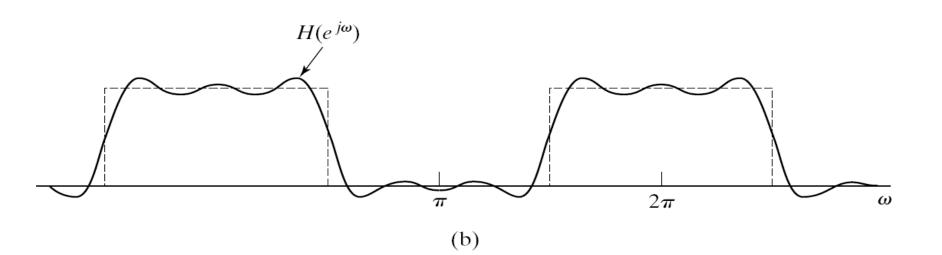
Where

$$w_r[n] = \begin{cases} 1, \ 0 \le n \le M \\ 0, \ otherwise \end{cases}$$

$$H(e^{j\omega}) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\theta}) W_r(e^{j(\omega-\theta)}) d\theta$$

Effects of Windowing





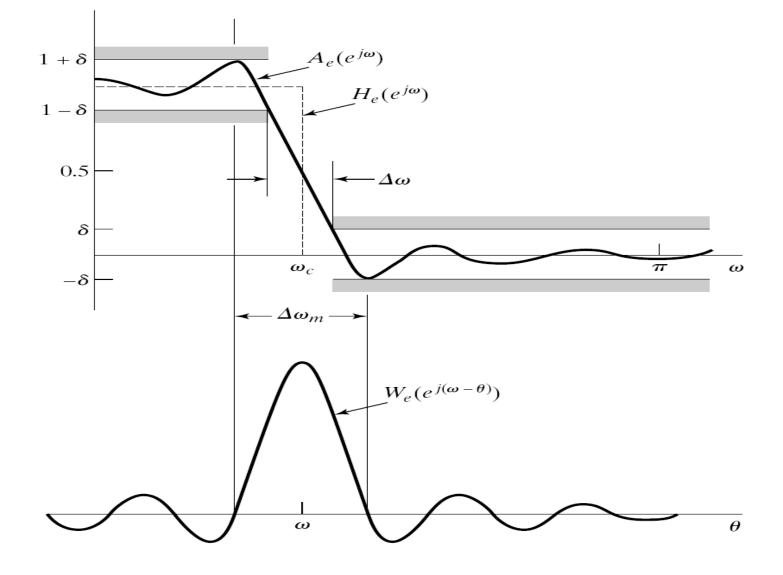
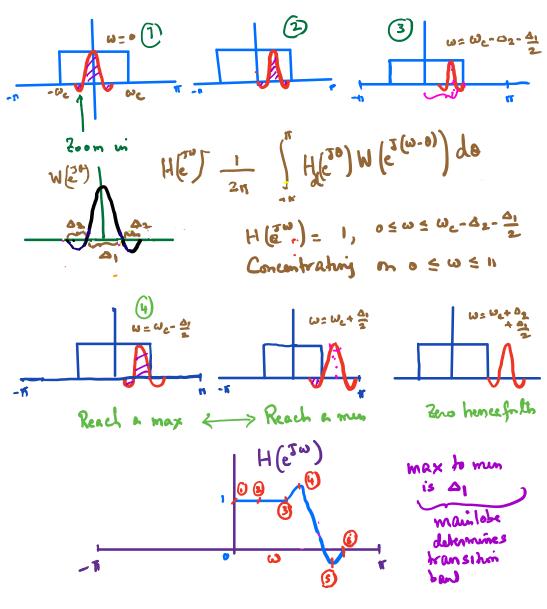


Illustration of type of approximation obtained at a discontinuity of the ideal frequency response.

