The University of Maine

DigitalCommons@UMaine

Electronic Theses and Dissertations

Fogler Library

Spring 5-2020

UAV 6DOF Simulation and Kalman Filter for Localizing Radioactive Sources

John G. Goulet Univeristy of Maine, john.goulet@maine.edu

Follow this and additional works at: https://digitalcommons.library.umaine.edu/etd



Part of the Engineering Physics Commons, and the Navigation, Guidance, Control and Dynamics

Commons

Recommended Citation

Goulet, John G., "UAV 6DOF Simulation and Kalman Filter for Localizing Radioactive Sources" (2020). Electronic Theses and Dissertations. 3182.

https://digitalcommons.library.umaine.edu/etd/3182

This Open-Access Thesis is brought to you for free and open access by DigitalCommons@UMaine. It has been accepted for inclusion in Electronic Theses and Dissertations by an authorized administrator of DigitalCommons@UMaine. For more information, please contact um.library.technical.services@maine.edu.

UAV 6DOF SIMULATION AND KALMAN FILTER FOR LOCALIZING RADIOACTIVE SOURCES

By

John George Goulet

B.S., University of Maine, 2017

A THESIS

Submitted in Partial Fulfillment of the Requirements for the Degree of Master of Engineering (in Engineering Physics)

The Graduate School
The University of Maine
May 2020

Advisory Committee:

C.T. Hess, Professor of Physics and Astronomy, Advisor

Sam Hess, Professor of Physics and Astronomy

David Rubenstein, President/Research Engineer, Maine Aerospace Consulting, LLC.

UAV 6DOF SIMULATION AND KALMAN FILTER FOR LOCALIZING RADIOACTIVE SOURCES

By John George Goulet

Thesis Advisor: Dr. C.T. Hess

An Abstract of the Thesis Presented in Partial Fulfillment of the Requirements for the Degree of Master of Engineering (in Engineering Physics) May 2020

Unmanned Aerial Vehicles (UAVs) expand the available mission-space for a wide range of budgets. Using MATLAB, this project has developed a six degree of freedom (6DOF) simulation of UAV flight, an Extended Kalman Filter (EKF), and an algorithm for localizing radioactive sources using low-cost hardware. The EKF uses simulated low-cost instruments in an effort to estimate the UAV state throughout simulated flight.

The 6DOF simulates aerodynamics, physics, and controls throughout the flight and provides outputs for each time step. Additionally, the 6DOF simulation offers the ability to control UAV flight via preset waypoints or in realtime via keyboard input.

Using low-cost instruments, the EKF fuses measurements with a nonlinear UAV model to estimate UAV states. The 6DOF simulation was used to compare the true UAV states with the estimated states. EKF results indicate appropriate estimation of states with the exception of UAV yaw. An additional sensor providing yaw information would improve estimation accuracy.

Radioactive sensors which are capable of providing position information are prohibitively expensive. The radioactive source localization algorithm utilizes count-based sensors such as a Geiger counter to estimate the location of a radioactive source. The algorithm constructs a three dimensional gradient using six measurements and attempts to

determine the source position from this gradient. The algorithm was developed such that a wide range of environmental parameters could be localized by swapping the Geiger counter with an alternative count-based instrument.

ACKNOWLEDGEMENTS

I would like to thank Dr. C.T. Hess and my entire committee for their understanding and assistance while working on this thesis remotely. Dr. C.T. Hess's patience, understanding, and input was a critical help throughout the completion of this thesis. I would like to thank Dr. Sam Hess for my first introduction to quadcopters and his responsiveness while working remotely. Additionally, I would like to thank Dr. David Rubenstein for the opportunity to learn from his expertise as well as his participation in hosting three independent studies. I would like to thank Dr. Alex Friess for all aviation related discussions and fueling my interest in aviation. I would like to thank Dr. Richard Eason for his assistance and flight training. I would like to thank my girlfriend, Katie Manzo for her love and continued support in everything I set my mind to. I would like to thank my parents, Ron and Jaye Goulet and my brothers, Raymond and Jason Goulet, for their assistance, dedication, and support over all these years. I would like to thank Will Riihiluoma, Katee Schultz, Mary Jane Yeckley, and Ben Hebert. Finally, I would like to thank anyone not explicitly mentioned that supported me during my time at the University of Maine.

CONTENTS

Α(CKNO	OWLEI	DGEMENTS	ii
LI	ST O	F TAB	LES	vi
LI	ST O	F FIGU	URES	vii
TA	ABLE	OF VA	ARIABLES	ix
1.	INT	RODU	TCTION	1
2.	ME	THOD	S	3
	2.1	UAV 1	Dynamics	3
		2.1.1	UAV Orientation	4
		2.1.2	Aerodynamics	6
		2.1.3	Basic Quadcopter Motion	8
		2.1.4	UAV Equations of Motion	9
	2.2	Contro	ols	10
		2.2.1	UAV Hover and Altitude Control	10
		2.2.2	UAV Roll, Pitch, and Horizontal Motion Control	11
	2.3	UAV (6DOF Simulation	13
	2.4	UAV S	Sensors	15
		2.4.1	GPS	15
			2.4.1.1 Pros	15
			2.4.1.2 Cons	15

		2.4.2	Altimeter	16
			2.4.2.1 Pros	16
			2.4.2.2 Cons	16
		2.4.3	LIDAR	16
			2.4.3.1 Pros	17
			2.4.3.2 Cons	17
		2.4.4	IMU (Inertial Measurement Unit)	17
			2.4.4.1 Pros	18
			2.4.4.2 Cons	19
	2.5	Extend	ded Kalman Filter	19
		2.5.1	Time Update	20
		2.5.2	Measurement Update	22
	2.6	Radioa	active Source Localization	23
		2.6.1	Estimation Logic	26
3.	RES	SULTS		31
	3.1	Simula	ation	31
		3.1.1	Waypoint Flight	31
		3.1.2	Manual Flight	36
	3.2	Kalma	n Filter	40
		3.2.1	Waypoint Flight	40
	3.3	Radioa	active Source Localization	43
		3.3.1	Case 1: 1mCi Source	44
		3.3.2	Case 2: 0.1mCi Source	49

4.	DIS	CUSSI	ON	50
	4.1	Simula	tion	50
	4.2	Kalma	n Filter	51
	4.3	Radioa	active Source Localization	51
		4.3.1	1mCi Case	51
		4.3.2	0.1mCi Case	54
5.	CO	NCLUS	ION	55
	5.1	Future	Work	55
		5.1.1	Simulation Verification	56
		5.1.2	Simulation Improvements	56
		5.1.3	Extended Kalman Filter	56
		5.1.4	Source Localization	56
		5.1.5	Source Localization In the EKF	57
ВΙ	BLIC	GRAP:	HY	58
ΑI	PPEN	DIX A	– UAV SIMULATION	60
AI	PPEN	DIX B	- MEASUREMENT MODELS	92
AI	PPEN	DIX C	– KALMAN FILTER	120
AI	PPEN	DIX D	- UTILITIES	170
ΑI	PPEN	DIX E	– RADIOACTIVE SOURCE LOCALIZATION	206
ВΙ	OGR	APHY	OF THE AUTHOR	217

LIST OF TABLES

1	Variable definitions	1X
1	Variable definitions (continued)	х
1	Variable definitions (continued)	xi
1	Variable definitions (continued)	xii
Table 2.1	Keyboard control inputs for UAV simulation	14
Table 2.2	Instrument models and quantities measured.	15
Table 2.3	Kalman state vector composition.	19
Table 2.4	Variable definitions for the Extended Kalman Filter	21
Table 3.1	UAV commanded waypoints	31
Table 4.1	Time until UAV reaches target waypoint	50

LIST OF FIGURES

Figure 2.1	UAV body-frame diagram	3
Figure 2.2	UAV Euler angles	5
Figure 2.3	All UAV Euler angles	6
Figure 2.4	UAV Yaw diagram.	9
Figure 2.5	Accelerometer measurement with zero net force	18
Figure 2.6	Localization algorithm measurement points	25
Figure 2.7	Localization algorithm logic for $A_0 \ge (A, A_+) \& \Delta d > 0.9m$	27
Figure 2.8	Localization algorithm logic for $A_0 \ge (A, A_+) \& 0.5m < \Delta d \le 0.9m$	28
Figure 2.9	Localization algorithm logic for $A_0 \ge (A, A_+) \& \Delta d \le 0.5m$	28
Figure 2.10	Localization algorithm logic for $(A_0 - \sigma_0) < \max(A_+, A) \& \Delta d \ge 1.5$	29
Figure 2.11	Block diagram illustrating radioactive source localization logic	30
Figure 3.1	Waypoint flight - UAV position vs time	32
Figure 3.2	Waypoint flight - UAV altitude vs time	32
Figure 3.3	Waypoint flight - UAV commanded position error vs time	33
Figure 3.4	Waypoint flight - UAV commanded distance error vs time	33
Figure 3.5	Waypoint flight - velocity vs time	34
Figure 3.6	Waypoint flight - acceleration vs time	34
Figure 3.7	Waypoint flight - Euler angles vs time	35
Figure 3.8	Waypoint flight - commanded Euler angle error vs time	35

Figure 3.9	Manual flight - UAV position vs time	36
Figure 3.10	Manual flight - UAV altitude vs time	37
Figure 3.11	Manual flight - velocity vs time	37
Figure 3.12	Manual flight - acceleration vs time	38
Figure 3.13	Manual flight - Euler angles vs time	38
Figure 3.14	Manual flight - commanded euler angle error vs time	39
Figure 3.15	Kalman and truth - position vs time	40
Figure 3.16	Kalman and truth - altitude vs time	41
Figure 3.17	Kalman and truth - velocity vs time	41
Figure 3.18	Kalman and truth - acceleration vs time	42
Figure 3.19	Kalman and truth - Euler angles vs time	42
Figure 3.20	Run convergence for the 1mCi and 0.1mCi cases	43
Figure 3.21	Number of iterations required for the UAV to localize the source within 1m	44
Figure 3.22	Average length of time before the UAV will start it's first localization run.	45
Figure 3.23	1mCi Source initialized 10m away - Kalman UAV position vs time	45
Figure 3.24	1mCi Source initialized 10m away - Kalman UAV altitude vs time	46
Figure 3.25	1mCi Source initialized 10m away - Kalman velocity vs time	46
Figure 3.26	1mCi Source initialized 10m away - Kalman acceleration vs time	47
Figure 3.27	1mCi Source initialized 10m away - Kalman Euler angles vs time	47

Figure 3.28		1mCi Source initialized 10m away - Kalman source distance from			
		UAV	vs time	48	
Fi	gure 4.1	Expe	ected activity measurements as distance increases	52	
Fi	gure 4.2	Prob	ability that the farther activity measurement will be greater		
		than	the closer activity measurement's mean	53	
			Table 1: Variable definitions		
	Variable		Definition	-	
	$B\vec{A}$		Sum of aerodynamic forces in the body frame.	-	
	A		Activity		
	A_{thresh}		Activity threshold		
	A_{+}		Activity measured along positive axis		
A_{-} Superscri			Activity measured along negative axis		
		pt B	Variable expressed in body frame.		
	b_x		body-frame x-coordinate		
	b_y		body-frame y-coordinate		
	b_z		body-frame z-coordinate		
	CG		Center of gravity		
	C_T		Thrust coefficient		
	C_D		Drag coefficient		
	$^Wec{D}$		Drag vector expressed in the wind frame.		
	$^{B}ec{D}$		Drag vector expressed in the body frame.		
	DCM		Direction cosine matrix		
	$_BT_I$		Inertial to body DCM		
	$_IT_B$		Body to inertial DCM		
	$_BT_W$		Body to wind DCM		

Table 1: Variable definitions (continued)

Variable	Definition	
$_WT_B$	Wind to body DCM	
d	Distance to a source	
${}^Bec{F}$	External forces expressed in the body frame.	
$oldsymbol{F}_{k-1}$	System-update matrix	
f_{k-1}	System update function to update state from x_{k-1} to x_k	
$^{I}ec{g}$	Local acceleration due to gravity expressed in the inertial frame.	
H	Angular momentum	
h_k	Measurement function	
$oldsymbol{H}_k$	measurement matrix	
$^{B}oldsymbol{I}$	Inertia matrix expressed in the body frame.	
K_p	Proportional gain	
K_d	Derivative gain	
K_i	Integral gain	
$oldsymbol{K}_k$	Kalman gain matrix	
L	Propeller length	
m	UAV mass	
${}^B ec{M}$	External torques expressed in the body frame.	
${}^Bec{M}_{T_i}$	Torque due to thrust from ith propeller expressed in the body frame.	
$^{B}ec{M}_{T}$	Torque due to thrust from all propellers in the body frame.	
NED	North-East-Down frame.	
$oldsymbol{P}_k^-$	a priori Estimation error covariance matrix	
\boldsymbol{P}_k^+	a posteriori Estimation error covariance matrix	
$oldsymbol{Q}_k$	System noise covariance	
$oldsymbol{R}_k$	Measurement noise covariance	

Table 1: Variable definitions (continued)

Variable	Definition
$^{B}\vec{r}_{\mathrm{prop}_{i}}$ Propeller position relative to the body frame.	
$^{I}\vec{r_{s}}ource$	Source position expressed in the inertial frame.
$^{I}ec{r}_{UAV}$	UAV inertial position
S_{prop}	Propeller reference area
S_{UAV}	UAV reference area
$^Bec{T_i}$	Thrust vector from ith propeller expressed in the body frame.
$^Bec{T}$	Sum of propeller thrust vectors expressed in the body frame.
u	Body-frame x-velocity
u	System input vector
V	Airspeed
$^Bec{v}$	Translational velocity of the body expressed in the body frame.
v	Body-frame y-velocity
w	Body-frame z-velocity
x_k	True state estimate at time k
\hat{x}_k^-	a priori state estimate
\hat{x}_k^+	a posteriori state estimate
w_{k-1}	System noise
y_k	Measurement vector
α	Angle of attack
β	Side-slip angle
Δz	Error from target altitude.
$\Delta \dot{z}$	Error from target vertical velocity.
$\Delta\phi$	Error from target roll
$\Delta \dot{\phi}$	Error from target roll

Table 1: Variable definitions (continued)

Variable	Definition	
$\Delta \theta$	Error from target pitch	
$\Delta\dot{ heta}$	Error from target pitch rate	
θ	Pitch	
$\dot{ heta}$	Pitch rate	
θ_c	Commanded pitch	
λ	Propeller rotation speed squared.	
$ u_k$	Measurement noise	
ρ	Density of air	
σ_{+}	Standard deviation of activity measured along positive axis.	
σ_{-}	Standard deviation of activity measured along negative axis.	
ϕ	Roll	
$\dot{\phi}$	Roll rate	
ϕ_c	Commanded roll	
ψ	Yaw	
$\dot{\psi}$	Yaw rate	
χ	Obstacle position	
$\vec{\omega}$	Angular velocity of the body.	

CHAPTER 1

INTRODUCTION

Unmanned aerial vehicle (UAV) popularity has skyrocketed given the numerous applications and uses they provide. UAVs typically require no fuel (most are powered by electric motors), require little space for takeoff, provide a cost-effective means for payload transportation, and can travel to hazardous locations. Some of the many fields that utilize UAVs include aerospace, forestry, search and rescue, remote sensing, photography, remote imaging, mapping, and exploration.

The ability to quickly navigate throughout hazardous locations allows for the mapping of regions unsuitable for humans. These regions may have high concentrations of radioactivity, harmful gasses, or any number of qualities harmful to humans. This thesis focuses on environments with high concentrations of radioactivity. Measuring the location of radioactive sources typically requires the use of high cost, stationary sensors. Low cost sensors, such as Geiger counters, are count-based and provide no information on the position or direction of a radioactive source. By combining the mobility of a UAV with a Geiger counter (or another count-based instrument), an algorithm has been developed to estimate the position of radioactive sources. The algorithm is not limited to localize radioactive sources. Any count-based instrument could be used for the purpose of measuring a particular environmental parameter of interest.

Estimating the position of radioactive materials using low and high cost sensors has been studied before in [1, 3, 8]. These studies use stationary sensors which may be difficult or impossible to setup in hazardous locations. Additionally, these studies are unable to detect concentrations of radioactivity at a range of altitudes.

The development of an algorithm for localizing a radioactive source was split into three sections. First, a UAV simulation environment was developed in MATLAB for the purpose of testing UAV flight characteristics and source localization. Next, an Extended Kalman

Filter was developed for the purpose of estimating UAV position and attitude. Finally, the localization algorithm was created and verified from the simulation.

CHAPTER 2

METHODS

2.1 UAV Dynamics

The UAV is assumed to be a rigid-body quadcopter whose body frame origin is located at its center of mass (CG). Figure 2.1 shows the body axes from a top-down view of a UAV. The inertial frame of reference is a north-east-down (NED) frame where north, east, and down represent the positive x, y, and z axes respectively. While this is not a true inertial frame, it is sufficient for the purpose of simulating quadcopter flight over a small region.

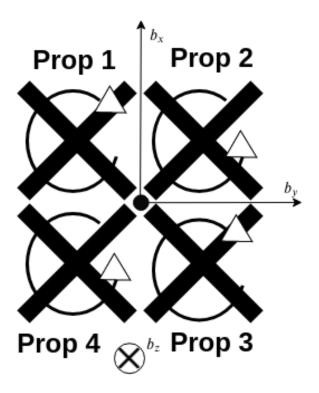


Figure 2.1. UAV body-frame diagram. Diagram indicates body-frame origin, propeller numbering, and direction of propeller rotation. Note the direction of propellers 1 and 3 rotate opposite propellers 2 and 4.

As most UAVs are battery powered, the CG is taken to be time-invariant allowing a simplified version of Euler's rigid body equations of motion to be used as shown in (2.1).

The superscript "B" before a variable indicates that the quantity is formulated in the body-frame.

$$m^{B}\dot{\vec{v}} = {}^{B}\vec{F} - m^{B}\vec{\omega} \times {}^{B}\vec{v}$$

$${}^{B}\boldsymbol{I}\dot{\vec{\omega}} = {}^{B}\vec{\tau} - {}^{B}\vec{\omega} \times {}^{B}\boldsymbol{I}\vec{\omega}$$
(2.1)

Quantities ${}^B\vec{F}$ and ${}^B\vec{\tau}$ represent all inertial forces (non-fictitious) and torques acting on the CG expressed in the body frame. The additional forces acting on the body include gravity, drag, and thrust. Additional torques are nonzero only when UAV propellers have different rotation speeds. ${}^B\pmb{I}$ is the inertia tensor of the UAV with respect to the body frame, ${}^B\vec{v}$ is the translational velocity, and $\vec{\omega}$ is the angular velocity of the body. Note that for clarity, the body-frame is to be the assumed frame of reference unless indicated otherwise.

2.1.1 UAV Orientation

To transform between NED and body frames, a 3-2-1 rotation matrix was constructed using Euler angles ϕ , θ , and ψ (roll, pitch, and yaw). Roll is defined as a rotation about the \hat{b}_x axis with respect to the NED x-y plane, pitch is a rotation about the \hat{b}_y axis with respect to the NED x-y plane, and yaw is a rotation about the \hat{b}_z axis with respect to the NED x-z plane. These definitions are shown in Figure 2.2. An illustration of the Euler angles describing UAV attitude is shown in Figure 2.3. The rates of change of the Euler angles are determined using (2.2). The derivation of (2.2) can be found from a variety of sources such as [5] and is not provided.

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} 1 & \sin \phi \tan \theta & \cos \phi \tan \theta \\ 0 & \cos \phi & -\sin \phi \\ 0 & \sin \phi \sec \theta & \cos \phi \sec \theta \end{bmatrix} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$$
(2.2)

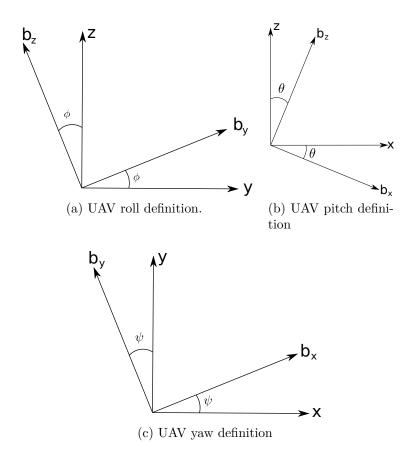


Figure 2.2. UAV Euler angles

Equation 2.3 shows the complete direction cosine matrix (DCM) for transforming from the body frame to the inertial frame. The opposite transform, from inertial to body, can be obtained by taking the matrix transpose of (2.3).

$$IT_{B} = \begin{bmatrix} \cos\theta\cos\psi & \cos\psi\sin\theta\sin\phi - \cos\phi\sin\psi & \sin\phi\sin\psi + \cos\phi\cos\psi\sin\theta \\ \cos\theta\sin\psi & \cos\phi\cos\psi + \sin\theta\sin\phi\sin\psi & \cos\phi\sin\theta\sin\psi - \cos\psi\sin\phi \\ -\sin\theta & \cos\theta\sin\phi & \cos\theta\cos\phi \end{bmatrix}$$
(2.3)

$$_{\boldsymbol{B}}\boldsymbol{T}_{\boldsymbol{I}} = {}_{\boldsymbol{I}}\boldsymbol{T}_{\boldsymbol{B}}^{T} \tag{2.4}$$

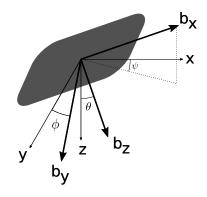


Figure 2.3. All UAV Euler angles

2.1.2 Aerodynamics

Aerodynamic forces acting on a quadcopter UAV include lift, drag, and thrust. In many quadcopter models, lift and drag are neglected due to their small quantities. The aerodynamic model presented includes drag and thrust forces.

Drag is computed in the wind-frame (superscript W) as shown in (2.5). The wind-frame is a frame of reference with the positive x-axis lying along the velocity vector of the aircraft relative to the surround air. The positive z-axis points perpendicular to the x-axis and below the UAV. The positive y-axis completes the right-handed coordinate system.

$${}^{W}\vec{D} = 0.5\rho V^{2}S_{UAV}C_{D}\begin{bmatrix} -1\\0\\0\end{bmatrix}$$

$$(2.5)$$

In (2.5), ρ is the density of air, V is the UAV velocity relative to the surrounding air, S is the reference area of the UAV, and C_D is the coefficient of drag. $^W\vec{D}$ must be transformed to the body-frame for use in (2.1). The body-to-wind transform matrix is shown in (2.6). The reverse is, again, found by taking its transpose as shown in (2.7). In (2.6), α is the angle of attack and β is the side-slip angle computed using body-frame velocities u, v, and w, as defined in (2.8) and (2.9) respectively.

$$\mathbf{W} \mathbf{T}_{\mathbf{B}} = \begin{bmatrix} \cos \alpha \cos \beta & \sin \beta & -\cos \beta \sin \alpha \\ -\cos \alpha \sin \beta & \cos \beta & \sin \alpha \sin \beta \\ \sin \alpha & 0 & \cos \alpha \end{bmatrix}$$
(2.6)

$$_{B}T_{W} = _{W}T_{B}^{T} \tag{2.7}$$

$$\alpha = \arctan(\frac{w}{u}) \tag{2.8}$$

$$\beta = real(\arcsin(\frac{v}{\sqrt{u^2 + w^2}})) \tag{2.9}$$

Finally, the body-frame drag is shown in (2.10). There is assumed to be no torque on the body from drag.

$${}^{B}\vec{D} = {}_{B}T_{W}{}^{W}\vec{D} \tag{2.10}$$

The thrust force was determined by modeling each propeller blade as a wing slicing the air at a speed equal to the tangential velocity half-way along each propeller. Variable λ is defined as propeller rotation speed squared, allowing propeller thrust to be written as shown in (2.11). Refer to Figure 2.1 to see that the propellers are fixed in the \hat{b}_x - \hat{b}_y plane. Assuming the propellers are fixed in the body xy plane (as indicated in Figure 2.1), thrust must act along the $-\hat{b}_z$ direction.

$${}^{B}\vec{T}_{i} = \begin{bmatrix} 0\\0\\-1 \end{bmatrix} 0.5\rho \lambda_{i} \left(\frac{L}{2}\right)^{2} S_{prop} C_{T}$$

$$(2.11)$$

$${}^{B}\vec{T} = \sum_{i=1}^{4} {}^{B}\vec{T}_{i} \tag{2.12}$$

Thrust forces from each propeller are summed to produce the total thrust force acting on the UAV (2.12). For the *i*th propeller, the cross product of propeller position and propeller thrust results in a torque as shown in (2.13).

$${}^{B}\vec{M}_{T_{i}} = {}^{B}\vec{r}_{\text{prop}_{i}} \times {}^{B}\vec{T}_{i} \tag{2.13}$$

$${}^{B}\vec{M}_{T} = \sum_{i=1}^{4} {}^{B}\vec{M}_{T_{i}} \tag{2.14}$$

Summing the drag force in (2.10) and the thrust force in 2.12 results in the total aerodynamic force acting on the body expressed in the body-frame (2.15).

$${}^B\vec{A} = {}^B\vec{D} + {}^B\vec{T} \tag{2.15}$$

2.1.3 Basic Quadcopter Motion

With thrust defined in the previous section, a discussion on how a quadcopter achieves translational motion may be helpful for those less familiar. Refer to Figure 2.1 for body-axes and propeller numbering.

Roll can be achieved by setting the following conditions: $\lambda_1 = \lambda_4$, $\lambda_2 = \lambda_3$, and finally $\lambda_1 > \lambda_2$ (recall that λ_i is the *i*th propeller rotation speed squared). Under this condition, propellers 1 and 4 will produce a greater thrust than propellers 2 and 3 resulting in a torque about \hat{b}_x (2.13).

The condition for changes in pitch are similar to those for roll. Setting the conditions: $\lambda_1 = \lambda_2$, $\lambda_4 = \lambda_3$, and $\lambda_1 > \lambda_4$ results in a greater thrust force from propellers 1 and 2, thus creating a torque about the \hat{b}_y axis.

If the body x and y axes are aligned with the NED x and y axes, increasing the roll angle will tilt the body z axis in the in the NED $-\hat{y}$ direction, accelerating the UAV east $(+\hat{y}$ direction). Similarly, a positive pitch angle will accelerate the UAV south $(-\hat{x})$.

Yaw motion is less intuitive than roll and pitch. Recall that propellers 1 and 3 rotate opposite the direction of propellers 2 and 4. When all propellers rotate uniformly, the total angular momentum of the system is zero (2.16). Yaw rotation can be induced by changing the propeller rotation speed of diagonal propellers. Figure 2.4 indicates that propellers 1 and 3 rotate faster than propellers 2 and 4. Using (2.17), increasing counter-clockwise propeller speeds will cause the UAV body to rotate clockwise about the \hat{b}_z axis.

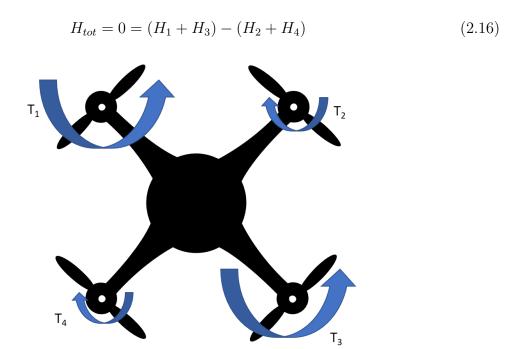


Figure 2.4. UAV Yaw diagram. Propellers 1 and 3 rotate faster than propellers 2 and 4. This will induce a clockwise motion about the UAV.

https://www.clipart.email/download/1486936.html

$$0 = (H_1 + H_3) - (H_2 + H_4) + H_{UAV}$$

$$-H_{UAV} = (H_1 + H_3) - (H_2 + H_4)$$
(2.17)

2.1.4 UAV Equations of Motion

The expanded equations of motion from (2.1) along with all other equations used to model UAV motion are provided below in (2.18) - (2.20) for convenience. Recall that items

in bold indicate matrix or vector quantities. All vectors are written in the body frame unless otherwise noted.

$${}^{B}\dot{\vec{v}} = {}_{B}T_{I}{}^{I}\vec{g} + \frac{1}{m}{}^{B}\vec{A} - {}^{B}\vec{\omega} \times {}^{B}\vec{v}$$

$$(2.18)$$

$${}^{B}\dot{\vec{\omega}} = {}^{B}\boldsymbol{I}^{-1}({}^{B}\vec{M} - {}^{B}\vec{\omega} \times {}^{B}\boldsymbol{I}^{B}\vec{\omega})$$
(2.19)

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} 1 & \sin \phi \tan \theta & \cos \phi \tan \theta \\ 0 & \cos \phi & -\sin \phi \\ 0 & \sin \phi \sec \theta & \cos \phi \sec \theta \end{bmatrix} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$$
(2.20)

2.2 Controls

2.2.1 UAV Hover and Altitude Control

The UAV defaults to hovering at a constant altitude if no commands are input. Equation 2.21 shows the required λ setting to hover while under straight and level flight conditions.

$$\lambda_{\text{hover}} = \frac{mg}{2\rho(0.5L_{prop})^2 S_{prop} C_T}$$
 (2.21)

If the UAV has nonzero roll or pitch, (2.21) will not provide adequate thrust to maintain straight and level flight. Equation 2.22 shows the general form (2.21) that applies for all practical flight conditions.

$$\lambda_{\text{hover}} = \frac{mg}{2\rho(0.5L_{prop})^2 S_{prop} C_T \cos\phi \cos\theta}$$
 (2.22)

For changes in altitude, a proportional-derivative (PD) controller was used to command reasonable changes in propeller rotation speed. The general form of the PD controller is shown in (2.23). K_p and K_d are the proportional and derivative gains which were determined experimentally. Δz is the error between the target altitude (z_t) and the current altitude (z). $\Delta \dot{z}$ is the error between the target z velocity and the actual NED z velocity. The target z velocity is always is always set to zero. If both errors are zero, λ is equal to λ_{hover} .

$$\lambda_{alt} = (1 - K_p \Delta z + K_d \Delta \dot{z}) \lambda_{hover} \tag{2.23}$$

2.2.2 UAV Roll, Pitch, and Horizontal Motion Control

From Chapter 2.1.3, all horizontal motion is directly related to changes in roll and/or pitch angles. Those angles are controlled using a proportional-integral-derivative (PID) controller. The general form of the PID controller used is shown in (2.24).

$$\phi_c = K_p \Delta \phi + K_d \Delta \dot{\phi} + K_i \int_0^T \Delta \phi dt$$

$$\theta_c = K_p \Delta \theta + K_d \Delta \dot{\theta} + K_i \int_0^T \Delta \theta dt$$
(2.24)

The lefthand side of (2.24) (ϕ_c and θ_c) is the roll/pitch angle to be commanded this timestep. The integral term is the sum of all errors leading up to the current simulation time. Note that a maximum rotation angle of five degrees is enforced throughout the simulation. If (2.24) would command a roll or pitch greater than five degrees, the commanded angle is instead set to five degrees. This was done to improve control stability.

