

Optimal Linear Phase FIR Filter Design

Lecture By Prof. Meyer

ECE 161A

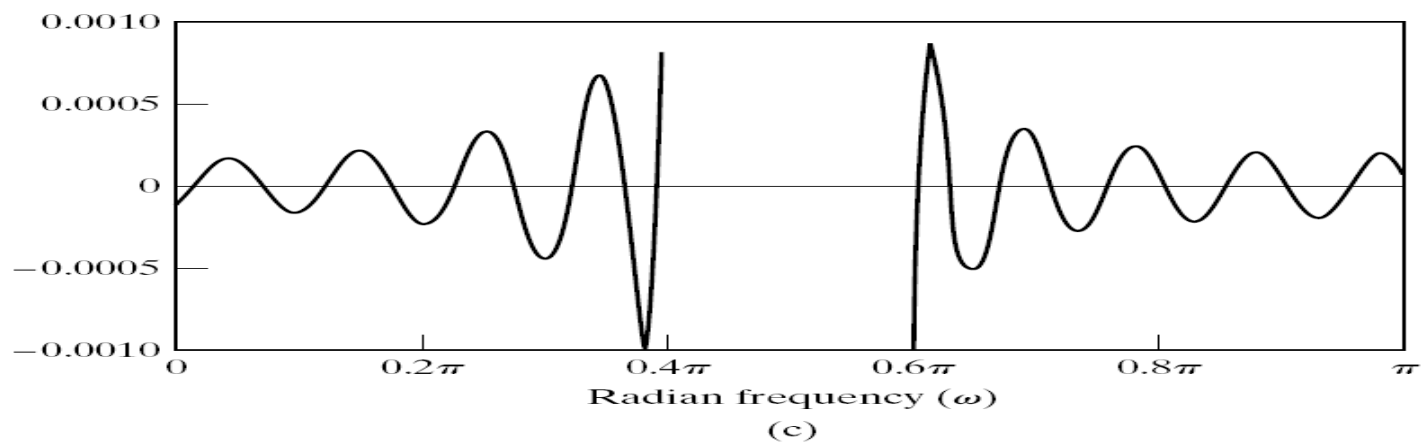
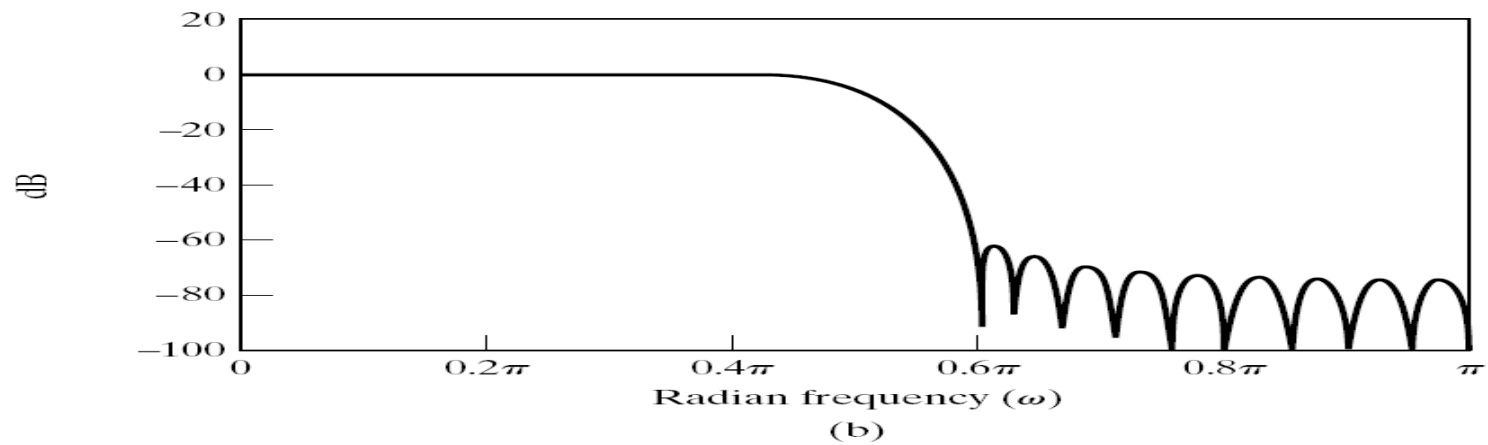
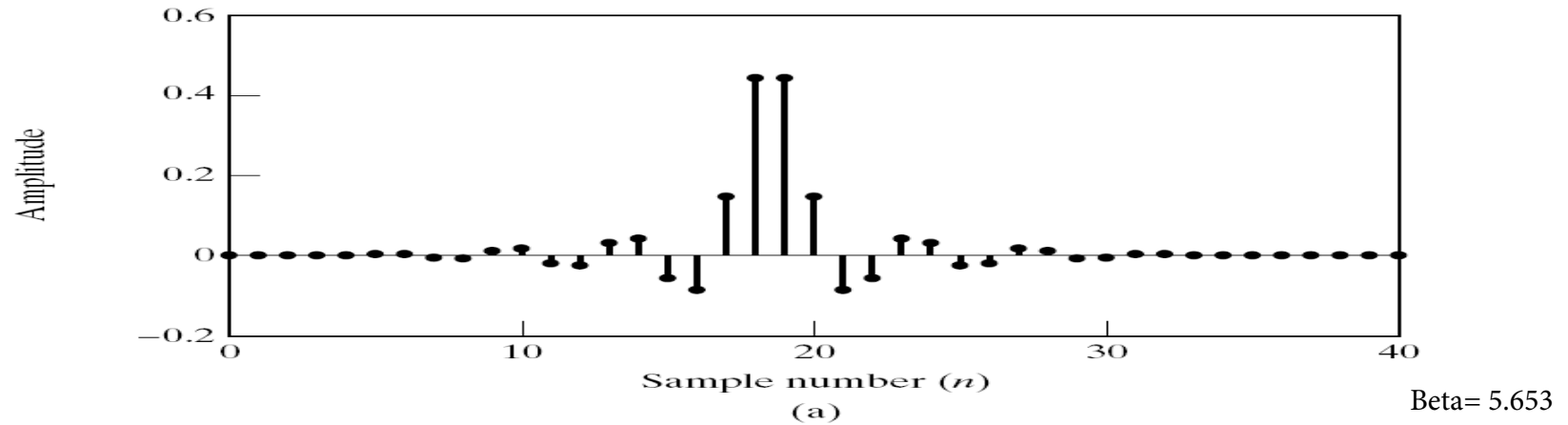


Figure 7.25 Response functions for Example 7.8. (a) Impulse response ($M = 37$). (b) Log magnitude. (c) Approximation error.