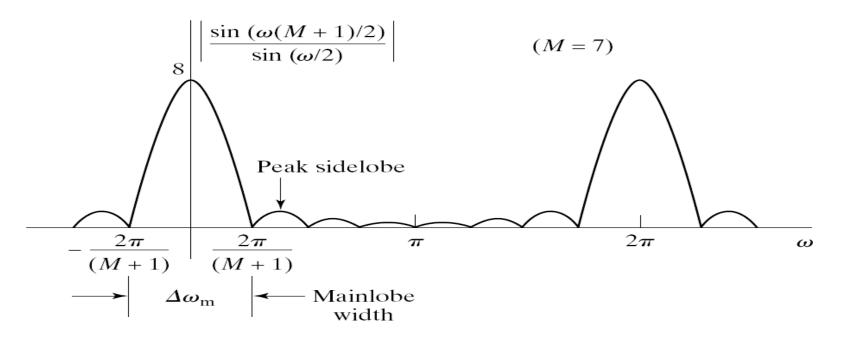


Sidelober determini max distortion

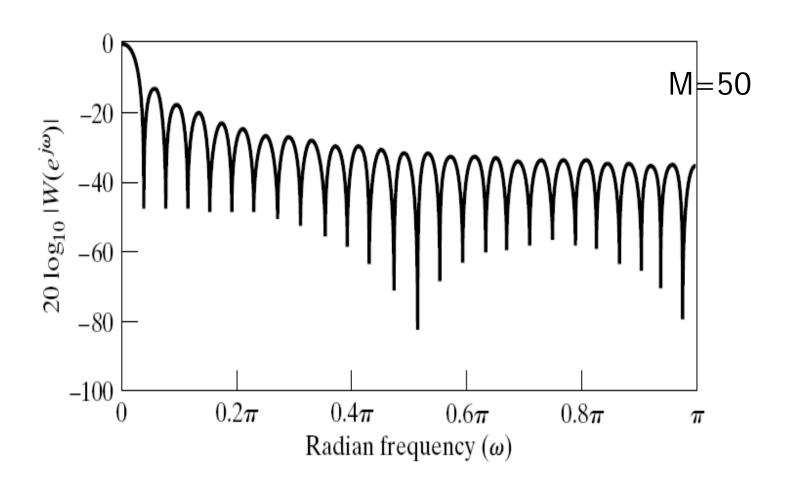
Rectangular Window

$$W_{R}(e^{j\omega}) = \sum_{n=0}^{M} e^{-j\omega} = e^{-\frac{j\omega M}{2}} \frac{\sin \frac{\omega(M+1)}{2}}{\sin \frac{\omega}{2}}$$

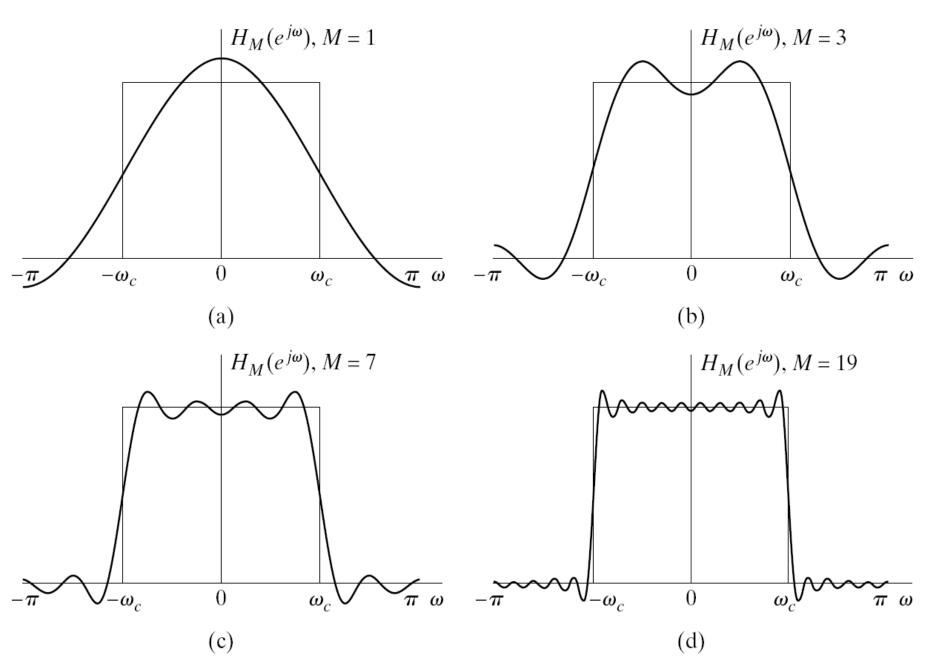
- Main Lobe Width: $\frac{4\pi}{M+1}$
- Sidelobe Magnitude= -13 db
- Stopband Attenuation=-21db