With ϕ_c and θ_c known, these commanded angles were used to compute a difference in propeller rotation speeds $(\Delta \lambda)$ based on the desired motion. Each propeller is mounted 45 degrees from the CG, allowing (2.11) to be rewritten as shown in (2.25).

$$M_{i} = \pm T_{i}L_{prop}\cos(45^{\circ})$$

$$M_{i} = \pm \frac{1}{8}\rho L_{prop}^{3}S_{prop}C_{T}\lambda_{i}\cos(45^{\circ})$$

$$M = \frac{1}{8}\rho L_{prop}^{3}S_{prop}C_{T}\cos(45^{\circ})(\pm\lambda_{1}\pm\lambda_{2}\pm\lambda_{3}\pm\lambda_{4})$$

$$(2.25)$$

The signs of λ in (2.25) are determined by the desired direction of motion. If the desired direction of travel is along the b_y direction, (2.25) becomes (2.26).

$$M = \frac{1}{8} \rho L_{prop}^{3} S_{prop} C_{T} \cos(45^{\circ}) (\lambda_{1} + \lambda_{4} - (\lambda_{2} + \lambda_{3}))$$

$$M = \frac{1}{8} \rho L_{prop}^{3} S_{prop} C_{T} \cos(45^{\circ}) (\lambda_{1,4} - \lambda_{2,3})$$

$$M = \frac{1}{8} \rho L_{prop}^{3} S_{prop} C_{T} \cos(45^{\circ}) (\Delta \lambda_{y})$$
(2.26)

Referring back to (2.1), the lefthand side of the torque term is set to the righthand side of (2.27). Equation 2.26 is the τ term.

$$\theta_c = \omega_y \Delta t + 0.5 \dot{\omega}_y (\Delta t)^2$$

$$\dot{\omega}_y = 2 \frac{\theta_c - \omega_y \Delta t}{(\Delta t)^2}$$
(2.27)

$$B \mathbf{I} \dot{\vec{\omega}} = {}^{B} \vec{\tau} - \vec{\omega} \times {}^{B} \mathbf{I} \vec{\omega}$$

$$2I_{yy} \frac{\theta_{c} - \omega_{y} \Delta t}{(\Delta t)^{2}} = \frac{1}{8} \rho L_{prop}^{3} S_{prop} C_{T} \cos(45^{\circ}) (\Delta \lambda_{y}) - (\vec{\omega} \times {}^{B} \mathbf{I} \vec{\omega})_{y}$$
(2.28)

In (2.27) and (2.28), Δt is the simulation timestep and $(\vec{\omega} \times {}^{B}\boldsymbol{I}\vec{\omega})_{y}$ refers to the y-component of the resulting cross product. Solving for $\Delta \lambda_{y}$ gives (2.29).

$$\Delta \lambda_y = \frac{8}{\rho L_{nron}^3 S_{prop} C_T \cos(45^\circ)} \left(2I_{yy} \frac{\theta_c - \omega \Delta t}{(\Delta t)^2} - \left(\vec{\omega} \times {}^B \mathbf{I} \vec{\omega} \right)_y \right)$$
(2.29)

The result of (2.29) is used to set each propeller λ without changing the result of λ_{alt} .

$$\lambda_{1,y} = 0.25 \Delta \lambda_y$$

$$\lambda_{2,y} = -\lambda_{1,y}$$

$$\lambda_{3,y} = \lambda_{2,y}$$

$$\lambda_{4,y} = \lambda_{1,y}$$

$$(2.30)$$

If there are no desired changes in pitch, the vector containing all values of λ are set as follows:

$$\lambda = \lambda_{alt} \begin{bmatrix} 1\\1\\1\\1 \end{bmatrix} + \begin{bmatrix} \lambda_{1,y}\\\lambda_{2,y}\\\lambda_{3,y}\\\lambda_{4,y} \end{bmatrix}$$
(2.31)

Deriving $\Delta \lambda_x$ follows the same procedure for $\Delta \lambda_y$. Replace each y subscript with x in (2.26) through (2.29) and the steps are identical. Unpacking the result of $\Delta \lambda_x$ follows the following format:

$$\lambda_{1,x} = 0.25 \Delta \lambda_x$$

$$\lambda_{2,x} = \lambda_{1,x}$$

$$\lambda_{3,x} = -\lambda_{1,x}$$

$$\lambda_{4,x} = \lambda_{3,x}$$

$$(2.32)$$

For any combination of roll and pitch, λ for each propeller is then found by summing $\lambda_{i,x}$ and $\lambda_{i,y}$ as shown in (2.33).

$$\lambda = \lambda_{alt} \begin{bmatrix} 1 \\ 1 \\ 1 \\ 1 \end{bmatrix} + \begin{bmatrix} \lambda_{1,y} \\ \lambda_{2,y} \\ \lambda_{3,y} \\ \lambda_{4,y} \end{bmatrix} + \begin{bmatrix} \lambda_{1,x} \\ \lambda_{2,x} \\ \lambda_{3,x} \\ \lambda_{4,x} \end{bmatrix}$$

$$(2.33)$$

2.3 UAV 6DOF Simulation

Using the dynamics outlined in Chapter 2.1 to simulate UAV flight and the controls outlined in Chapter 2.2, a six degree-of-freedom (6DOF) simulation was constructed in MATLAB. UAV physical parameters are set using "initialize_uav.m" which is provided in Appendix D. The simulation records the following states: UAV NED position $^{I}\vec{r}_{UAV}$; body velocity $^{B}\vec{v}$; angular velocity $\vec{\omega}$; Euler angles ϕ , θ , and ψ ; obstacle position $^{I}\vec{\chi}$; and source position relative to the UAV $^{I}\vec{r}_{source}$. A basic obstacle position tracking is supported, but

there is no UAV logic implemented to avoid obstacles. These simulated values were used as truth to construct the Extended Kalman Filter and radioactive source position estimates.

$$\left[x = {}^{I}\vec{r}_{UAV} \quad {}^{B}\vec{v} \quad \vec{\omega} \quad \phi \quad \theta \quad \psi \quad {}^{I}\vec{\chi} \quad {}^{I}\vec{r}_{source}\right]$$
(2.34)

The UAV can receive inputs to command translational motion via two inputs. The first, by presetting waypoints which are passed into the simulation. Waypoints take form of a column vector where there first element contains the time for the command to take place and elements two through four contain the desired NED position. An example waypoint is shown in (2.35).

$$\begin{bmatrix} t_1 \\ r_{North} \\ r_{East} \\ r_{Down} \end{bmatrix}$$
 (2.35)

Alternatively, the UAV can be controlled using keyboard inputs outlined in Table 2.1. Setting the value of "showRealtimePlot = 1" will provide realtime display of the UAV. Waypoint control and keyboard control can be used simultaneously with keyboard control overriding waypoint control. The MATLAB code which runs the simulation is provided in Appendix A. Simulation results are shown in Chapter 3.1.

Table 2.1. Keyboard control inputs for UAV simulation.

Key	Command
W	Translate along $+b_x$ direction
\mathbf{S}	Translate along $-b_x$ direction
d	Translate along $+b_y$ direction
a	Translate along $-b_y$ direction

2.4 UAV Sensors

Consumer-grade quadcopters utilize several instruments for position and attitude information throughout a flight. Following the project goals, four low-cost, well documented sensors were chosen and their specifications used in the creation of sensor models. Table 2.2 provides the model number and quantity measured for each instrument.

Table 2.2. Instrument models and quantities measured.

Instrument	Model	Quantity Measured
GPS	GlobalTop MTK3339	Position and Velocity
Altimeter	Bosch BMP388	Altitude
LIDAR	Garmin Lidar-Lite V3	Body-X Obstacle position
IMU	Bosch BNO055	Acceleration and angular velocity

A brief discussion on the pros and cons of each instrument is presented below.

2.4.1 GPS

Global positioning system (GPS) uses a minimum of five satellites to provide a reliable position, velocity, and time solution. Position measurements triangulate your position using three satellites, while velocity measurements use the Doppler shift of the incoming transmission to determine velocity at a much higher accuracy.

2.4.1.1 Pros

- High accuracy. Position accuracy of \pm 3m and velocity accuracy of \pm 0.1m.
- Not typically prone to bias or random walk

2.4.1.2 Cons

- Requires satellite signal, severely limiting suitable environments.
- Low frequency. Typical sample rates of 1Hz.

2.4.2 Altimeter

An altimeter compares the pressure difference between a reference pressure and the current pressure to determine altitude. If altitude relative to sea level (true altitude) is known throughout the flightpath, an altimeter provides high accuracy in its altitude measurements.

2.4.2.1 Pros

- High accuracy. Typical accuracy of about \pm 0.5m.
- High frequency of measurements. 50 90 Hz can be expected.
- Lightweight

2.4.2.2 Cons

• Requires ground level true altitude to be known throughout flightpath.

2.4.3 LIDAR

LIDAR (LIght Detection And Ranging) sensors operate by transmitting a laser and measuring the duration between laser transmission and detection. With the index of refraction known through the medium at which the sensor is operating within, the distance measured by the LIDAR sensor is given in (2.36) where c is the speed of light in a vacuum, n is the index of refraction of the medium, and Δt is the time between laser transmission and detection.

$$\Delta r = \frac{c}{2n} \Delta t \tag{2.36}$$

LIDAR sensors are used in a variety of applications such as mapping terrain for a particular region. The purpose of a LIDAR sensor in this project was for obstacle detection. While obstacle avoidance has not been implemented in this project, the addition of LIDAR models and outputs allows for future inclusion.

2.4.3.1 Pros

- High frequency
- High accuracy

2.4.3.2 Cons

• Expensive

2.4.4 IMU (Inertial Measurement Unit)

The final instrument used is an inertial measurement unit (IMU). An IMU contains at minimum a three-axis accelerometer and a 3-axis gyroscope while newer models may contain magnetometers. An IMU is capable of providing position and attitude information at high frequencies. This information, however, is prone to 'drift' from the true values. Determining velocity from acceleration requires integration from the accelerometer measurement. Any errors in the accelerometer measurement will accumulate when integrated for the velocity measurement. This results in an error accumulation that is linear for velocity and quadratic for position. The same issue is present when determining Euler angles from gyroscope measurements. Position and velocity drift is solved by fusing the GPS and altimeter measurements with the IMU measurements. Only the problem of attitude drift remains.

When the accelerometer measures the magnitude of acceleration to be +1g, the accelerometer can be used as a drift-free method to compute roll and pitch angles. An accelerometer measures proper acceleration, or more simply, acceleration relative to free-fall. When the magnitude of measured acceleration is equal to the local acceleration due to gravity, the components of acceleration can be used to determine UAV roll and pitch [pedley_tilt_2013, 13, 6]. Figure 2.5 illustrates the measured acceleration for a fixed accelerometer which has been tilted with roll angle ϕ and pitch angle θ . Recall that

the acceleration is relative to free-fall, which results in a measured acceleration of +1g when all forces are equal.

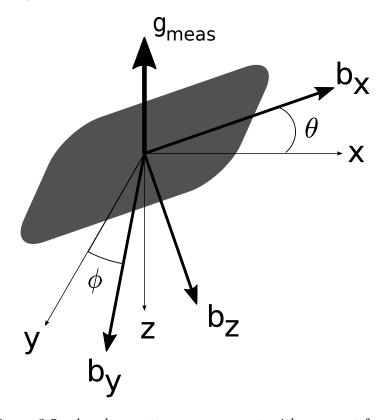


Figure 2.5. Accelerometer measurement with zero net force.

Equation 2.37 provides the trigonometric expressions for computing roll and pitch when the accelerometer is subject to zero net force. While onboard a UAV, this will typically occur during a stable hover.

$$\phi = \arctan\left(\frac{a_y}{a_z}\right)$$

$$\theta = \arctan\left(\frac{-a_x}{\sqrt{a_y^2 + a_z^2}}\right)$$
(2.37)

2.4.4.1 Pros

- High frequency (100 Hz)
- Low cost
- Small form factor

• Capable of producing position and attitude measurements.

2.4.4.2 Cons

- Subject to drift
- Typically will have some form of bias that needs to be estimated.

2.5 Extended Kalman Filter

An Extended Kalman filter (EKF) was created to estimate the true UAV states throughout the duration of a flight. The regular Kalman filter produces an optimal estimate of states described by a linear system [10]. Kalman filters follow a two step process, the first, a time-update step which propagates the state from the k-1 timestep to timestep k. The second, a measurement-update step which improves the state estimate using available measurements. The EKF extends the Kalman filter for nonlinear systems.

For a UAV, the state vector will typically be composed of attitude and position vectors along with their derivatives. The state vector for this EKF is given in (2.38). All vectors in x are relative to the NED frame. The definitions of all variables are presented in Table 2.3.

$$x = \begin{bmatrix} I_{\vec{r}} & I_{\vec{v}} & I_{\vec{a}} & \phi & \theta & \psi & I_{\vec{\chi}} & I_{\vec{s}} \end{bmatrix}$$
 (2.38)

Table 2.3. Kalman state vector composition.

Variable	Definition
$^{I}ec{r}$	UAV NED Position Vector
$^{I}\vec{v}$	UAV NED Velocity Vector
${}^Iec{a}$	UAV NED Acceleration Vector
ϕ	UAV Roll
θ	UAV Pitch
ψ	UAV Yaw
$I_{\vec{S}}$ $I_{\vec{S}}$	UAV NED Obstacle Position
$I\vec{s}$	NED Estimated Source Position

The EKF receives measurements from the following types of instruments:

- GPS
- Altimeter
- LIDAR
- Inertial measurement unit (IMU)

Using the instruments listed previously in Table 2.2, the measurement vector y_k was then defined as shown in (2.39). If a particular instrument is not available at time k, it is not included in y_k .

$$y_k = \begin{bmatrix} y_{\text{GPS}} & y_{\text{altimeter}} & y_{\text{lidar}} & y_{\text{IMU}} \end{bmatrix}$$
 (2.39)

Adopting the convention in [17], the EKF system and measurement equations are presented in (2.40) - (2.43). Variable definitions are given in Table 2.4. The notation used in (2.42) defines w_k as a random variable with a mean of 0 and covariance \mathbf{Q}_k .

$$x_k = f_{k-1}(x_{k-1}, u_{k-1}, w_{k-1}) (2.40)$$

$$y_k = h_k(x_k, \nu_k) \tag{2.41}$$

$$w_k \sim (0, \mathbf{Q}_k) \tag{2.42}$$

$$v_k \sim (0, \mathbf{R}_k) \tag{2.43}$$

All EKF code is provided in Appendix C.

2.5.1 Time Update

The time-update step produces an *a priori* state estimate \hat{x}_k^- and error covariance P_k^- for time k from time k-1 as shown in (2.44) and (2.45).

$$\hat{x}_{k}^{-} = f_{k-1}(\hat{x}_{k-1}^{+}, u_{k-1}, 0) \tag{2.44}$$

Table 2.4. Variable definitions for the Extended Kalman Filter. Variable Definition True state estimate at time k x_k $\hat{x}_k^-\\ \hat{x}_k^+$ a priori state estimate a posteriori state estimate f_{k-1} System update function to update state from x_{k-1} to x_k uSystem input vector w_{k-1} System noise Measurement vector y_k Measurement function h_k Measurement noise ν_k Q_k System noise covariance Measurement noise covariance R_k $oldsymbol{P}_k^- \ oldsymbol{P}_k^+$ a priori Estimation error covariance matrix a posteriori Estimation error covariance matrix F_{k-1} System-update matrix H_k measurement matrix Kalman gain matrix K_k

$$P_k^- = F_{k-1} P_{k-1}^+ F_{k-1}^T + Q_{k-1}$$
(2.45)

The system update function shown in (2.44) takes inputs from the previous *a posteriori* state estimate and the gyroscope (designated as u_{k-1}). The gyroscope angular rates are used to compute Euler rates and Euler angles. The time-update equations performed in f_{k-1} are given in (2.46).

$$\vec{r}_{k} = \vec{r}_{k-1} + \vec{v}_{k-1}\Delta t + 0.5\vec{a}_{k-1}(\Delta t)^{2}$$

$$\vec{v}_{k} = \vec{v}_{k-1} + \vec{a}_{k-1}\Delta t$$

$$\vec{a}_{k} = \left[(-\mathbf{I}\mathbf{T}_{B}\frac{g}{\cos\phi\cos\theta})_{x} \quad (-\mathbf{I}\mathbf{T}_{B}\frac{g}{\cos\phi\cos\theta})_{y} \quad a_{z,k-1} \right]$$

$$\phi_{k} = \phi_{k-1} + \dot{\phi}_{k-1}\Delta t$$

$$\theta_{k} = \theta_{k-1} + \dot{\theta}_{k-1}\Delta t$$

$$\psi_{k} = \psi_{k-1} + \dot{\psi}_{k-1}\Delta t$$

$$\vec{\chi}_{k} = \chi_{k-1} - \vec{v}_{k-1}\Delta t$$

$$(2.46)$$

All terms other than \vec{a}_k follow elementary kinematics. The \vec{a}_k term estimates horizontal acceleration to be a function of the roll and pitch angle with no vertical acceleration. Vertical acceleration remains constant during the time-update step.

The acceleration term does not hold true when the vertical acceleration is nonzero. The horizontal terms will produce adequate estimates which are updated from the accelerometer and GPS. The vertical term, however, relies entirely on the altimeter, accelerometer, and GPS. The high sample rates of the altimeter and accelerometer provide reliable estimates of vertical acceleration.

The second part of the time-update step is to update the error covariance of the state using (2.45). The system-update matrix \mathbf{F}_{k-1} is computed by taking the Jacobian of f_{k-1} evaluated at the last state estimate as shown in (2.47).

$$\mathbf{F}_{k-1} = \frac{\partial f_{k-1}}{\partial x} \Big|_{x_{k-1}^+} \tag{2.47}$$

Term Q_{k-1} represents process noise in the system. The noise can come from numerous sources, but represents inaccuracies in the system-update function. For example, the model does nothing to predict variations in wind which may occur during a standard flight. A well-tuned process noise matrix helps fuse the time-update step with the measurement-update step. Low elements in Q favor the model while high Q values indicate low reliability in the model and have the filter favor the measurements.

2.5.2 Measurement Update

The measurement-update step in the EKF takes all measurements available at time k and updates the *a priori* state estimate \hat{x}_k^- to the *a posteriori* state estimate \hat{x}_k^+ . If any measurements are available, the Kalman gain (2.48), *a posteriori* state estimate (2.49), and *a posteriori* error covariance (2.50) are computed.

$$\boldsymbol{K}_{k} = \boldsymbol{P}_{k}^{-} \boldsymbol{H}_{K}^{T} (\boldsymbol{H}_{k} \boldsymbol{P}_{k}^{-} \boldsymbol{H}_{k}^{T} + \boldsymbol{R}_{k})^{-1}$$
(2.48)

$$\hat{x}_k^+ = \hat{x}_k^- + \mathbf{K}_k(y_k - h_k(\hat{x}_k^-)) \tag{2.49}$$

$$\boldsymbol{P}_{k}^{+} = (\boldsymbol{I} - \boldsymbol{K}_{k} \boldsymbol{H}_{k}) \boldsymbol{P}_{k}^{-} \tag{2.50}$$

To compute the Kalman gain, two matrices must be constructed in advance, the measurement matrix (\mathbf{H}_k) and the measurement noise covariance (\mathbf{R}_k) . Similar to \mathbf{F}_{k-1} , the measurement matrix (2.52) is the Jacobian of the measurement function which outputs measurements from the state vector. Equation 2.51 shows each output term in the measurement function $h_k(\hat{x}_k^-, 0)$. Note that in h_{IMU} , roll and pitch are only used if the UAV is in a stable hover (see Chapter 2.4.4).

$$h_{\text{gps}} = \begin{bmatrix} {}^{I}\vec{r} & {}^{I}\vec{v}_{x,y} \end{bmatrix}$$

$$h_{\text{altimeter}} = -{}^{I}\vec{r}_{z}$$

$$h_{\text{lidar}} = ({}_{B}T_{I}{}^{I}\vec{\chi})_{x} \qquad (2.51)$$

$$h_{\text{IMU}} = \begin{bmatrix} {}_{B}T_{I}{}^{I}\vec{a} & \phi & \theta \end{bmatrix}$$

$$h_{k} = \begin{bmatrix} h_{\text{gps}} & h_{\text{altimeter}} & h_{\text{lidar}} & h_{\text{IMU}} \end{bmatrix}$$

$$\mathbf{H}_{k} = \frac{\partial h_{k}}{\partial x} \Big|_{x\overline{z}} \qquad (2.52)$$

The measurement covariance matrix \mathbf{R}_k remains constant between timesteps. This matrix was built using specifications for each instrument listed in Table 2.2.

2.6 Radioactive Source Localization

Following the completion of the 6DOF simulation and the EKF, an algorithm estimating the position of a radioactive source was created. The measurements received were assumed to take the form of counts where a desired count rate could be determined.

This allows for measurements from a traditional (and low cost) Geiger counter as well as any consumer-grade CCD [4].

Measurements from a count-based device can be modelled as a Poisson distribution. One of the challenges in working with such a device is that the standard deviation is equal to the square root of the number of counts recorded (2.53). As such, longer recording times produce favorable measurements. Measurement duration, is limited by UAV maximum flight time.

$$\sigma = \sqrt{A} \tag{2.53}$$

The general idea of the algorithm is to construct a gradient by recording measurements at six different points in space for a uniform duration as shown in Figure 2.6. The UAV then flies to the region with the greatest gradient. Recursively running the algorithm allows the UAV to converge on the radioactive source. The decay rate near the source (A_0) is assumed to be approximately known.

When the UAV is commanded to estimate radioactive source position, the following steps are taken:

- 1. Record current position as the gradient center.
- 2. Fly one meter north of the gradient center.
- 3. Hold position for 30 seconds to record counts.
- 4. Repeat steps 2 and 3 flying south, east, west, down, and up.
- 5. Compute estimated source position.
- 6. Fly to estimated source position and return to step 1.

The distance flown and measurement duration listed may be varied before running the simulation. Note that the UAV will never be commended to fly lower than 10cm above the ground.

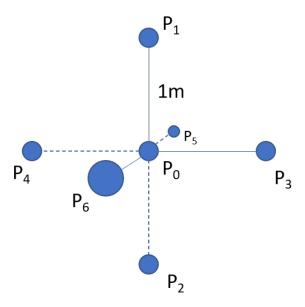


Figure 2.6. Localization algorithm measurement points. The UAV begins at P_0 and flies to P_1 - P_6 , stopping at each point to measure radioactivity for 30 seconds. Note that P_5 and P_6 are into the page and out of the page respectively.

To trigger the algorithm, the background activity should be known and an activity threshold must be set. If the last full second of counts is above the threshold, the position estimation algorithm is triggered. To minimize background radioactivity triggering the estimation algorithm, the activity threshold was set such that the probability of background radiation being greater than or equal to the activity threshold was nearly zero. In all test cases presented in Chapter 3.3, activity threshold is set to five counts per second and background is set to one count per second. The probability of background exceeding the five counts per second was determined using (2.54) to be 0.37%.

$$P(k > \lambda) = \sum_{k=0}^{\infty} \frac{\lambda^k e^{-\lambda}}{k!}$$
 (2.54)

The source localization code is presented in Appendix E.

2.6.1 Estimation Logic

For some distance d away from a source, (2.55) can be used to compute the distance from a radioactive source. A_0 is the known activity at distance d_0 and A is the source activity recorded within the timespan (30 seconds by default).

$$d = d_0 \sqrt{\frac{A_0}{A}} \tag{2.55}$$

Each axis is observed separately. Recall that two sets of data are taken along each axis. Thus we have two values for d: d_- and d_+ . Additionally, the activity at both locations can be used to determine which direction the source lies. If $A_+ > A_-$, then the source must lie in the positive direction. The estimated distance along this axis is determined by the difference between d_- and d_+ which is defined as Δd . There are two scenarios to examine. The first, and most common, occurs when A_+ and A_- are less than A_0 . The second, when a measured activity is greater than A_0 . All possible outcomes are presented below. Note r_i represents the ith axis where i is either the north axis, east axis, or down axis. All outcomes listed below also require (2.56) to be satisfied. If this condition is not met, both measured activities fall within the same standard deviation. This would permit only small or zero UAV motion.

$$|\Delta A_{+,-}| > \sqrt{\min(A_+, A_-)}$$

 $|\Delta A_{+,-}| > \min(\sigma_+, \sigma_-)$ (2.56)

 $A_0 \geq (A_-, A_+)$ & $\Delta d > 0.9m$: Under these conditions, the source is significantly closer to one measurement location than the other. As such, the measurement with more counts is used to determine source distance. Figure 2.7 illustrates an example of when this may occur. Equation 2.57 shows the equation used if $A_+ > A_-$. If $A_- > A_+$, then replace d_+ with d_- .

$$r_i = \operatorname{sign}(\Delta A)d_+ \tag{2.57}$$

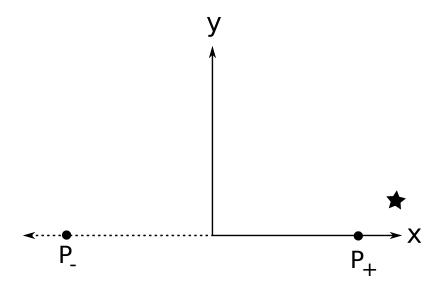


Figure 2.7. Localization algorithm logic for $A_0 \ge (A_-, A_+) \& \Delta d > 0.9m$. Measurement points represented by P_+ and P_- . The star shows the relative source location.

 $A_0 \ge (A_-, A_+)$ & $0.5m < \Delta d \le 0.9m$: This condition is likely to occur when the source does not lie close to a single measurement point, but lies near the line segment between the two points as shown in Figure 2.8. Equation 2.58 shows the equation used if $A_+ > A_-$.

$$r_i = \operatorname{sign}(\Delta d)|d_+ - 1\mathbf{m}| \tag{2.58}$$

 $A_0 \ge (A_-, A_+)$ & $\Delta d \le 0.5m$: This condition is likely to occur when the source lies near the gradient center. See Figure 2.9 for an illustration.

$$r_i = \operatorname{sign}(\Delta d) \frac{|d_+ - d_-|}{2} \tag{2.59}$$

 $(A_0 - \sqrt{A_0}) < \max(A_+, A_-)$ & $\Delta d \ge 1.5$: If this condition is met, the result is that one of the measurements is greater than A_0 meaning it is actually closer to the source than r_0 . The UAV disregards the lower activity measurement and flies to the point where the measurement was taken. Figure 2.10 provides an example of this scenario.

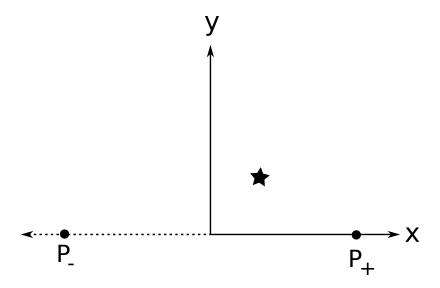


Figure 2.8. Localization algorithm logic for $A_0 \ge (A_-, A_+) \& 0.5m < \Delta d \le 0.9m$. Measurement points represented by P_+ and P_- . The star shows the relative source location.

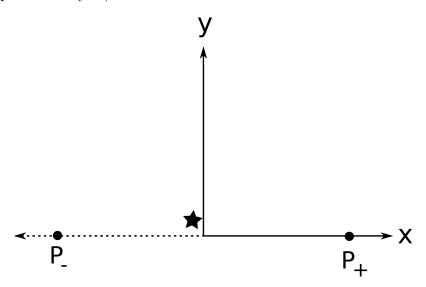


Figure 2.9. Localization algorithm logic for $A_0 \ge (A_-, A_+)$ & $\Delta d \le 0.5m$. Measurement points represented by P_+ and P_- . The star shows the relative source location.

$$r_i = r_{max,i} - r_{center,i} (2.60)$$

Once r_i has been determined from the scenarios listed above, there are checks to prevent poor measurements from compromising the algorithm. For example, (2.61) shows the maximum possible source distance, along any axis, within 1σ of A_0 . If r_i is greater

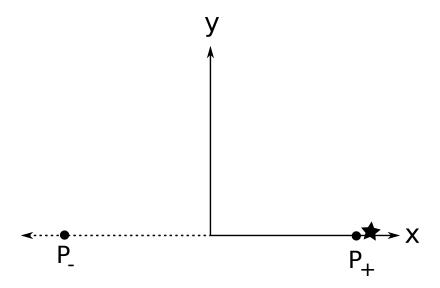


Figure 2.10. Localization algorithm logic for $(A_0 - \sigma_0) < \max(A_+, A_-) \& \Delta d \ge 1.5$. Measurement points represented by P_+ and P_- . The star shows the relative source location.

than r_{max} , r_i is set to zero. This is likely to occur if the source is located more than one meter along a plane orthogonal to the current axis.

$$r_{max} = r_0 \frac{\sqrt{A_0 + \sqrt{A_0}}}{A_{thresh}} \tag{2.61}$$

An additional check requires that the difference in measured activity must be greater than the minimum standard deviation as shown in (2.62). If this condition is violated, the UAV is either too far from the source to produce unique measurements or the UAV is nearly centered on the source.

$$\Delta A > \sqrt{A_{min}} \tag{2.62}$$

When r_i is set for the three axes, they are added to the center gradient position to create the new source position estimate (2.63).

$${}^{I}\vec{r}_{source} = \begin{bmatrix} r_{north} \\ r_{east} \\ r_{down} \end{bmatrix} + {}^{I}\vec{r}_{center}$$

$$(2.63)$$

Figure 2.11 provides a block diagram of the algorithm logic.

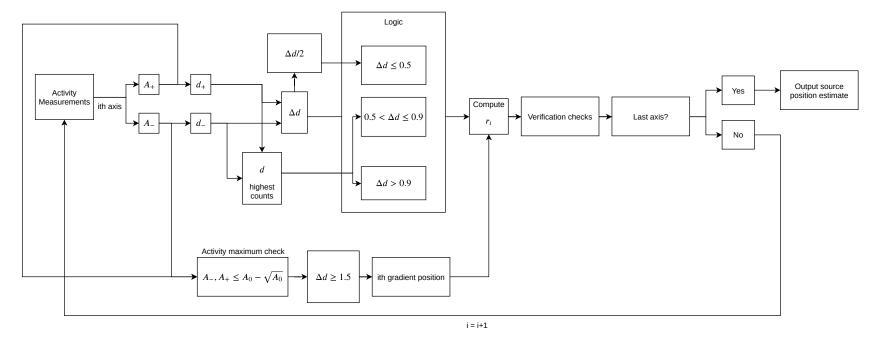


Figure 2.11. Block diagram illustrating radioactive source localization logic.

CHAPTER 3

RESULTS

3.1 Simulation

The results listed below include simulation outputs only. The first set of plots use waypoints to command the UAV. The second set comes from a simulation run where keyboard inputs were used to command the UAV arbitrarily.

3.1.1 Waypoint Flight

The UAV was commanded to fly to the waypoints listed in Table 3.1. Figures 3.1 - 3.8 illustrate the UAV flight dynamics.