Pros and Cons of Window based Design

■ Advantages

- Easy to design
- Can be applied to general linear system design

■ Disadvantages

- Exceeds the specs everywhere except at the edges of the passband and stopband
- δ_1 and δ_2 cannot be independently controlled. Have to design more conservatively for the smaller of the two

Objectives of Optimal Design

- Control δ_1 and δ_2 separately
- Spread the ripples out over all of the passband and stopband

Optimal Filter Design

- Design Specifications

$$(\omega_p, \omega_s, M, \delta_1, \delta_2) \Rightarrow (\omega_p, \omega_s, M, K(=\frac{\delta_1}{\delta_2}), \delta(=\delta_2))$$

- Parks and McClellan Approach: given

$$(\omega_p, \omega_s, M, K) \text{ minimize } \delta$$

- Type I filter Design: (M even)

$$H(e^{j\omega}) = A_e(e^{j\omega})e^{-j\frac{\omega M}{2}}$$

$$A_e(e^{j\omega}) = \sum_{n=-L}^L h_e[n]e^{-j\omega n}, \quad L = \frac{M}{2}$$

$$h_e[n] = h_e[-n] \quad \text{and} \quad h[n] = h_e[n-L], \quad 0 \leq n \leq M$$

Optimal Filter Design (Cont.)

Using the symmetry in the coefficients

$$A_e(e^{j\omega}) = h_e[0] + 2 \sum_{n=1}^L h_e[n] \cos \omega n = \sum_{K=0}^L a_k (\cos \omega)^k, \quad -\pi \leq \omega \leq \pi$$

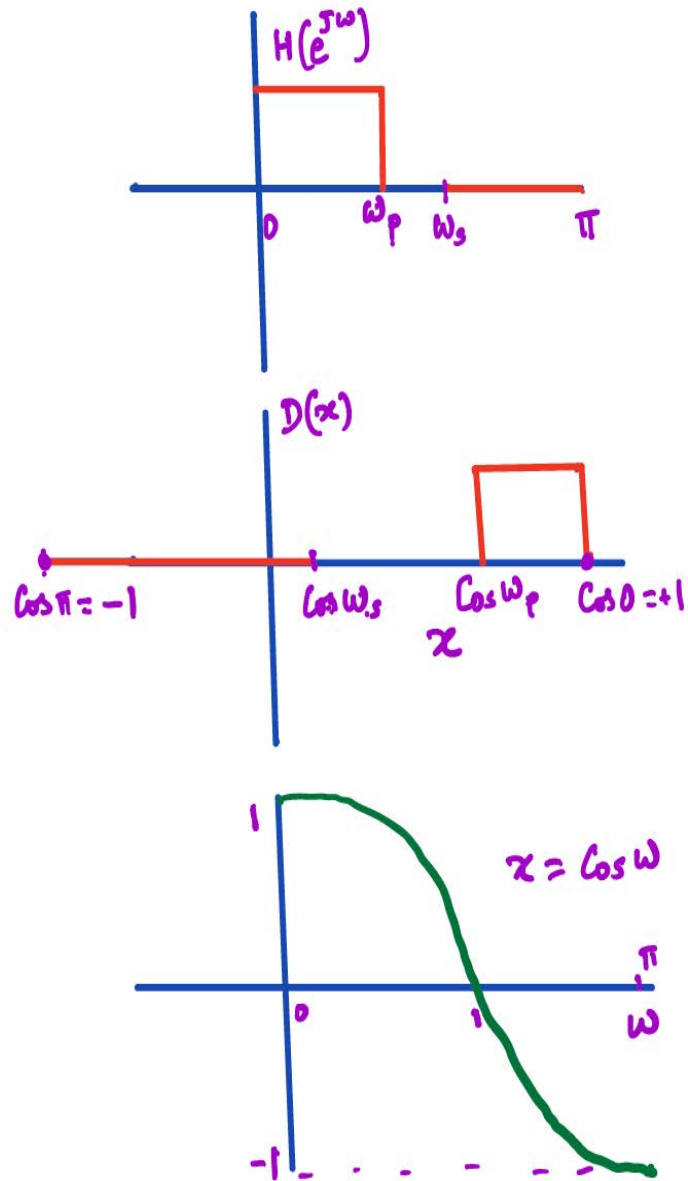
$$= \sum_{k=0}^L a_k x^k \Big|_{x=\cos \omega} = P(x), \quad -1 \leq x \leq 1$$

- Can View Filter Design as a Polynomial Approximation problem

Desired Filter

$$H_d(e^{j\omega}) = \begin{cases} 1, & 0 \leq \omega \leq \omega_p \\ 0, & \omega_s \leq \omega \leq \pi \end{cases}$$

$$D(x) = \begin{cases} 1, & \cos \omega_p \leq x \leq 1 \\ 0, & -1 \leq x \leq \cos \omega_s \end{cases}$$



