

Problem 8.1

Lateral mean momentum eq

$$\frac{1}{\delta} \frac{\delta \langle P(x, y) \rangle}{\delta y} + \frac{\delta \langle v^2 \rangle}{\delta y} = 0$$

after integration

$$\int_0^\delta \frac{1}{\delta} \frac{\delta \langle P(x, y) \rangle}{\delta y'} dy' + \int_0^\delta \frac{\delta \langle v^2 \rangle}{\delta y'} dy' = 0$$

$$\frac{1}{\delta} (\langle P(x, y) \rangle - \langle P_{wall}(x) \rangle) + \langle v^2(y) \rangle - \langle v^2(0) \rangle = 0$$

The velocity at the wall ($y=0$) is zero

$$\frac{1}{\delta} (\langle P(x, y) \rangle - \langle P_{wall}(x) \rangle) + \langle v^2(y) \rangle = 0$$

Taking the derivative with x

$$\frac{1}{\delta} \left(\frac{\delta \langle P(x, y) \rangle}{\delta x} - \frac{\delta \langle P_{wall}(x) \rangle}{\delta x} \right) = 0$$

$$\Rightarrow \frac{\delta \langle P \rangle}{\delta x} = \frac{\delta \langle P_{wall} \rangle}{\delta x}$$

8.2

(a) N.S momentum equations $\frac{D\mathbf{U}}{Dt} = -\frac{1}{\delta} \nabla P + \nu \nabla^2 \mathbf{U}$

$$\text{Reynolds equations } \frac{D \langle U_j \rangle}{Dt} = \nu \nabla^2 \langle U_j \rangle - \frac{\delta \langle u_i \cdot u_j \rangle}{\delta x_i} - \frac{1}{\delta} \frac{\delta \langle P \rangle}{\delta x_j}$$

Subtract 2 from 1

$$\frac{D\mathbf{U}}{Dt} - \frac{D \langle U_j \rangle}{Dt} = -\frac{1}{\delta} \nabla P + \nu \nabla^2 \mathbf{U} - \nu \nabla^2 \langle U_j \rangle + \frac{\delta \langle u_i \cdot u_j \rangle}{\delta x_i} + \frac{1}{\delta} \frac{\delta \langle P \rangle}{\delta x_j}$$

Since

$$v = V - \langle v_j \rangle \text{ and } p' = p - \langle p \rangle$$

$$\frac{DV}{Dt} - \frac{D\langle v_j \rangle}{Dt} = \frac{-1}{f} \nabla p + v \nabla^2 v_j + \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} + \frac{1}{f} \frac{\delta \langle p \rangle}{\delta x_j}$$

$$\frac{DV}{Dt} - \frac{D\langle v_j \rangle}{Dt} = v \nabla^2 v_j + \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} - \frac{1}{f} \left(\nabla p - \frac{\delta \langle p \rangle}{\delta x_j} \right)$$

$$\frac{DV}{Dt} - \frac{D\langle v_j \rangle}{Dt} = v \nabla^2 v_j + \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} - \frac{1}{f} \frac{\delta p'}{\delta x_j}$$

Since

$$\frac{Dv_j}{Dt} = \frac{\delta v_j}{\delta t} + \frac{\delta (v_i \cdot v_j)}{\delta x_i}$$

$$\begin{aligned} \left\langle \frac{Dv_j}{Dt} \right\rangle &= \frac{\delta \langle v_j \rangle}{\delta t} + \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} = \frac{\delta \langle v_j \rangle}{\delta t} + \\ &\quad \frac{\langle v_i \rangle \delta \langle v_j \rangle}{\delta x_i} + \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} \end{aligned}$$

$$\frac{D\langle v_j \rangle}{Dt} = \left\langle \frac{Dv_j}{Dt} \right\rangle - \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i}$$

$$\begin{aligned} \frac{Dv_j}{Dt} - \left[\left\langle \frac{Dv_j}{Dt} \right\rangle - \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} \right] &= v \nabla^2 v_j + \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} \\ &\quad - \frac{1}{f} \frac{\delta p'}{\delta x_j} \end{aligned}$$

$$\frac{\delta u_j}{\delta t} + (\langle u_i \rangle + u_i) \frac{\delta u_j}{\delta x_i} = -u_i \frac{\delta (\langle u_j \rangle)}{\delta x_i} + \frac{\delta (\langle u_i \cdot u_j \rangle)}{\delta x_i} + \nabla^2 u_j - \frac{1}{f} \frac{\delta p'}{\delta x_j}$$