Table 3.1. UAV commanded waypoints

Time (s)	North (m)	East (m)	Down (m)
0	0	0	-1
10	5	5	-5
30	-10	10	-0.2
50	0	0	-10
100	20	-20	-1

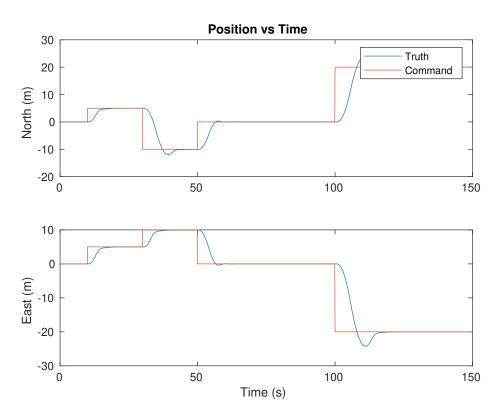


Figure 3.1. Waypoint flight - UAV position vs time

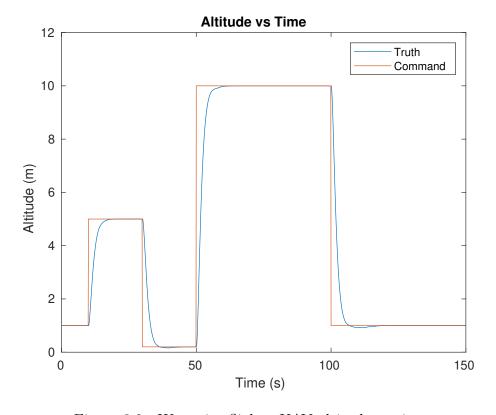


Figure 3.2. Waypoint flight - UAV altitude vs time

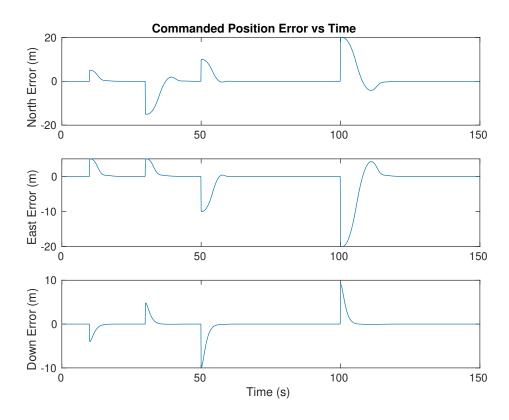


Figure 3.3. Waypoint flight - UAV commanded position error vs time

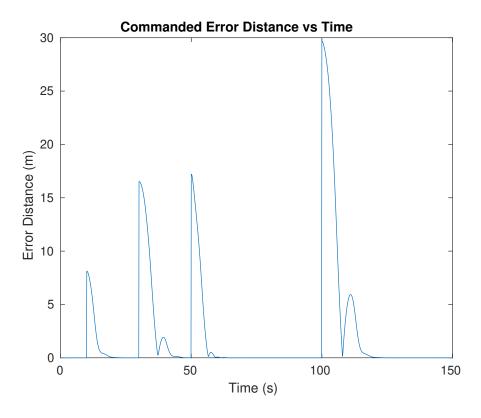


Figure 3.4. Waypoint flight - UAV commanded distance error vs time

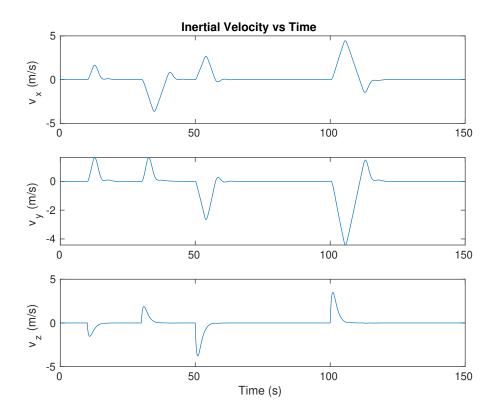


Figure 3.5. Waypoint flight - velocity vs time

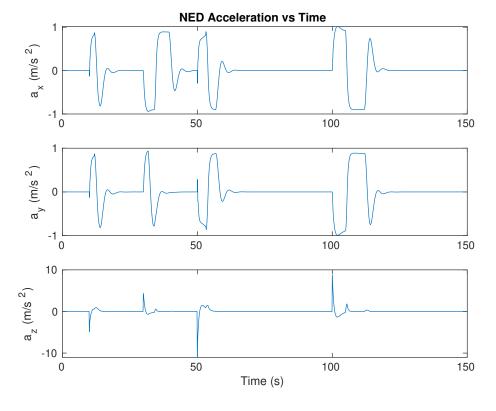


Figure 3.6. Waypoint flight - acceleration vs time

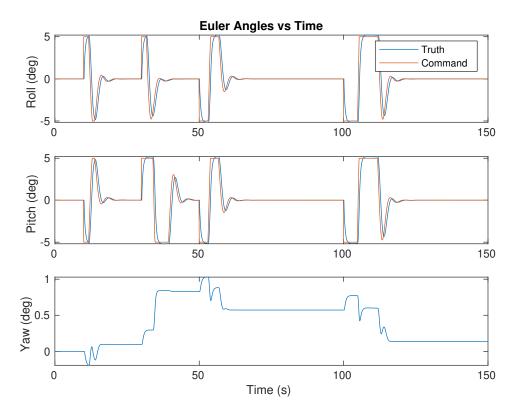


Figure 3.7. Waypoint flight - Euler angles vs time

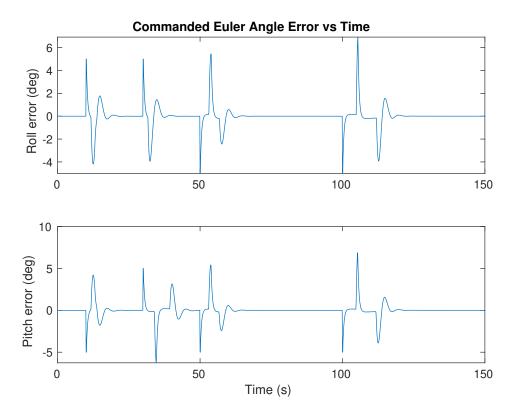


Figure 3.8. Waypoint flight - commanded Euler angle error vs time

3.1.2 Manual Flight

Figures 3.9 - 3.14 illustrate the simulated flight dynamics when a user is controlling the UAV via realtime keyboard inputs.

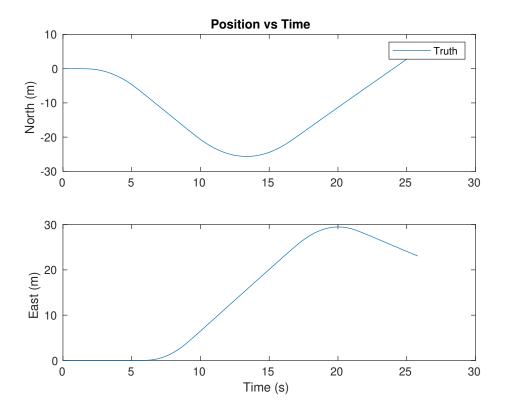


Figure 3.9. Manual flight - UAV position vs time

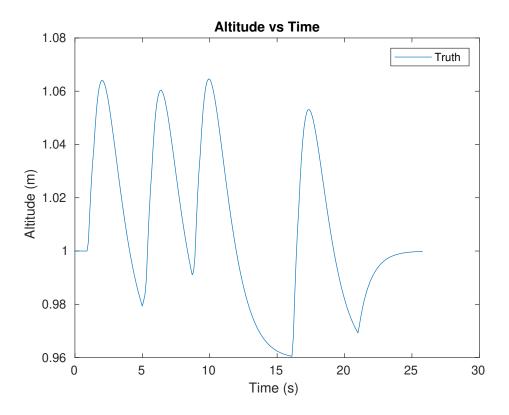


Figure 3.10. Manual flight - UAV altitude vs time

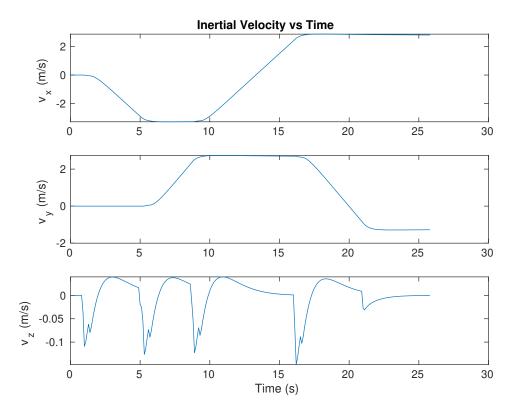


Figure 3.11. Manual flight - velocity vs time

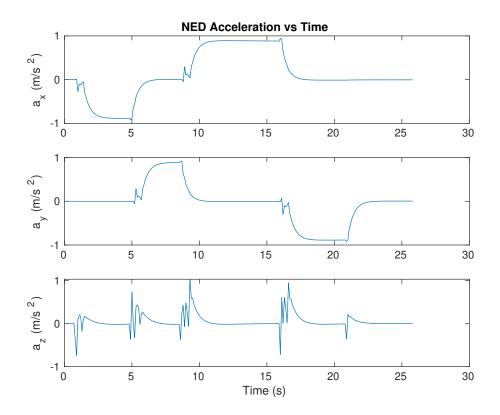


Figure 3.12. Manual flight - acceleration vs time

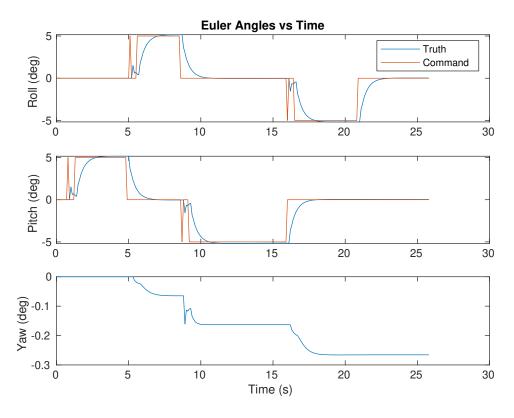


Figure 3.13. Manual flight - Euler angles vs time

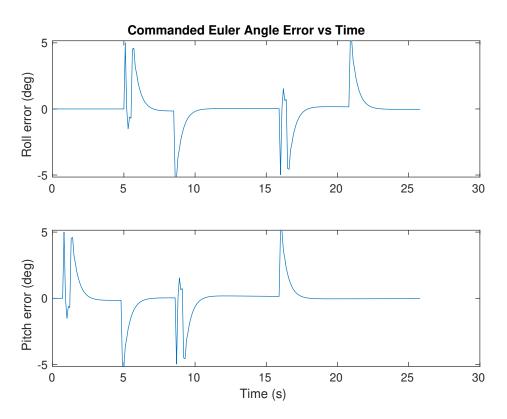


Figure 3.14. Manual flight - commanded euler angle error vs time

3.2 Kalman Filter

3.2.1 Waypoint Flight

Plots from the Kalman filter output are presented in Figures 3.15 - 3.19.

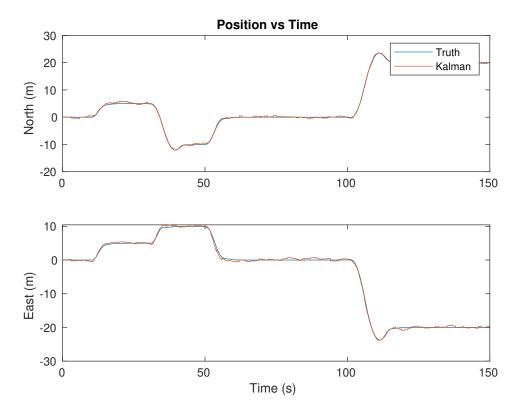


Figure 3.15. Kalman and truth - position vs time

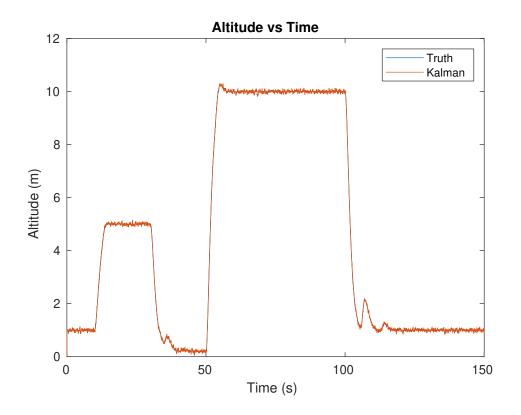


Figure 3.16. Kalman and truth - altitude vs time $\,$

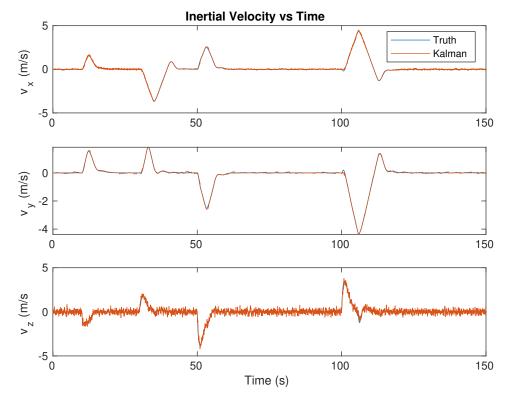


Figure 3.17. Kalman and truth - velocity vs time

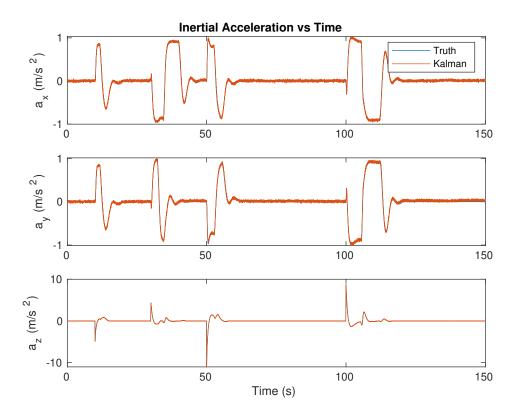


Figure 3.18. Kalman and truth - acceleration vs time

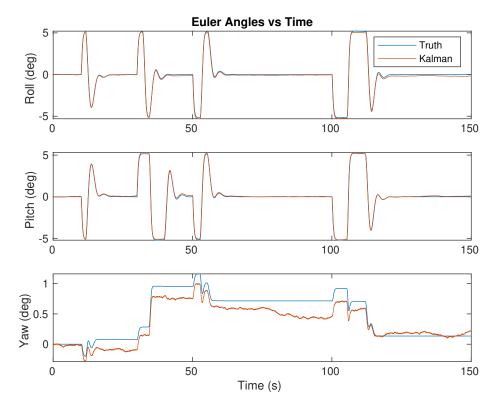


Figure 3.19. Kalman and truth - Euler angles vs time

3.3 Radioactive Source Localization

The final set of results enables radioactive source detection. Two cases are presented below. The first case assumes a 1mCi source is located at a distance ranging from 1m to 25m. 100 runs were performed holding the initial distance from the source constant while generating a random starting location for the source. These runs simulated 1800 seconds of flight time, assumed an average background activity of 1 count/sec, and used an activity threshold of 5 counts/sec.

Case 2 uses a source ten times weaker (0.1mCi) representing capability for the algorithm to localize a weak source. All other conditions were unchanged from the first case.

Figure 3.20 reveals the number of runs which converge within 1m. Figure 3.21 indicates the average number of iterations required for a run to converge within 1m. The upper plot uses error bars to show minimum and maximum number of iterations while the lower plot shows standard deviations. Only runs which were able to localize the source within 1m are shown. Figure 3.22 shows the average duration of time spent idle before the localization algorithm is triggered.

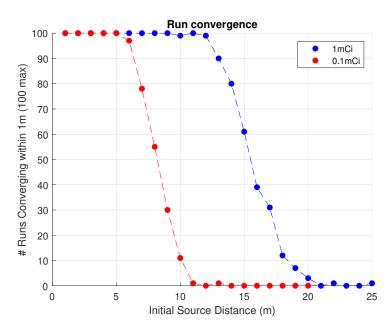


Figure 3.20. Run convergence for the 1mCi and 0.1mCi cases.

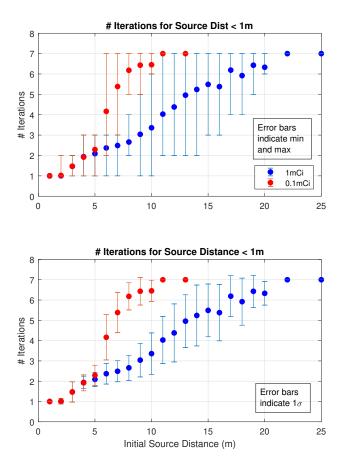


Figure 3.21. Number of iterations required for the UAV to localize the source within 1m. Only runs that were able to localize the source are plotted. Seven iterations is the maximum number of iterations possible within the constrained simulation time.

3.3.1 Case 1: 1mCi Source

For the 1mCi source, 90% of the runs converged within 1m of the radioactive source when initialized within 13m. The 1mCi source was assumed to record 1000 counts/sec at a distance of 1m.

Simulation and Kalman plots for a single run where the source was localized 10m away are presented in Figures 3.23 - 3.28.

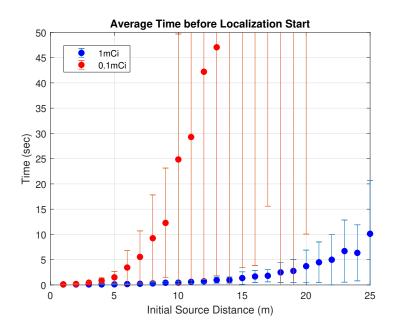


Figure 3.22. Average length of time before the UAV will start it's first localization run. The y-axis is cut off at 50 seconds.

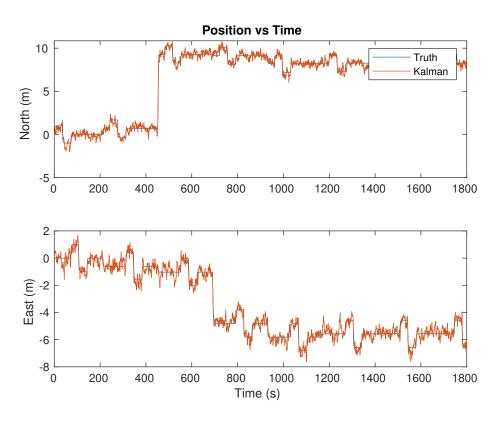


Figure 3.23. 1mCi Source initialized 10m away - Kalman UAV position vs time

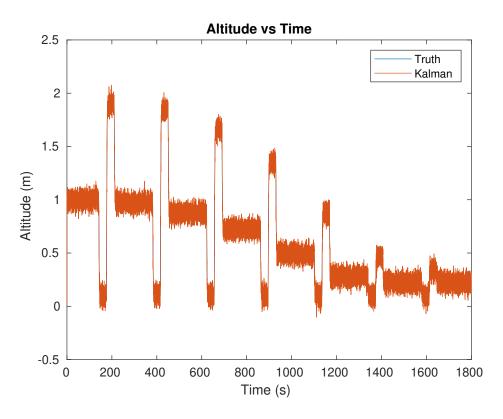


Figure 3.24. 1mCi Source initialized 10m away - Kalman UAV altitude vs time

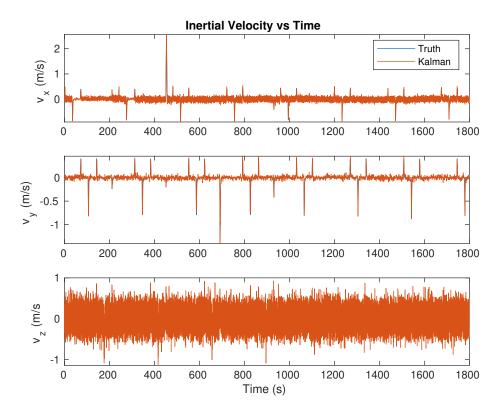


Figure 3.25. 1mCi Source initialized 10m away - Kalman velocity vs time

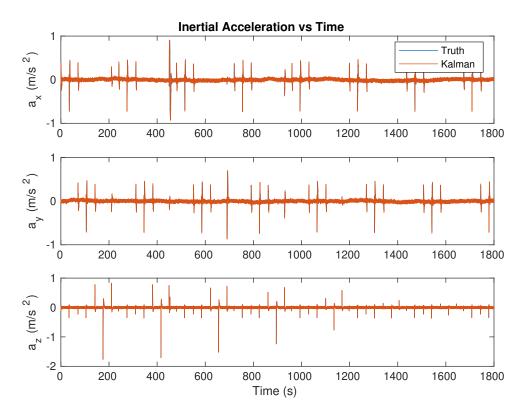


Figure 3.26. 1mCi Source initialized 10m away - Kalman acceleration vs time

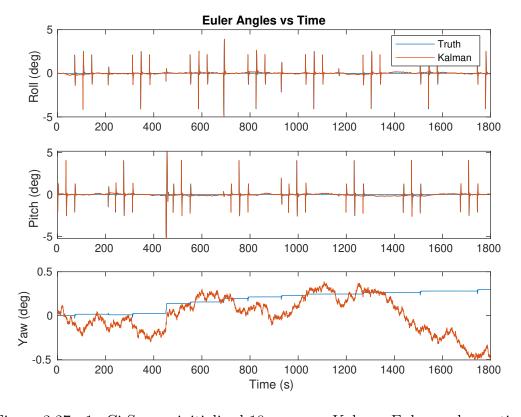


Figure 3.27. 1mCi Source initialized 10m away - Kalman Euler angles vs time

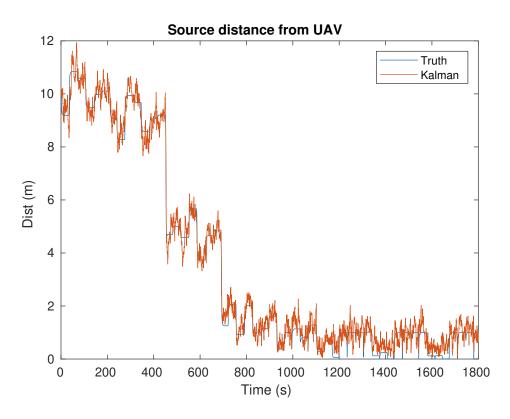


Figure 3.28. 1 mCi Source initialized 10 m away - Kalman source distance from UAV vs time

3.3.2 Case 2: 0.1mCi Source

Figure 3.20 shows that greater than 90% of runs will converge if the source is initialized within 6m. The 0.1 mCi source was assumed to record 100 counts/sec at a distance of 1 m.

CHAPTER 4

DISCUSSION

4.1 Simulation

The figures presented in Chapter 3.1 suggest the 6DOF UAV simulation is stable and provide a reasonable model of UAV motion in the absence of wind. The position vs time plots for waypoint commands in Figures 3.1 and 3.2 show that the UAV reaches each location without significant overshoot. Table 4.1 shows the UAV time of flight until it is within 10cm of its destination moving less than 5cm/sec.

Table 4.1. Time until UAV reaches target waypoint. This is defined when the UAV is within 10cm of the location and has a velocity magnitude of less than 5cm/sec.

Waypoint	Time of flight (sec)
1	9.4
2	15.2
3	9.9
4	19.5

For all simulations, the maximum allowable roll or pitch angle was set to five degrees. The PID controller clearly follows this as shown in Figures 3.7 and 3.13. In Figure 3.13 a MATLAB limitation results in the short spikes preceding the extended command lines. When a key is held, inputs are not fired repeatedly until after a short duration. At t = 5sec, the roll key was pressed and held, but did not begin repeatedly firing until shortly after as is clearly shown in Figure 3.13.

A simulation limitation can also be seen in Figures 3.7 and 3.13. In Chapter 2.2, there is no control for yaw motion. Why are yaw changes present? Referring back to (2.20), a nonzero roll, pitch, and ω_y will result in an nonzero yaw rate of change $(\dot{\psi})$.

4.2 Kalman Filter

As seen in the figures presented in Chapter 3.2, the Kalman Filter adequately estimates all state vectors with the most noticeable error occurring when estimating yaw. Improving the yaw estimate would require the addition of an additional sensor, such as a magnetometer.

Estimating roll and pitch angles from accelerometer measurements effectively mitigates the integration error accumulated from the gyroscope measurements. Figures 3.19 and 3.27 provide no indication error accumulation within 180 or 1800 seconds respectively. This method for mitigating gyroscope error should work well for a wide variety of quadcopter applications. The condition required for a valid accelerometer angle measurement is often satisfied throughout quadcopter flight.

4.3 Radioactive Source Localization

4.3.1 1mCi Case

For a source with radioactivity equal to 1mCi, Figure 3.20 shows that 90% of runs converge when the initial source distance ranges from 1m to 13m (inclusive). Between 13m and 20m, the number of runs that converge within the simulation time rapidly diminishes. Beyond 20m, one run was able to converge at 21m and 25m. This should be regarded as two fortunate runs.

The number of iterations until convergence within 1m (shown in Figure 3.21) gradually increases from 1 iteration to 7 iterations beyond 20m. From Figure 4.1, the decline of radioactivity with distance is much more gradual compared to the 0.1mCi case.

The gradual climb results from increasing initial distance which in turn decreases the accuracy of measurements as shown in Figure 4.1 Additionally, only runs that converge within 1m of the source are shown in Figure 3.21. It should be expected that if a run will converge, it will require more iterations to converge as distance increases.

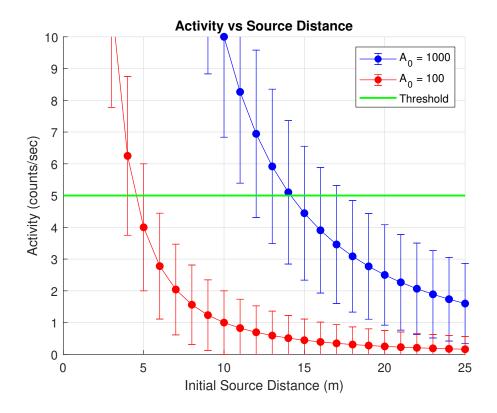


Figure 4.1. Expected activity measurements as distance increases. An activity threshold of five counts per second was used in both cases. The activity 1m from the source is assumed to be 1000 counts/sec and 100 counts/sec for the 1mCi and 0.1mCi source respectively.

Comparing Figures 3.20 and 4.1 reveals the cause of the rapid decline in run convergence begining beyond 12m (13m had 90% convergence, but prior to 12m, all runs had 99%–100% convergence). Assume the UAV is located 12m from the source and that the source is located along a measurement axis (which gives the best algorithm performance). Two measurements will be taken along this axis, one at 11m, and one at 13m. From Figure 4.1, the activity measured (within one standard deviation) for the 11m and 13m measurement is $A_{11m} = 8.26 \pm 2.87$ counts/sec and $A_{13m} = 5.91 \pm 2.43$ counts/sec respectively. The upper end of A_{13m} is greater than the mean of A_{11m} . As the source distance continues to increase, the difference in average activity continues to decrease. Recall that for a set of measurements to be used, the difference between activities at two measurement points must be greater than the standard deviation of the lower activity

measurement. Beyond this 12m mark, the probability that a set of measurements will produce any useful localization result rapidly diminishes.

As the probability of obtaining a usable result diminishes, the probability that a detrimental set of measurements is obtained will increase. Figure 4.2 shows the probability that the farther measurement will record a **greater** activity than the average activity of the closer measurement if the source lies along a measurement axis. As such, this plot represents the most favorable scenario for the algorithm.

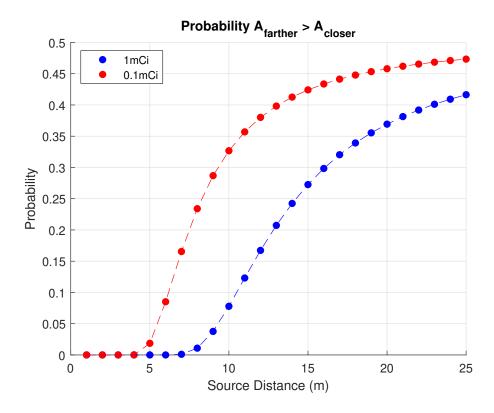


Figure 4.2. Probability that the farther activity measurement will be greater than the closer activity measurement's mean. For example: For the 1mCi source, when the localization algorithm is run at a distance of 15m (and lies along a measurement axis), the probability that the 16m measurement produces a greater result than the average activity at 14m is 27%.

A UAV searching for radioactive sources would need to have the activity threshold met while in flight. Figure 3.22 shows the average time until activity threshold is exceeded. On average, the activity threshold is exceeded within one second when initialized within 14m and 4m for the 1mCi and 0.1mCi case respectively. For a particular mission, this can be used to determine a maximum UAV travel speed.

4.3.2 0.1mCi Case

The 0.1mCi case was used to illustrate algorithm effectiveness for measuring algorithm effectiveness for a weak radioactive source. Figure 3.20 shows that 90% of runs converge when the source is initialized within 6m. Beyond 6m, run convergence decreases rapidly until reaching a distance of 10m. Beyond 10m, one run converged at 11m and 13m, while all other runs were unable to converge within 1m.

In Figure 3.21, there is a noticeable jump between 5m and 6m in the number of iterations required for a run to converge. Again, consider the case where the radioactive source lies along a measurement axis. If the source is 5m away, we will record measurements at distances of 4m and 6m. From Figure 4.1, the error bars between 4m and 6m have minimal overlap and the average activity to be measured is expected to be above the activity threshold. When then source is 6m away, the 5m and 7m activity measurements reveal that the 7m measurement is within one standard deviation of the 5m measurement (the opposite is not true). Additionally, the mean of both measurements falls below the activity threshold. The combination of these two factors leads to iterations with unusable measurements, which results in the significant jump from in iterations required between 5m and 6m.

Beyond 6m, the activity threshold is outside one standard deviation of any possible measurement. Additionally, the standard deviation at each measurement location will enclose the other measurement's mean. For example, if the source is initialized at 7m, the standard deviation of activity at 8m encloses the average activity at 6m and vice-versa. As the source distance increases, the difference between average activities will continue to decrease.

CHAPTER 5

CONCLUSION

UAVs are capable of expanding the available mission-space to environments unsuitable for humans. Regions with high concentrations of radioactive materials may produce lethal doses rendering them inaccessible. An algorithm has been developed to localize radioactive sources in an effort to improve the ability to safely perform experiments and missions in these areas.

Testing the algorithm required a model capable of simulating UAV flight characteristics. The simulated UAV can be controlled via keyboard input or by predetermined waypoints. Simulation results are presented in Chapter 3.1.

In addition to the simulation, an Extended Kalman Filter (EKF) was developed for use in estimating UAV states. The EKF has been shown to adequately estimate all states presented in Table 2.4 with the exception of the yaw Euler angle. This particular state is limited by the instruments assumed to be onboard a typical UAV.

Finally, localizing a radioactive source has been shown for a 1mCi source and a 0.1mCi source. Both sources were simulated for 1800 seconds. For the 1mCi source, the UAV was shown to converge within 1m of the radioactive source in $\geq 90\%$ until initialized 13m away. For the 0.1mCi source, the UAV converged within 1m in $\geq 90\%$ of runs until initialized 6m away from the source.

5.1 Future Work

This project leaves numerous avenues available for improvement. Listed below are the possible improvements which could be made to the project.

5.1.1 Simulation Verification

The simulation was developed and tested without true flight data for verification. Using the physical properties of a UAV, the simulation could be verified or improved via flight test.

5.1.2 Simulation Improvements

The fidelity of the simulation could be improved by modeling additional factors in flight. These factors include wind, electrical / mechanical interations, and improvements to the PID controller. A model for the effects of an electric motor on propeller dynamics, along with an alternative dynamics formulation, can be found in [11].

5.1.3 Extended Kalman Filter

As previously discussed, an additional sensor added to the EKF which provides yaw information would vastly reduce the total state estimation error. A magnetometer is such a sensor which could be used to determine the angle between magnetic north and the body-x axis.

An additional EKF improvement would be to expand the state vector to estimate any gyroscope or accelerometer bias. Such an improvement would lead to a more robust filter with improved hardware compatibility. In addition, this would help mitigate the yaw drift visible in Figure 3.27.

5.1.4 Source Localization

Additional sensors capable of measuring counts from radioactive sources would improve the probability of measuring activity near the true mean of the source. As a result, this would improve the speed at which the UAV can converge on a source and improve the maximum distance that the UAV can detect a source.

A method for detecting radioactivity as outlined in [4] would provide a light, cost-effective, option as any consumer-grade CCD (such as a cheap web camera) would

produce measurements of radioactivity. Using a CCD for the source localization algorithm would require a wrapper to simulate counts from CCD outputs.

5.1.5 Source Localization In the EKF

Moving the source localization algorithm into the EKF may provide numerous benefits to the algorithm. If the localization algorithm were part of the EKF, the inclusion of additional sensors would improve measurement reliability and thus improve algorithm effectiveness.

The initial state estimate would prove useful if any prior information about the source is known. For example, if the source is known to be located north of the UAV initial position, this information can be used to produce a better estimate of the source position.

Finally, radioactivity is known to have detrimental effects on electronics. Improving radiation hardening technology is a current area of research [18, 12, 15]. It may be possible to use these detrimental effects to improve localization accuracy in the EKF.

BIBLIOGRAPHY

- [1] Henry Ernest Baidoo-Williams. "Novel techniques for estimation and tracking of radioactive sources". PhD thesis. Iowa City, Iowa, USA: University of Iowa, Jan. 2014. DOI: 10.17077/etd.comm5gze. URL: https://ir.uiowa.edu/etd/1539.
- [2] Shawn S Brackett. "Integrated Environment and Proximity Sensing for UAV Applications". PhD thesis. University of Maine, 2017. 263 pp. url: https://digitalcommons.library.umaine.edu/etd/2796/.
- [3] Jren-Chit Chin et al. "Accurate localization of low-level radioactive source under noise and measurement errors". In: Proceedings of the 6th ACM conference on Embedded network sensor systems SenSys '08. the 6th ACM conference. Raleigh, NC, USA: ACM Press, 2008, p. 183. ISBN: 978-1-59593-990-6. DOI: 10.1145/1460412.1460431. URL: http://portal.acm.org/citation.cfm?doid=1460412.1460431.
- [4] John A. Cummings et al. "Detection and Analysis of Uncharged Particles Using Consumer-grade CCDs:" in: *Health Physics* 118.6 (June 2020), pp. 583–592. ISSN: 0017-9078. DOI: 10.1097/HP.000000000001211. URL: http://journals.lww.com/10.1097/HP.0000000000001211 (visited on 05/05/2020).
- [5] Bernard Etkin and Lloyd D. Reid. *Dynamics of flight: stability and control.* 3rd ed. New York: Wiley, 1996. 382 pp. ISBN: 978-0-471-03418-6.
- [6] Chirstopher J. Fisher. *Using An Accelerometer for Inclination Sensing | DigiKey www.digikey.com/*. Digi-Key. Contributed By Convergence Promotions LLC. May 6, 2011. URL: https://www.digikey.com/en/articles/techzone/2011/may/using-an-accelerometer-for-inclination-sensing.
- [7] Thor I. Fossen. Handbook of Marine Craft Hydrodynamics and Motion Control: Fossen/Handbook of Marine Craft Hydrodynamics and Motion Control. Chichester, UK: John Wiley & Sons, Ltd, Apr. 8, 2011. ISBN: 978-1-119-99413-8 978-1-119-99149-6. DOI: 10.1002/9781119994138. URL: http://doi.wiley.com/10.1002/9781119994138 (visited on 03/17/2018).
- [8] Kristofer Henderson et al. "Tracking Radioactive Sources through Sensor Fusion of Omnidirectional LIDAR and Isotropic Rad-Detectors". In: 2017 International Conference on 3D Vision (3DV). 2017 International Conference on 3D Vision (3DV). Qingdao: IEEE, Oct. 2017, pp. 97–106. ISBN: 978-1-5386-2610-8. DOI: 10.1109/3DV.2017.00021. URL: https://ieeexplore.ieee.org/document/8374562/.
- [9] Hui Liu and Yingwei Yao. "A moving radioactive source tracking and detection system". In: 2009 43rd Annual Conference on Information Sciences and Systems. 2009 43rd Annual Conference on Information Sciences and Systems (CISS). Baltimore, MD, USA: IEEE, Mar. 2009, pp. 50–54. ISBN: 978-1-4244-2733-8. DOI: 10.1109/CISS.2009.5054689. URL: http://ieeexplore.ieee.org/document/5054689/.