ω	$x = \cos \omega$
0	1
ω_p	$\cos \omega_p$
ω_s	$\cos \omega_s$
π	-1

Problem Statement

Define the following closed sets

$$F_{\omega} = [0, \omega_p] \cup [\omega_s, \pi]$$

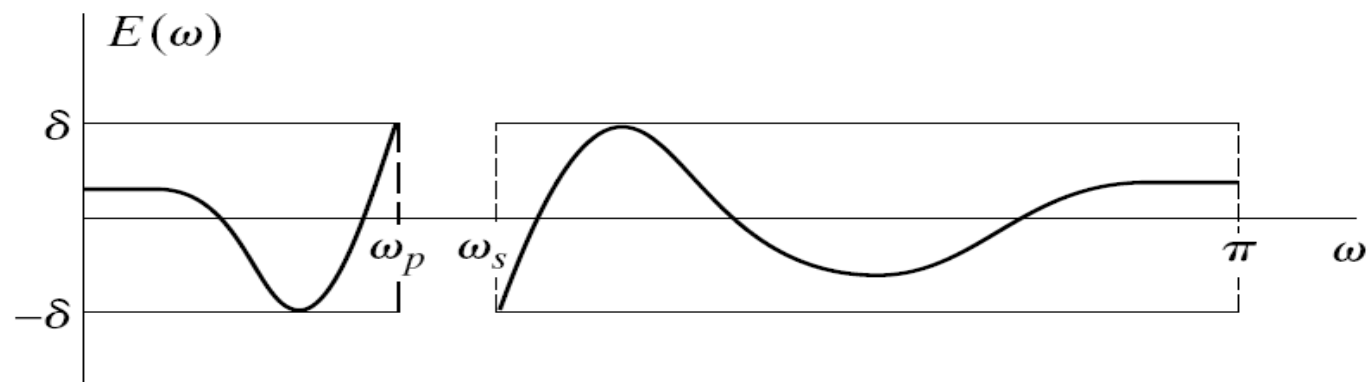
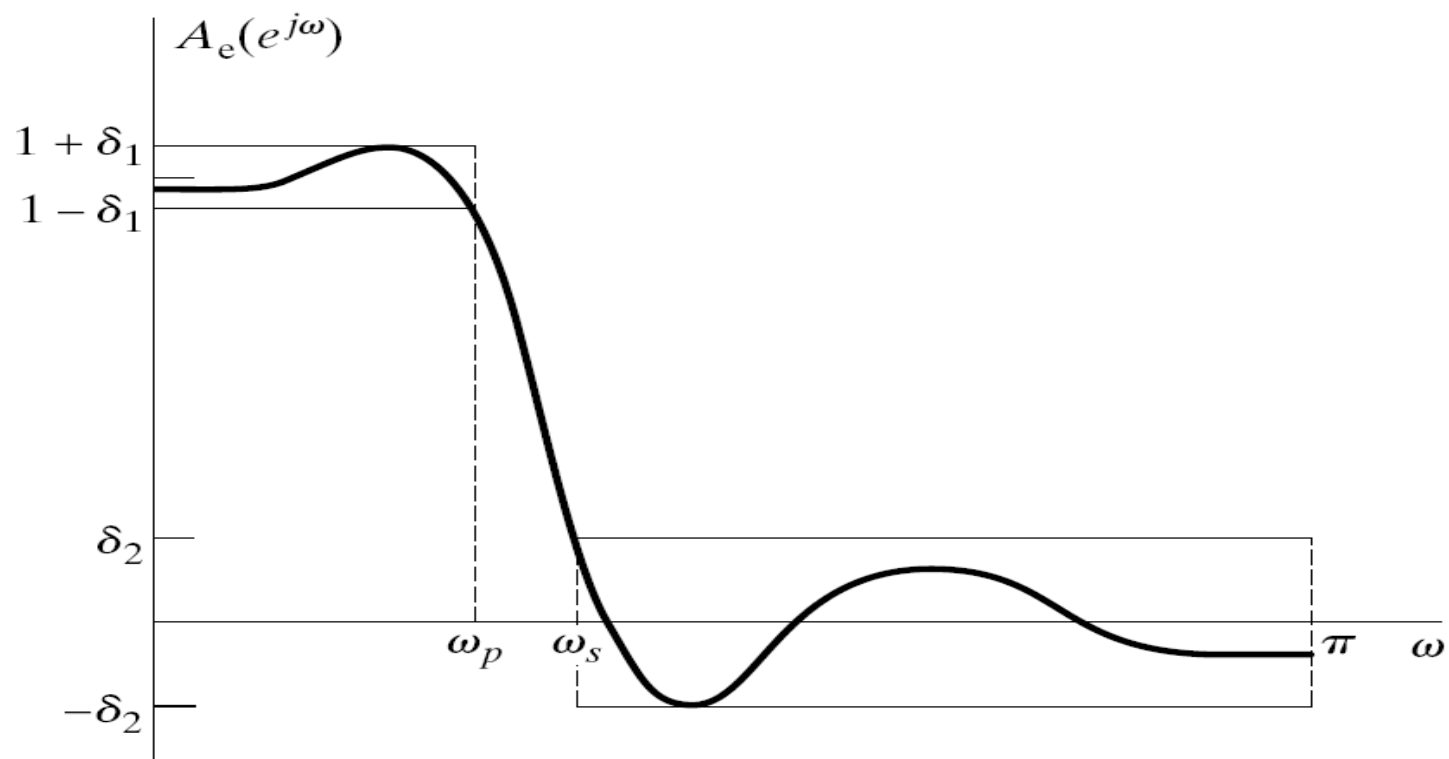
$$F_x = [-1, \cos \omega_s] \cup [\cos \omega_p, 1]$$

Error Functions

$$E(\omega) = W(\omega)[H_d(e^{j\omega}) - A_e(e^{j\omega})]$$

$$E(x) = W(x)[D(x) - P(x)]$$

$$\text{where } W(\omega) = \begin{cases} \frac{1}{K}, & 0 \leq \omega \leq \omega_p \\ 1, & \omega_s \leq \omega \leq \pi \end{cases} \quad \text{and } K = \frac{\delta_1}{\delta_2}$$



Optimization Problem

Max Approximation Error

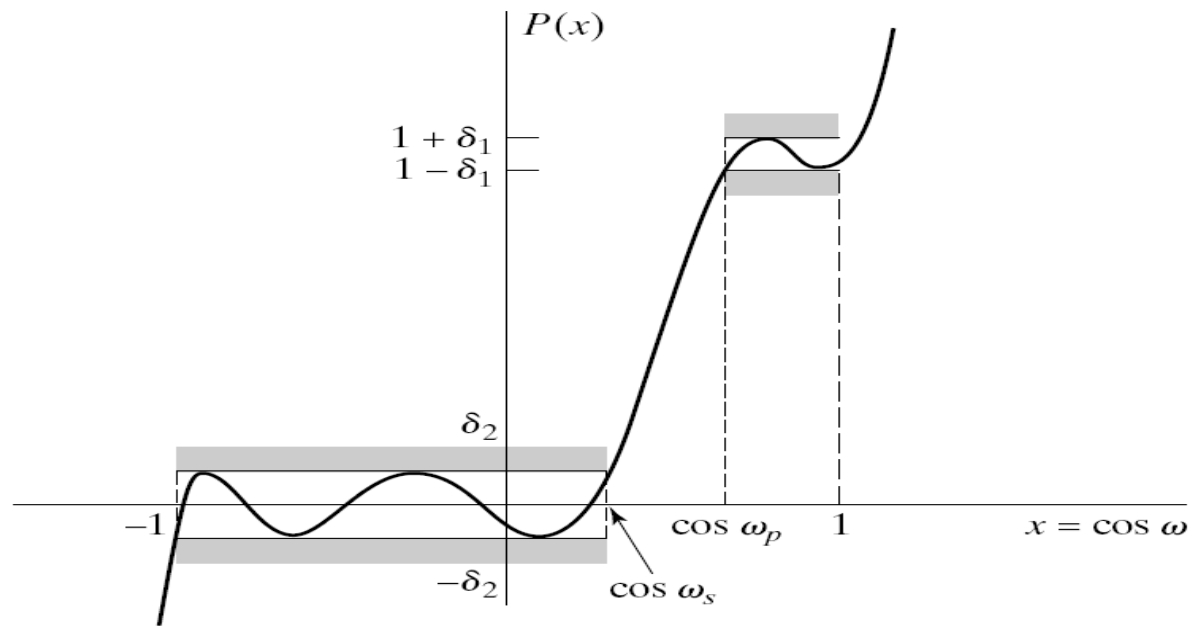
$$M(h_e[n]) = \max_{\omega \in F_\omega} |E(\omega)| = \max_{\omega \in F_\omega} W(\omega) |H_d(e^{j\omega}) - A_e(e^{j\omega})|$$

