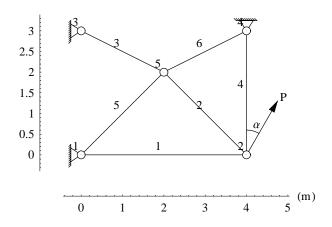
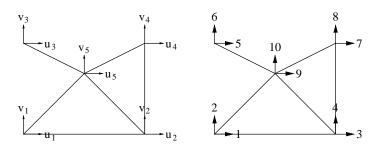
CHAPTER FOUR

Trusses, Beams, and Frames

Example 4.1: Six-bar truss (p. 226)

All members have the same cross-sectional area and are of the same material, $E=200\,\mathrm{GPa}$ and $A=0.001\,m^2$. The load $P=20\,\mathrm{kN}$ and acts at an angle $\theta=30\,^\circ$. The dimensions in meters are shown in the figure.





For numerical calculations the N-mm units are convenient. The displacements will be in mm and the stresses in MPa. The complete computations are as follows.

Specified nodal loads

Node	dof	Value
9	$\mathbf{u_2}$	10000.
2	V ₂	17320.5

Global equations at start of the element assembly process

$$E = 200000$$
 $A = 1000$.

Substituting into the truss element equations we get

$$\begin{pmatrix} 50000. & 0. & -50000. & 0. \\ 0. & 0. & 0. & 0. \\ -50000. & 0. & 50000. & 0. \\ 0. & 0. & 0. & 0. \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {1, 2, 3, 4} global degrees of freedom.

Locations for element contributions to a global vector: $\begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix}$

$$\text{and to a global matrix:} \left\{ \begin{bmatrix} [1,\ 1] & [1,\ 2] & [1,\ 3] & [1,\ 4] \\ [2,\ 1] & [2,\ 2] & [2,\ 3] & [2,\ 4] \\ [3,\ 1] & [3,\ 2] & [3,\ 3] & [3,\ 4] \\ [4,\ 1] & [4,\ 2] & [4,\ 3] & [4,\ 4] \\ \end{bmatrix} \right.$$

$$E = 200000$$
 $A = 1000$.

Substituting into the truss element equations we get

$$\begin{pmatrix} 35355.3 & -35355.3 & -35355.3 & 35355.3 \\ -35355.3 & 35355.3 & 35355.3 & -35355.3 \\ -35355.3 & 35355.3 & 35355.3 & -35355.3 \\ 35355.3 & -35355.3 & -35355.3 & 35355.3 \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ u_5 \\ v_5 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {3, 4, 9, 10} global degrees of freedom.

Locations for element contributions to a global vector: $\begin{bmatrix} 3\\4\\9\\10 \end{bmatrix}$

and to a global matrix:
$$\begin{bmatrix} [3,\,3] & [3,\,4] & [3,\,9] & [3,\,10] \\ [4,\,3] & [4,\,4] & [4,\,9] & [4,\,10] \\ [9,\,3] & [9,\,4] & [9,\,9] & [9,\,10] \\ [10,\,3] & [10,\,4] & [10,\,9] & [10,\,10] \end{bmatrix}$$

$$E = 200000$$
 $A = 1000$.

Element node Global node number
$$x$$
 y
$$1 5 2000. 2000.$$

$$2 3 0 3000.$$

$$x_1 = 2000. y_1 = 2000. x_2 = 0 y_2 = 3000.$$

$$L = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = 2236.07$$
 Direction cosines: $\ell_s = \frac{x_2 - x_1}{L} = -0.894427$
$$m_s = \frac{y_2 - y_1}{L} = 0.447214$$

Substituting into the truss element equations we get

$$\begin{pmatrix} 71554.2 & -35777.1 & -71554.2 & 35777.1 \\ -35777.1 & 17888.5 & 35777.1 & -17888.5 \\ -71554.2 & 35777.1 & 71554.2 & -35777.1 \\ 35777.1 & -17888.5 & -35777.1 & 17888.5 \end{pmatrix} \begin{pmatrix} u_5 \\ v_5 \\ u_3 \\ v_3 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {9, 10, 5, 6} global degrees of freedom.

Locations for element contributions to a global vector:
$$\begin{bmatrix} 9\\10\\5\\6 \end{bmatrix}$$

$$E = 200000$$
 $A = 1000$.

Substituting into the truss element equations we get

$$\begin{pmatrix} 0. & 0. & 0. & 0. \\ 0. & 66666.7 & 0. & -66666.7 \\ 0. & 0. & 0. & 0. \\ 0. & -66666.7 & 0. & 66666.7 \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {3, 4, 7, 8} global degrees of freedom.