- [10] Rudolph Emil Kalman. "A New Approach to Linear Filtering and Prediction Problems". In: *Transactions of the ASME–Journal of Basic Engineering* 82 (Series D 1960), pp. 35–45.
- [11] Bouzgou Kamel et al. "Dynamic modeling, simulation and PID controller of unmanned aerial vehicle UAV". In: 2017 Seventh International Conference on Innovative Computing Technology (INTECH). 2017 Seventh International Conference on Innovative Computing Technology (INTECH). Luton: IEEE, Aug. 2017, pp. 64–69. ISBN: 978-1-5090-3989-0. DOI: 10.1109/INTECH.2017.8102445. URL: http://ieeexplore.ieee.org/document/8102445/.
- [12] Andrew S. Keys and Michael D. Watson. "Radiation Hardened Electronics for Extreme Environments". In: (Jan. 1, 2007), p. 4.
- [13] Manon Kok, Jeroen D. Hol, and Thomas B. Schön. "Using Inertial Sensors for Position and Orientation Estimation". In: Foundations and Trendső in Signal Processing 11.1 (2017), pp. 1–153. ISSN: 1932-8346, 1932-8354. DOI: 10.1561/2000000094. arXiv: 1704.06053. URL: http://arxiv.org/abs/1704.06053.
- [14] Mathworks. MATLAB. 2019.
- [15] George C. Messenger. *Radiation hardening*. type: dataset. McGraw-Hill Education, 2014. DOI: 10.1036/1097-8542.566850. URL: http://accessscience.com/content/566850.
- [16] Mark Pedley. Tilt Sensing Using a Three-Axis Accelerometer. 2014. URL: https://cache.freescale.com/files/sensors/doc/app_note/AN3461.pdf.
- [17] Dan Simon. Optimal state estimation: Kalman, H [infinity] and nonlinear approaches. OCLC: ocm64084871. Hoboken, N.J. Wiley-Interscience, 2006. 526 pp. ISBN: 978-0-471-70858-2.
- [18] R. Sorge et al. "JICG MOS transistors for reduction of radiation effects in CMOS electronics". In: 2018 IEEE Topical Workshop on Internet of Space (TWIOS). 2018 IEEE Topical Workshop on Internet of Space (TWIOS). Anaheim, CA: IEEE, Jan. 2018, pp. 17–19. ISBN: 978-1-5386-1294-1. DOI: 10.1109/TWIOS.2018.8311401. URL: http://ieeexplore.ieee.org/document/8311401/.
- [19] Chih-Hung Wu, Wei-Zhou Hong, and Shing-Tai Pan. "Performance Evaluation of Extended Kalman Filtering for Obstacle Avoidance of Mobile Robots". In: *Hong Kong* (2015), p. 5.

APPENDIX A

UAV SIMULATION

```
function A = aerodynamic_forces_moments(x, windVel, u, UAV)
 |% aerodynamic_forces_moments - Computs aerodynamics forces and
     moments
  \% acting on the UAV
  %
4
  % USAGE:
  %
       aerodynamic_forces_moments(x, windVel, u, UAV)
6
  %
7
  % INPUTS
  %
      x:
                state vector
9
      windVel: velocity of the wind in the wind frame (m/s)
10
  \%
      UAV:
                structure containing UAV constants
11
  % OUTPUTS
               [6 x 1] vector where the first three elements contain
  \%
      A:
13
  %
               aero forces (N) and the last three contain aero
14
     moments (N*m^2)
  %
      aeroForce:
                        Aero forces in body frame (N)
  %
                        Aero Moments (N*m)
      aeroMom:
16
  [\sim, \sim, \sim, \text{density}] = \text{atmosisa}(-x(3)); \% \text{density} (kg/m^3)
18
19
  % unpack state
20
  uavVelInBody = [x(4), x(5), x(6)]; % NED velocity
22
```

```
\% initialize variables
  propLength = norm(UAV.propVects(:, 1)); \% propeller length (m)
  propVelInBodySquared = u*(propLength/2)^2; % body frame propeller
     speed
27
  \% wind frame conversions
28
  [aoa, ssa] = get_aoa_ssa(uavVelInBody);
29
  uavVelInWind = DCM body2wind(uavVelInBody, aoa, ssa);
30
  velWithWind = uavVelInWind + windVel; % total relative air
31
     velocity (wind frame)
32
  \% Drag force and moment (wind frame)
33
  dragInWind = 1/4 * [-1/2 * density * velWithWind(1)^2 * UAV.
34
     propArea * UAV.CD; 0; 0; % drag (N)
  dragInBody = DCM_wind2body(dragInWind, aoa, ssa);
  \% Thrust force and moment (body frame)
  thrustInBody = zeros(3, 4);
37
  thrustMomInBody = zeros(3, 4);
  dragMomInBody = zeros(3, 4);
  for i = 1:4 \% four props
40
      velSquared = propVelInBodySquared(i);
41
      thrustInBody(:, i) = [0; 0; -1/2 * density * velSquared * UAV.
42
         propArea * UAV.CT]; % Thrust (N)
      thrustMomInBody(:, i) = cross(UAV.propVects(:, i)/2,
43
         thrustInBody(:, i)); % Thrust moment (N*m)
```

```
dragMomInBody(:, i) = cross(UAV.propVects(:, i)/2, dragInBody)
  end
  dragMomInBody = zeros(3, 4); % drag moment (N*m)
  \% Aero force and moment in body frame
  aeroForce = sum(dragInBody, 2) + sum(thrustInBody, 2);
48
  aeroMom = sum(dragMomInBody, 2) + sum(thrustMomInBody, 2);
49
  A = [aeroForce; aeroMom];
50
  end
51
  function [uDelta, angleTarget, angleErrorSum, rollCommand,
     pitchCommand] = compute_uDelta(controllerInput, x, Kp, Td, Ti,
     angleDeadband, UAV, dt, angleErrorSum, target_pos_ned)
  % compute_uDelta - Computes change in u to achieve desired input
  %
3
  % INPUTS
      {\tt controllerInput:} \quad [2\ x\ 1]\ +\!\!/\!\!-\ 1\ {\tt from\ keyboard\ or\ joystick}
  \%
     input
           [+/- bx, +/- by]. Note bx stands for body-x direction.
  %
           Example: [1, -1] would mean roll for +bx and -by
  \%
```

x: [18 x 1] state vector

%

```
%
      uDelta: [4 x 1] control input delta to be added to uHover to
     achieve
  %
      commanded input.
  %
17
  % NOTE
       propeller arrangement is as follows [1 2] with [1 2] in +bx
  %
19
  %
                                                      and 2, 3 in +by
                                             [4]
                                                  3]
20
  %
^{21}
22
  % unpack input
23
  bxInput = controllerInput(1);
  byInput = controllerInput(2);
25
26
  \% pos
27
  r_uav_ned = [x(1), x(2), x(3)];
28
29
  % vel
30
  v_uav_body = [x(4), x(5), x(6)]';
32
  % body angular velocity
  rollRate = x(7);
  pitchRate = x(8);
  yawRate = x(9);
  omega = [rollRate, pitchRate, yawRate]';
  % euler angles (rad)zVelInertial
38
  roll = x(10);
  pitch = x(11);
```

```
yaw = x(12);
42
  % angle error sums
  rollErrorSum = angleErrorSum(1);
  pitchErrorSum = angleErrorSum(2);
46
  %%
47
  [\sim, \sim, \sim, \text{density}] = \text{atmosisa}(-x(3)); \% \text{density} (kg/m^3)
49
  propLength = norm(UAV. propVects(1:3, 1)); \% meters
50
51
  gain pos2angle = 0.05;
  gain_vel2angle = 0.13;
  \% if {
m target\_pos\_ned} is {
m set}, {
m override} {
m controller} {
m commands}
54
   if ~isempty(target_pos_ned)
55
       [target_pos_body] = DCM_ned2body(target_pos_ned, [roll; pitch;
56
           yaw]);
       r_uav_body = DCM_ned2body(r_uav_ned, [roll; pitch; yaw]);
57
       bx\_error = target\_pos\_body(1) - r\_uav\_body(1);
       by\_error = target\_pos\_body(2) - r\_uav\_body(2);
       bz\_error = target\_pos\_body(3) - r\_uav\_body(3);
       vel\_error = 0 - v\_uav\_body;
62
       % roll and pitch targets are set by position errors
63
       pitchTarget = -(gain_pos2angle * bx_error + gain_vel2angle *
64
          vel_error(1));
```

```
rollTarget = gain_pos2angle * by_error + gain_vel2angle *
65
         vel\_error(2);
       if abs(pitchTarget) > abs(UAV.maxRotation)
           pitchTarget = sign(pitchTarget) * UAV.maxRotation;
67
      end
68
       if abs(rollTarget) > abs(UAV.maxRotation)
69
           rollTarget = sign(rollTarget) * UAV.maxRotation;
70
      end
71
  else
72
      % input gives all or nothing +/- input (rad)
73
      pitchTarget = -bxInput * UAV.maxRotation; % negative pitch
74
         angle results in +bx motion
      rollTarget = byInput * UAV.maxRotation; % positive roll angle
75
         results in +by motion
  end
76
  % angle errors (radians)
  rollError = rollTarget - roll;
  rollErrorSum = rollErrorSum + rollError;
  pitchError = pitchTarget - pitch;
  pitchErrorSum = pitchErrorSum + pitchError;
  \% angle rate errors (rad/s)
  rollRateError = 0 - rollRate;
  pitchRateError = 0 - pitchRate;
86
  % commanded pitch and roll based on gain K.
```

```
pitchCommand = Kp * ((pitchError) + Td * (pitchRateError) + 1/Ti *
       (pitchErrorSum * dt));
   rollCommand = Kp * ((rollError) + Td * (rollRateError) + 1/Ti * (
      rollErrorSum * dt));
   % uDeltaFun terms
   inertialTerm = cross (omega, UAV.inertiaMatrix*omega);
   thrustTerm = 8/(\text{propLength}^3 * \cos d(45) * \text{density} * \text{UAV.propArea} *
93
       UAV.CT);
   uDeltaFun = @(angleError, angleRateCurrent, I) ...
       2*I * (angleError - angleRateCurrent * dt)/(dt^2);
95
96
   \% If difference between target angle and current angle is less
97
      than the set
   \% deadband, do not issue a command.
   if abs(pitchTarget - pitch) < angleDeadband
99
       bxDeltaU = 0;
100
   else
101
       % rotation about y-axis (pitch) results in bx motion
102
       bxDeltaU = thrustTerm * ...
103
            (uDeltaFun(pitchCommand, pitchRate, UAV.inertiaMatrix(2,
104
               2)) - inertialTerm(2));
   end
   if abs(rollTarget - roll) < angleDeadband
106
       byDeltaU = 0;
107
   else
108
       % rotation about x-axis (roll) results in by motion
109
```

```
byDeltaU = thrustTerm * ...
110
            (uDeltaFun(rollCommand, rollRate, UAV.inertiaMatrix(1, 1))
111
                - inertialTerm(1));
   end
113
   % decode uDelta to correct propellers.
114
   \% bxDeltaU = u12 - u34
115
   u1x = 1/4 * bxDeltaU;
116
   u2x = u1x;
117
   u3x = -u1x;
118
   u4x = u3x;
119
120
   \% byDeltaY = u14 - u23
121
   u1y = 1/4 * byDeltaU;
122
   u2y = -u1y;
123
   u3y = u2y;
124
   u4y = u1y;
125
126
   % sum each u value
127
   u1 = u1x + u1y;
   u2 = u2x + u2y;
   u3 = u3x + u3y;
   u4 = u4x + u4y;
131
132
   % construct output
133
   uDelta = [u1, u2, u3, u4];
134
   angleTarget = [rollTarget, pitchTarget]';
135
```

```
angleErrorSum = [rollErrorSum, pitchErrorSum]';
end
```

```
function get_keypress (~, keyData)
 |% get_keypress - Determines key that was pressed and outputs
     appropriate
  % commands for the simulation
  % Key that was pressed. Always will be a lowercase string such as
     'space'
  key = keyData.Key;
7
  \% initialize outputs
  bxInput = 0;
  byInput = 0;
  if strcmp (key, 'w')
12
      bxInput = 1;
      disp('w');
14
  elseif strcmp(key, 's')
15
      bxInput = -1;
16
      disp('s');
17
  elseif strcmp(key, 'd')
18
      byInput = 1;
19
      disp('d');
20
  elseif strcmp(key, 'a')
```

```
byInput = -1;
disp('a');
elseif strcmp(key, 'q')
setappdata(gcf, 'stopsim', 1);
disp('q');
end
controllerInput = [bxInput, byInput]';
setappdata(gcf, 'controllerInput', controllerInput); % saves
controllerInput
end
```

```
function [yout, zout] = initialize_sim(plots_flag,
     r_source_inertial, A0)
  |% initialize_sim - Initialize and run UAV simulation
  %
3
  |% Syntax: [yout, zout] = initialize_sim(plots_flag,
     r_source_inertial, A0)
  %
  % INPUTS
  %
      plots_flag: ([0] or 1) raise flag for plots. Default is 0
  %
      r_source_inertial (optional): [3 x 1] vector containing
     inertial position of
  %
                                       a radioactive source.
  %
      A0 (optional): Sets the activity of the radioactive source
10
     measured 1cm
  %
      away from the source. Default is 1000
11
 %
12
```

```
% OUTPUTS
  \%
       yout:
                 Structure containing all saved simulation outputs
  %
                 Structure containing simulated measurements.
       zout:
16
   if nargin < 1
17
       plots flag = 0;
18
  end
19
20
  % make sure Utilities folder is in path
  addpath(genpath(fullfile('...', 'Utilities'))); % add Utilities to
      path
  addpath(genpath('./Measurements')); % add measurements to path
  UAV = initialize_uav; % initialize uav parameters
25
26
  \% initialize state vector
  r\_uav\_ned \, = \, \left[ \, 0 \; , \; \; 0 \; , \; \; -1 \, \right] \; ; \; \% \; \; inertial \; \; position \; \; (m)
29
  \% source location relative to inertial frame
   if nargin < 2
       randVec = random_vector(10);
32
       if \operatorname{randVec}(3) > -r_{uav_{ned}}(3)
            randVec(3) = -randVec(3);
34
       end
35
       r_source_inertial = r_uav_ned + randVec;
36
   else
37
       r_source_inertial = r_uav_ned + r_source_inertial;
38
```

```
end
40
  vel\_uav\_body = [0, 0, 0, 0, 0]'; % velocities and angular
     velocities (m/s and rad/s)
  eulerAngles = [deg2rad(0), deg2rad(0), deg2rad(0)]'; % [roll,
     pitch, yaw | Euler Angles in radians
  r\_obstacle\_ned = [20, 0, -2]'; % Obstacle position. Initialize
     such that obstacle is not a factor.
  obstacle_pos_from_body_ned = r_obstacle_ned - r_uav_ned; %
     position from body to obstacle in ned
  r_uav2source_inertial = (r_source_inertial - r_uav_ned); % Uav to
      source vector in inertial frame
  x0 = [r_uav_ned; vel_uav_body; eulerAngles;
     obstacle_pos_from_body_ned; r_uav2source_inertial]; % initial
     state
47
  \% wind velocity
  windVel = [0, 0, 0];
49
  \% time settings
  t_{max} = 100;
  dt = 0.1; % note that setting this lower than 0.1 will result in a
      slower-than-realtime simulation
  tspan = [0 t_max];
55
  % control settings
  % angle gains
```

```
Kp_angle = 3; % proportional gain
  Td_angle = 0.5; % derivative sample time
  Ti_angle = 15; % time for sum of all past errors to be eliminated
  % thrust gain
  Kp\_thrust = 1 * dt;
  % hover control gain
  Kp\_hover = 1e-1;
64
65
  deadband_angle = deg2rad(0); % radians
66
67
  waypoint1 = [10, 5, 5, -5];
68
  waypoint2 = [30, -10, 10, -0.2];
69
  waypoint3 = [50, 0, 0, -10];
70
  waypoint4 = [70, 20, -20, -1];
71
72
  fly2source\_flag = 0;
73
  waypoints = [waypoint1; waypoint2; waypoint3; waypoint4]';
  \% waypoints = [];
76
  showRealtimePlot = 0;
78
  A_{\text{thresh}} = 5;
  A_{background} = 1;
  if nargin < 3
81
      A0 = 1000;
82
  end
83
84
```

```
% run simulation
  yout = run_sim(tspan, dt, x0, windVel, UAV, showRealtimePlot,
     Kp_angle, Td_angle, Ti_angle, Kp_thrust, Kp_hover,
     deadband_angle, r_source_inertial, waypoints, A_thresh,
     A_background, A0, fly2source_flag);
  zout = simulate_measurements(yout);
  %save([datestr(now, 'yyyy-mm-ddTHHMMSS'), '.mat'])
  if plots_flag == 1
89
  %
        simulation plots (yout);
90
      %measurement_plots(yout, zout);
91
      measurement_plots(yout);
92
  end
93
```

```
function many_runs(num_runs, dist_from_source, output_path, A0)
1
2
       if nargin < 3
            current_datetime = datestr(now, 'yyyy-mm-ddTHHMMSS');
            output_path = fullfile('.', current_datetime);
       end
6
       mkdir(output_path);
7
       for i = 1:num\_runs
8
            disp(['A0 = ', num2str(A0), 'Run number: ', num2str(i)]);
9
            r_source_inertial = random_vector(dist_from_source);
10
            \label{eq:condition} $\text{r\_uav\_ned} = [0\,,\ 0\,,\ -1]'; \% \text{ inertial position } (m)$
11
            if r_source_inertial(3) > -r_uav_ned(3)
12
                r\_source\_inertial(3) = -r\_source\_inertial(3);
13
            end
14
```

```
function realtime_plot(x, figureNum, source_pos_ned)
  % realtime_plot plot position and orientation of UAV in real time
  %
3
  % USAGE: realtime_plot(x)
  %
5
  % INPUT
  %
      \mathbf{x}:
           state vector
7
  arrowLen = 5; % length modifier for plots
  % unpack current state
  rNED = [x(1), x(2), x(3)]';
12
  euler Angles = [x(10), x(11), x(12)];
13
14
  \% obtain body frame coordinates in NED frame
15
  bodyXInNED = DCM_body2ned([1, 0, 0]', eulerAngles) * arrowLen;
16
  bodyYInNED = DCM_body2ned([0, 1, 0]', eulerAngles) * arrowLen;
17
  bodyZInNED = DCM\_body2ned([0, 0, 1]', eulerAngles) * arrowLen;
19
```

```
figure (figureNum);
  plot3 (rNED(1), rNED(2), rNED(3));
^{21}
  xlabel('North');
  ylabel('East');
  zlabel('Down');
  title ('UAV position and orientation');
  hold on;
  quiver3 (rNED(1), rNED(2), rNED(3), bodyXInNED(1), bodyXInNED(2),
     bodyXInNED(3)); % body x vector in NED
  quiver3 (rNED(1), rNED(2), rNED(3), bodyYInNED(1), bodyYInNED(2),
     bodyYInNED(3)); % body y vector in NED
  quiver3 (rNED(1), rNED(2), rNED(3), bodyZInNED(1), bodyZInNED(2),
     bodyZInNED(3)); % body z vector in NED
30
  \% plot source position
31
  plot3 (source_pos_ned(1), source_pos_ned(2), source_pos_ned(3), 'o'
     );
33
  axis([-30, 30, -30, 30, -30, 0])
  hold off
  drawnow;
  end
```

```
function yout = run_sim(tSpan, dt, x, windVel, UAV,
    showRealtimePlot, KpAngle, KdAngle, KiAngle, KpThrust, KpHover,
    angleDeadband, true_source_pos, waypoints, A_thresh,
    A_background, A0, fly2source_flag)
```

```
% run_sim - runs simulation from given initial conditions
  %
3
  % USAGE
  %
      run_sim(tSpan, dt, xInit, windVel, UAV, rSourceInertial,
     showRealtimePlot)
  % INPUTS
  %
                   [1 x 2] or [2 x 1] array containing start and end
      tSpan:
     time (seconds)
  %
                   time step (seconds)
      dt:
  %
                   [18 x 1] state vector
      x:
  %
      windVel:
                  [3 x 1] wind velocity vector
10
  %
      UAV:
                   Structure containing UAV constants
11
  %
      rSourceInertial: [3 x 1] inertial position of radiation
12
     source
  %
      showRealtimePlot: 1 to show controllable realtime plot, 0 to
13
      distable
  %
                   proportional gain for angle control
      KpAngle:
14
  %
      KdAngle:
                   derivative gain for angle control
                   integral gain for angle control
  %
      KiAngle:
16
  %
                   Proportional gain for thrust
      KpThrust:
17
  %
      KpHover:
                   Proportional gain for hover
  %
      angleDeadband: angle error were command is not required.
      true_source_pos: [3 x 1] True source position in NED frame
  \%
  %
                  [4 x N] matrix containing waypoints
      waypoints:
  %
      A thresh:
                   Activity threshold used to trigger a source
22
     gradient estimate
  %
                      Average background counts per second
      A background:
```

```
%
                   Activity of radioactive source located 1cm away
      A0:
24
  %
      fly2source_flag: Flag used to command the UAV to disregard
25
     other controls
  %
                           and fly to the estimated source position.
  %
  % OUTPUTS
  %
      yout: structure containing all simulated states and additional
29
      analysis information
30
  \max Loops = ceil((tSpan(2) - tSpan(1))/dt); \% \max loops in sim
  \% initialize outputs
32
  xout = zeros(18, maxLoops);
  dxdt\_out = zeros(18, maxLoops);
34
  tout = zeros(1, maxLoops);
35
  uout = zeros(4, maxLoops);
36
  angle_target_out = zeros(2, maxLoops);
  yout = struct();
38
  yout.true_source_pos = true_source_pos;
  yout.source.A0 = A0;
40
  yout.source.A_thresh = A_thresh;
  yout.source.A_background = A_background;
  source.counts = zeros(1, maxLoops);
  source pos ned store = [];
44
45
  % Initialize times
  time = tSpan(1);
```

```
time no measurements = 0; % time must be greater than
     time_no_measurements for a measurement to be performed
49
  hover\_alt = x(3);
  % Initialize radiation measurement parameters
  % radiation measurement parameters
  r0 = 1;
              % distance from A0 during A0 measurements (m)
54
  measurement deadtime = 30; % minimum time between gradient
     measurements
  meas_duration = 30; % duration of measurements at each point
  measurement num = 0;
57
  gradient_store_counts = zeros(6, meas_duration * 10);
  gradient_center_ned = [];
  time stop meas = 0;
60
61
  measuring_gradient_flag = 0;
  r_{measurements\_ned} = zeros(3, 6);
  at\_target\_flag = 0;
  counts\_1sec = zeros(1, 10);
  estimation_start_times = [];
  % initialize figure
  figureNum = 99; % figure number
  figure (figureNum);
70
71
  angleErrorSum = [0, 0]'; % initialize angle error sum
```

```
73
  j = 1; \% loop index
74
  while time < tSpan(2)
      time = round(time, 6);
76
                     ~~~~~Source Position Logic
77
      tempstruct.x = x;
78
      tempstruct.t = time;
79
      % Determine counts for this timestep and counts for the last
80
         second
      counts_dt = counts_sim(tempstruct, dt, A0, A_background);
81
      counts\_1sec(1:9) = counts\_1sec(2:10);
82
      counts\_1sec(10) = counts\_dt;
83
84
      % detection_flag is raised if the last second of counts are
85
         greater
      % than activity threshold A thresh.
86
      if fly2source_flag == 1
87
           detection_flag = check_near_source_counts(counts_1sec,
              A_thresh, A_background);
      else
           detection_flag = 0;
      end
91
      \%detection_flag = 0;
      if (detection_flag == 1 || measuring_gradient_flag == 1) && (
93
         time > time_no_measurements )
           measuring_gradient_flag = 1;
94
```

```
if measurement_num = 0 % if we are just starting our
              measurements
                estimation_start_times = [estimation_start_times, time
                   ];
                [r_measurements_ned, gradient_center_ned] =
                   get_gradient_waypoints(x);
               measurement\_num = 1;
                at\_target\_flag = 0;
99
               count num = 0;
100
           end
101
           % have uav fly to current measurement position.
102
           target_pos_ned = r_measurements_ned(:, measurement_num);
103
           % check if uav is at our target measurement spot
104
           if at_target_flag == 0
105
                at_target_flag = check_uav_at_target(x,
106
                   r_measurements_ned(:, measurement_num));
                if at target flag == 1
107
                    time_stop_meas = time + meas_duration;
108
                end
109
           end
           % if time_stop_meas is empty and we are at our target, set
               time_stop_meas
           if at target flag == 1
112
                if time >= time stop meas
113
                    measurement\_num = measurement\_num + 1;
114
                    at\_target\_flag = 0;
115
                    count_num = 0;
116
```

```
else
                        % time <= time stop meas
117
                    % if we are at the target, record counts
118
                    count_num = count_num + 1;
                    gradient_store_counts(measurement_num, count_num)
                       = counts_dt;
               end
           end
122
           % if measurement_num == 7, we are done saving measurements
123
               . Estimate
           % source position from gradient_store_counts
124
           if measurement_num == 7
125
                measuring_gradient_flag = 0;
126
                source_pos_ned = estimate_source_pos(
127
                   gradient_store_counts, gradient_center_ned,
                   r_measurements_ned, meas_duration, A0, A_background
                   , r0, A_thresh, true_source_pos);
                source_pos_ned_store = [source_pos_ned_store, [time;
128
                   source_pos_ned ]];
                time_no_measurements = time + measurement_deadtime; %
129
                   do perform another gradient measurement for this
                   time
               measurement\_num = 0;
                target_pos_ned = source_pos_ned;
131
                waypoints = [waypoints, [time; target_pos_ned]];
132
               \% sort waypoints by time
133
                [\sim, waypoint\_ind] = sort(waypoints(1, :), 2);
134
                waypoints = waypoints(:, waypoint_ind);
135
```

```
end
136
137
       end
       %
139
140
       % if we are measuring a gradient, always use those waypoints.
141
        if measuring_gradient_flag == 0
142
            target_pos_ned = [];
143
            % check if we are flying to a waypoint
144
            if ~isempty (waypoints)
145
                waypoint\_ind = find(time >= waypoints(1, :), 1, 'last'
146
                    );
                if ~isempty (waypoint_ind)
147
                     target_pos_ned = waypoints(2:4, waypoint_ind);
148
                     hover\_alt = target\_pos\_ned(3);
149
                end
150
            end
151
       end
       % if key was pressed, update controllerInput accordingly
153
        set (figureNum , 'KeyPressFcn', @get_keypress);
154
       controllerInput = getappdata(figureNum, 'controllerInput');
155
        if isempty(controllerInput)
156
            controllerInput = [0, 0];
157
       end
158
159
```

```
% controls
160
       [uDelta, angTarget, angleErrorSum, rollCommand, pitchCommand]
161
          = \dots
           compute_uDelta(controllerInput, x, KpAngle, KdAngle,
162
               KiAngle, angleDeadband, UAV, dt, angleErrorSum,
               target_pos_ned);
       if ~isempty(target_pos_ned)
163
           uHover = u_for_hover(x, UAV, KpHover, target_pos_ned,
164
              rollCommand, pitchCommand);
       else
165
           uHover = u_for_hover(x, UAV, KpHover, [0, 0, hover_alt]',
166
              rollCommand, pitchCommand);
       end
167
       u = uHover + KpThrust .* uDelta;
168
169
       setappdata(gcf, 'controllerInput', [0, 0]'); % reset
170
          controllerInput for future commands
171
       % get aerodynamic forces and moments
172
       aeroForcesMomentsInBody = aerodynamic_forces_moments(x,
173
          windVel, u, UAV);
174
       % compute state rates
175
       dxdt = uav_eom(x, aeroForcesMomentsInBody, UAV);
176
177
       % store variables
178
       % variables to store
179
```

```
xout(:, j) = x;
180
       dxdt_out(:, j) = dxdt;
181
       tout(:, j) = time;
       uout(:, j) = u;
183
       angle_target_out(:, j) = angTarget;
184
       source.counts(:, j) = counts_dt;
185
186
       % update state
187
       x = x + dxdt.*dt;
188
       time = time + dt;
189
       j = j + 1;
190
191
       % terminate loop if UAV has hits ground
192
        if x(3) >= 0
193
            break
194
       end
195
196
       % plot output every tenth of a second
197
        if showRealtimePlot == 1
198
            realtime_plot(x, figureNum, true_source_pos);
       end
201
        if getappdata(gcf, 'stopsim') = 1
202
            break
203
       end
204
          pause (0.01); I don't think this is needed anymore
205
   end
206
```

```
% Cut unused array slots if simulation stops early
   timeStopped = time;
208
   numIterations = floor((timeStopped - tSpan(1))/dt);
   xout = xout(:, 1:numIterations);
   dxdt_out = dxdt_out(:, 1:numIterations);
   tout = tout(:, 1:numIterations);
   uout = uout(:, 1:numIterations);
213
   angle_target_out = angle_target_out(:, 1:numIterations);
214
   source.counts = source.counts(:, 1:numIterations);
215
216
   \% convert all body frame elements to inertial frame
217
   % velocity
218
   vel\_ned = DCM\_body2ned(xout(4:6, :), xout(10:12, :));
219
   xout(4:6, :) = vel\_ned;
220
   % acceleration
221
   accel_ned = DCM_body2ned(dxdt_out(4:6, :), xout(10:12, :));
222
   dxdt out (4:6, :) = accel ned;
223
224
   \% Change variables in xout to match the kalman state vector
225
   angvel\_body = xout(7:9, :);
   xout(7:9, :) = accel_ned;
   \% add structure with outputs to store
   yout.t = round(tout, 6); \% to fix overflow
230
   yout.x = xout;
231
   yout.source.position_estimate = source_pos_ned_store;
232
   yout.source.counts = source.counts;
233
```

```
yout.source.estimation_start_times = estimation_start_times;
yout.angvel_body = angvel_body;
yout.dxdt = dxdt_out;
yout.controls.u = uout;
yout.controls.angle_target = angle_target_out;
yout.controls.waypoints = waypoints;

delete(figure(figureNum));
end
```

```
\% Run simulation multiple times and save the results
2
  for j = 1:2
3
       if j == 1
4
           source\_distances = 1:1:25;
           A0 = 1000;
       elseif j == 2
7
          A0 = 100;
           source_distances = 1:1:20;
      end
10
      output_dir = fullfile('D:\Shared\SavedRuns', ['A0_', num2str(
11
         A0)]);
      num_runs = 100;
12
       for i = source distances
13
           dist_from_source = source_distances(i);
14
           disp(['Source distance: ', num2str(i)]);
15
```

```
output_path = fullfile(output_dir, ['distance_', sprintf(')
16
             %02i', dist_from_source), 'm_', 'A0_', num2str(A0)]);
          many_runs(num_runs, dist_from_source, output_path, A0);
      end
18
  end
  function uHover = u for hover(x, UAV, KpHover, target pos ned,
     rollCommand, pitchCommand)
 |% u_for_hover - Determine motor speed squared required to maintain
      constant
  |% altitude.
  %
4
  % INPUTS
      x: [18 x 1] state vector
  %
  %
                   Structure containing UAV physical parameters
      UAV:
7
  %
8
```

```
20
  % euler angles
^{21}
  phi = x(10);
  theta = x(11);
  psi = x(12);
25
  if ~isempty(target_pos_ned)
26
       target_down = target_pos_ned(3);
27
   else
28
       target\_down = x(3);
29
  end
30
31
  if target\_down > -0.1
32
       target\_down = -0.1;
33
  end
34
35
  % get propeller length
  propLength = norm(UAV.propVects(:, 1)); % prop length (m)
37
  [\sim, \sim, \sim, \text{density}] = \operatorname{atmosisa}(-x(3));
  uHover = (UAV. mass * g) / (2 * density * (propLength/2)^2 * UAV.
      propArea * UAV.CT * cos(rollCommand) * cos(pitchCommand));
42
  \% altitude control
  velInertial = DCM_body2ned([uBody, vBody, wBody]', [phi, theta,
      psi]');
```

```
wInertial = velInertial(3);
wError = 0 - wInertial;
zError = target_down - x(3);

uControl = (1 - KpHover*(zError) - 2*KpHover*wError) * uHover;
% output
uHover = uControl .* [1, 1, 1, 1]';
end
```

```
function dxdt = uav_eom(x, A_body, UAV)
  % uav_eom - Equations of motion for UAV
  %
3
  % USAGE
  %
      uav_eom(x, A_body, mass, inertiaMatrix)
  %
  % INPUTS
  %
              [18 x 1] state vector
      x:
  %
      A_body: [6 x 1] aerodynamic forces and moments in body frame.
     First
           three terms are forces, last three are moments.
  %
  \%
      UAV:
               Structure containing UAV constants
11
  %
12
  % OUTPUTS
13
  %
      dxdt:
             [18 x 1] state vector derivative with respect to time
14
15
```

```
g = 9.8; % gravity (m/s^2)
  \% unpack inputs
17
  vel\_body = [x(4), x(5), x(6)]';
  angvel = [x(7), x(8), x(9)];
19
  eulerangles = [x(10), x(11), x(12)];
20
^{21}
  \% convert aero forces and moments to inertial frame
  F_{aero\_body} = A_{body}(1:3);
23
  M aero body = A body (4:6);
  % outputs
25
  r_dot = DCM_body2ned(vel_body, eulerangles); % inertial frame
  v_{dot} = (DCM_{ned2body}([0, 0, UAV.mass*g]', eulerangles) +
     F_aero_body - UAV.mass * cross(angvel, vel_body)) / UAV.mass; %
      body frame
  angvel\_dot = \dots
      UAV. inertia Matrix^(-1) * (M_aero_body - cross(angvel, UAV.
29
         inertiaMatrix*angvel)); % body frame
  if angvel_dot(3) \sim = 0
      angvel_dot(3);
31
  end
  angvel_to_euler_rates_matrix = angVel_to_eulerRates(eulerangles);
  eulerRates = angvel_to_euler_rates_matrix*angvel;
  r obstacle dot = -DCM body2ned(vel body, eulerangles); % inertial
     frame. Assumes obstacle is stationary
  r_uav_to_source_dot = -DCM_body2ned(vel_body, eulerangles);
37
```