$$M(a_k) = \max_{x \in F_x} |E(x)| = \max_{x \in F_x} W(x) |D(x) - P(x)|$$

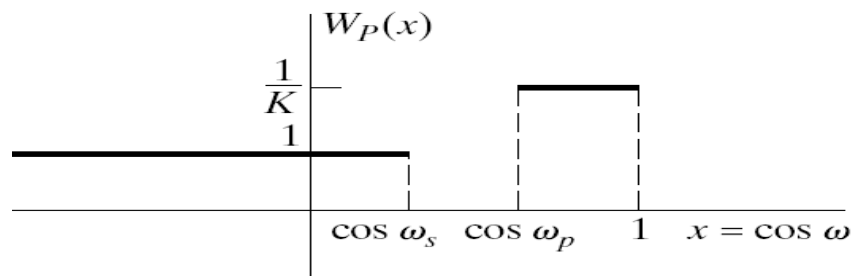
Mini-Max Criterion (Cost Function)

$$\min_{h_e[n]} M(h_e[n]) = \min_{h_e[n]} [\max_{\omega \in F_\omega} W(\omega) |H_d(e^{j\omega}) - A_e(e^{j\omega})|]$$

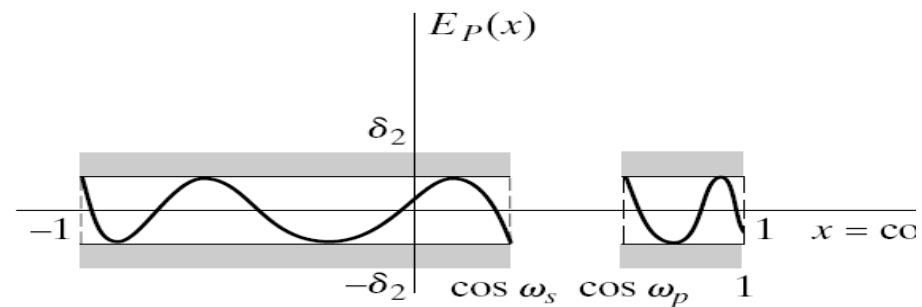
$$\min_{a_k} M(a_k) = \min_{a_k} [\max_{x \in F_x} W(x) |D(x) - P(x)|]$$



(a)



(b)



(c)

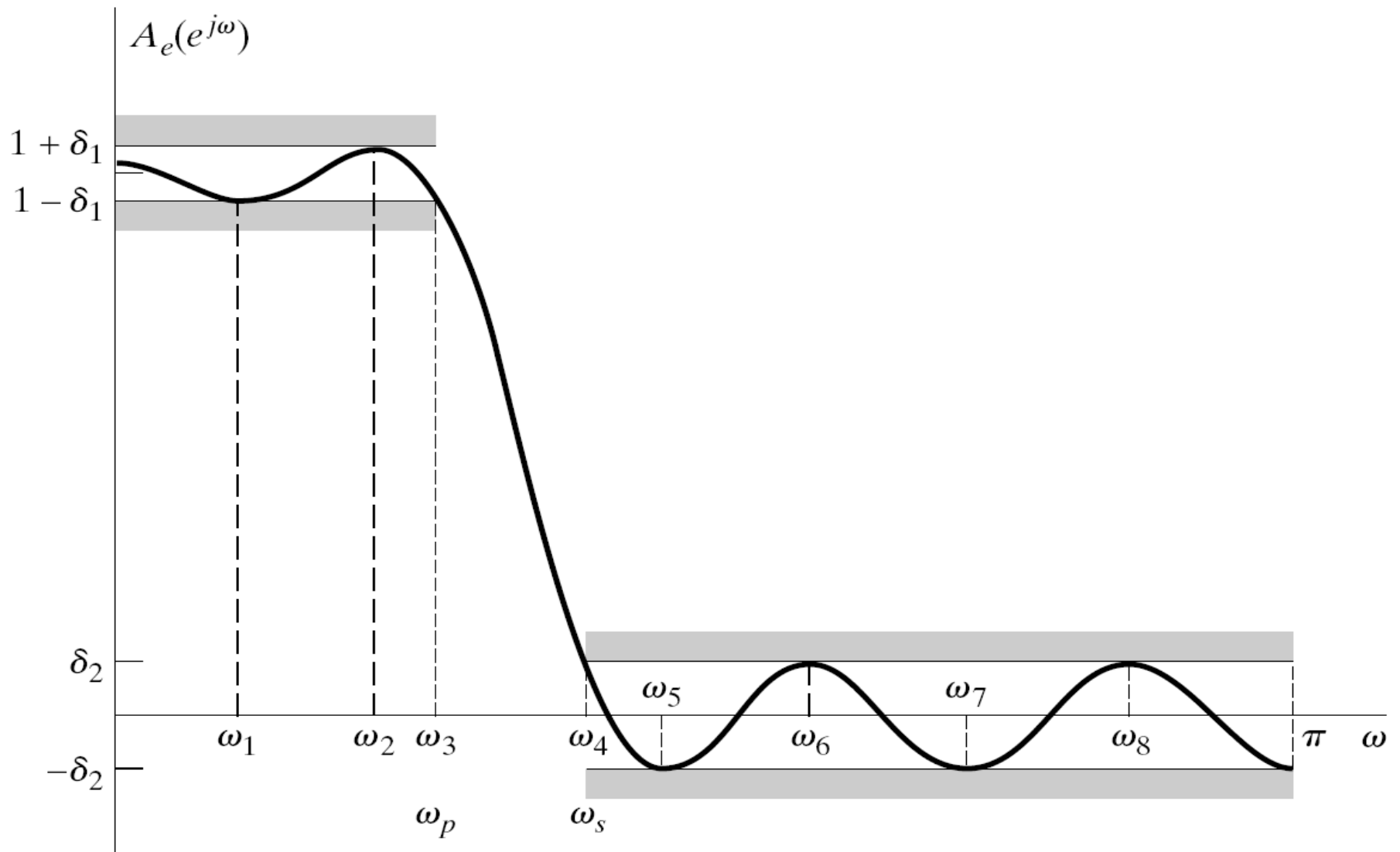
Figure 7.36 Equivalent polynomial approximation functions as a function of $x = \cos \omega$. (a) Approximating polynomial. (b) Weighting function. (c) Approximation error.