Since

$$\frac{du_j}{dt} = \frac{\delta u_j}{\delta t} + (\langle u_i \rangle + u_i) \frac{\delta u_j}{\delta x_i}$$

$$\Rightarrow \frac{du_j}{dt} = -u_i \frac{\delta (\langle u_j \rangle)}{\delta x_i} + \frac{\delta (\langle u_i \cdot u_j \rangle)}{\delta x_i} + \nabla^2 u_j - \frac{1}{f} \frac{\delta p'}{\delta x_j}$$

(b) Multiplying by u_j to the result of part a

$$u_j \cdot \frac{\delta u_j}{\delta t} + (\langle u_j \rangle + u_j) \cdot u_j \cdot \frac{\delta u_j}{\delta x_i} = -u_i \cdot u_j \cdot \frac{\delta (\langle u_j \rangle)}{\delta x_i} + u_j \cdot \frac{\delta (\langle u_i \cdot u_j \rangle)}{\delta x_i} + \nabla^2 u_j u_j - u_j \cdot \frac{1}{f} \frac{\delta p'}{\delta x_j}$$

Since

$$u_j \cdot \frac{\delta u_j}{\delta t} = \frac{\delta u_j^2}{\delta t} = 2 \cdot u_j \cdot \frac{\delta u_j}{\delta t}$$

$$\Rightarrow \frac{1}{2} \cdot \frac{\delta u_j^2}{\delta t} = u_j \cdot \frac{\delta u_j}{\delta t} = \frac{\delta}{\delta t} \left(\frac{1}{2} u_j \cdot u_j \right)$$

$$\frac{\delta}{\delta t} \left(\frac{1}{2} u_j \cdot u_j \right) + \langle u_i \rangle \frac{\delta}{\delta x_i} \left(\frac{1}{2} u_j \cdot u_j \right) + \frac{\delta}{\delta x_i} \left(\frac{1}{2} u_i \cdot u_j \cdot u_j \right)$$

$$= -u_i \cdot u_j \cdot \frac{\delta (\langle u_j \rangle)}{\delta x_i} + u_j \cdot \frac{\delta (\langle u_i \cdot u_j \rangle)}{\delta x_i} + \nabla^2 u_j u_j - u_j \cdot \frac{1}{f} \frac{\delta p'}{\delta x_j}$$

$$\frac{Dv_j}{Dt} - \left[\frac{\delta \langle v_j \rangle}{\delta t} + \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} - \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} \right] = v \nabla^2 v_j + \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} - \frac{1}{\rho} \frac{\delta p'}{\delta x_j}$$

$$\frac{Dv_j}{Dt} = \frac{\delta \langle v_j \rangle}{\delta t} - \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} = v \nabla^2 v_j - \frac{1}{\rho} \frac{\delta p'}{\delta x_j}$$

$$\frac{\delta v_j}{\delta t} + \frac{\delta (v_i \cdot v_j)}{\delta x_i} - \frac{\delta \langle v_j \rangle}{\delta t} - \frac{\delta \langle v_i \cdot v_j \rangle}{\delta x_i} = v \nabla^2 v_j - \frac{1}{\rho} \frac{\delta p'}{\delta x_j}$$

Using $v = V - \langle v \rangle$

$$\Rightarrow \frac{\delta v_j}{\delta t} + \frac{\delta}{\delta x_i} (v_i \cdot v_j - \langle v_i \cdot v_j \rangle) = v \nabla^2 v_j - \frac{1}{\rho} \frac{\delta p'}{\delta x_j}$$