APPENDIX B

MEASUREMENT MODELS

```
function [altitude_measured, t_altimeter] = altimeter_model(yout)
  % altimeter_model - Simulate altimeter reading
3
      % altimeter specs
       [\sim, \sim, \sim, \text{ altimeter}, \sim, \sim] = \text{get\_sensor\_specs}();
5
      % unpack yout
7
       t = yout.t;
       altTruth = -yout.x(3, :);
9
10
       t_altimeter = round(t(1): 1/altimeter.sampleRate: t(end), 6);
11
       altAtTimeStep = interp1(t', altTruth', t_altimeter')';
12
13
       altitude_measured = altAtTimeStep + altimeter.sigma .* randn
14
          (1, length (altAtTimeStep));
15
  end
```

```
% INPUTS:
  %
      yout [struct]
7
  % OUTPUTS:
  %
      counts_recorded - counts output during time span dt.
10
      % unpack state
11
      x = yout.x;
12
      time = yout.t;
13
      if length(yout.t) > 1
14
           dt = yout.t(2) - yout.t(1);
15
      end
16
      [~, ~, ~, ~, ~, source_ned] = unpack_state_vector(x);
17
18
      source_distance = sqrt(source_ned(1, :).^2 + source_ned(2, :)
19
         ^2 + source_ned(3, :).^2;
20
       activity = A0 .* 1 ./ (source_distance.^2); % activity falls
^{21}
         off as 1/r^2
22
      % Probability for a count in a given timestep is represented
23
         using
      % intensity divided by timestep. Counts must be integers.
      % Example: if intensity / dt = 0.1, then give a 10 %
25
         probability for a
      \% count to be measured.
26
      countAvePerTimestep = activity .* dt; % average counts in one
27
         timestep
```

```
28
29 % determine random value for counts
30 counts_from_source = poissrnd(countAvePerTimestep);
31 counts_from_backround = poissrnd(A_background .* dt);
32 counts_recorded = counts_from_source + counts_from_backround;
33
34 end
```

```
function [gps_position, gps_velocity, t_gps, gps_course,
     ned_origin_in_lla | = gps_model(yout)
  % gps_model - model readings from GPS receiver (MTK3339)
  |% Syntax: [position, velocity, t_gps, ned_origin_in_lla] =
     gps model (yout)
  %
  % INPUTS
  %
      yout: Simulation output structure
6
  %
7
  % OUTPUTS
  %
      position: [3 x N] Geodetic position [Lat, Long, Alt] (deg, deg
     , m)
  %
      groundspeed: [1 x N] Magnitude of horizontal vel (m/s)
      course: [1 x N] Direction of horizontal vel in NED (degrees)
  %
11
  \%
      t_gps: [1 x N] time output of GPS measurements (sec)
12
  %
      ned_origin_in_lla: [latitude, longitude, altitude]
13
  %
          containing origin of local NED frame (degrees, degrees,
14
     meters)
15
```

```
% MTK3999 GPS Module
  [\sim, \sim, \text{gps}, \sim, \sim, \sim] = \text{get\_sensor\_specs}();
  ned\_origin\_in\_lla = [44.902236, -68.669829, 0]'; % starting GPS
19
     position (UMaine mall)
20
  % unpack inputs
^{21}
  t = round(yout.t, 6); % simulation times. Rounded to sixth decimal
22
      place
  gpsTruthIndex = find (mod(t, gps.sampleRate) == 0); % determine
     indices to put in GPS model from truth index
  gps_pos_ned_truth = yout.x(1:3, gpsTruthIndex); % [3 x N] array of
      positions in local NED frame (meters)
  gps_vel_ne_truth = yout.x(4:5, gpsTruthIndex); % [3 x N] array of
     velocities in local NED frame (meters)
  t_gps = round(t(gpsTruthIndex), 6); % measurement times
27
  % gps noise
28
  gps_pos_noise = gps.sigmaPos .* randn(3, length(t_gps));
  gps_vel_noise = gps.sigmaVel .* randn(2, length(t_gps));
31
  \% gps measurements
  gps_position = gps_pos_ned_truth + gps_pos_noise;
33
  gps_velocity = gps_vel_ne_truth + gps_vel_noise;
  gps\_course = atan2d(gps\_velocity(2, :), gps\_velocity(1, :));
35
  end
36
```

```
function [accelerometer_measurements_body, gyro_measurements,
     t_imu, eulerangle_gyro, roll_pitch_accelerometer] = imu_model(
     yout)
2 | % imu_model - Models IMU and outputs accelerometer and gyroscope
     values
  %
3
  % INPUTS
      yout: structure containing simulation outputs
  %
5
  %
6
  % OUTPUTS
  %
      accelerometer_measurements_body: [3 x N] accelerations in body
      frame (m/s^2)
      gyro_measurements: [3 x N] angular velocities (rad/s)
  %
9
  %
      t_imu: [1 x n] IMU measurement times (s)
10
  %
      sampleRate: sample rate of IMU (Hz)
11
12
      random walk flag = 0; % enable or disable random walk for gyro
13
          / accelerometer
14
      % Simulate Measurements
      [accelerometer_measurements_body, t_imu,
         roll_pitch_accelerometer] = accelerometer_model(yout,
         random_walk_flag);
       [gyro_measurements, eulerangle_gyro] = gyro_model(yout,
         random_walk_flag);
19
  end
```

```
% IMU Composition
  function [accelerometer_measured, t_accelerometer,
     roll_pitch_accelerometer] = accelerometer_model(yout,
     random_walk_flag)
  |\% accelerometer\_model - outputs measured accelerometer values and
     times
  %
25
  % INPUTS
26
  %
      yout [struct]: Simulation outputs
27
  %
      random_walk_flag [1, 0]: Flag to enable random walk output
28
  % OUTPUTS
  %
      accelerometer_measured [3 x N]: Simulated accelerometer
30
     measurements
     t_accelerometer [1 x N]: Simulated accelerometer measurement
     times
32
      % Accelerometer Specs
33
       [accelerometer, \sim, \sim, \sim, \sim, \sim] = get_sensor_specs();
35
      % unpack inputs
      t = yout.t;
37
       t_{accelerometer} = round(t(1):1/accelerometer.sampleRate:t(end))
38
          , 6); % measurement times
       eulerangles = yout.x(10:12, :);
39
       accelerations_from_sim_ned = yout.dxdt(4:6, :);
40
```

```
accelerations_from_sim_body = DCM_ned2body(
41
         accelerations_from_sim_ned + [0; 0; 9.8], eulerangles);
42
      % generate true accelerometer values by interpolating
43
         simulation results based
      % on accelerometer sample time
44
      accelerometer_truth = interp1(t', accelerations_from_sim_body
45
         ', t_accelerometer')';
46
      % accelerometer is modeled as a random walk process.
47
      if random_walk_flag == 1
          random_walk_noise = cumsum(randn(3, length(
49
              accelerometer_truth)), 2);
      else
          random_walk_noise = zeros(3, length(accelerometer_truth));
51
      end
52
      accelerometer bias = accelerometer.initBias + accelerometer.
         biasStability .* random_walk_noise;
      accelerometer_noise = accelerometer.sigma .* randn(3, length(
         accelerometer_truth));
      accelerometer_measured = accelerometer_truth +
         accelerometer_noise + accelerometer_bias;
      % roll and pitch estimate from accelerometer. These are only
57
         accurate when the
      % only force present is gravity.
58
      ax = accelerometer\_measured(1, :);
59
```

```
ay = accelerometer\_measured(2, :);
60
      az = accelerometer_measured(3, :);
       roll = atan2(ay, az);
      pitch = atan2(-ax, sqrt(ay.^2 + az.^2));
63
       [roll_pitch_accelerometer] = [roll; pitch];
  end
66
67
  function [gyro_measured, eulerAngles_measured] = gyro_model(yout,
     random_walk_flag)
  \% gyro\_model - simulates measured values for gyroscope
  %
70
  % INPUTS
71
  %
      yout [struct]: Simulation outputs
72
      random_walk_flag [1, 0]: Flag to enable random walk output
  \%
73
  % OUTPUTS
74
      gyro measured [3 x N]: Simulated gyroscope measurements
  \%
75
  %
      eulerAngles_measured [3 X N]: Simulated euler angle
76
     measurements
      % Gyroscope specs
78
      [~, gyro, ~, ~, ~, ~] = get_sensor_specs();
80
      % unpack inputs
81
      t = yout.t;
82
      t_{gyro} = round(yout.t(1):1/gyro.sampleRate:yout.t(end), 6); \%
83
          measurement times
```

```
ang_vel_from_sim = yout.angvel_body;
85
      % generate true gyro values by interpolating simulation
          results based
      % on gyro sample time
       gyro_truth = interp1(t', ang_vel_from_sim', t_gyro')';
88
89
      % gyro is modeled as a random walk process.
90
       if random walk flag == 1
91
           random_walk_noise = cumsum(randn(3, length(gyro_truth)),
92
              2);
       else
93
           random_walk_noise = zeros(3, length(gyro_truth));
94
       end
95
       gyro_bias = gyro.initBias + gyro.biasStability .*
96
          random_walk_noise;
       gyro_noise = gyro.sigma .* randn(3, length(gyro_truth));
97
       gyro_measured = gyro_truth + gyro_noise + gyro_bias;
98
99
      % Get euler angles from measurements
100
       eulerAngles_measured = zeros(3, length(gyro_measured)); %
101
          initialize array
       eulerAngles measured(:, 1) = yout.x(10:12, 1); % initial Euler
           Angles
       for i = 2: length (gyro_measured)
103
           angVel2EulerMatrix = angVel_to_eulerRates(
104
              eulerAngles_measured (:, i-1);
```

```
eulerRatesMeasured = angVel2EulerMatrix * gyro\_measured(:, i-1); eulerAngles\_measured(:, i) = eulerAngles\_measured(:, i-1) \\ + eulerRatesMeasured * 1/gyro.sampleRate; end end end end end
```

```
function [lidar_distance_body, t_lidar] = lidar_model(yout)
  %lidar_model - Simulate lidar measurement in body frame
  %
3
  % Syntax: [lidar_distance_body, t_lidar] = lidar_model(yout)
  %
5
  %
6
7
  % lidar specs
  [\sim, \sim, \sim, \sim, \text{lidar}, \sim] = \text{get\_sensor\_specs}();
10
  % Lidar measurements available
  t_lidar = round(yout.t(1):1/lidar.sampleRate:yout.t(end), 6);
12
  obstacle_distances_from_sim_ned = yout.x(13:15, :);
13
  eulerangles = yout.x(10:12, :);
14
  [obstacle\_distances\_from\_sim\_body, \sim] = DCM\_ned2body(
15
     obstacle_distances_from_sim_ned, eulerangles);
16
  |\%| generate uncorrupted lidar values by interpolating simulation
     results
```

```
lidar_truth = interp1(yout.t', obstacle_distances_from_sim_body',
     t_lidar')';
  % lidar measurement
  lidar_noise = lidar.sigma .* randn(3, length(lidar_truth));
  lidar_distance_body = lidar_truth + lidar_noise;
23
  % currently, lidar only measures in +body x direction
  lidar distance body = [lidar distance body(1, :); zeros(1, length(
     lidar_distance_body)); zeros(1, length(lidar_distance_body))];
26
  % if distance would be negative, set measured distance equal to
     zero
  lidar\_distance\_body(:, lidar\_distance\_body(1, :) < 0) = 0;
28
  end
29
  function measurement_plots(yout_truth, zout)
  %measurement_plots - plot true state against measurements
```

```
function measurement_plots(yout_truth, zout)

measurement_plots - plot true state against measurements

measurements

measurement plots(yout_truth, zout)

symbol yout_truth, zout)

unpack inputs
t = yout_truth.t;
x = yout_truth.x;
controls = yout_truth.controls;

if nargin == 2
```

```
imu = zout.imu;
12
      gps = zout.gps;
      altimeter = zout.altimeter;
      lidar = zout.lidar;
15
      source = zout.source;
  end
17
18
  % unpack state
19
  [pos_ned_truth, vel_ned_truth, accel_ned_truth, eulerangles_truth,
      obstacle_ned_truth, uav2source_ned_truth] =
     unpack_state_vector(x);
  angVelTruthInBody = yout_truth.angvel_body;
22
  if nargin = 1
23
24
      if ~isempty (yout_truth.source.position_estimate)
^{25}
          % Source distance estimate error
           source_pos_estimate = [[0; pos_ned_truth(:, 1)], yout_truth
27
              .source.position_estimate];
           source_pos_truth_ned = uav2source_ned_truth +
              pos_ned_truth;
           source_pos_estimate = interp1(source_pos_estimate(1, :)',
             source_pos_estimate(2:4, :)', t, 'previous', 'extrap')
30
           source_pos_error = source_pos_truth_ned -
31
              source_pos_estimate;
```

```
source_dist_error = zeros(1, length(source_pos_error));
           for i = 1:length(source_pos_error)
               source_dist_error(i) = norm(source_pos_error(:, i));
           end
35
           figure (1)
36
           plot(t, source_dist_error);
37
           xlabel ('Time (s)')
38
           ylabel ('Distance error (m)');
39
           title ('Source Distance error')
40
      end
41
       if is field (controls, 'waypoints')
42
           controls. waypoints = [[t(1); x(1:3, 1)], controls.
43
              waypoints |;
           uav_commanded_pos = interp1 (controls.waypoints(1, :)',
44
              controls.waypoints(2:4, :)', t, 'previous', 'extrap')';
           figure(2);
^{45}
           subplot(2, 1, 1);
           plot(t, pos_ned_truth(1, :), t, uav_commanded_pos(1, :));
47
           ylabel ('North (m)');
           title ('Position vs Time')
           legend('Truth', 'Command')
52
           subplot (2, 1, 2)
53
           plot(t, pos_ned_truth(2, :), t, uav_commanded_pos(2, :))
54
           ylabel('East (m)');
55
           xlabel('Time (s)');
56
```

```
figure (213);
           ned2enu = [0, 1, 0; 1, 0, 0; 0, 0, -1];
           pos_enu_truth = zeros(size(pos_ned_truth));
60
           uav_commands_enu = zeros(size(pos_ned_truth));
61
           for i = 1:length(pos_ned_truth)
62
               pos_enu_truth(:, i) = ned2enu * pos_ned_truth(:, i);
63
               uav_commands_enu(:, i) = ned2enu * uav_commanded_pos
64
                   (:, i);
           end
           subplot (3, 1, 1);
66
           plot(t, pos\_enu\_truth(1, :), t, uav\_commands\_enu(1, :));
67
           legend('Truth', 'Command');
68
           ylabel ('East (m)');
69
           title ('Position vs Time');
70
           subplot(3, 1, 2);
71
           plot(t, pos_enu_truth(2, :), t, uav_commands_enu(2, :));
           ylabel ('North (m)');
           subplot(3, 1, 3);
           plot(t, pos\_enu\_truth(3, :), t, uav\_commands\_enu(3, :));
           ylabel('Up (m)')
76
           xlabel('Time (sec)');
77
78
79
80
           % Altitude
           figure (3)
82
```

```
{\tt plot} \left(\, t \;,\; -pos\_ned\_truth \left(\, 3 \;,\; \; :\, \right) \;,\; \; t \;,\; \; -uav\_commanded\_pos \left(\, 3 \;,\; \; :\, \right) \,\right)
83
              ylabel ('Altitude (m)');
              xlabel('Time (s)');
85
              title ('Altitude vs Time')
86
              legend('Truth', 'Command')
87
88
             % Position error
89
              pos_error = uav_commanded_pos - pos_ned_truth;
90
              dist_error = zeros(1, length(pos_error));
91
              for i = 1:length(pos_error);
92
                   dist\_error(i) = norm(pos\_error(:, i));
93
              end
94
95
              figure (4)
96
              subplot(3, 1, 1);
97
              plot(t, pos_error(1, :));
              ylabel ('North Error (m)');
              title ('Commanded Position Error vs Time');
100
101
              subplot (3, 1, 2);
102
              plot(t, pos\_error(2, :));
103
              ylabel('East Error (m)');
104
105
              subplot(3, 1, 3);
106
              plot(t, pos_error(3, :));
107
              ylabel ('Down Error (m)');
108
```

```
xlabel('Time (s)')
109
110
            % Distance error
111
             figure(5);
112
             plot(t, dist_error);
113
             title ('Commanded Error Distance vs Time')
114
             ylabel ('Error Distance (m)');
115
             xlabel ('Time (s)')
116
        else
117
             figure (2);
118
             subplot (2, 1, 1);
119
             plot(t, pos_ned_truth(1, :));
120
             ylabel('North (m)');
121
             title ('Position vs Time')
122
             legend('Truth')
123
124
125
             subplot (2, 1, 2)
126
             plot(t, pos_ned_truth(2, :))
127
             ylabel ('East (m)');
128
             xlabel('Time (s)');
130
             figure (3)
131
             plot(t, -pos_ned_truth(3, :));
132
             ylabel ('Altitude (m)');
133
            xlabel('Time (s)');
134
             title ('Altitude vs Time')
135
```

```
legend('Truth')
136
       end
137
       % Velocity
139
140
        figure (6);
141
       subplot (3, 1, 1);
142
       plot(t, vel_ned_truth(1, :));
143
        ylabel('v_x (m/s)');
144
        title ('Inertial Velocity vs Time')
145
146
       subplot (3, 1, 2)
147
        plot(t, vel_ned_truth(2, :));
148
        ylabel('v_y (m/s)');
149
150
        subplot(3, 1, 3);
151
        plot(t, vel_ned_truth(3, :))
152
       ylabel('v_z (m/s)');
153
        xlabel('Time (s)');
154
       % Acceleration
156
        figure(7);
157
        subplot (3, 1, 1);
158
       plot(t, accel_ned_truth(1, :))
159
        ylabel('a_x (m/s^2)');
160
        title ('NED Acceleration vs Time')
161
162
```

```
subplot (3, 1, 2);
163
        plot(t, accel_ned_truth(2, :))
164
        ylabel ('a_y (m/s^2)');
165
166
        subplot (3, 1, 3);
167
        plot(t, accel_ned_truth(3, :))
168
        ylabel('a_z (m/s^2)');
169
        xlabel('Time (s)');
170
171
       % Angular Velocity
172
        figure (8);
173
        subplot (3, 1, 1);
174
        plot(t, rad2deg(angVelTruthInBody(1, :)))
175
        ylabel('\omega_x (deg/s)');
176
        title ('Angular Velocity vs Time');
177
178
        subplot(3, 1, 2);
179
        plot(t, rad2deg(angVelTruthInBody(2, :)))
180
       ylabel('\omega_y (deg/s)');
181
        subplot (3, 1, 3);
183
        plot(t, rad2deg(angVelTruthInBody(3, :)))
184
       ylabel('\omega_z (deg/s)');
185
186
       % Euler Angles
187
        figure (9)
188
189
```

```
subplot (2, 1, 1);
190
       plot(t, rad2deg(eulerangles_truth(1, :)), t, rad2deg(controls.
191
           angle_target(1, :));
        title ('Euler Angles vs Time')
192
        ylabel('Roll (deg)')
193
       legend('Truth', 'Command');
194
195
       subplot (2, 1, 2);
196
       plot(t, rad2deg(eulerangles_truth(2, :)), t, rad2deg(controls.
197
           angle_target(2, :)));
        ylabel ('Pitch (deg)')
198
        xlabel('Time (sec)');
199
200
   %
          subplot(3, 1, 3);
201
   \%
          plot(t, rad2deg(eulerangles_truth(3, :)))
202
   %
          ylabel ('Yaw (deg)');
203
   %
          xlabel ('Time (s)');
204
205
       % Euler angle error
206
        eulerangle_error = controls.angle_target - eulerangles_truth
207
           (1:2, :);
        figure (10);
208
       subplot (2, 1, 1);
209
        plot(t, rad2deg(eulerangle_error(1, :)));
210
        ylabel('Roll error (deg)');
211
        title ('Commanded Euler Angle Error vs Time')
212
213
```

```
subplot (2, 1, 2);
214
        plot(t, rad2deg(eulerangle_error(2, :)))
215
       ylabel ('Pitch error (deg)')
216
        xlabel ('Time (s)')
217
218
       % source position relative to UAV
219
       figure (11);
220
       subplot (3, 1, 1);
221
        plot(t, uav2source_ned_truth(1, :))
222
        ylabel('s_x');
223
        title ('NED Source position from UAV vs Time');
224
225
       subplot(3, 1, 2);
226
        plot(t, uav2source_ned_truth(2, :));
227
       ylabel('s_y');
228
^{229}
       subplot (3, 1, 3);
230
        plot(t, uav2source_ned_truth(3, :));
231
       xlabel('Time (s)');
232
        ylabel('s_z');
233
       % source distance from UAV
       source_dist = zeros(1, length(uav2source_ned_truth));
236
        for i = 1:length(uav2source_ned_truth)
237
            source_dist(i) = norm(uav2source_ned_truth(:, i));
238
       end
239
        figure (12)
^{240}
```

```
plot(t, source_dist)
241
       xlabel ('Time (s)')
242
       ylabel('Dist (m)');
        title ('Source distance from UAV');
^{245}
   end
247
   if nargin = 2
248
       % euler angles interpolated for same imu timestep
249
       eulerangles_truth_interpolated = interp1(t', eulerangles_truth
250
           ', imu.t')';
       % Position
251
       gpsPosNED = gps.position;
252
253
       figure();
254
       subplot(2, 1, 1);
255
       plot(t, pos_ned_truth(1, :), gps.t, gpsPosNED(1, :));
256
       ylabel ('North (m)');
257
        title ('Position vs Time')
258
       legend('Truth', 'gps');
259
       subplot (2, 1, 2)
261
       plot(t, pos_ned_truth(2, :), gps.t, gpsPosNED(2, :));
262
       ylabel ('East (m)');
263
       xlabel('Time (s)');
264
265
       % Altitude
266
```

```
figure()
267
       plot(t, -pos\_ned\_truth(3, :), gps.t, -gpsPosNED(3, :),
268
           altimeter.t, altimeter.altitude);
       ylabel('Altitude (m)');
269
       xlabel('Time (s)');
270
        title ('Altitude vs Time')
271
       legend('Truth', 'gps', 'Altimeter');
272
273
       % Velocity
274
       gpsVelocityInNE = gps.velocity;
275
       figure();
276
       subplot (3, 1, 1);
277
       plot(t, vel_ned_truth(1, :), gps.t, gpsVelocityInNE(1, :));
278
       ylabel('v_x (m/s)');
279
        title ('Inertial Velocity vs Time')
280
       legend('Truth', 'gps');
281
282
       subplot (3, 1, 2)
283
       plot(t, vel_ned_truth(2, :), gps.t, gpsVelocityInNE(2, :));
284
       ylabel('v_y (m/s)');
       subplot(3, 1, 3);
287
       plot(t, vel_ned_truth(3, :))
288
       ylabel('v_z (m/s)');
289
       xlabel('Time (s)');
290
291
       % Acceleration
292
```

```
accelerometer_ned = DCM_body2ned(imu.accelerometer,
293
            eulerangles_truth_interpolated);
        figure();
294
        subplot (3, 1, 1);
295
        plot(t, accel_ned_truth(1, :), imu.t, accelerometer_ned(1, :))
296
        ylabel('a_x (m/s^2)');
297
        title ('NED Acceleration vs Time')
298
        legend('Truth', 'imu');
299
300
        subplot (3, 1, 2);
301
        plot(t, accel_ned_truth(2, :), imu.t, accelerometer_ned(2, :))
302
        ylabel ('a_y (m/s^2)');
303
304
        subplot (3, 1, 3);
305
        plot(t, accel_ned_truth(3, :), imu.t, accelerometer_ned(3, :))
306
            ;
        ylabel('a_z (m/s^2)');
307
        xlabel('Time (s)');
308
        % Angular Velocity
        figure();
311
        subplot (3, 1, 1);
312
        \operatorname{plot}(t, \operatorname{rad2deg}(\operatorname{angVelTruthInBody}(1, :)), \operatorname{imu.t}, \operatorname{rad2deg}(\operatorname{imu}.
313
            gyroscope(1, :));
        ylabel('\omega_x (deg/s)');
314
```

```
title ('Gyroscope Measurements vs Time');
315
        legend('Truth', 'imu');
316
317
        subplot (3, 1, 2);
318
        \operatorname{plot}(t, \operatorname{rad2deg}(\operatorname{angVelTruthInBody}(2, :)), \operatorname{imu.t}, \operatorname{rad2deg}(\operatorname{imu.t})
319
            gyroscope(2, :));
        ylabel('\omega_y (deg/s)');
320
321
        subplot (3, 1, 3);
322
        plot(t, rad2deg(angVelTruthInBody(3, :)), imu.t, rad2deg(imu.
323
            gyroscope(3, :));
        ylabel('\omega_z (deg/s)');
324
325
        % Euler Angles
326
        figure()
327
328
        subplot (3, 1, 1);
329
        plot(t, rad2deg(eulerangles_truth(1, :)), imu.t, rad2deg(imu.
330
            eulerangles (1, :)));
        title ('Euler Angles vs Time')
331
        ylabel ('Roll (deg)')
332
        legend('Actual', 'imu');
333
334
        subplot (3, 1, 2);
335
        plot(t, rad2deg(eulerangles_truth(2, :)), imu.t, rad2deg(imu.
336
            eulerangles(2, :));
        ylabel ('Pitch (deg)')
337
```

```
338
       subplot(3, 1, 3);
339
       plot(t, rad2deg(eulerangles_truth(3, :)), imu.t, rad2deg(imu.
340
          eulerangles (3, :));
       ylabel('Yaw (deg)');
341
       xlabel('Time (s)');
342
343
       % Distance to obstacle
344
       lidar_dist_ned = DCM_body2ned(lidar.distance,
345
          eulerangles_truth_interpolated);
       figure();
346
       subplot(3, 1, 1)
347
       plot(t, obstacle_ned_truth(1, :), lidar.t, lidar_dist_ned(1,
348
          :));
       ylabel('\chi_N (m)');
349
        title ('Obstacle position relative to UAV vs Time')
350
351
       subplot (3, 1, 2)
352
       plot(t, obstacle_ned_truth(2, :), lidar.t, lidar_dist_ned(2,
353
          :));
       ylabel('\chi_E (m)')
354
355
       subplot (3, 1, 3)
356
       plot(t, obstacle_ned_truth(3, :), lidar.t, lidar_dist_ned(3,
357
           :));
       ylabel('\chi_D (m)');
358
       xlabel('Time (s)');
359
```

```
legend('Truth', 'Lidar');
360
361
       % counts plot
        figure();
363
        plot(t, source.counts);
364
        xlabel('Time (s)');
365
        ylabel('Counts');
366
        title ('Counts vs Time');
367
368
       \% source position relative to UAV
369
        figure();
370
        subplot (3, 1, 1);
371
        plot(t, uav2source_ned_truth(1, :))
372
        ylabel('s_x');
373
        title ('NED Source position from UAV vs Time');
374
375
        subplot (3, 1, 2);
376
        plot(t, uav2source_ned_truth(2, :));
377
        ylabel('s_y');
378
        subplot (3, 1, 3);
380
        plot(t, uav2source_ned_truth(3, :));
381
        xlabel('Time (s)');
382
        ylabel('s_z');
383
   end
384
385
   end
386
```

```
function [zout] = simulate_measurements(yout)
  %simulate_measurements - simulate measurements from truth
  %
  % Syntax: zout = simulate_measurements(yout)
  %
5
  \% zout contents:
  %
      zout.imu.[accelerometer, gyroscope, t, eulerangles]
  %
      zout.gps.[position, velocity, t, ned_origin_in_lla]
  %
      zout.altimeter.[altitude, t]
9
      zout.lidar.[measurement, t]
  \%
  % initialize structures
  zout = struct('imu', [], 'gps', []);
13
  imu = struct();
  gps = struct();
15
  altimeter = struct();
16
  lidar = struct();
17
  source = struct();
18
19
  % simulate measurements
  [imu.accelerometer, imu.gyroscope, imu.t, imu.eulerangles, imu.
     accelerometer_roll_pitch] = imu_model(yout); % simulate
     accelerometer measurements
22
  [gps.position, gps.velocity, gps.t, gps.course, gps.
     ned_origin_in_lla] ...
```

```
= gps_model(yout); % simulate gps measurements
24
25
  [altimeter.altitude, altimeter.t] = altimeter_model(yout); %
     simulate altimeter measurements (m)
  [lidar.distance, lidar.t] = lidar_model(yout); % simulate lidar
     distances
29
  %[source.counts, source.t] = counts_sim(yout); % simulate counts
  source.counts = yout.source.counts;
31
  source.t = yout.t;
32
  source.position_estimate = yout.source.position_estimate;
33
34
  \% create structures
35
  zout.imu = imu;
36
  zout.gps = gps;
  zout.altimeter = altimeter;
  zout.lidar = lidar;
  zout.source = source;
  end
```