Alternation Theorem

- Alternation Theorem: Minimax Cost function has an unique minimum, and the minimum has at least $(L+2)$ alternations.
- If $\delta = \min_{a_k} [\max_{x \in F_x} |E(x)|]$ then we can find

$$x_1 < x_2 < \dots < x_{L+2} \text{ where } E(x_i) = -E(x_{i+1})$$

and $|E(x_i)| = \delta$



Typical example of a lowpass filter approximation that is optimal according to the alternation theorem for $L=7$

Alternation Points

$$P(x) = \sum_{k=0}^L a_k x^k$$

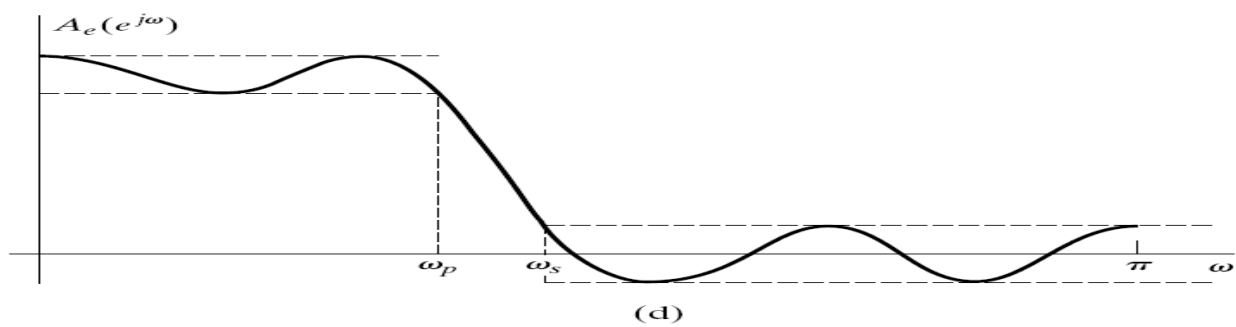
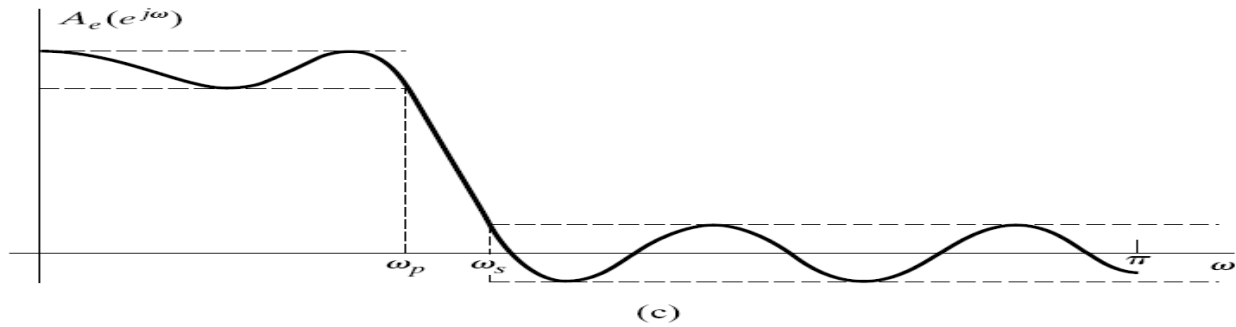
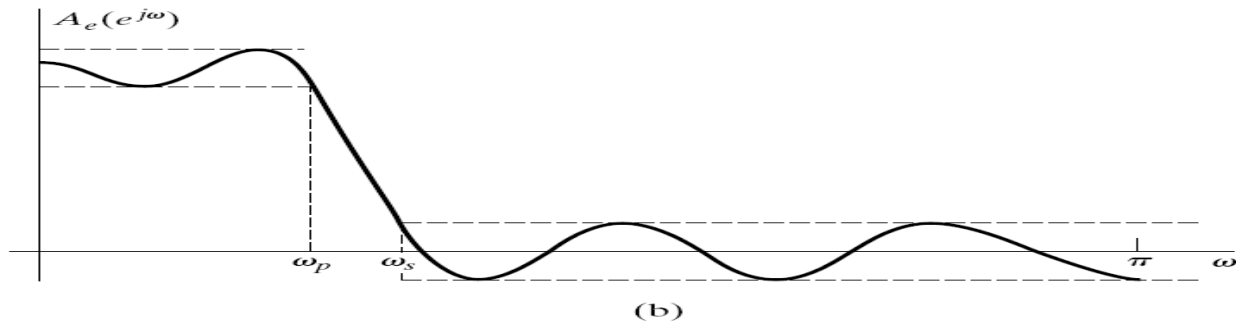
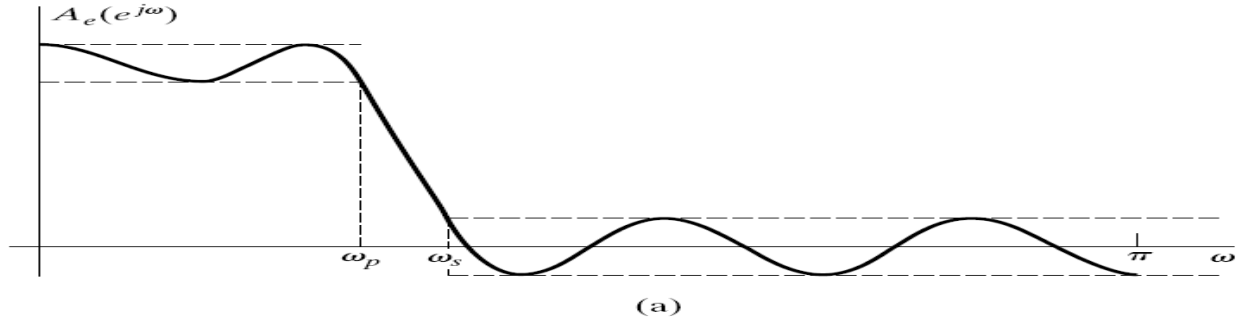
$$\begin{aligned} \frac{dP(\cos \omega)}{d\omega} &= \frac{\partial P(x)}{\partial x} \frac{dx}{d\omega} = \sum_{k=0}^L k a_k x^{k-1} (-\sin \omega) \\ &= \sum_{k=0}^{L-1} (k+1) a_{k+1} x^k (-\sin \omega) = -P'(x) \sin \omega \end{aligned}$$