Since

$$\begin{aligned} \frac{\delta}{\delta x_i} (v_i \cdot v_j - \langle v_i \cdot v_j \rangle) &= \frac{\delta}{\delta x_i} (v_i \langle v_j \rangle + v_j \langle v_i \rangle + v_i \cdot v_j - \langle v_i \cdot v_j \rangle) \\ &= v_i \frac{\delta}{\delta x_i} (\langle v_j \rangle) + \langle v_i \rangle \frac{\delta}{\delta x_i} v_j + v_i \frac{\delta v_j}{\delta x_i} - \frac{\delta}{\delta x_i} (\langle v_i \cdot v_j \rangle) \end{aligned}$$

$$\begin{aligned} \Rightarrow \frac{\delta v_j}{\delta t} + v_i \frac{\delta}{\delta x_i} (\langle v_j \rangle) + \langle v_i \rangle \frac{\delta v_j}{\delta x_i} + v_i \frac{\delta v_j}{\delta x_i} - \frac{\delta (\langle v_i \cdot v_j \rangle)}{\delta x_i} \\ = v \nabla^2 v_j - \frac{1}{\rho} \frac{\delta p'}{\delta x_j} \end{aligned}$$

$$\begin{aligned} \frac{\delta v_j}{\delta t} + \langle v_i \rangle \frac{\delta v_j}{\delta x_i} + v_i \frac{\delta v_j}{\delta x_i} &= -v_i \frac{\delta}{\delta x_i} (\langle v_j \rangle) + \frac{\delta (\langle v_i \cdot v_j \rangle)}{\delta x_i} \\ &\quad + v \nabla^2 v_j - \frac{1}{\rho} \frac{\delta p'}{\delta x_j} \end{aligned}$$

Taking the average and let $\langle U_i \rangle = 0$

$$k = \left\langle \frac{1}{2} u_j \cdot u_j \right\rangle$$

$$\begin{aligned} \frac{dk}{dt} + \langle U_i \rangle \frac{dk}{dx_i} + \frac{\delta}{\delta x_i} \left\langle \frac{1}{2} u_i \cdot u_j \cdot u_j \right\rangle \\ = -\langle u_i \cdot u_j \rangle \frac{\delta}{\delta x_i} \langle u_j \rangle + v \langle u_j \nabla^2 u_j \rangle - \frac{1}{f} \frac{\delta \langle u_j \cdot p' \rangle}{\delta x_j} \end{aligned}$$

Since $v \langle u_j \nabla^2 u_j \rangle = 2 \cdot v \cdot \frac{\delta}{\delta x_i} \langle u_j \cdot s_{ij} \rangle - \epsilon$

$$\begin{aligned} T_i = \left\langle \frac{1}{2} u_i \cdot u_j \cdot u_j \right\rangle - 2 \cdot v \cdot \langle u_j \cdot s_{ij} \rangle + \frac{\langle u_j \cdot p' \rangle}{f} \\ \Rightarrow \frac{dk}{dt} + \langle U_i \rangle \frac{dk}{dx_i} + \frac{\delta}{\delta x_i} \left\langle \frac{1}{2} u_i \cdot u_j \cdot u_j \right\rangle \end{aligned}$$

$$\begin{aligned} = -\langle u_i \cdot u_j \rangle \frac{\delta}{\delta x_i} \langle u_j \rangle + 2 \cdot v \cdot \frac{\delta}{\delta x_i} \langle u_j \cdot s_{ij} \rangle \\ - \epsilon - \frac{1}{f} \frac{\delta \langle u_j \cdot p' \rangle}{\delta x_j} \end{aligned}$$

$$\begin{aligned} \Rightarrow \frac{dk}{dt} + \langle U_i \rangle \frac{dk}{dx_i} + \frac{\delta}{\delta x_i} \left(\left\langle \frac{1}{2} u_i \cdot u_j \cdot u_j \right\rangle - 2v \langle u_j \cdot s_{ij} \rangle \right. \\ \left. + \frac{\langle u_j \cdot p' \rangle}{f} \right) = -\langle u_i \cdot u_j \rangle \frac{\delta}{\delta x_i} \langle u_j \rangle - \epsilon \end{aligned}$$