APPENDIX C

KALMAN FILTER

```
function P0 = initial_covariance_matrix()
2 |% initial_covariance_matrix - outputs initial covariance matrix
     based on
3 % IMU variance
  % populate sensor specs used in covariance matrix
  [\sim, \text{ gyro}, \sim, \sim, \sim, \sim] = \text{get\_sensor\_specs}();
  P0_{pos} = zeros(3, 18);
  P0_{vel} = zeros(3, 18);
  P0\_accel = zeros(3, 18);
  P0_{\text{euler}} = zeros(3, 18);
11
  P0_chi = zeros(3, 18);
  P0\_source = zeros(3, 18);
14
  P0 = vertcat (P0_pos, P0_vel, P0_accel, P0_euler, P0_chi, P0_source
     );
  end
  function H = linearized_measurement_matrix(x1_minus, hx)
  |% linearized_measurement_matrix - linearize measurement function
     about state
  % estimate
4 %
```

```
% Syntax: H = linearized_measurement_matrix(x1_minus, hx)
  %
6
  % INPUTS
  %
       x1_minus [18 x 1]: state vector for kth state without
      measurement update
  %
10
      % unpack state
11
       [\sim, \sim, accel\_ned, eulerangles, obstacle\_ned, \sim] =
12
          unpack_state_vector(x1_minus);
13
      % GPS included
14
       if hx(1) \sim 0
15
           H_gps = linearized_h_gps();
16
       else
17
           H_{gps} = zeros(5, 18);
       end
19
20
      % altimeter included
^{21}
       if hx(6) \sim 0
            H_altimeter = linearized_h_altimeter();
       else
            H_{altimeter} = zeros(1, 18);
25
       end
26
27
      % lidar
28
       if hx(7) \sim 0
29
```

```
H_lidar = linearized_h_lidar(eulerangles, obstacle_ned);
       else
31
           H_{lidar} = zeros(1, 18);
       end
33
34
      % imu
35
       if hx(8) \sim 0
36
           H_imu = linearized_h_imu(accel_ned, eulerangles);
37
       else
38
           H_{imu} = zeros(5, 18);
39
       end
40
41
      % if we are accelerating, we can't use gravity for attitude
42
          measurements.
       if hx(11) = 0
43
           H_{imu}(4:5, :) = zeros(2, 18);
44
       end
45
46
      \% source of interest
47
       H_source = linearized_h_source(x1_minus);
49
      % create H
      H = vertcat (H_gps, H_altimeter, H_lidar, H_imu, H_source);
51
52
  end
53
  function H_gps = linearized_h_gps()
```

```
% linearize gps terms in measurement function about x1_minus
      dpos_dx = [eye(3), zeros(3, 15)];
      dvel_dx = [zeros(2, 3), eye(2, 3), zeros(2, 12)];
59
60
      % Linearized GPS Measurement Matrix
61
62
      H_gps = vertcat(dpos_dx, dvel_dx);
63
  end
64
65
  function H_altimeter = linearized_h_altimeter()
66
  \% linearize altimeter term in measurement function about x1_minus
67
68
      H_{altimeter} = [0, 0, -1, zeros(1, 15)];
69
70
  end
71
72
  function H_lidar = linearized_h_lidar(eulerangles, chi)
  %linearized_h_lidar - linearize lidar terms in measurement
     function about x1_minus
  %
  % Syntax: H_lidar = linearized_h_lidar(x1_minus)
  %
77
  \% h_{LIDAR} = chi(1)*cos(theta)*cos(psi) + chi(2)*cos(theta)*sin(
     psi) - chi(3)*sin(theta)
79
      % unpack euler angles
80
```

```
theta = eulerangles(2);
       psi = eulerangles(3);
       % chi terms
       dLidar_dChi = [\cos(theta)*\cos(psi), \cos(theta)*\sin(psi), -\sin(theta)*\sin(psi)]
84
          theta);
85
       % euler angle terms
86
       dLidar\_dphi = 0;
87
       dLidar_dtheta = -chi(1)*sin(theta)*cos(psi) - chi(2)*sin(theta)
88
          *\sin(psi) - chi(3)*\cos(theta);
       dLidar_dpsi = -chi(1)*cos(theta)*sin(psi) + chi(2)*cos(theta)*
89
          cos(psi);
       dLidar_deuler = [dLidar_dphi, dLidar_dtheta, dLidar_dpsi];
90
91
       H_lidar = [zeros(1, 9), dLidar_deuler, dLidar_dChi, zeros(1,
92
          3)];
   end
94
   function H_imu = linearized_h_imu(accel_ned, eulerangles)
       % body acceleration
97
       daccel\_dpos = zeros(3);
       daccel dvel = zeros(3);
99
       [~, daccel_daccel] = DCM_ned2body([1, 1, 1]', eulerangles);
100
       [d_bTi_d_phi, d_bTi_d_theta, d_bTi_d_psi] =
101
          jacobian_DCM_ned2body(eulerangles);
```

```
daccel_deuler = [d_bTi_d_phi * accel_ned, d_bTi_d_theta *
102
          accel_ned, d_bTi_d_psi * accel_ned];
       daccel\_dobstacle = zeros(3);
103
       daccel\_dsource = zeros(3);
104
105
       H imu accelerometer = ...
106
            [daccel_dpos, daccel_dvel, daccel_daccel, daccel_deuler,
107
               daccel_dobstacle, daccel_dsource];
108
       % accelerometer roll and pitch
109
       H_accelerometer\_roll = [zeros(1, 9), 1, zeros(1, 8)];
110
       H_{accelerometer\_pitch} = [zeros(1, 10), 1, zeros(1, 7)];
111
112
       H_{imu} = \dots
113
            [H_imu_accelerometer; H_accelerometer_roll;
114
               H_accelerometer_pitch];
115
   end
116
117
   function H_source = linearized_h_source(~)
   %linearized_h_source - linearize source of interest term in
      measurement function
   %
120
   % Syntax: H_source = linearized_h_source(x1_minus)
   %
122
  % not used yet
```

```
function F = linearized_state_update_matrix(x0, dt)
  % linearized_state_update_matrix - state update matrix used to
     propagate
  %
      covariance matrix (P0).
3
      % Make sure velo is a column vector. If it's not, throw error
5
      if size (x0, 2) \sim 1
6
           error('x must be a column vector');
7
      end
8
9
      % create parts of update matrix
10
      F_pos = get_position_update_matrix(dt);
11
      F_vel = get_velocity_update_matrix(dt);
      F_accel = get_acceleration_update_matrix();
13
      F_euler = get_eulerAngles_update_matrix();
      F_obstacle = get_obstacle_update_matrix(dt);
15
      F_source = get_source_update_matrix();
16
17
      % combine smaller matrices into complete update matrix
18
      F = vertcat(...)
19
           F_pos, F_vel, F_accel, F_euler, F_obstacle, F_source);
20
  end
21
22
```

```
function F_pos = get_position_update_matrix(dt)
  % get_position_update_matrix - compute position part of update
     matrix
      % matrix terms refer to the term that is multiplied by the
          state.
       pos\_term = eye(3);
27
       vel\_term = dt .* eye(3);
28
       accel term = 1/2 \cdot dt^2 \cdot eve(3);
29
       eulerangle\_term = zeros(3);
30
       obstacle\_term = zeros(3);
31
       source\_term = zeros(3);
32
33
      F_{pos} = \dots
34
           [pos_term, vel_term, accel_term, eulerangle_term,
35
              obstacle_term, source_term];
36
  end
37
  function F_vel = get_velocity_update_matrix(dt)
  % get_velocity_update_matrix - compute velocity part of update
     matrix
41
       pos\_term = zeros(3);
42
       vel\_term = eye(3);
43
       accel\_term = dt .* eye(3);
44
       eulerangle\_term = zeros(3);
45
```

```
obstacle\_term = zeros(3);
       source\_term = zeros(3);
47
       F_{vel} = \dots
           [pos_term, vel_term, accel_term, eulerangle_term,
              obstacle_term, source_term];
  end
52
  function F_accel = get_acceleration_update_matrix()
53
       pos\_term = zeros(3);
54
       vel\_term = zeros(3);
55
       accel\_term = eye(3);
56
       eulerangle\_term = zeros(3);
57
       obstacle\_term = zeros(3);
58
       source\_term = zeros(3);
59
60
       F accel = ...
           [pos_term, vel_term, accel_term, eulerangle_term,
62
              obstacle_term, source_term];
  end
  function F_euler = get_eulerAngles_update_matrix()
66
       pos\_term = zeros(3);
67
       vel\_term = zeros(3);
68
       accel\_term = zeros(3);
69
       eulerangle\_term = eye(3);
70
```

```
obstacle\_term = zeros(3);
71
       source\_term = zeros(3);
72
       F_{\text{euler}} = \dots
            [pos_term, vel_term, accel_term, eulerangle_term,
               obstacle_term, source_term];
  end
77
   function F_obstacle = get_obstacle_update_matrix(dt)
78
79
       pos\_term = zeros(3);
80
       vel\_term = -dt .* eye(3);
81
       accel\_term = zeros(3);
82
       eulerangle\_term = zeros(3);
83
       obstacle\_term = eye(3);
84
       source\_term = zeros(3);
85
86
       F_{obstacle} = \dots
87
            [pos_term, vel_term, accel_term, eulerangle_term,
               obstacle_term, source_term];
  end
  function F_source = get_source_update_matrix()
  \% this function does nothing for now
94
       pos\_term = zeros(3);
95
```

```
vel_term = zeros(3);
accel_term = zeros(3);
eulerangle_term = zeros(3);

obstacle_term = zeros(3);

source_term = zeros(3);

F_source = ...

[pos_term, vel_term, accel_term, eulerangle_term,
obstacle_term, source_term];
end
```

```
function R = measurement_covariance_matrix()
  %measurement_covariance_matrix - defines measurement covariance
     matrix
  %
3
  % Syntax: R = measurement_covariance_matrix()
  %
  % INPUTS
  %
      ySize: Used to determine size of R matrix
  % get sensor specification structures
  [accelerometer, ~, gps, altimeter, lidar, source] =
     get_sensor_specs();
11
  % gps terms
12
  sigma_gps_pos = gps.sigmaPos;
  sigma_gps_vel = gps.sigmaVel; % gps vel (m/s)
```

```
15
  \% altimeter term
16
  sigma_altimeter = altimeter.sigma; % altimeter altitude (m)
18
  % lidar term
  sigma_lidar = lidar.sigma; % lidar distance (m)
20
21
  \% accelerometer term
22
  sigma_accelerometer = accelerometer.sigma; % m/s^2
23
  sigma_accelerometer_roll_pitch = 0.1; \% rad/s^2
24
  % source terms
25
  sigma_source = source.sigma;
26
27
  % R matrix
28
  R = diag([...]
29
      sigma_gps_pos, sigma_gps_pos, sigma_gps_pos, sigma_gps_vel,
30
         sigma_gps_vel, ...
      sigma_altimeter, sigma_lidar, sigma_accelerometer,
31
         sigma_accelerometer, sigma_accelerometer, ...
      sigma_accelerometer_roll_pitch, sigma_accelerometer_roll_pitch
32
      sigma_source, sigma_source, sigma_source]).^2;
  end
```

```
function [region_struct, region_num, source_pos_estimate] =
     measurement_inside_region(region_struct, x0_plus, counts,
     region_num)
2 | measurement_inside_region - Record counts, position, and time
     inside a region
  %
3
  % Syntax: [counts, pos_ned, time] = measurement_inside_region()
  %
5
  %
6
7
      % unpack inputs
8
      [uav_pos_ned, ~, ~, ~, ~, ~] = unpack_state_vector(x0_plus);
9
10
      % initialize source_pos_estimate
11
      source_pos_estimate = [];
12
      % set thresholds to define region
13
                               % 1m diameter region. This means a
      region diameter = 0.1;
14
         0.5m deviation from r_region will stop that region.
15
       if region_num == 0
           if ~isempty (region_struct(1).center)
17
               error ('Region is set, but region number is zero.')
18
           else
19
               region_num = 1;
20
               region_struct(region_num).center = uav_pos_ned;
21
           end
23
      end
```

```
24
      % distance from region center to uav
25
      dist_region_center_to_uav = norm(uav_pos_ned - region_struct(
         region_num).center);
      % if we are out of the region, increment region_num and save
         the center of
      % the region
29
      if dist region center to uav > region diameter
30
           region_num = region_num + 1;
31
           if region_num <= 3
32
               region_struct(region_num).center = uav_pos_ned;
33
           end
34
      end
35
36
      % If our region num is less than or equal to three, save the
37
         uav position
      % and counts
38
      \% if region_num \ll 3
39
             region_struct(region_num).uav_pos_ned = [region_struct(
      \%
         region_num).uav_pos_ned, uav_pos_ned];
      %
             region_struct(region_num).counts = [region_struct(
41
         region_num).counts, counts];
      % else % else, compute source position estimate
                       % 100 counts per second
      %
             A0 = 100;
43
      %
             A_{background} = 10;
45
```

```
%
            % determine region with smallest number of counts
46
      %
             region_least_counts = min([length(region_struct(1).
47
         counts), length(region_struct(2).counts), length(
         region_struct(3).counts)]);
      %
             avg_counts_per_sec = zeros(1, 3);
49
             for i = 1:3
      %
50
                 secs_in_region = length(region_struct(i).counts) /
      %
51
          100; % 10 counts per second
      %
                 avg_counts_per_sec(i) = sum(region_struct(i).counts)
52
          / secs_in_region;
      %
             end
53
54
             activity_ratio = (A0 - A_background) ./
      %
55
         avg_counts_per_sec;
56
      %
             source pos estimate = [0, 0, 0];
      %
             for i = 3:-1:2
                 for j = 2:-1:1
      %
      %
                     source_pos_estimate = source_pos_estimate + (
         activity_ratio(i) .* region_struct(i).center./norm(
         region_struct(i).center)) - (activity_ratio(j) .*
         region_struct(j).center./norm(region_struct(j).center));
      %
                 end
      %
             end
62
63
```

```
% all_pos = [region_struct(1).uav_pos_ned, region_struct
              (2).uav_pos_ned, region_struct(3).uav_pos_ned];
          % all_counts = [region_struct(1).counts, region_struct(2).
              counts , region_struct(3).counts];
66
          % all_unit_pos = zeros(3, length(all_pos));
67
          \% for i = 1: length(all\_pos)
68
                all\_unit\_pos(:, i) = all\_pos(:, i) . / norm(all\_pos
69
              (:, i));
          % end
70
71
          % activity_ratio = (1./all_counts .* (A0-A_background))
72
              .^{(1/2)};
73
          % source_pos_estimate = sum(diff(activity_ratio, 1, 2) .*
74
              diff(all_unit_pos, 1, 2), 2);
          % reset region_struct and region_num
           region_struct = struct('center', [], 'uav_pos_ned', [],
77
              counts', []);
           region_num = 0;
78
      end
80
  end
```

```
function [x1_plus, P1_plus] = measurement_update(x1_minus,
P1_minus, y1)
```

```
%measurement_update - Perform measurement update step
  %
3
4 | Syntax: [x1_plus, P1_plus] = measurement_update(x1_minus,
     P1_minus)
  %
  % INPUTS
  %
      x1_minus [18 x 1]: state vector for kth state without
     measurement update
  %
     P1_minus [18 x 18]: covariance matrix for kth state without
     measurement
  %
           update
      y1 [N x 1]: measurement vector for kth state. Max size = 11,
10
     \min \text{ size} = 6
      originLLA [3 x 1]: origin of NED position as [latitude,
     longitude, altitude]
  %
12
  % OUTPUTS
  %
      x1_plus [18 x 1]: best state vector estimate for kth state
14
      P1_plus [18 x 18]: best error covariance matrix estimate
  %
15
      % Check if measurement_update can be performed. Skip if all
17
         measurement
      % values have been set to zero.
18
      if any (y1 \sim 0)
19
          % obtain state variables in measurement units
20
          hx = state_to_measurement(x1_minus, y1);
22
```

```
% construct state update matrix
          H = linearized_measurement_matrix(x1_minus, hx);
          % obtain measurement covariance matrix
26
          R = measurement_covariance_matrix();
28
          % Remove rows in H and R if there are no respective
29
              measurements.
          % Remove elements in hx
30
          % REMOVE IF USING COUNTS HERE
31
           y1(13) = 0;
32
           hx(y1 == 0) = [];
33
          H(y1 = 0, :) = [];
34
          R(y1 = 0, :) = [];
35
          R(:, y1 == 0) = [];
36
           y1(y1 == 0) = [];
37
          % compute Kalman Gain
          K = P1_{minus} * H' * (H * P1_{minus} * H' + R)^(-1);
          % measurement update of state estimate
42
           x1_plus = x1_minus + K * (y1 - hx);
43
44
          % measurement update of error covariance
45
           P1_{plus} = (eye(length(P1_{minus})) - K*H) * P1_{minus};
46
       else % no measurements are available. Skip measurement step
47
           x1_plus = x1_minus;
48
```

```
P1_plus = P1_minus;
end
end
end
```

```
function plots_kalmanfilter(yout_truth, yout_kalman, zout)
  %plots_kalmanfilter - plot kalman filter outputs against truth
     outputs
  %
3
  % Syntax: plots_kalmanfilter(yout_truth, yout_kalman)
  %
5
  % Long description
7
      % unpack inputs
8
      % truth state
9
      x_{truth} = yout_{truth.x};
10
      accel_truth = yout_truth.dxdt(4:6, :);
11
      t_truth = yout_truth.t;
13
      % kalman filter state
      x_kalman = yout_kalman.x;
15
      t_kalman = yout_kalman.t;
16
17
      ned2enu = [0, 1, 0; 1, 0, 0; 0, 0, -1];
18
19
       if nargin > 2
20
           % measurements
21
           gps = zout.gps;
22
```

```
lidar = zout.lidar;
           imu = zout.imu;
           source = zout.source;
       end
26
       if nargin = 2
28
29
           % Position
30
           figure();
31
           subplot (2, 1, 1);
32
           plot(t_truth, x_truth(1, :), t_kalman, x_kalman(1, :));
33
           ylabel('North (m)');
34
           title ('Position vs Time')
35
           legend('Truth', 'Kalman')
36
37
           subplot(2, 1, 2);
38
           plot(t_truth, x_truth(2, :), t_kalman, x_kalman(2, :));
           ylabel ('East (m)');
40
           xlabel('Time (s)');
           figure()
43
           posTruthNED = ned2enu * x_truth(1:3, :);
           posKalmanNED = ned2enu * x_kalman(1:3, :);
45
           subplot(3, 1, 1);
46
           plot(t_truth, posTruthNED(1, :), t_kalman, posKalmanNED(1,
47
               :));
           ylabel ('East (m)');
48
```

```
title ('Position vs Time');
             legend('Truth', 'Kalman');
             subplot (3, 1, 2);
             plot(t_truth, posTruthNED(2, :), t_kalman, posKalmanNED(2,
52
                  :));
             ylabel('North (m)');
53
             subplot(3, 1, 3);
54
             \label{eq:plot_struth} \begin{array}{ll} \texttt{plot}\left(\,\texttt{t\_truth}\,\,,\,\,\,\texttt{posTruthNED}\left(\,3\,\,,\,\,\,:\,\right)\,\,,\,\,\,\,\texttt{t\_kalman}\,\,,\,\,\,\,\texttt{posKalmanNED}\left(\,3\,\,,\,\,\,\right) \\ \end{array}
55
                  :));
             xlabel('Time (sec)');
             ylabel('Up (m)');
57
58
             % Altitude
59
             figure()
60
             plot(t_{truth}, -x_{truth}(3, :), t_{kalman}, -x_{kalman}(3, :));
             ylabel ('Altitude (m)');
62
             xlabel('Time (s)');
             title ('Altitude vs Time')
             legend('Truth', 'Kalman');
             % velocity
67
             figure();
             subplot (3, 1, 1);
69
             ylabel('v_x (m/s)');
71
             title ('Inertial Velocity vs Time')
72
             legend('Truth', 'Kalman');
73
```

```
subplot(3, 1, 2)
           plot(t_truth, x_truth(5, :), t_kalman, x_kalman(5, :));
           ylabel('v_y (m/s)');
77
78
           subplot (3, 1, 3)
79
           80
           ylabel('v_z (m/s');
81
           xlabel('Time (s)');
82
83
           % Accelerations
84
           figure();
85
           subplot(3, 1, 1);
86
           \label{eq:plot_truth} plot\left(t\_truth\;,\;\; accel\_truth\left(1\;,\;\;:\right)\;,\;\; t\_kalman\;,\;\; x\_kalman\left(7\;,\;\;:\right)\;\right)
87
              ;
            title ('Inertial Acceleration vs Time')
           ylabel('a_x (m/s^2)')
           legend('Truth', 'Kalman');
           subplot (3, 1, 2);
           plot(t_truth, accel_truth(2, :), t_kalman, x_kalman(8, :))
               ;
           ylabel('a_y (m/s^2)');
95
           subplot(3, 1, 3);
           plot(t_truth, accel_truth(3, :), t_kalman, x_kalman(9, :))
97
               ;
```

```
ylabel('a_z (m/s^2)');
            xlabel('Time (s)');
100
           % Euler angles
101
            figure();
102
            subplot(3, 1, 1);
103
            plot(t_truth, rad2deg(x_truth(10, :)), t_kalman, rad2deg(
104
               x_kalman(10, :));
            ylabel('Roll (deg)');
105
            title ('Euler Angles vs Time')
106
            legend('Truth', 'Kalman');
107
108
            subplot(3, 1, 2);
109
            plot(t_truth, rad2deg(x_truth(11, :)), t_kalman, rad2deg(
110
               x_kalman(11, :));
            ylabel('Pitch (deg)');
111
112
            subplot (3, 1, 3);
113
            plot(t_truth, rad2deg(x_truth(12, :)), t_kalman, rad2deg(
114
               x_kalman(12, :));
            ylabel('Yaw (deg)');
            xlabel('Time (s)');
116
117
           % % Obstacle distance
118
           % figure();
119
           \% subplot (3, 1, 1);
120
```

```
\% plot(t_truth, x_truth(13, :), t_kalman, x_kalman(13, :))
121
           % ylabel('\chi_N (m)')
122
           % title ('Inertial Obstacle distance vs Time')
123
           % legend ('Truth', 'Kalman');
124
125
           \% subplot (3, 1, 2);
126
           % plot(t_truth, x_truth(14, :), t_kalman, x_kalman(14, :))
127
               ;
           % ylabel('\chi_E (m)')
128
129
           \% subplot (3, 1, 3);
130
           \% plot (t_truth, x_truth (15, :), t_kalman, x_kalman (15, :))
131
           % ylabel('\chi_D (m)');
132
           \% xlabel('Time (s)')
133
134
           % source
135
           % source position relative to UAV
136
            source_pos_ned = x_{truth}(1:3, 1) + x_{truth}(16:18, 1);
137
            kalman\_source\_pos\_from\_uav = [source\_pos\_ned(1) - x\_kalman]
138
               (1, :); source_pos_ned(2) - x_kalman(2, :);
               source_pos_ned(3) - x_kalman(3, :)];
            figure();
139
            subplot(3, 1, 1);
140
            plot(t_truth, x_truth(16, :), t_kalman,
141
               kalman_source_pos_from_uav(1, :))
```

```
ylabel('s_x');
142
            title ('NED Source position from UAV vs Time');
143
            subplot (3, 1, 2);
145
            plot(t_truth, x_truth(17, :), t_kalman,
146
               kalman_source_pos_from_uav(2, :))
            ylabel('s_y');
147
148
            subplot(3, 1, 3);
149
            plot (t_truth, x_truth(18, :), t_kalman,
150
               kalman_source_pos_from_uav(3, :))
            xlabel('Time (s)');
151
            ylabel('s_z');
152
            legend('Truth', 'Kalman')
153
154
            % source distance from UAV
155
            source\_dist\_truth = zeros(1, length(x\_truth(15, :)));
156
            source_dist_kalman= zeros(1, length(x_kalman(15, :)));
157
            for i = 1: length(x_truth)
                source\_dist\_truth(i) = norm(x\_truth(16:18, i));
            end
160
            for i = 1: length(x_kalman)
161
                source_dist_kalman(i) = norm(
162
                   kalman_source_pos_from_uav(1:3, i));
            end
163
            figure()
164
```

```
plot(t_truth, source_dist_truth, t_kalman,
165
               source_dist_kalman)
            xlabel ('Time (s)')
            ylabel('Dist (m)');
167
            title ('Source distance from UAV');
168
            legend('Truth', 'Kalman');
169
170
       end
171
172
        if nargin > 2
173
            gps\_pos\_ned = gps.position;
174
            figure();
175
            subplot(2, 1, 1);
176
            plot(t_{truth}, x_{truth}(1, :), t_{kalman}, x_{kalman}(1, :), gps
177
               t, gps\_pos\_ned(1, :));
            ylabel ('North (m)');
178
            title ('Position vs Time')
179
            legend('Truth', 'Kalman', 'GPS')
180
181
            subplot (2, 1, 2);
            plot(t_t), x_tuth(2, :), t_kalman, x_kalman(2, :), gps
183
               .t, gps\_pos\_ned(2, :));
            ylabel('East (m)');
184
            xlabel('Time (s)');
185
186
            % Altitude
187
            figure()
188
```

```
189
              gps.t \;,\; -gps\_pos\_ned \left( 3 \;,\;\; : \right) \;) \;;
           ylabel ('Altitude (m)');
           xlabel('Time (s)');
191
           title ('Altitude vs Time')
192
           legend('Truth', 'Kalman', 'GPS');
193
194
           % velocity
195
           figure();
196
           subplot(3, 1, 1);
197
           plot(t_truth, x_truth(4, :), t_kalman, x_kalman(4, :));
198
           ylabel('v_x (m/s)');
199
            title ('Inertial Velocity vs Time')
200
           legend('Truth', 'Kalman');
201
202
           subplot(3, 1, 2)
203
           plot(t_truth, x_truth(5, :), t_kalman, x_kalman(5, :));
204
           ylabel('v_y (m/s)');
205
206
           subplot (3, 1, 3)
           plot(t_truth, x_truth(6, :), t_kalman, x_kalman(6, :));
           ylabel('v_z (m/s');
           xlabel('Time (s)');
210
211
           % Accelerations
212
           figure();
213
           subplot (3, 1, 1);
214
```

```
215
                ;
             title ('Inertial Acceleration vs Time')
216
            ylabel('a_x (m/s^2)')
            legend('Truth', 'Kalman');
218
219
            subplot(3, 1, 2);
220
            plot(t_truth, accel_truth(2, :), t_kalman, x_kalman(8, :))
221
                ;
            ylabel('a_y (m/s^2)');
222
223
            subplot (3, 1, 3);
224
            \label{eq:plot_truth} plot\left(t\_truth\;,\;\; accel\_truth\left(3\;,\;\;:\right)\;,\;\; t\_kalman\,,\;\; x\_kalman\left(9\;,\;\;:\right)\;\right)
225
            ylabel ('a_z (m/s^2)');
226
            xlabel('Time (s)');
227
228
            % Euler angles
229
            figure();
230
            subplot (3, 1, 1);
231
            plot(t_truth, rad2deg(x_truth(10, :)), t_kalman, rad2deg(
                x_kalman(10, :));
            ylabel('Roll (deg)');
             title ('Euler Angles vs Time')
234
            legend('Truth', 'Kalman');
235
236
            subplot (3, 1, 2);
237
```

```
plot(t_truth, rad2deg(x_truth(11, :)), t_kalman, rad2deg(
238
                                                                                                                        x_kalman(11, :));
                                                                                                ylabel('Pitch (deg)');
239
240
                                                                                                subplot (3, 1, 3);
^{241}
                                                                                               plot\left(t\_truth\;,\; rad2deg\left(x\_truth\left(12\;,\;\;:\right)\right)\;,\;\; t\_kalman\;,\;\; rad2deg\left(x\_truth\left(12\;,\;\;:\right)\right)\;,\;\; t\_t\_truth\left(12\;,\;\;:\right)\;,\;\; t\_truth\left(12\;,\;\;:\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_truth\left(12\;,\;\::\right)\;,\;\; t\_trut
^{242}
                                                                                                                        x_kalman(12, :));
                                                                                                ylabel('Yaw (deg)');
243
                                                                                                xlabel('Time (s)');
244
245
                                                                                             % Obstacle distance
246
                                                                                                lidar_dist_ned = DCM_body2ned(lidar.distance, imu.
247
                                                                                                                         eulerangles);
                                                                                                figure();
248
                                                                                                subplot(3, 1, 1);
249
                                                                                                plot (t_truth, x_truth (13, :), t_kalman, x_kalman (13, :),
250
                                                                                                                         lidar.t, lidar_dist_ned(1, :));
                                                                                                ylabel ('\chi_N (m)')
251
                                                                                                 title ('Inertial Obstacle distance vs Time')
252
                                                                                                legend('Truth', 'Kalman', 'LIDAR');
                                                                                                subplot(3, 1, 2);
255
                                                                                                plot(t_{t_{1}}, x_{t_{1}}, x_{t_{2}}, t_{1}, t_{1}, x_{t_{2}}, t_{1}, t_{1}, x_{t_{2}}, t_{1}, t_{2}, t_{
256
                                                                                                                         lidar.t, lidar\_dist\_ned(2, :));
                                                                                                ylabel ('\chi_E (m)')
257
258
                                                                                                subplot (3, 1, 3);
259
```

```
plot (t_truth, x_truth (15, :), t_kalman, x_kalman (15, :),
260
               lidar.t, lidar_dist_ned(3, :));
            ylabel('\chi_D (m)');
261
            xlabel ('Time (s)')
262
263
            % source estimate
264
            % source position relative to UAV
265
            figure();
266
            subplot(3, 1, 1);
267
            plot (t_truth, x_truth(16, :), t_kalman, x_kalman(16, :))
268
            ylabel('s_x');
269
            title ('NED Source position from UAV vs Time');
270
271
            subplot(3, 1, 2);
272
            plot (t_truth, x_truth (17, :), t_kalman, x_kalman (17, :));
273
            ylabel('s_y');
274
            subplot (3, 1, 3);
276
            plot(t_truth, x_truth(18, :), t_kalman, x_kalman(18, :));
277
            xlabel('Time (s)');
            ylabel('s_z');
280
            % counts plot
281
            figure();
282
            plot(source.t, source.counts);
283
            xlabel('Time (s)');
284
            ylabel('Counts');
285
```

```
title ('Counts vs Time');
end
end
end
```

```
function Q = process_noise_matrix(dt)
  % process_noise_matrix - outputs process noise matrix
2
3
      k = 0.1; % manually tuned gain for filter
4
5
      [~, gyro, ~, ~, ~, ~] = get_sensor_specs();
6
7
      % process noise parts
8
      Q_pos = position_process_noise();
9
      Q_vel = velocity_process_noise();
10
      Q_acceleration = acceleration_process_noise();
11
      Q_euler = euler_angle_process_noise(dt, gyro);
12
      Q_obstacle = obstacle_process_noise();
      Q_source = source_process_noise();
      % process noise matrix
16
      Q = k .* vertcat(Q_pos, Q_vel, Q_acceleration, Q_euler,
17
         Q_obstacle, Q_source);
  end
18
19
  function Q_pos = position_process_noise()
20
  \% position part of process noise matrix
22
```

```
k_{pos} = 0;
23
       pos\_term = k\_pos .* eye(3);
24
       vel\_term = zeros(3);
       accel\_term = zeros(3);
       eulerAngle\_term = zeros(3);
       obstacle\_term = zeros(3);
28
       source\_term = zeros(3);
29
      Q_pos = [pos_term, vel_term, accel_term, eulerAngle_term,
30
          obstacle_term, source_term];
31
  end
32
33
  function Q_vel = velocity_process_noise()
  % velocity part of process noise matrix
35
36
      k_{vel} = 0.1;
37
       pos term = zeros(3);
38
       vel\_term = k\_vel .* eye(3);
39
       accel\_term = zeros(3);
40
       eulerAngle\_term = zeros(3);
       obstacle\_term = zeros(3);
       source\_term = zeros(3);
44
       Q_vel = [pos_term, vel_term, accel_term, eulerAngle_term,
          obstacle_term, source_term];
  end
47
```

```
function Q_acceleration = acceleration_process_noise()
      k_accel = 0.1;
49
      pos\_term = zeros(3);
      vel\_term = zeros(3);
51
      accel\_term = k\_accel .* eye(3);
      eulerAngle\_term = zeros(3);
53
      obstacle\_term = zeros(3);
54
      source\_term = zeros(3);
55
56
       Q_acceleration = [pos_term, vel_term, accel_term,
57
          eulerAngle_term , obstacle_term , source_term ];
  end
59
  function Q_euler = euler_angle_process_noise(dt, gyro)
60
      k_euler = 1;
61
      pos\_term = zeros(3);
62
      vel term = zeros(3);
63
      accel\_term = zeros(3);
64
      eulerAngle_term = 1*k_euler .* gyro.sigma^2 .* dt^2 .* diag
          ([10, 10, .1]);
      obstacle\_term = zeros(3);
      source\_term = zeros(3);
68
      Q_euler = [pos_term, vel_term, accel_term, eulerAngle_term,
          obstacle_term, source_term];
  end
71
```

```
function Q_obstacle = obstacle_process_noise()
       k_obstacle = 0.1;
       pos\_term = zeros(3);
       vel\_term = zeros(3);
75
       accel\_term = zeros(3);
76
       eulerAngle\_term = zeros(3);
77
       obstacle_term = k_obstacle .* eye(3);
78
       source\_term = zeros(3);
79
       Q_obstacle = [pos_term, vel_term, accel_term, eulerAngle_term,
80
           obstacle_term, source_term];
81
  end
82
83
  function Q_source = source_process_noise()
84
       pos\_term = zeros(3);
85
       vel\_term = zeros(3);
86
       accel term = zeros(3);
87
       eulerAngle\_term = zeros(3);
88
       obstacle\_term = zeros(3);
       source\_term = 10 .* eye(3);
       Q_source = [pos_term, vel_term, accel_term, eulerAngle_term,
          obstacle_term, source_term];
  end
```

```
%
3
  % Syntax: [x_out, P_out, t_out] = run_kalman_filter(x, P, tspan)
  %
  % Long description
7
  % Need accelerometer and gyro specs
9
       [\sim, \text{ gyro\_specs}, \sim, \sim, \sim, \sim] = \text{get\_sensor\_specs}();
10
11
      % Populate UAV specs
12
      UAV = initialize_uav();
13
14
      % time settings
15
       t = tspan(1);
16
       t_final = tspan(2);
17
       dt = 1/gyro_specs.sampleRate; % timestep should be set to
18
          accelerometer sample time.
       t_out = t:dt:t_final; % array of times
19
20
      % unpack imu measurements
^{21}
       gyro_meas = zout.imu.gyroscope;
       imu\_index = find(zout.imu.t == t); \% where to start imu
          measurements
24
      % initialize outputs
25
       x_{out} = zeros(18, length(t_{out}));
26
       P_{out} = zeros(18, 18, length(t_out));
27
```

```
% run kalman filter for the length of array t_out
29
       t = t + dt; % kalman filter needs to start at t0 + dt
       for kalman_index = (imu_index + 1):length(t_out)
31
32
           % obtain imu measurement and perform time update
33
           gyro\_reading = gyro\_meas(:, kalman\_index - 1);
34
           [x1\_minus, P1\_minus] = time\_update(x0\_plus, P0\_plus,
35
              gyro_reading, dt, UAV);
36
           % update
37
           if mod(t, 0.01) = 0
38
               % obtain measurement vector
39
               [y1] = simulate_measurement_vector(t, zout);
40
               % perform measurement update
41
               [x1_plus, P1_plus] = measurement_update(x1_minus,
42
                  P1_minus, y1);
           else
43
               x1_plus = x1_minus;
               P1_{plus} = P1_{minus};
           end
46
47
           % update current time
48
           t = t + dt;
49
           t = round(t, 6);
50
51
           % store state and covariance matrix
52
```

```
x_out(:, kalman_index) = x1_plus;

P_out(:, :, kalman_index) = P1_plus;

x0_plus = x1_plus;

P0_plus = P1_plus;

end

end

end

end
```

```
function [yout_truth, yout_kalman, zout] = sim_kalman_filter(
     savedflight_filepath)
  %sim_kalman_filter - Simulate kalman filter
  \%
3
  |% Syntax: [yout_truth, yout_kalman, zout] = sim_kalman_filter(
     savedflight_filepath)
  % Need to run simulation to populate measurements
  addpath (genpath ('./../Simulation/'));
  addpath(genpath('./../Utilities/'));
9
  % run sim without plots
10
  if nargin == 0
11
      [yout_truth, zout] = initialize_sim(0);
12
  elseif nargin = 1 % load input saved flight
13
      saved_flight_vars = load(savedflight_filepath);
14
      yout_truth = saved_flight_vars.yout;
15
```

```
zout = saved_flight_vars.zout;
  else
17
       error('sim_kalman_filter should only have 0 or 1 input');
  end
19
  % time settings
  tSpan = [0, yout\_truth.t(end)]; % dt = 0.01 sec
23
  % Get initial state
  x_{init} = yout_{truth.x(:, 1)};
25
  x_{init}(end-2:end) = [0, 0, 0]';
26
27
  % Get initial covariance matrix
  P_init = initial_covariance_matrix();
29
  tic
30
  [x_out, P_out, t_out] = run_kalman_filter(x_init, P_init, tSpan,
     zout);
  toc
32
  yout_kalman.x = x_out;
  yout_kalman.P = P_out;
  yout_kalman.t = t_out;
  plots_kalmanfilter(yout_truth, yout_kalman);
38
  end
39
```

```
function [y1] = simulate_measurement_vector(time, zout)
```

```
|%simulate_measurement_vector - Simulate measurement vector based
     on sample times
  %
3
  |% Syntax: [y1, counts] = simulate_measurement_vector(time, zout)
  %
  % if gps is available:
      y1 = [y_gps, y_altimeter, y_lidar, y_imu, y_source]'
  % if gps is not available, but altimeter is available:
     y1 = [y \text{ altimeter}, y \text{ lidar}, y \text{ imu}, y \text{ source}]'
  % if gps and altimeter are not available, lidar, imu, and source
     should always be
  % available.
  %
      y1 = [y_lidar, y_imu, y_source]'
12
13
      % unpack inputs
14
      gps\_measurements = zout.gps;
15
      altimeter measurements = zout.altimeter;
16
      lidar_measurements = zout.lidar;
17
      imu = zout.imu;
18
      source = zout.source;
      % Fix time overflow. Rounding to 6 decimal places should be
          more than enough
      time = round(time, 6);
23
      % Populate sensor specs. No need for altimeter or gyro
^{24}
```

```
[accelerometer_specs, ~, gps_specs, altimeter_specs, ~,
25
         source_specs = get_sensor_specs();
      % If gps would be available, find simulated measurement
27
      if mod(time, round(1/gps\_specs.sampleRate, 6)) == 0
           gps_index = find (gps_measurements.t == time);
29
           y_gps = [gps_measurements.position(:, gps_index);
30
              gps_measurements.velocity(:, gps_index);
          % if altitude reading for gps is less than zero, disregard
31
               the measurement.
           if y_gps(3) < 0
32
               y_gps(3) = 0;
33
           end
34
       else
35
           y_gps = [0; 0; 0; 0; 0];
36
      end
37
      % check for altimeter
39
40
       if mod(time, round(1/altimeter_specs.sampleRate, 6)) = 0
           y_altimeter = altimeter_measurements.altitude(:,
              altimeter_measurements.t == time);
      else
43
           y_altimeter = 0;
44
      end
45
46
      % remaining sensors should always be available
47
```

```
% lidar
      y_lidar = lidar_measurements.distance(1, lidar_measurements.t
49
         = time);
50
      % disregard lidar measurement if it is greater than 20m or
51
         equal to zero.
       if y_{lidar} = 0 \mid y_{lidar} > 20
52
           y_{lidar} = 0;
53
       elseif y_lidar < 0 % lidar should never be negative
54
           error ("lidar reading negative: %d", y_lidar);
55
      end
56
57
      % imu
58
      if mod(time, round(1/accelerometer\_specs.sampleRate, 6)) == 0
59
           y_accelerations = imu.accelerometer(:, imu.t == time);
60
           y_accelerometer_ind = find(imu.t = time);
           if time > 1.01
               last_second_accel = imu.accelerometer(:,
                  y_accelerometer_ind -100:y_accelerometer_ind);
               last\_second\_accel\_roll\_pitch = imu.
                  accelerometer_roll_pitch(:, y_accelerometer_ind
                  -100:y_accelerometer_ind);
               norm_last_second_accel = zeros(1, length(
                  last_second_accel));
               for i = 1:length(norm_last_second_accel)
                   norm_last_second_accel(i) = norm(last_second_accel
67
                      (:, i));
```

```
end
               if abs(9.8 - mean(norm\_last\_second\_accel)) > 0.001
                    y_accelerometer_roll_pitch = [0; 0];
               else
71
                    y_accelerometer_roll_pitch = mean(
                       last_second_accel_roll_pitch , 2);
                    if any(rad2deg(y_accelerometer_roll_pitch) > 5)
73
                        y_accelerometer_roll_pitch = [0;0];
74
                    end
75
76
               end
77
           else
78
               y_accelerometer_roll_pitch = [0; 0];
79
           end
80
       else
81
           error ('IMU should be available every timestep');
82
       end
84
      % source
       y_{source} = [0; 0; 0; 0]; \% initialize y_{source}
       if mod(time, round(1/source\_specs.sampleRate, 6)) == 0
           counts = source.counts(source.t == time);
           y \text{ source}(1) = counts;
89
      end
90
      % find the most recent source_position estimate if one exists
91
      % source_pos_estimate_ind = find(time >= source.
92
          position_estimate(1, :), 1, 'last');
```

```
% if ~isempty(source_pos_estimate_ind)
93
       %
              y_{source}(2:4) = source.position_estimate(2:4)
94
          source_pos_estimate_ind);
       %
              if time > source.position_estimate(1,
          source_pos_estimate_ind) + .009
       %
                  y source (2:4) = [0;0;0];
       %
              end
97
       % end
98
99
       % create output
100
       y1 = [y_gps; y_altimeter; y_lidar; y_accelerations;
101
          y_accelerometer_roll_pitch; y_source];
102
       if length(y1) \sim 16
103
            error ('y1 was not fully populated.');
104
       end
105
   end
106
```

```
function hx = state_to_measurement(x1_minus, y1)
% state_to_measurement - convert state vector to measurement units
%
% Measurements are as follows:
% GPS: [latitude, longitude, altitude, groundspeed, course] (deg , deg, m, m/s, deg)
% Altimeter: [altitude] (m)
% LIDAR: [distance] (m)
% External sensor (Geiger counter): [counts, p2, p3, p4]
```

```
%
           note p2 - p4 are unused
10
      % unpack state
       [pos, vel, accel, eulerangles, obstacle_pos, source_pos] =
12
          unpack_state_vector(x1_minus);
13
      % initialize output
14
15
      % Populate hx if y1 contains a corresponding measurement.
16
17
      \% gps
18
      hx_gps = state_to_gps(pos, vel);
19
       hx_gps(y1(1:5) == 0) = 0;
20
21
      % altimeter
22
       if y1(6) \sim = 0
23
           hx_altimeter = state_to_altimeter(pos);
       else
25
           hx_altimeter = 0;
       end
      % lidar
       if y1(7) \sim 0
30
           hx_lidar = state_to_lidar(eulerangles, obstacle_pos);
31
       else
32
           hx_lidar = 0;
33
       end
34
```

```
35
      % imu
36
       if y1(8) \sim 0
           hx_imu = state_to_imu(accel, eulerangles);
38
       else
           hx_imu = [0; 0; 0; 0; 0];
40
       end
41
      % angle reading from accelerometer may not be good
42
       if y1(11) = 0
43
           hx_imu(4:5) = [0; 0];
44
       end
45
46
      % source
47
       hx_source = state_to_source(source_pos);
48
49
      % output
50
      hx = [hx_gps; hx_altimeter; hx_lidar; hx_imu; hx_source];
52
      \% throw error if y1 and hx do not have the same length.
       if length(y1) \sim length(hx)
           error ('y1 and hx should have the same length')
55
       end
57
  end
59
  function hx_gps = state_to_gps(pos_ned, vel_ned)
60
  % convert state vector into GPS measurement units
```

```
62
      % gps only measures groundspeed.
63
      vel_ne = vel_ned(1:2);
      hx\_gps = [pos\_ned; vel\_ne];
  end
68
  function hx_altimeter = state_to_altimeter(pos_ned)
  \% convert state vector into altimeter measurement units
71
      hx\_altimeter = -pos\_ned(3); \% meters
72
73
  end
74
75
  function hx_lidar = state_to_lidar(eulerangles, obstacle_pos_ned)
76
  \% convert state vector into lidar measurement units
77
  %
78
  \% lidar is assumed to point in the +bx direction
80
      obstacle_pos_body = DCM_ned2body(obstacle_pos_ned, eulerangles
          );
      hx_lidar = obstacle_pos_body(1);
83
  end
85
86
  function hx_imu = state_to_imu(accel_ned, eulerangles)
```

```
% observables: [accel_body, roll, pitch]
       accel_body = DCM_ned2body(accel_ned + [0; 0; 9.8], eulerangles
89
          );
       roll = eulerangles (1);
       pitch = eulerangles(2);
92
       hx_imu = [accel_body; roll; pitch];
93
94
   end
95
96
   function hx_source = state_to_source(~)
97
   % convert state vector into source units
99
       hx\_source = [0, 0, 0, 0];
100
   end
101
```

```
function x1 = state_update(x0, dt, UAV, gyro)
% state_update - non-linear state update function.

Which is update function.

Which is update function.

The impact of the impact of
```

```
m = UAV. mass;
12
  \% Thrust is assumed to be equal and opposite to the weight of the
     UAV. Note however that thrust always acts in the -body z
     direction
  thrust\_body = [0, 0, -m*g / (cos(eulerangles0(1)) * cos(
     eulerangles 0(2)));
  thrust_ned = DCM_body2ned(thrust_body, eulerangles0);
16
  \% alter gyro input
17
  eulerrates 0 = angVel_to_eulerRates (eulerangles 0) * gyro;
18
19
  % State Update
20
21
  pos1 = pos0 + vel0 .* dt + 1/2 .* accel0 .* dt^2;
22
  vel1 = vel0 + accel0 .* dt; % velocity in z is assumed to be
     almost always constant
  accel1 = [thrust\_ned(1)/m; thrust\_ned(2)/m; accel0(3)];
  eulerangles1 = eulerangles0 + eulerrates0 * dt;
  obstacle_pos1 = obstacle_pos0 - vel0 .* dt;
  source_pos1 = source_pos0;
  % updated state
  x1 = [pos1; vel1; accel1; eulerangles1; obstacle_pos1; source_pos1
     ];
  end
```

```
function [x1_minus, P1_minus] = time_update(x0_plus, P0_plus,
     gyro_meas, dt, UAV)
  |% time_update - Performs time_update step for the Kalman filter
  %
3
  |% Usage: [x1_minus, P1_minus] = time_update(x0_plus, P0_plus, Q,
     UAV, imu_meas)
  %
5
  % INPUTS
  %
      x0_plus: [18 x 1] + state vector for k-1th state
7
  %
      P0_plus: [18 x 18] + covariance matrix for -1th state
      imu_meas: [6 x 1] IMU measurements for k-1th state (accel,
  %
     gyro)
  %
      Q: [18 x 18] process noise matrix
      UAV: [struct] structure containing UAV parameters
  \%
  %
12
  % OUTPUTS
      x1_minus: [18 x 1] state vector for kth state without
14
     measurement update
  %
     P1_minus: [18 x 18] covariance matrix for kth state without
     measurement update
16
  % Populate process noise covariance matrix
17
  Q = process_noise_matrix(dt);
18
19
  % compute partial derivative matrix
 | F0 = linearized_state_update_matrix(x0_plus, dt);
```