Alternation points can be found by
examining where the derivative is zero

Potential Alternation Points

- $P'(x)$ is a polynomial of degree $(L-1)$ and so has $(L-1)$ zeros which can correspond to the alternation points
- Error can be δ at the passband and stopband edges. So ω_p and ω_s can be alternation points
- $\sin \omega$ is zero at $\omega = 0$ and $\omega = \pi$ and so they are candidates for alternation points.

Maximum number of alternation points = $(L-1) + 2 + 2 = L+3$

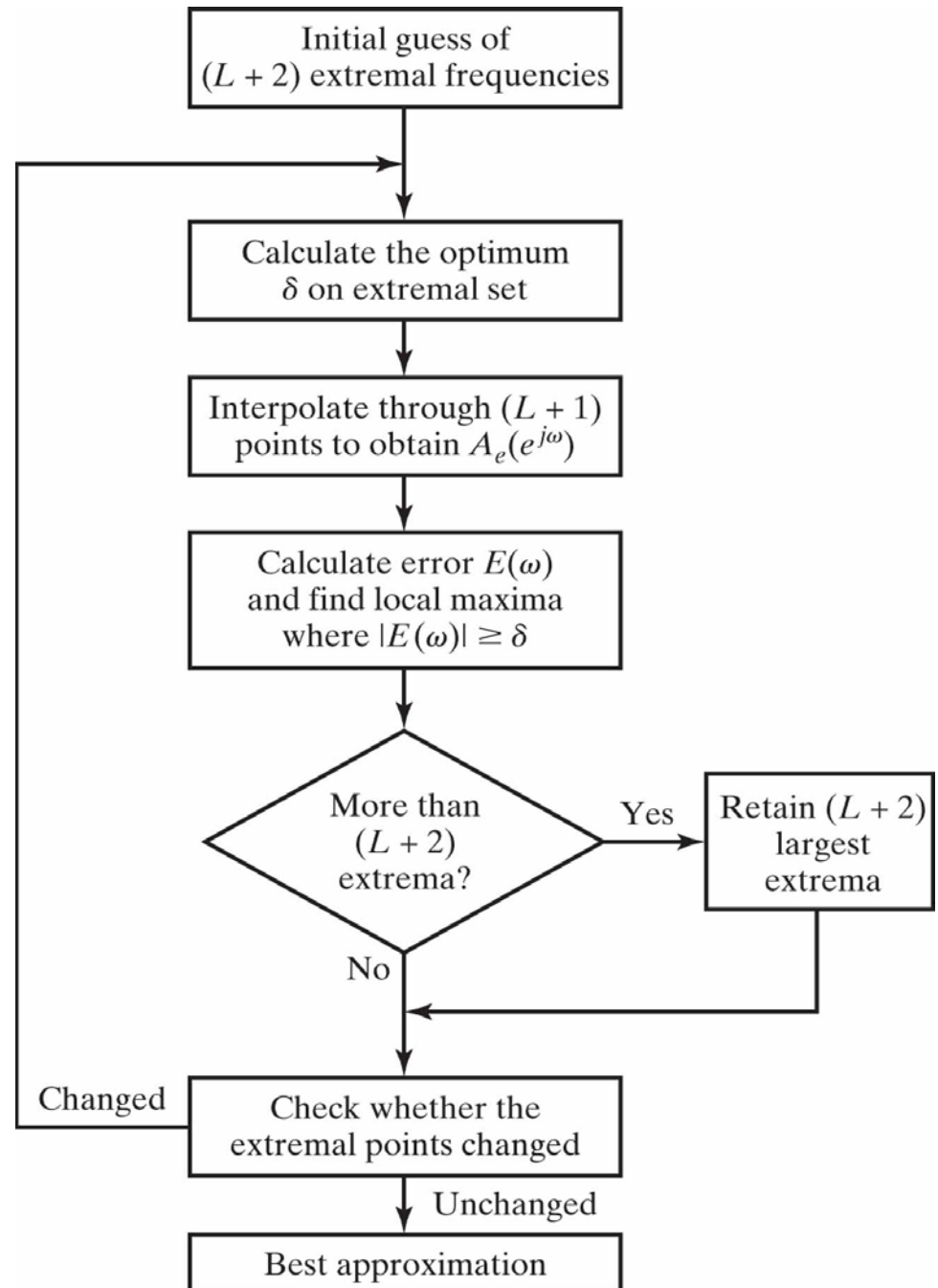


Possible optimum lowpass filter approximations for $L=7$

Figure 7.50 Flowchart of Parks–McClellan algorithm.

$$A_e(e^{j\omega}) = P(x) \Big|_{x=\cos \omega} = \sum_{k=0}^L a_k x^k$$

Note: $A_e(e^{j\omega})$ and $P(x)$ are uniquely defined by their values at $(L+1)$ points.