Rectangular Window

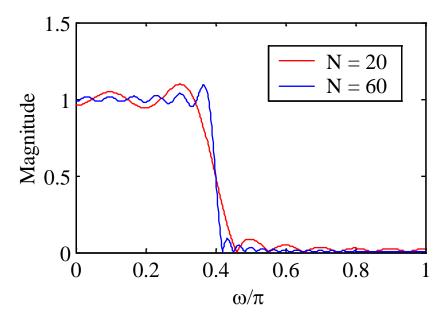


Gibbs Phenomena



Gibbs Phenomenon

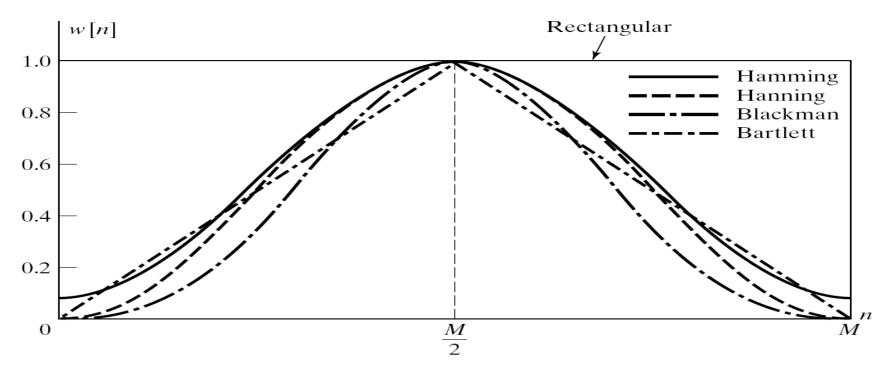
 Gibbs phenomenon - Oscillatory behavior in the magnitude responses of causal FIR filters obtained by truncating the impulse response coefficients of ideal filters



M = N

Gibbs Phenomenon

- Presence of oscillatory behavior in is basically due to:
 - 1) $h_d[n]$ is infinitely long and not absolutely summable, and hence filter is unstable $H_t(e^{j\omega})$
 - 2) Rectangular window has an abrupt transition to zero



Rectangular

$$w[n] = \begin{cases} 1, & 0 \le n \le M, \\ 0, & otherwise \end{cases}$$

Hann

$$w[n] = \begin{cases} 0.5 - 0.5\cos(2\pi n/M), & 0 \le n \le M \\ 0, & otherwise \end{cases}$$

Bartlett (triangular)

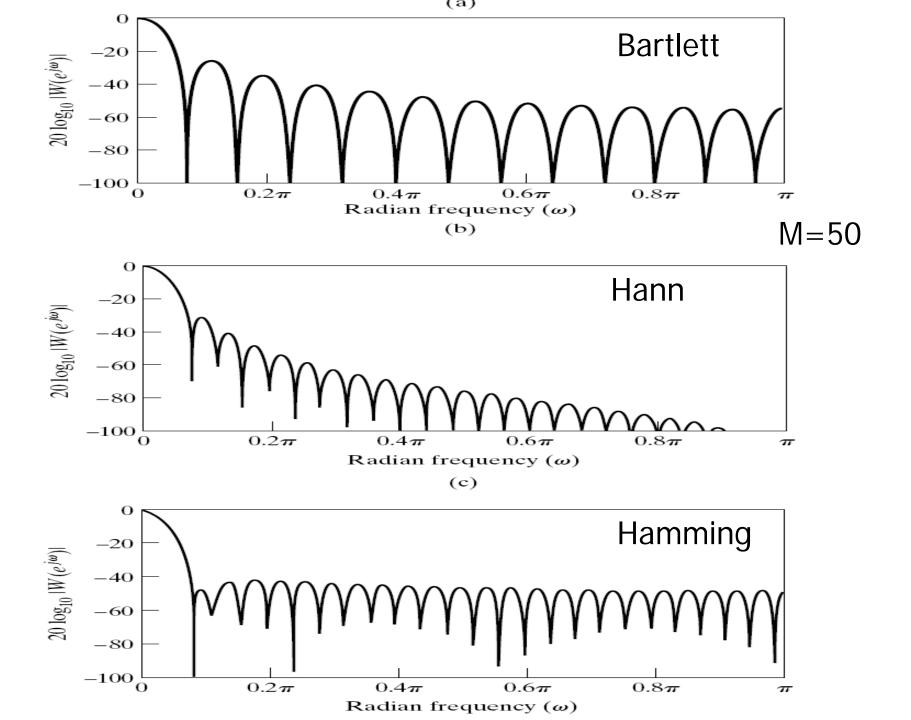
$$w[n] = \begin{cases} 2n/M, & 0 \le n \le M2\\ 2-2n/M, & M/2 \le n \le M\\ 0, & otherwise \end{cases}$$