APPENDIX D

UTILITIES

```
function angVel_to_eulerRates_matrix = angVel_to_eulerRates(
     euler Angles)
  % output 3x3 transformation matrix converting angular velocity to
     euler
  % rates
  %
  % Syntax: angVel_to_eulerRates_matrix = angVel_to_eulerRates(
     eulerAngles)
  %
  % INPUTS
       eulerAngles: [3 x 1] containing euler angles in radians
  % OUTPUTS
      angVel_to_eulerRates_matrix: [3x3] containing angular velocity
  \%
10
      to euler
  %
           rates transformation
11
12
  phi = eulerAngles(1);
  theta = eulerAngles(2);
  angVel_to_eulerRates_matrix = [...
16
       1, \sin(\phi)*\tan(\phi), \cos(\phi)*\tan(\phi); ...
17
       0, \cos(\mathrm{phi}), -\sin(\mathrm{phi}); ...
18
       0, \sin(\phi) *\sec(\phi), \cos(\phi) *\sec(\phi);
20
```

end end

```
function [vNED, iTb] = DCM_body2ned(vBody, eulerAngles)
  |% DCM_body2ned - Transform vector in NED frame to body frame
  %
3
  % Syntax: [vNED, iTb] = DCM_body2ned(vBody, eulerAngles)
  %
5
  % INPUTS
  %
                       [3 x n] vectors in NED frame
      vBody:
  %
      eulerAngles:
                       [3 x n] vectors of euler angles [roll, pitch,
     yaw]' (rad)
  % OUTPUTS
  %
      vNED:
                   [3 x n] column vectors in NED frame
10
      iTb:
                       [3 x 3 x n] body to inertial transformation
  \%
11
12
  \% initialize outputs
13
  numVect = size(vBody, 2);
  vNED = zeros(3, numVect); % vector in NED
  iTb = zeros(3, 3, numVect); \% body to inertial DCM
17
  % unpack Euler Angles
  phi = eulerAngles(1, :);
                              % roll
19
  theta = eulerAngles(2, :); \% pitch
  psi = eulerAngles(3, :);
21
22
  \% 3-2-1 DCM giving iTb
```

```
Tphi = @(roll) [1, 0, 0; 0, cos(roll), sin(roll); 0, -sin(roll),
     cos(roll);
  Ttheta = @(pitch) [cos(pitch), 0, -sin(pitch); 0, 1, 0; sin(pitch)
     , 0, cos(pitch);
  Tpsi = @(yaw) [cos(yaw), sin(yaw), 0; -sin(yaw), cos(yaw), 0; 0,
     [0, 1];
27
  for i = 1:numVect
28
      bTi = Tphi(phi(i)) * Ttheta(theta(i)) * Tpsi(psi(i));
29
      iTb(:, :, i) = bTi';
30
      vNED(:, i) = iTb(:, :, i) * vBody(:, i);
31
  end
32
33
34
  end
35
```

```
function [vWind, wTb] = DCM_body2wind(vBody, aoa, ssa)
 % DCM_ned2body - Transform vector in NED frame to body frame
 %
3
 % Syntax: [vWind, wTb] = DCM_body2wind(vBody, aoa, ssa)
 %
5
 % INPUTS
 %
      vBody:
              [3 x n] column vectors in body frame
7
 %
              [1 x n] vector of angle of attack (rad)
      aoa:
8
 %
              [1 x n] vector of side slip angle (rad)
      ssa:
 % OUTPUTS
 %
                      [3 x n] column vectors in wind frame
      vWind:
```

```
%
      wTb:
                       [3 x 3 x n] body to wind transformation
12
13
  \% initialize outputs
  numVect = size(vBody, 2);
  vWind = zeros(3, numVect);
  wTb = zeros(3, 3, numVect);
                                % initialize inertial to body
17
     transformation matrix
18
  % Transforms
19
  Taoa = @(alpha) [cos(alpha), 0, -sin(alpha); 0, 1, 0; sin(alpha),
20
     0, cos(alpha);
  Tssa = @(beta) [cos(beta), sin(beta), 0; -sin(beta), cos(beta), 0;
      0, 0, 1;
22
  for i = 1:numVect
23
      wTb(:, :, i) = Tssa(ssa(i)) * Taoa(aoa(i));
^{24}
      vWind(:, i) = wTb(:, :, i) * vBody(:, i);
25
  end
26
  end
```

```
function [vBody, bTi] = DCM_ned2body(vNED, eulerAngles)

CM_ned2body - Transform vector in NED frame to body frame

Symmetry

Syntax: [vBody, bTi] = DCM_ned2body(vNED, eulerAngles)

Matrix

Syntax: [vBody, bTi] = DCM_ned2body(vNED, eulerAngles)
```

```
% INPUTS
  \%
      vNED:
                       [3 x n] column vectors in NED frame
7
  %
      eulerAngles:
                       [3 x n] vectors of euler angles [roll, pitch,
     yaw]' (rad)
  % OUTPUTS
  %
                       [3 x n] column vectors in body frame
      vBody:
  \%
      bTi:
                       [3 x 3 x n] inertial to body transformation
11
12
  \% initialize outputs
13
  numVect = size(vNED, 2);
14
  vBody = zeros(3, numVect);
  bTi = zeros(3, 3, numVect); % initialize inertial to body
     transormation matrix
17
  % unpack Euler Angles
18
  phi = eulerAngles(1, :); % roll
  theta = eulerAngles(2, :); \% pitch
  psi = eulerAngles(3, :);
                              % yaw
21
22
  \% 3-2-1 DCM
  Tphi = @(roll) [1, 0, 0; 0, cos(roll), sin(roll); 0, -sin(roll),
     cos(roll);
  Ttheta = @(pitch) [cos(pitch), 0, -sin(pitch); 0, 1, 0; sin(pitch)
     0, \cos(\text{pitch});
  Tpsi = @(yaw) [cos(yaw), sin(yaw), 0; -sin(yaw), cos(yaw), 0; 0,
     [0, 1];
27
```

```
for i = 1:numVect

bTi(:, :, i) = Tphi(phi(i)) * Ttheta(theta(i)) * Tpsi(psi(i));

vBody(:, i) = bTi(:, :, i) * vNED(:, i);

end

end

end

end
```

```
function [vWind, wTi] = DCM_ned2wind(vNED, eulerAngles, aoa, ssa)
  % DCM_ned2body - Transform vector in NED frame to body frame
  %
3
  % Syntax: [vWind, wTi] = DCM_ned2wind(vNED, eulerAngles, aoa, ssa)
  %
5
  % INPUTS
  %
                       [3 x n] column vectors in NED frame
      vNED:
7
  %
     eulerAngles:
                       [3 x n] vectors of euler angles [roll, pitch,
     yaw]' (rad)
  %
      aoa:
                       [1 x n] vector of angle of attack (rad)
  %
                       [1 x n] vector of side slip angle (rad)
      ssa:
  % OUTPUTS
  \%
                       [3 x n] column vectors in wind frame
      vWind:
12
  %
      wTi:
                       [3 x 3 x n] inertial to body transformation
13
14
  \% initialize outputs
15
  numVect = size(vNED, 2);
  vWind = zeros(3, numVect);
```

```
wTi = zeros(3, 3, numVect); % initialize inertial to body
     transormation matrix
19
  % unpack Euler Angles
  phi = eulerAngles(1, :); % roll
  theta = eulerAngles(2, :); \% pitch
  psi = eulerAngles(3, :);
                              % yaw
23
24
  \% 3-2-1 NED to body DCM
  Tphi = @(roll) [1, 0, 0; 0, cos(roll), sin(roll); 0, -sin(roll),
26
     cos(roll);
  Ttheta = @(pitch) [cos(pitch), 0, -sin(pitch); 0, 1, 0; sin(pitch)
     0, \cos(\text{pitch});
  Tpsi = @(yaw) [cos(yaw), sin(yaw), 0; -sin(yaw), cos(yaw), 0; 0,
     0, 1];
29
  \% Body to wind rotations
  Taoa = @(alpha) [cos(alpha), 0, -sin(alpha); 0, 1, 0; sin(alpha),
     0, cos(alpha);
  Tssa = @(beta) [cos(beta), sin(beta), 0; -sin(beta), cos(beta), 0;
      0, 0, 1;
  for i = 1:numVect
34
      bTi = Tphi(phi(i)) * Ttheta(theta(i)) * Tpsi(psi(i));
35
      wTb = Tssa(ssa(i)) * Taoa(aoa(i));
36
37
      wTi(:, :, i) = wTb * bTi;
38
```

```
vWind(:, i) = wTi(:, :, i) * vNED(:, i);
end
end
end
end
end
```

```
function [vBody, bTw] = DCM wind2body(vWind, aoa, ssa)
  % DCM_ned2body - Transform vector in NED frame to body frame
  %
3
  % Syntax: [vBody, bTw] = DCM_wind2body(vWind, aoa, ssa)
  %
  % INPUTS
  %
              [3 x n] column vectors in wind frame
7
  \%
              [1 x n] vector of angle of attack (rad)
      aoa:
  %
              [1 x n] vector of side slip angle (rad)
      ssa:
9
  % OUTPUTS
  %
                       [3 x n] column vectors in body frame
      vBody:
  %
      bTw:
                       [3 x 3 x n] wind to body transformation
12
  \% initialize outputs
  numVect = size(vWind, 2);
  vBody = zeros(3, numVect);
                               % initialize inertial to body
  bTw = zeros(3, 3, numVect);
     transormation matrix
18
  % Transforms
```

```
Taoa = @(alpha) [cos(alpha), 0, -sin(alpha); 0, 1, 0; sin(alpha),
     0, cos(alpha);
  Tssa = @(beta) [cos(beta), sin(beta), 0; -sin(beta), cos(beta), 0;
      0, 0, 1;
  for i = 1:numVect
23
      wTb = Tssa(ssa(i)) * Taoa(aoa(i));
24
      bTw(:, :, i) = wTb';
25
      vBody(:, i) = bTw(:, :, i) * vWind(:, i);
26
  end
27
28
29
  end
30
```

```
function [vNED, iTw] = DCM_wind2ned(vWind, eulerAngles, aoa, ssa)
  % DCM_ned2body - Transform vector in NED frame to body frame
  %
  % Syntax: [vNED, iTw] = DCM_wind2ned(vWind, eulerAngles, aoa, ssa)
  %
  % INPUTS
  %
      vwind:
                       [3 x n] column vectors in wind frame
  %
      eulerAngles:
                       [3 x n] vectors of euler angles [roll, pitch,
     yaw]' (rad)
  %
                       [1 x n] vector of angle of attack (rad)
      aoa:
9
  \%
                       [1 x n] vector of side slip angle (rad)
      ssa:
10
  % OUTPUTS
  %
                     [3 x n] column vectors in NED frame
      vNED:
```

```
%
       wTi:
                        [3 \times 3 \times n] inertial to wind transformation
13
14
  \% initialize outputs
  numVect = size(vWind, 2);
  vNED = zeros(3, numVect);
                                 % initialize inertial to body
  iTw = zeros(3, 3, numVect);
18
     transormation matrix
19
  % unpack Euler Angles
  phi = eulerAngles(1, :);
                                % roll
21
  theta = eulerAngles(2, :); \% pitch
22
  psi = eulerAngles(3, :);
23
24
  \% 3-2-1 NED to body DCM
25
  Tphi = \mathbb{Q}(\text{roll}) [1, 0, 0; 0, \cos(\text{roll}), \sin(\text{roll}); 0, -\sin(\text{roll}),
26
     cos(roll);
  Ttheta = @(pitch) [cos(pitch), 0, -sin(pitch); 0, 1, 0; sin(pitch)
      0, \cos(\text{pitch});
  Tpsi = @(yaw) [cos(yaw), sin(yaw), 0; -sin(yaw), cos(yaw), 0; 0,
     0, 1];
  \% Body to wind rotations
  Taoa = @(alpha) [cos(alpha), 0, -sin(alpha); 0, 1, 0; sin(alpha),
     0, cos(alpha);
  Tssa = @(beta) [cos(beta), sin(beta), 0; -sin(beta), cos(beta), 0;
      0, 0, 1;
33
```

```
for i = 1:numVect
    bTi = Tphi(phi(i)) * Ttheta(theta(i)) * Tpsi(psi(i));

wTb = Tssa(ssa(i)) * Taoa(aoa(i));

wTi = wTb * bTi;

iTw(:, :, i) = wTi';

vNED(:, i) = iTw(:, :, i) * vWind(:, i);

end

end

end

end
```

```
function [aoa, ssa] = get_aoa_ssa(vel_uav_body)
 |% get_aoa_ssa - compute angle of attack and side slip angle from
     velocity
  % in body frame
  %
4
  % Syntax: [aoa, ssa] = get_aoa_ssa(vel_uav_body)
  %
 % INPUTS:
      vel_uav_body: [3 x n] velocity vector of UAV in body frame (m/
     s )
  % OUTPUTS:
  %
      aoa:
                   angle of attack (rad)
10
  %
                   side slip angle (rad)
      ssa:
11
12
  u = vel\_uav\_body(1, :); \% body x-velocity
  v = vel\_uav\_body(2, :); \% body y-velocity
```

```
w = vel\_uav\_body(3, :); \% body z-velocity
16
  aoa = atan2(w, u); % angle of attack (rad)
  ssa = real(asin(v / norm([u, w]))); % side slip angle (rad)
18
  if isnan(ssa)
19
       ssa = 0;
  end
22
  if isnan(ssa)
23
       ssa = 0;
24
  end
25
26
  end
```

```
function eulerrates_to_angvel_matrix =
     get_eulerrates_to_angvel_matrix(eulerangles)
2 | %get_eulerrates_to_angvel_matrix - Output matrix to convert
     eulerrates to
 %angular velocities
  %
4
 % Syntax: eulerrates_to_angvel_matrix =
     get_eulerrates_to_angvel_matrix(eulerangles)
6
      phi = eulerangles (1);
7
      theta = eulerangles(2);
8
9
      eulerrates_to_angvel_matrix = [...
10
```

```
1, 0, -\sin(\text{theta});
11
       0, \cos(\mathrm{phi}), \sin(\mathrm{phi})*\cos(\mathrm{theta});
12
       0, -\sin(\phi), \cos(\phi) *\cos(\phi);
14
  end
  function [accelerometer, gyro, gps, altimeter, lidar, source] =
     get_sensor_specs()
  |%get_sensor_specs - outputs specs as a struct for each sensor
  %
  |\%| Syntax: [accelerometer, gyro, gps, altimeter, lidar, source] =
     get_sensor_specs()
5
      g = 9.8; % acceleration due to gravity
6
7
      % Accelerometer
       accelerometer.initBias = 0; % initial accelerometer bias (m/s
          ^{2}) [1e-3 * 80*g]
       accelerometer. bias Stability = 1e-5; % bias stability (drifts
10
          by this much per second) (m/s^2)
       accelerometer.sampleRate = 100; % Hz
11
       accelerometer.noiseDensity = 1e-6 * (150 * g); % accel output
12
          noise density (m/s^2) * Hz^{(-1/2)}
       accelerometer.sigma = (accelerometer.noiseDensity * sqrt(
13
          accelerometer.sampleRate)); % RMS of accelerometer noise (m
          /s^2
14
```

```
% Gyroscope
15
      gyro.initBias = deg2rad(0); % (rad/s) [1]
16
      gyro.biasStability = deg2rad(.0083); % bias stability - 30 deg
         /hr (rad/hr)
      gyro.noiseDensity = deg2rad(0.014); % noise density (rad/s) *
18
         Hz^{(-1/2)}
      gyro.sampleRate = accelerometer.sampleRate;
19
      gyro.sigma = gyro.noiseDensity * sqrt(gyro.sampleRate);
20
      gyro.eulerDrift = deg2rad(20) / 3600; % 20 degrees per hour (
21
         rad/s)
22
      % GPS
23
      gps.sigmaPos = 2.5/3; % position standard deviation (m)
24
      gps.sigmaVel = 0.1/3; % velocity standard deviation (m)
25
      gps.sampleRate = 1; \% (Hz)
26
27
      % altimeter
28
      altimeter.sigma = 0.11; % (m)
29
      altimeter.sampleRate = 50; % (Hz)
30
31
      % lidar
      lidar.sigma = 0.1; \% (m)
      % keep sample rate same as accelerometer. Typical is actually
         270 Hz
      lidar.sampleRate = accelerometer.sampleRate; % (Hz)
35
36
      % source
37
```

```
source.sigma = 0;
source.sampleRate = 10; % frequency at which to take a
measurement
end
```

```
function UAV = initialize_uav()
  % uav_initialization - initialize struct containing UAV parameters
  %
3
  % OUTPUTS:
       UAV - Structure containing physical and aerodynamic paramaters
       unique
       to the UAV.
  %
  %
  \% NOTE: propellers are numbered as follows:
  %
       \begin{bmatrix} 1 & 2 \end{bmatrix}
9
  %
       \begin{bmatrix} 4 & 3 \end{bmatrix}
10
  % mass and moments of inertia
  mass = 0.6; % mass of UAV (kg)
14
  % prop dimensions (meters)
  propLength = 0.1;
16
  propWidth = 0.02;
17
  propArea = propLength*propWidth;
18
19
  % principal moments (kg*m^2) may want to change this to moment of
      inertia
```

```
% of two thin rods crossed
  Ixx = 0.02;
  Iyy = 0.02;
  Izz = 0.05;
  % off-diagonal elements (kg*m^2)
  Ixy = 0;
  Ixz = 0;
  Iyx = 0;
28
  Iyz = 0;
  Izx = 0;
30
  Izy = 0;
31
32
  inertiaMatrix = [Ixx, Ixy, Ixz; Iyx, Iyy, Iyz; Izx, Izy, Izz]; %
     Inertia matrix for aircraft in body frame (kg*m^2)
34
  % body frame moment arms (meters)
  rProp1 = propLength*sind(45)*[1; -1; 0];
  rProp2 = propLength*sind(45)*[1; 1; 0];
37
  rProp3 = propLength*sind(45)*[-1; 1; 0];
  rProp4 = propLength*sind(45)*[-1; -1; 0];
  rProp = [rProp1, rProp2, rProp3, rProp4];
  % aerodynamic coefficients
  CD = 0.1; % drag coefficient
  CT = 0.7; % thrust coefficient
44
45
  % maximum allowable bank and pitch for UAV
```

```
maxRotationUAV = deg2rad(5); % radians

UAV = struct('mass', mass, 'inertiaMatrix', inertiaMatrix, ...

'propArea', propArea, 'propVects', rProp, 'CT', CT, 'CD', CD,

...

'maxRotation', maxRotationUAV);
```

```
function [d_iTb_d_phi, d_iTb_d_theta, d_iTb_d_psi] =
      jacobian_DCM_body2ned(euler_angles)
  |%jacobian_DCM_body2ned - Outputs the Jacobian of the body to
      inertial DCM
  %
3
  \% Syntax: [d_iTb_d_phi, d_iTb_d_theta, d_iTb_d_psi] =
      jacobian_DCM_body2ned(euler_angles)
5
       % euler angles
       phi = euler_angles(1);
7
       theta = euler\_angles(2);
       psi = euler_angles(3);
10
       % jacobian terms
11
       d_iTb_d_phi = [...
12
            0, \cos(psi)*\sin(theta)*\cos(phi) + \sin(phi)*\sin(psi), \cos(phi)
13
               phi)*sin(psi) - sin(phi)*cos(psi)*sin(theta);...
            0, -\sin(phi)*\cos(psi) + \sin(theta)*\cos(phi)*\sin(psi), -(
14
               \sin(\text{phi})*\sin(\text{theta})*\sin(\text{psi}) + \cos(\text{psi})*\cos(\text{phi});...
            0, \cos(\text{theta})*\cos(\text{phi}), -\cos(\text{theta})*\sin(\text{phi});...
15
```

```
];
16
         d_iTb_d_theta = [...
^{17}
               -\sin(\text{theta})*\cos(\text{psi}), \cos(\text{psi})*\cos(\text{theta})*\sin(\text{phi}), \cos(\text{psi})
                    phi)*cos(psi)*cos(theta);...
               -\sin(\text{theta})*\sin(\text{psi}), \cos(\text{theta})*\sin(\text{phi})*\sin(\text{psi}), \cos(\text{theta})
19
                    phi)*cos(theta)*sin(psi);...
               -\cos(\text{theta}), -\sin(\text{theta})*\sin(\text{phi}), -\sin(\text{theta})*\cos(\text{phi})
20
                    ; . . .
               ];
21
         d_iTb_d_psi = [...
22
               -\cos(\text{theta})*\sin(\text{psi}), -(\sin(\text{psi})*\sin(\text{theta})*\sin(\text{phi}) + \cos(\text{psi})
23
                    (phi)*cos(psi)), sin(phi)*cos(psi) - cos(phi)*sin(psi)*
                    sin (theta);...
               \cos(\text{theta})*\cos(\text{psi}), -\cos(\text{phi})*\sin(\text{psi}) + \sin(\text{theta})*\sin(
24
                    phi)*cos(psi), cos(phi)*sin(theta)*cos(psi) + sin(psi)*
                    sin (phi);...
               [0, 0, 0];
25
26
   end
```

```
function [d_bTi_d_phi, d_bTi_d_theta, d_bTi_d_psi] =
    jacobian_DCM_ned2body(euler_angles)

%jacobian_DCM_ned2body - Outputs the Jacobian of the inertial to
    body DCM

% Syntax: [d_bTi_d_phi, d_bTi_d_theta, d_bTi_d_psi] =
    jacobian_DCM_ned2body(euler_angles)
```

```
5
      % jacobian terms
6
      [d_iTb_d_phi, d_iTb_d_theta, d_iTb_d_psi] =
         jacobian_DCM_body2ned(euler_angles);
8
      % outputs are the transpose of the iTb terms
      d_bTi_d_phi = d_iTb_d_phi;
10
      d_bTi_d_theta = d_iTb_d_theta';
11
      d_bTi_d_psi = d_iTb_d_psi;
12
13
  end
14
```

```
function [d angvel T eulerrates dphi, d angvel T eulerrates dtheta
     , d_angvel_T_eulerrates_dpsi] =
    jacobian_eulerrates_to_angvel_matrix(eulerangles)
 |%jacobian_eulerrates_to_angvel_matrix - Jacobian of Euler rates to
     angular
 %velocity matrix
 %
4
 % Syntax: [d_angvel_T_eulerrates_dphi,
    d_angvel_T_eulerrates_dtheta, d_angvel_T_eulerrates_dpsi] =
    jacobian_eulerrates_to_angvel_matrix(eulerangles)
 %
 % Long description
7
 % unpack eulerangles
 | phi = eulerangles(1);
```

```
theta = eulerangles(2);
12
  \% partial derivative of eulerrates matrix with respect to phi
   d_angvel_T_eulerrates_dphi = [...
14
       0, 0, 0;
15
       0, -\sin(\mathrm{phi}), \cos(\mathrm{phi})*\cos(\mathrm{theta});
16
       0, -\cos(\mathrm{phi}), -\sin(\mathrm{phi})*\cos(\mathrm{theta});
17
18
  \% partial derivative of eulerrates matrix with respect to theta
19
   d_angvel_T_eulerrates_dtheta = [...]
20
       0, 0, -\cos(\text{theta});
21
       0, 0, -\sin(\mathrm{phi})*\sin(\mathrm{theta});
22
       0, 0, -\cos(\text{phi})*\sin(\text{theta});
23
24
  \% partial derivative of eulerrates matrix with respect to psi
25
   d_angvel_T_eulerrates_dpsi = zeros(3);
27
   end
28
   function posNED = lla_to_ned(originLLA, posLLA)
  |% lla_to_ned - converts geodetic coordings (latitude, longitude,
      altitude)
```

```
%
      originLLA: [1 x N] Reference coordinates and altitude. Where
     local NED
  %
          frame is at its origin
  %
      posLLA: [3 x N] position in geodetic coordinates [lat; long;
     altitude]
  %
11
  % OUTPUTS
      posNED: [3 x N] position in NED coordinates
  \%
13
14
  if size (posLLA, 1) \sim = 3
15
      error ('All inputs must have dimensions [3 x N]. posLLA has
16
         dimensions %d', posLLA);
  end
17
18
  rEarth = 1e3 * 6371; \% radius of Earth (m)
19
20
  northPos = (posLLA(1, :) - originLLA(1)) .* pi/180 .* rEarth;
  22
  downPos = -posLLA(3, :);
  posNED = [northPos; eastPos; downPos];
  end
  function v = random vector (magnitude)
1
     %random_vector - outputs a random vector with a constant
2
         magnitude
```