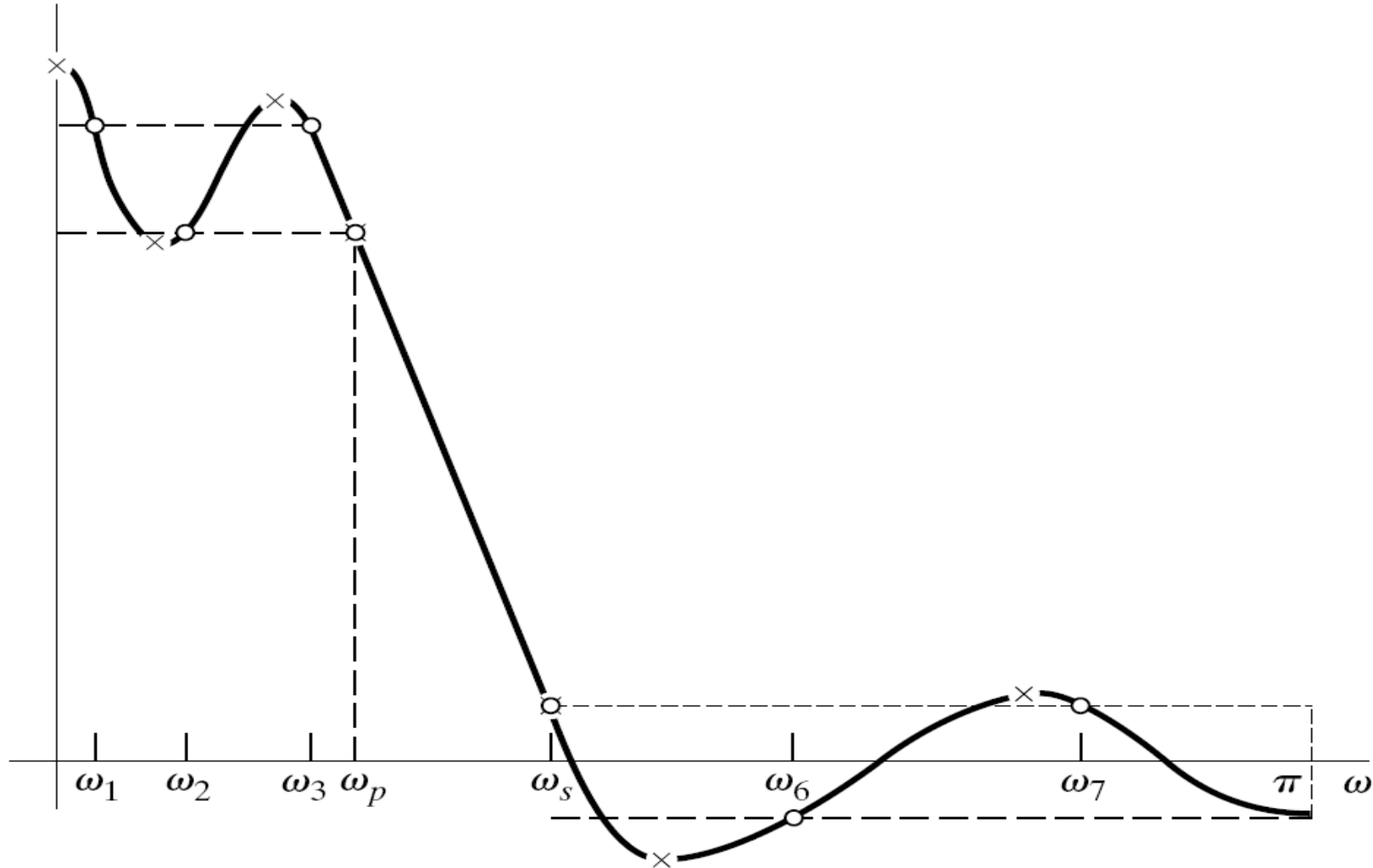
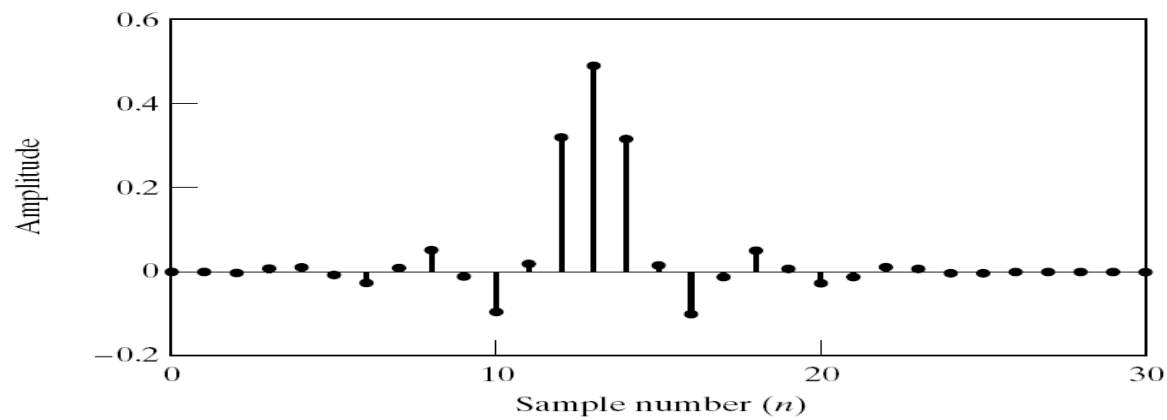
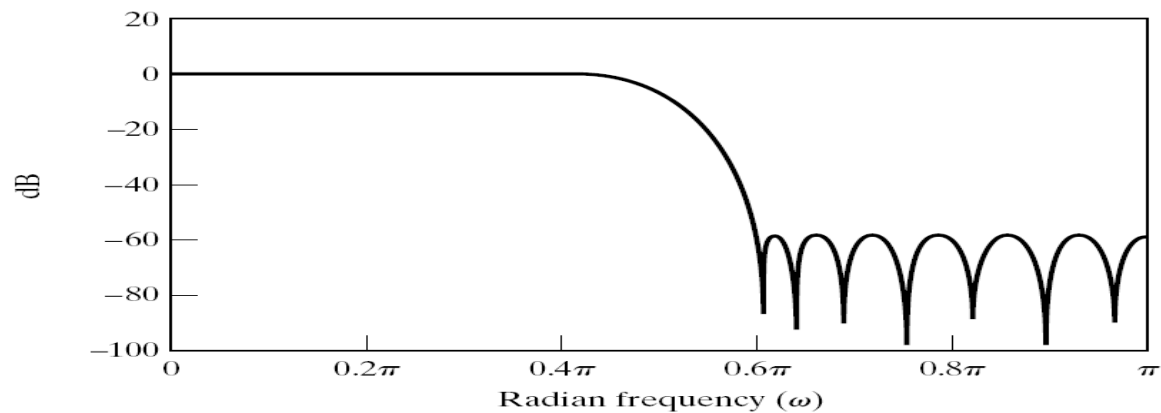