~~For~~ Fluctuating flux of energy $T_i' = \left\langle \frac{1}{2} u_i \cdot u_j \cdot u_j \right\rangle - 2v \langle u_j \cdot s_{ij} \rangle + \frac{\langle u_j \cdot p' \rangle}{f}$

Production term: $P = -\langle u_i \cdot u_j \rangle \frac{\delta}{\delta x_i} \langle u_j \rangle$

$$\Rightarrow \frac{dk}{dt} + v \cdot T_i' = P - \epsilon$$

8.3)

$$\vec{F}_D = \frac{1}{2} C_D A_x \rho V^2$$

$$\vec{F}_B = (\rho_L - \rho_g) g V$$

a) Using force balance including drag force & buoyancy force

$$F_b = (\rho_L - \rho_g) g V$$

$$F_D = \frac{1}{2} C_D A_x \rho_L V^2$$

$$F_b = F_D \Rightarrow (\rho_L - \rho_g) g V = \frac{1}{2} C_D A_x \rho_L V^2$$

where A_x is the cross sectional area of the spherical bulb and V is its volume

$$A_x = \frac{\pi D_{av}^2}{4} \quad , \quad V = \frac{\pi D_{av}^3}{6}$$

$$V_h = \sqrt{\frac{4(\rho_L - \rho_g) D_{av} \cdot g}{3 C_D \rho_L}}$$

Problem 8.4

- 1) Group 1: Mean diameter of 1mm and volume fractions of 3%
 2) Group 2: " 1.5mm 1%
 3) Group 3: " 2.0mm " " " 1%

$$V_{2\phi} = 0.6 D_{dv} d_{dv} / V_N$$

a)

$$V_N = \sqrt{\frac{4(\rho_L - \rho_g) D_{dv} \cdot g}{3 C_D \rho_L}} \quad (1)$$

Under the condition of room temp and 1 atm

$$\rho_L = 999.21 \frac{\text{kg}}{\text{m}^3}, \quad \rho_g = 1.205 \text{ kg/m}^3$$

$$\text{Substituting in (1)} \quad D_{dv} = [1 \times 10^{-3}, 1.5 \times 10^{-3}, 2.0 \times 10^{-3}] \text{ m}$$

$$V_{N1} = 0.163 \text{ m/s} \Rightarrow V_{2\phi 1} = 0.6 D_{dv1} \cdot d_{dv1} \cdot V_{N1} = 2.938 \times 10^{-6} \text{ m}^2/\text{s}$$

$$V_{N2} = 0.19988 \text{ m/s} \Rightarrow V_{2\phi 2} = 0.6 D_{dv2} \cdot d_{dv2} \cdot V_{N2} = 1.7989 \times 10^{-6} \text{ m}^2/\text{s}$$

$$V_{N3} = 0.23 \text{ m/s} \Rightarrow V_{2\phi 3} = 0.6 D_{dv3} \cdot d_{dv3} \cdot V_{N3} = 2.7696 \times 10^{-6} \text{ m}^2/\text{s}$$

Normalized velocity contributions

$$\frac{V_{2\phi 1}}{V_{CL}} = 2.798, \quad \frac{V_{2\phi 2}}{V_{CL}} = 1.73, \quad \frac{V_{2\phi 3}}{V_{CL}} = 2.6378$$

(b) $\alpha = 5\%$

$$D_{dve} = \frac{3}{5} \cdot D_{dv1} + \frac{1}{5} D_{dv2} + \frac{1}{5} D_{dv3} = 1.3 \text{ mm}$$

$$V_{Ne} = \sqrt{\frac{4(\rho_L - \rho_g) D_{dve} \cdot g}{3 C_D \rho_L}} = \cancel{0.17 \text{ m/s}} \quad 0.186 \text{ m/s}$$

$$V_{2\phi e} = 0.6 D_{dve} \cdot d_{dve} \cdot V_{Ne} = 7.257 \times 10^{-6} \text{ m}^2/\text{s}$$

$$\frac{V_{2\phi e}}{V_{CL}} = 6.911$$

[Void fraction has the greatest influence on $V_{2\phi}$, since α is high for equivalent group $V_{2\phi}$ will be higher than the others combined]