Hamming

$$w[n] = \begin{cases} 0.5 - 0.5\cos(2\pi n/M), & 0 \le n \le M \\ 0, & otherwise \end{cases}$$

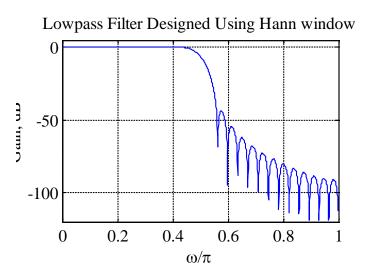
$$w[n] = \begin{cases} 0.54 - 0.46\cos(2\pi n/M), & 0 \le n \le M \\ 0, & otherwise \end{cases}$$

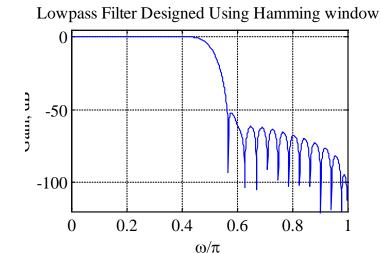
Window Type	Peak Sidelobe Amplitude (relative)	Approximat e Width of Mainlobe	Peak Approximat ion Error 20 logδ (db)	Equivalent Kaiser Windows β	Transition Width of Equivalent Kaiser Window
Rectangular	-13	$4\pi/(M+1)$	-21	0	$1.81\pi/M$
Bartlett	-25	$8\pi/M$	-25	1.33	$2.37\pi/M$
Hann	-31	$8\pi/M$	-44	3.86	$5.01\pi/M$
Hamming	-41	$8\pi/M$	-53	4.86	$6.27\pi/M$
Blackman	-57	$12\pi/M$	-74	7.04	$9.19\pi / M$



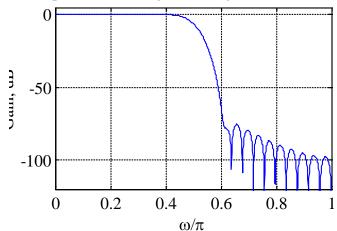
FIR Filter Design Example Copyright © 2005, S. K. Mitra

Lowpass filter of length 51 and $\omega_c = \pi/2$





Lowpass Filter Designed Using Blackman window



Window Based Design

Given specifications: $\delta_1, \delta_2, \omega_p$ and ω_s We employ the following procedure

- 1. Compute $\delta = \min(\delta_1, \delta_2)$ $\Delta \omega = \omega_p - \omega_s$
- Compute $20\log_{10}\delta$ and select window type
- Choose M, the filter order, to meet transition width
- Filter Coefficients are given by

$$h[n] = h_d[n]w[n], 0 \le n \le M$$

$$where \ \omega_c = (\omega_p + \omega_s)/2,$$

$$h_d[n] = \frac{\sin(\omega_c(n - \alpha))}{\pi(n - \alpha)}, \alpha = \frac{M}{2}$$

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 $20 \log \delta = -26 db$.

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Filter Length

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Filter Length

$$\delta\omega = \frac{5.01\pi}{M} = .1\pi \text{ or } M \approx 50.$$

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Filter Length

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$$h[n] = h_d[n] w_{hanning}[n], 0 \le n \le M = 50$$

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, where $\alpha =$

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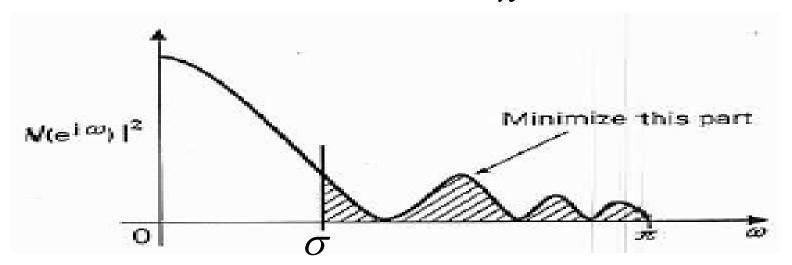
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where

$$h_d[n] = \frac{\sin \omega_c(n-\alpha)}{\pi(n-\alpha)}$$
, where $\alpha = \frac{M}{2} = 25$.