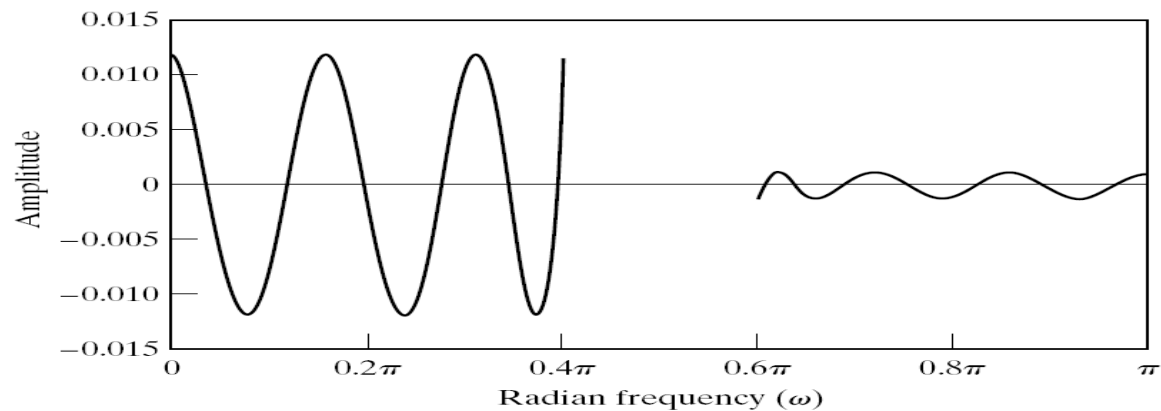
Figure 7.40 Illustration of the Parks–McClellan algorithm for equiripple approximation.



(a)



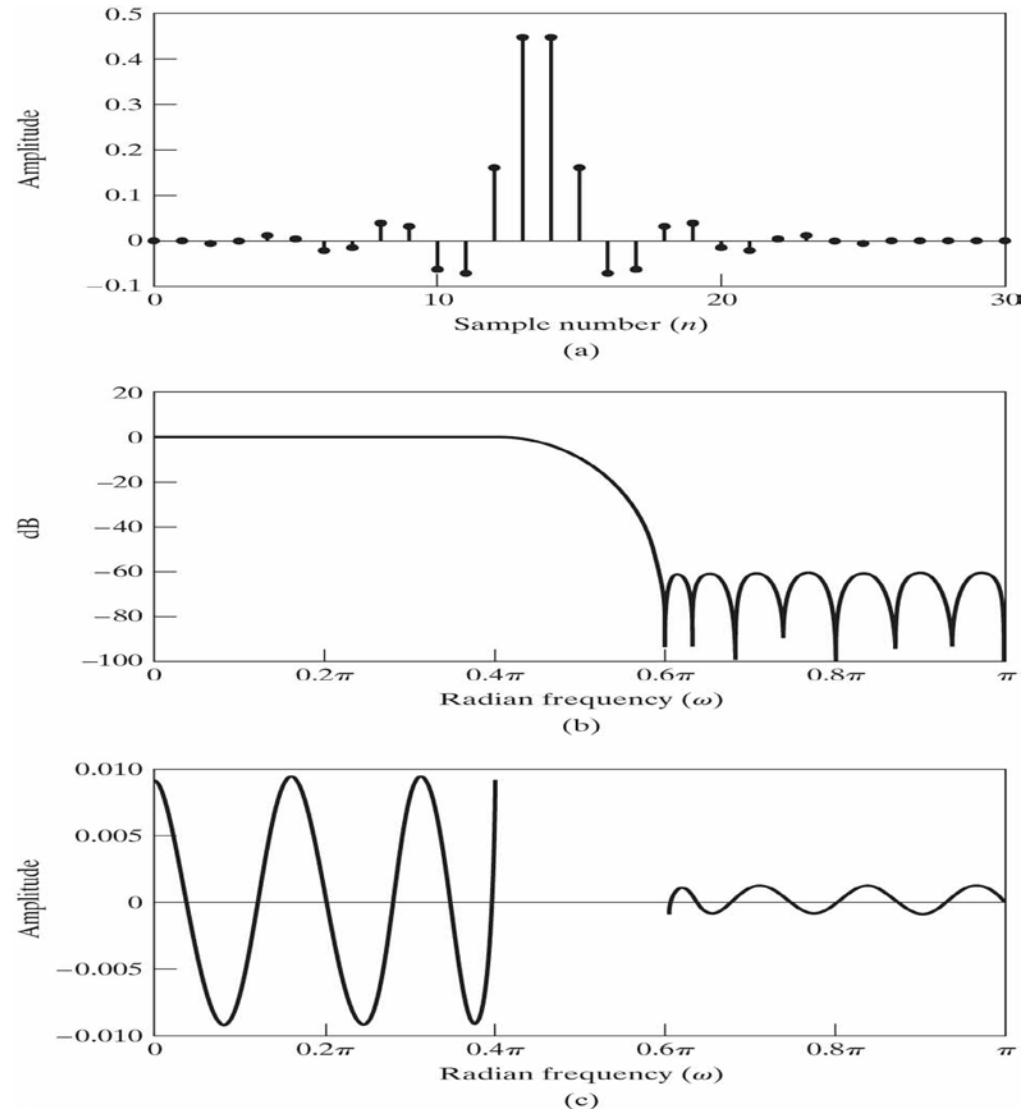
(b)



(c)

Figure 7.43 Optimum type I FIR lowpass filter for $\omega_p = 0.4\pi$, $\omega_s = 0.6\pi$, $K = 10$, and $M = 26$. (a) Impulse response. (b) Log magnitude of the frequency response. (c) Approximation error (unweighted).

Figure 7.53 Optimum type II FIR lowpass filter for $\omega_p = 0.4\pi$, $\omega_s = 0.6\pi$, $K = 10$, and $M = 27$. (a) Impulse response. (b) Log magnitude of frequency response. (c) Approximation error (unweighted).



$$\omega_p = .1\pi, \omega_s = .15\pi, K = 1 (\delta_1 = \delta_2)$$