3

```
v = randn(3, 1);
v_normalized = v ./ norm(v);
v = magnitude .* v_normalized;
end
```

```
function [all_final_source_distance_meters,
     all_first_iteration_percent_dist_covered,
     all_num_iterations_within_1m, convergence_array,
     all_first_iteration_time = score_saved_runs(path_to_runs)
 |%score_saved_runs - score runs
  %
3
  % Syntax: [all_final_source_distance_meters, [
     all_first_iteration_percent_dist_covered,
     all_num_iterations_within_1m = score_saved_runs(path_to_runs)
  %
5
      if nargin < 1
7
          path_to_runs = '.';
      end
      filenames = dir(fullfile(path_to_runs, '*.mat'));
10
      filenames = {filenames.name};
11
12
      all_final_source_distance_meters = zeros(1, length(filenames))
13
      all_first_iteration_percent_dist_covered = zeros(1, length(
14
         filenames));
```

```
all_first_iteration_dist_covered = zeros(1, length(filenames))
15
      all_num_iterations_within_1m = zeros(1, length(filenames));
      all_first_iteration_time = zeros(1, length(filenames));
17
18
      for i = 1:length (filenames)
19
          run_name = filenames{i};
20
           run_output = load (fullfile (path_to_runs, run_name));
21
           first estimate distance covered,
22
              first_iteration_percent_dist_covered,
              final_source_distance, num_iterations_within_1m,
              init_distance, first_iteration_time] =
              score_source_pos_estimation(run_output.yout);
           all_first_iteration_percent_dist_covered(i) =
23
              first_iteration_percent_dist_covered;
           all_final_source_distance_meters(i) =
24
              final_source_distance;
           all_num_iterations_within_1m(i) = num_iterations_within_1m
           all_first_iteration_dist_covered(i) =
              first_estimate_distance_covered;
           all_first_iteration_time(i) = first_iteration_time;
      end
28
29
      % scoring plots
30
        % final source distance
32
```

```
%
         figure (1)
33
  %
         edges = [0:50: ceil (max(all_final_source_distance_meters)
34
     .*100)+50;
  %
         histogram (all_final_source_distance_meters.*100, edges, '
     FaceAlpha', 1);
         xlabel ('Source Distance (cm)')
  %
         ylabel ('Runs');
37
  %
        %xticks(-1000:10:ceil(max(all_final_source_distance_meters)
38
     .*100 + 1000);
  %
         title ('Final source distance')
39
  %
40
  %
        % first iteration percent distance
41
  %
         figure (2)
42
         minBin = floor(min(all_first_iteration_percent_dist_covered)
43
     ) - rem(floor(min(all_first_iteration_percent_dist_covered)),
     10) - 10;
  %
         maxBin = floor(max(all first iteration percent dist covered)
44
     ) - rem(floor(max(all_first_iteration_percent_dist_covered)),
     10) + 10;
  %
         edges = [minBin:5:maxBin];
45
  %
         histogram (all_first_iteration_percent_dist_covered, edges, '
46
     FaceAlpha', 1)
  %
         xlabel('% closer');
  %
         ylabel ('Runs')
48
  \%
         title ('First source distance reduction')
49
  %
         xticks ([minBin:10:maxBin]);
50
  %
51
```

```
%
        % number of iterations until within 1m
  \%
         figure (3)
53
      unique_iteration_counts = unique(all_num_iterations_within_1m)
          ;
       total_iteration_counts = zeros(1, length(
          unique_iteration_counts));
  \%
         for i = 1:length(total_iteration_counts)
56
  \%
             iterationNum = unique_iteration_counts(i);
57
  %
             total iteration counts(i) = sum(
58
     all_num_iterations_within_1m == iterationNum);
  %
         end
59
         bar(unique_iteration_counts, total_iteration_counts);
  %
60
  %
         xlabel('Number of iterations until <= 1m');</pre>
61
  %
         ylabel ('Number of runs')
62
  \%
         title ('Iterations for distance <= 1m')
63
64
      % converges, will converge, does not converge within 1m
65
      num_runConverges = length(all_final_source_distance_meters(
66
         all_final_source_distance_meters < 1.0));
      num_willConverge = length(all_final_source_distance_meters(
67
         all_final_source_distance_meters < 9 &
         all_final_source_distance_meters > 1.0));
      num willNotConverge = 100 - num runConverges -
         num willConverge;
69
      convergence_array = [init_distance, num_runConverges,
70
         num_willConverge , num_willNotConverge ];
```

```
71
       categories = categorical({ 'Converges', 'Will Converge', 'Does
72
          not converge'; });
  %
         figure (4)
  %
         bar(categories, [num_runConverges, num_willConverge,
75
     num_willNotConverge]);
  %
         title ('Convergence within Sim Time')
76
  %
         ylabel ('Runs')
77
78
      % first iteration time
79
  %
         figure (5);
80
  %
         edges = 0:1: ceil (max(all_first_iteration_time));
81
         histogram(all_first_iteration_time, edges, 'FaceAlpha', 1);
  %
82
  %
         xlabel ('Time (sec)')
83
  %
         ylabel ('Runs');
84
  %
         title ('Time for activity threshold to be exceeded.');
85
86
  end
  function [first_estimate_distance_covered,
     first_iteration_percent_dist_covered, final_source_distance,
     num_iterations_within_1m, init_distance, first_iteration_time]
     = score_source_pos_estimation(yout)
91
      x = yout.x;
92
```

```
% unpack state
93
       [pos_ned, ~, ~, ~, ~, ~] = unpack_state_vector(x);
       uav_init_pos = pos_ned(:, 1);
       true source pos = yout.true source pos;
98
       source_pos_estimates = yout.source.position_estimate;
99
       estimation_start_times = yout.source.estimation_start_times;
100
101
       init_distance = norm(true_source_pos - uav_init_pos);
102
103
      \% -----get percent distance closed on first iteration
104
      % distance from first estimated position
105
       first_estimate_distance_covered = init_distance - norm(
106
          true_source_pos - source_pos_estimates(2:4, 1));
107
      % percent distance closed on first iteration
108
       first_iteration_percent_dist_covered = ((
109
          first_estimate_distance_covered / init_distance)) * 100;
       %~~~~~~~~ get distance from source at end of sim
111
       final_source_distance = norm(true_source_pos -
112
          source_pos_estimates(2:4, end));
113
```

```
~~~~~~ first iteration time
114
       first_iteration_time = estimation_start_times(1);
115
116
       %----- get number of iterations required to get
117
          within 1m of source ~~~~
       source_pos_error = zeros(3, size(source_pos_estimates, 2));
118
       source_dist_error = zeros(1, size(source_pos_estimates, 2));
119
       for i = 1: size (source pos estimates, 2)
120
           source_pos_error(:, i) = true_source_pos -
121
              source_pos_estimates(2:4, i);
           source_dist_error(i) = norm(source_pos_error(:, i));
122
       end
123
       num_iterations_within_1m = find(source_dist_error <= 1, 1);
124
       if isempty (num_iterations_within_1m)
125
           num\_iterations\_within\_1m = NaN;
126
       end
127
128
   end
129
```

```
function B = skew(A)
% Converts a vector into 3x3 skew-symmetric form.
%
% Syntax: B = skew(A)

if any(size(A) > 3)
error('A must be a 3x1 or 1x3 vector');
```

```
end
9
   if isnumeric (A)
10
        B = zeros(3,3);
11
   end
_{14} | B(1,2) = -A(3);
_{15} | B(1,3) = A(2);
_{16} | B(2,1) = A(3);
_{17} | B(2,3) = -A(1);
_{18} | B(3,1) = -A(2);
_{19} | B(3,2) = A(1);
20
   end
^{21}
```

```
function counts_1sec = store_1sec_counts(zout, time)
  %store_1sec_counts - Store last second of counts
  %
3
4 % Syntax: counts_1sec_new = store_1sec_counts(counts_1sec_old,
     counts)
  %
5
6
      [~, ~, ~, ~, ~, source_specs] = get_sensor_specs();
7
      counts_all = zout.source.counts;
8
      counts_time = zout.source.t;
9
10
```

```
% if we would be between measurements, round time to nearest
11
         tenths place to
      % construct counts_1sec
12
      if (mod(time, round(1/source_specs.sampleRate, 6)) ~= 0)
13
           time_tenths_place = get_digits_after_decimal(time, 1);
14
           time = floor(time) + time_tenths_place/10;
15
      end
16
      time = round(time, 6);
17
18
       if (mod(time, round(1/source\_specs.sampleRate, 6)) == 0) && (
19
         time >= round(1/source_specs.sampleRate, 6))
          % get one seconds worth of counts to determine if gradient
20
               detection
          % should start
21
           counts_ind = find (counts_time == time);
22
                            \% if time > 1.0, should have enough
           if time >= 1.0
23
              measurements
               time_1sec_earlier = round(time - 0.9, 6);
               counts_ind_1_sec_earlier = find (counts_time ==
                  time_1sec_earlier);
           else \% time -1 sec would be negative.
               counts\_ind\_1\_sec\_earlier = 1;
           end
28
           counts_1sec = counts_all(counts_ind_1_sec_earlier:
29
              counts_ind);
30
```

```
% Pad zeros to end of counts_1sec if length is less than
31
              10. This should
          % only happen when time <= 1.0 sec
           if time \leq 1.0
               counts_1sec = [counts_1sec, zeros(1, source_specs.
34
                  sampleRate - length(counts_1sec));
           elseif length (counts_1sec) ~= 10
35
               error ('Counts_1sec has length less than 10 after one
36
                  sec: Length = \%d, Time = \%d', length (counts_1sec),
                  time);
           end
37
       elseif time < round(1/source_specs.sampleRate, 6)
38
           counts_1sec = zeros(1, source_specs.sampleRate);
39
       else
40
           error ('Unable to create 1 sec worth of counts. Time = %d',
41
               time);
      end
42
43
  end
44
  function [pos_ned, vel_ned, accel_ned, eulerangles, obstacle_ned,
     source_ned | = unpack_state_vector(x)
  |%unpack_state_vector - Outputs state vector elements
  %
3
  |% Syntax: [pos_ned, vel_ned, accel_ned, eulerangles, obstacle_ned,
      source_ned | = unpack_state_vector(x)
5 %
```

```
\% Output state vector elements for use in other functions.
  %
7
  % INPUT
      x [18 x N] - state vector or array of state vectors.
  %
10
      % ensure x is a column vector or an array of column vectors
11
       if \operatorname{size}(x, 1) \sim 18
12
           error ('State vector "x" must contain 18 elements and must
13
              be given as a column vector or an array of column
              vectors.');
       end
14
15
       pos\_ned = x(1:3, :);
16
       vel_ned = x(4:6, :);
17
       accel\_ned = x(7:9, :);
18
       eulerangles = x(10:12, :);
19
       obstacle ned = x(13:15, :);
20
       source_ned = x(16:18, :);
21
  end
```

```
function [time_reached, command_duration] =
   time_until_waypoint_reached(yout)

%time_until_waypoint_reached - determine time until waypoint is
   reached

% Syntax: waypoints_reached = time_until_waypoint_reached(yout)

% Waypoints_reached = time_until_waypoint_reached(yout)
```

```
% Long description
      x = yout.x;
7
      pos = x(1:3, :);
      vel = x(4:6, :);
      t = yout.t;
10
      waypoints = yout.controls.waypoints;
11
12
      % threshold
13
       dist thresh = 0.1;
14
      vel_mag_thresh = 0.05;
15
16
      time_reached = zeros(1, size(waypoints, 2));
17
      command_duration = zeros(1, size(waypoints, 2));
18
       for i = 1:length (waypoints)
19
           target_pos = waypoints(2:4, i);
20
           target_vel = [0, 0, 0];
^{21}
           pos_error = target_pos - pos;
           vel_error = target_vel - vel;
23
           dist_error = zeros(1, length(pos_error));
           vel_mag_error = zeros(1, length(vel_error));
           for j = 1:length(pos_error)
               dist\_error(j) = norm(pos\_error(:, j));
               vel_mag_error(j) = norm(vel_error(:, j));
28
           end
           ind = find(dist_error < dist_thresh & vel_mag_error <
30
              vel_mag_thresh, 1);
           time\_reached(i) = t(ind);
31
```

```
command_duration(i) = t(ind) - waypoints(1, i);

end

end

end
```

```
1
  A1 = @(r1) 1000/(r1^2);
  law\_cosines = @(a, b, theta\_c) a^2+b^2 - 2*a*b*cos(theta\_c);
4
  dist_array = 1:1:50;
5
  prob_wrongDir_best_all = zeros(1, length(dist_array));
  prob_wrongDir_worst_all = zeros(1, length(dist_array));
  prob_wrongDir_mid_all = zeros(1, length(dist_array));
9
  count = 0;
10
  prob\_wrongDir\_best = 0;
  for dist = dist array
12
       dist
13
      A\_closeMean\_best = A1(dist -1);
      A_farMean_best = A1(dist+1);
16
       dist_worst = sqrt(law_cosines(dist, 1, 90));
17
      A\_closeMean\_worst = A1(dist\_worst);
18
19
       dist mid close = sqrt(law cosines(dist, 1, 45));
20
      dist_mid_far = sqrt(law_cosines(dist, -1, 45));
21
22
      A_closeMean_mid = A1(dist_mid_close);
23
```

```
A_farMean_mid = A1(dist_mid_far);
25
      prob wrong Dir best = 0;
      prob\_wrongDir\_worst = 0;
      prob\_wrongDir\_mid = 0;
29
      for i = 0.500
30
31
           prob_Aclose_best = pdf('Poisson', i, A_closeMean_best);
32
           prob_Afar_greater_Aclose_best = 1-cdf('Poisson', i,
33
             A_farMean_best);
           prob_wrongDir_best = prob_wrongDir_best + prob_Aclose_best
34
              *(prob_Afar_greater_Aclose_best);
35
           prob_Aclose_worst = pdf('Poisson', i, A_closeMean_worst);
36
           prob_Afar_greater_Aclose_worst = 1-cdf('Poisson', i,
37
              A closeMean worst);
           prob_wrongDir_worst = prob_wrongDir_worst +
              prob_Aclose_worst*prob_Afar_greater_Aclose_worst;
           prob_Aclose_mid = pdf('Poisson', i, A_closeMean_mid);
           prob_Afar_greater_Aclose_mid = 1-cdf('Poisson', i,
             A_farMean_mid);
           prob_wrongDir_mid = prob_wrongDir_mid + prob_Aclose_mid*(
              prob_Afar_greater_Aclose_mid);
43
44
      end
```

```
count = count + 1;
45
      prob_wrongDir_best_all(count) = prob_wrongDir_best;
46
      prob_wrongDir_worst_all(count) = prob_wrongDir_worst;
47
      prob_wrongDir_mid_all(count) = prob_wrongDir_mid;
48
  end
51
  % plot(dist_array, prob_wrongDir_best_all, dist_array,
     prob wrongDir worst all, dist array, prob wrongDir mid all);
  \% legend('\theta_0 = 0 \circ', '\theta_0 = 90 \circ', '\theta_0 =
     45 \circ');
  % xlabel('Distance (m)');
  % ylabel('Probability');
  % title ('Probability of Incorrect Source Direction');
57
  plot(dist_array, prob_wrongDir_best_all, dist_array,
     prob_wrongDir_worst_all);
  legend('\theta_0 = 0 \circ', '\theta_0 = 90 \circ');
  xlabel('Distance (m)');
  ylabel('Probability');
  title ('Probability of Incorrect Source Direction');
```

APPENDIX E

RADIOACTIVE SOURCE LOCALIZATION

```
function detection_flag = check_near_source_counts(counts,
     A_thresh, A_background)
 |%check_near_source_video - Check if near a source to trigger
     gradient test
  %
3
  % Syntax: detection_flag = check_near_source_video(counts,
     A_thresh)
  %
  % INPUTS
      counts [N x 1, 1 x N]: array of counts
  %
7
  %
      A thresh: value that must be exceeded by sum of all elements
      in
  %
                           array "counts"
9
  % OUTPUTS
  %
      detection_flag: flag raised if sum(counts) exceeds threshold.
11
12
      % A_thresh is number of counts required to trigger a gradient
      % measurement
14
      if nargin < 2
          error('Activity threshold unset')
16
      end
17
18
      if sum(counts) - A_background >= A_thresh
19
          detection_flag = 1;
20
```

```
function at target flag = check uav at target(x, r measurement ned
     )
      % check if we are at the waypoint
2
      deadzone = 0.1;
3
      % unpack inputs
4
      r_uav_ned = [x(1), x(2), x(3)]';
5
      v_uav_body = [x(4), x(5), x(6)];
6
      if ~any(abs(r_uav_ned - r_measurement_ned) > deadzone) && ~any
7
          (abs(v_uav_body - [0; 0; 0]) > deadzone)
           at\_target\_flag = 1;
      else
9
           at\_target\_flag = 0;
      end
  end
12
```

```
function source_pos_ned = estimate_source_pos(counts_gradient,
    r_gradient_center_ned, measurement_positions_ned, duration, A0,
    A_background, r0, A_thresh, true_source_ned)

%estimate_source_pos - Estimate source position in NED

% Syntax: source_pos_ned = estimate_source_pos(x,
    counts_gradient, r_gradient_center_ned)
```

```
%
5
      % Long description
6
      % error checking
8
       if length (counts_gradient) ~= duration * 10
           error ('counts_gradient should have a size of duration * 10
10
              <sup>,</sup> );
       end
11
12
      % A_thresh sets maximum distance
13
       dist_max = r0 * sqrt((A0 + sqrt(A0)) / abs(A_thresh));
14
15
       std\_A0 = sqrt(A0);
16
17
       source\_dist = [];
18
       vec\_row\_count = 0;
19
20
       for i = 1:2:6
21
           vec_row_count = vec_row_count + 1;
           counts_plus = counts_gradient(i, :);
           pos_plus_ned = measurement_positions_ned(:, i);
           counts_minus = counts_gradient(i + 1, :);
           pos\_minus\_ned = measurement\_positions\_ned(:, i + 1);
26
27
           delta_pos = pos_plus_ned - pos_minus_ned;
28
           unit_delta_pos = delta_pos ./ norm(delta_pos); % unit
29
              vector
```

```
% get average counts per second
           avg_counts_plus = mean(counts_plus) * 10 - A_background;
           avg\_counts\_minus = mean(counts\_minus) * 10 - A\_background;
           delta_counts = avg_counts_plus - avg_counts_minus;
35
          % get source distance along axis
36
           source_dist_plus = (r0 * sqrt(A0 / avg_counts_plus));
37
           source_dist_minus = (r0 * sqrt(A0 / avg_counts_minus));
38
           source_dist_array = [source_dist_plus, source_dist_minus];
39
           source_dist_diff = abs(norm(source_dist_plus) - norm(
40
             source_dist_minus));
41
           source_dist_axis = sign(delta_counts) * source_dist_diff /
42
               2 .* unit delta pos;
43
           avg_counts_array = [avg_counts_plus, avg_counts_minus];
           [max_counts, max_counts_ind] = max(avg_counts_array);
           if abs(delta_counts) > sqrt(min([avg_counts_plus,
              avg_counts_minus])) || (avg_counts_plus > A0 - std_A0
             && avg\_counts\_minus > A0 - std\_A0)
48
               if source_dist_diff > 0.9
49
                   source_dist_axis = sign(delta_counts) * (
50
                      source_dist_array(max_counts_ind)) .*
                      unit_delta_pos;
```

```
elseif source_dist_diff > 0.5
                    source\_dist\_axis = sign(delta\_counts) * abs(
                       source_dist_array(max_counts_ind) - 1) .*
                       unit_delta_pos;
                else
                    source_dist_axis = sign(delta_counts) *
54
                       source_dist_diff / 2 .* unit_delta_pos;
                end
55
56
           end
57
           % if one measurement is much greater than A0, just use
59
              that
           % position
           if \max_{\text{counts}} + \text{sqrt}(A0) > A0
               % if source_dist_diff is less than 1, use
62
                   source_dist_diff for
               % distance estimation
                if source_dist_diff >= 1.5
                    if \max_{\text{counts}_{\text{ind}}} = 1
                         source_dist_axis = (pos_plus_ned -
                            r_gradient_center_ned) .* unit_delta_pos;
                    else
                         source_dist_axis = (pos_minus_ned -
69
                            r_gradient_center_ned) .* unit_delta_pos;
                    end
70
```

```
end
           end
74
75
          %source_dist_axis = r0 * sign(delta_counts) * sqrt(A0 ./
76
              abs(delta_counts)) .* unit_delta_pos;
77
          % check if our values are usable.
78
          % standard deviation of counts is given by sqrt(counts).
79
          % if delta_counts < max(standard_deviation), do not use
80
           delta_counts_thresh = max([sqrt(avg_counts_plus), sqrt(
81
              avg_counts_minus)|);
82
          % source_dist_plus - source_dist_minus should equal 2. Set
83
               thresholds
           source_dist_diff_error = 0.5;
           source_dist_diff_flag = (source_dist_diff > 1 -
              source_dist_diff_error) && (source_dist_diff < 1 +
              source_dist_diff_error + 1);
           source_dist_diff_flag = 1;
           if any(abs(source_dist_axis) > dist_max) ||~
88
              source_dist_diff_flag || any(isnan(source_dist_axis))
               source\_dist\_axis = [0, 0, 0];
           end
91
```

```
source_dist = [source_dist, source_dist_axis];
92
93
       end
       source_pos_ned = sum(source_dist, 2) + r_gradient_center_ned;
       source_pos_error = true_source_ned - source_pos_ned;
       % source is not underground
       if source_pos_ned(3) > 0
99
           source pos ned(3) = 0;
100
       end
101
102
   end
103
```

```
function [measurement_positions_ned, gradient_center_ned] =
     get_gradient_waypoints(x)
 |%get_waypoint_gradient - output UAV waypoint from measurement
     number and state
  %
3
4 % Syntax: measure_gradient_waypoint = get_waypoint_gradient(x, t,
     measurement_num)
  %
  % Long description
7
      region radius = 1;
8
9
      r_uav_ned = [x(1), x(2), x(3)]';
10
11
```

```
gradient_center_ned = r_uav_ned;
12
      measurement_positions_ned(:, 1) = gradient_center_ned + [
13
         region_radius; 0; 0];
      measurement_positions_ned(:, 2) = gradient_center_ned - [
14
         region_radius; 0; 0];
      measurement_positions_ned(:, 3) = gradient_center_ned + [0;
15
         region_radius; 0];
      measurement_positions_ned(:, 4) = gradient_center_ned - [0;
16
         region_radius; 0];
      measurement_positions_ned(:, 5) = gradient_center_ned + [0; 0;
17
          region_radius];
      measurement_positions_ned(:, 6) = gradient_center_ned - [0; 0;
18
          region_radius];
19
       if measurement_positions_ned (3, 5) > -0.1
20
           difference = gradient\_center\_ned(3) - (-0.1);
21
           measurement_positions_ned(3, 5) = -0.1;
           measurement\_positions\_ned(3, 6) = gradient\_center\_ned(3) +
23
               difference;
      end
  end
```

```
function [measuring_gradient_flag , at_target_flag ,
   gradient_center_ned , target_pos_ned] =
   radiation_source_gradient (...
```

```
x, time, at_target_flag, gradient_center_ned,
2
                 measurement_num, measurement_positions)
      measuring_gradient_flag = 1;
3
          if at_target_flag == 0
               [measurement_positions, gradient_center_ned,
                  at target flag, measurement num =
                  get_waypoint_gradient(x, gradient_center_ned,
                 measurement_num, measurement_positions);
          end
6
          target_pos_ned = measurement_positions(:, measurement_num)
             ;
          %UPDATE WAYPOINTS OUTSIDE OF FUNCTION
          % if t_stop_meas is empty and we are at our target, set
9
             t_stop_meas
          if isempty (t stop meas)
10
               if at_target_flag == 1
11
                   t stop meas = time + 30;
12
                   t_stop_meas = round(t_stop_meas, 6);
13
               end
14
           else
              % if we are at the target and t < t_stop_meas, record
                 counts
               if time <= round(t stop meas, 6) && at target flag ==
                 1
                   gradient_counts = [gradient_counts, counts_dt];
18
               elseif time > t stop meas % if t > t stop meas, save
19
                 our recorded counts and increase measurement_num
```

```
t_stop_meas = [];
                   gradient_store_counts(measurement_num, :) =
                      gradient_counts;
                   gradient_counts = [];
                   measurement\_num = measurement\_num + 1;
                   at\_target\_flag = 0;
24
               end
25
           end
26
          \% if measurement_num = 7, we are done saving measurements
27
              . Estimate
          % source position from gradient_store_counts
           if measurement num == 7
29
               measuring_gradient_flag = 0;
30
               source_pos_ned = estimate_source_pos(
31
                  gradient_store_counts, gradient_center_ned,
                  measurement_positions, meas_duration, A0, r0,
                  A thresh);
               source_pos_ned_store = [source_pos_ned_store, [time;
32
                  source_pos_ned]];
               do_not_measure_deadtime = time + 30; % do perform
                  another gradient measurement for 30 sec
               measurement_positions = [];
               measurement\_num = 0;
35
               at\_target\_flag = 0;
36
               t_stop_meas = [];
37
               target_pos_ned = source_pos_ned;
38
               waypoints = [waypoints, [time; target_pos_ned]];
39
```

end end end

BIOGRAPHY OF THE AUTHOR

John George Goulet was born in Lewiston, Maine on April 21, 1994. He was raised there and graduated from Lewiston High School in 2012. He attended the University of Maine and graduated in 2017 with a Bachelor's degree in Engineering Physics. John George Goulet is a candidate for the Master of Engineering degree in Engineering Physics from the University of Maine in May 2020.