Optimal Window $W(e^{j\omega}) = \sum_{n=0}^{\infty} w[n]e^{-j\omega n}$

Prolate Spheroidal Sequence $\Phi_s = \frac{1}{\pi} \int_{\sigma}^{\pi} |W(e^{j\omega})|^2 d\omega$



Optimization Problem: Minimize
$$\Phi_s$$
 subject to
$$\frac{1}{2\pi} \int_0^{\pi} \left| W(e^{j\omega}) \right|^2 d\omega = 1 \text{ or } \sum_{k=0}^{M} w^2[n] = 1$$

Solution to this problem is the Optimal Window.

Optimal Window

Solution: Form the matrix $P=[P_{mn}]$ such that

$$P_{mn} = \frac{\sin(m-n)\sigma}{m-n}, \quad 0 \le m, n \le M$$

The window sequence w[n] is formed from the elements of the eigenvector corresponding to the largest eigenvalue of P. The eigenvector can be shown to be unique.

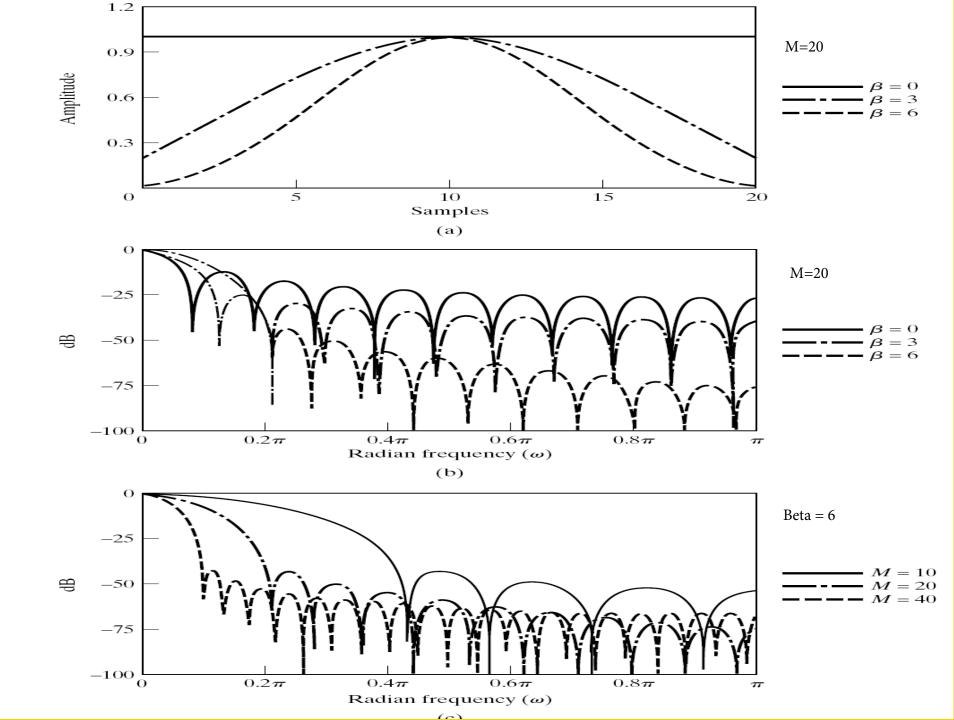
Kaiser Window

$$w[n] = \frac{I_0[\beta(1 - (\frac{n - \alpha}{\alpha})^2)^{\frac{1}{2}}]}{I_0(\beta)}, \ 0 \le n \le M, \alpha = M/2$$

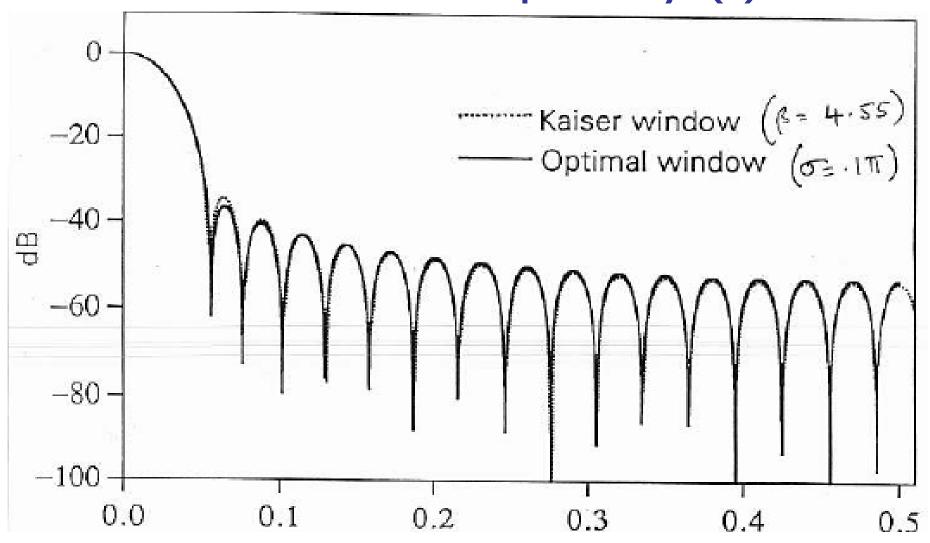
• $I_0(.)$ is zeroth order modified Bessel function of the First Kind

$$I_0(x) = \sum_{m=0}^{\infty} \left[\frac{(.5x)^m}{m!} \right]^2$$

- B controls sidelobe level (Stopband Attenuation)
- The filter order M controls the Mainlobe width



Normalized frequency ()



Kaiser Window based design

Design Method: define

$$\Delta\omega = \omega_s - \omega_p$$

$$A = -20\log_{10} \delta$$
, where $\delta = \min(\delta_1, \delta_2)$

• Choose β as

$$\beta = \begin{cases} .1102(A - 8.7) & , A > 50 \\ .5842(A - 21)^{0.4} + .07886(A - 21), & 21 \le A \le 50 \\ 0, & A < 21 \end{cases}$$

$$M = \frac{A - 8}{2.285 \Delta \omega}$$

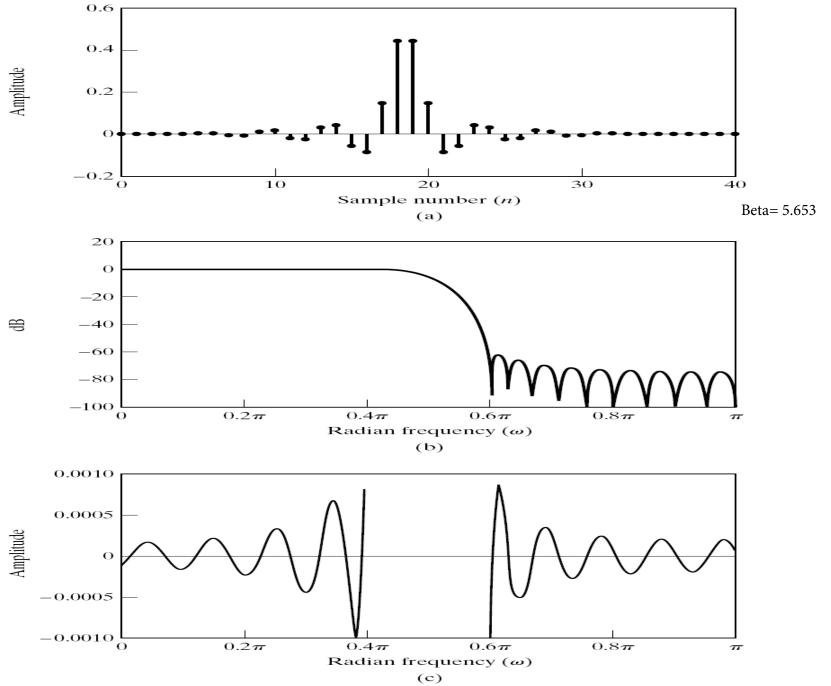


Figure 7.25 Response functions for Example 7.8. (a) Impulse response (M=37). (b) Log magnitude. (c) Approximation error.

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sidelobe level parameter β .

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$$\beta = .5842(A-21)^{0.4} + .07886(A-21) = .58425^{0.4} + .07886 \times 5 = 1.506$$

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Filter Order

$$M = \frac{A - 8}{2.285\delta\omega} = \frac{18}{2.285.1\pi} = \lceil 25.071 \rceil = 26$$

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, where $\alpha = \frac{M}{2} = 13$.



Pros and Cons of Window based Design

Advantages

- Easy to design
- Can be applied to general linear system design

Disadvantages

- Exceeds the specs everywhere except at the edges of the passband and stopband
- δ_1 and δ_2 cannot be independently controlled. Have to design more conservatively for the smaller of the two