Locations for element contributions to a global vector: $\begin{bmatrix} 3 \\ 4 \\ 7 \\ 8 \end{bmatrix}$

and to a global matrix:
$$\begin{bmatrix} [3,\ 3] & [3,\ 4] & [3,\ 7] & [3,\ 8] & [4,\ 4] & [4,\ 7] & [4,\ 8] & [7,\ 3] & [7,\ 4] & [7,\ 7] & [7,\ 8] & [8,\ 3] & [8,\ 4] & [8,\ 7] & [8,\ 8] & [8,\ 8] & [8,\ 7] & [8,\ 8]$$

$$\begin{pmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \\ u_5 \\ v_5 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 10000. \\ 17320.5 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

$$\begin{split} E &= 200000 \qquad A = 1000. \\ Element node \qquad Global node number \qquad x \qquad y \\ 1 \qquad \qquad 1 \qquad \qquad 0 \qquad 0 \\ 2 \qquad \qquad 5 \qquad \qquad 2000. \qquad 2000. \\ x_1 &= 0 \qquad y_1 &= 0 \qquad x_2 &= 2000. \qquad y_2 &= 2000. \\ L &= \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} &= 2828.43 \\ Direction cosines: \ell_s &= \frac{x_2 - x_1}{L} &= 0.707107 \qquad m_s &= \frac{y_2 - y_1}{L} &= 0.707107 \end{split}$$

Substituting into the truss element equations we get

$$\begin{pmatrix} 35355.3 & 35355.3 & -35355.3 & -35355.3 \\ 35355.3 & 35355.3 & -35355.3 & -35355.3 \\ -35355.3 & -35355.3 & 35355.3 & 35355.3 \\ -35355.3 & -35355.3 & 35355.3 & 35355.3 \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ u_5 \\ v_5 \end{pmatrix} = \begin{pmatrix} 0.7 \\ 0$$

The element contributes to {1, 2, 9, 10} global degrees of freedom.

Locations for element contributions to a global vector: $\begin{bmatrix} 1\\2\\9\\10 \end{bmatrix}$

and to a global matrix:
$$\begin{bmatrix} [1,\,1] & [1,\,2] & [1,\,9] & [1,\,10] \\ [2,\,1] & [2,\,2] & [2,\,9] & [2,\,10] \\ [9,\,1] & [9,\,2] & [9,\,9] & [9,\,10] \\ [10,\,1] & [10,\,2] & [10,\,9] & [10,\,10] \\ \end{bmatrix}$$

$$\begin{pmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \\ u_5 \\ v_5 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 10000. \\ 17320.5 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

$$\begin{split} E &= 200000 \qquad A = 1000. \\ Element node \qquad Global node number \qquad x \qquad y \\ 1 \qquad \qquad 5 \qquad \qquad 2000. \qquad 2000. \\ 2 \qquad \qquad 4 \qquad \qquad 4000. \qquad 3000. \\ x_1 &= 2000. \qquad y_1 &= 2000. \qquad x_2 &= 4000. \qquad y_2 &= 3000. \\ L &= \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = 2236.07 \\ Direction cosines: \ell_s &= \frac{x_2 - x_1}{L} = 0.894427 \qquad m_s &= \frac{y_2 - y_1}{L} = 0.447214 \end{split}$$

Substituting into the truss element equations we get

$$\begin{pmatrix} 71554.2 & 35777.1 & -71554.2 & -35777.1 \\ 35777.1 & 17888.5 & -35777.1 & -17888.5 \\ -71554.2 & -35777.1 & 71554.2 & 35777.1 \\ -35777.1 & -17888.5 & 35777.1 & 17888.5 \end{pmatrix} \begin{pmatrix} u_5 \\ v_5 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {9, 10, 7, 8} global degrees of freedom.

Locations for element contributions to a global vector: $\begin{bmatrix} 9 \\ 10 \\ 7 \\ 8 \end{bmatrix}$

and to a global matrix:
$$\begin{pmatrix} [9,\,9] & [9,\,10] & [9,\,7] & [9,\,8] \\ [10,\,9] & [10,\,10] & [10,\,7] & [10,\,8] \\ [7,\,9] & [7,\,10] & [7,\,7] & [7,\,8] \\ [8,\,9] & [8,\,10] & [8,\,7] & [8,\,8] \end{pmatrix}$$

Adding element equations into appropriate locations we have

1	85355.3	35355.3	-50000.	0	0	0	0	0	-35355.3	-35355
	35355.3	35355.3	0	0	0	0	0	0	-35355.3	-35355
l	-50000.	0	85355.3	-35355.3	0	0	0	0	-35355.3	35355
	0	0	-35355.3	102022.	0	0	0	-66666.7	35355.3	-35355
	0	0	0	0	71554.2	-35777.1	0	0	-71554.2	35777
	0	0	0	0	-35777.1	17888.5	0	0	35777.1	-17888
	0	0	0	0	0	0	71554.2	35777.1	-71554.2	-35777
l	0	0	0	-66666.7	0	0	35777.1	84555.2	-35777.1	-17888
	-35355.3	-35355.3	-35355.3	35355.3	-71554.2	35777.1	-71554.2	-35777.1	213819.	0
	-35355.3	-35355.3	35355.3	-35355.3	35777.1	-17888.5	-35777.1	-17888.5	0	106488

Essential boundary conditions

Node	dof	Valu
1	$\begin{matrix} u_1 \\ v_1 \end{matrix}$	0 0
3	$\mathbf{u_3}\\\mathbf{v_3}$	0 0
4	$\mathbf{u_4}$	0 0

Remove {1, 2, 5, 6, 7, 8} rows and columns.

After adjusting for essential boundary conditions we have

$$\begin{pmatrix} 85355.3 & -35355.3 & -35355.3 & 35355.3 \\ -35355.3 & 102022. & 35355.3 & -35355.3 \\ -35355.3 & 35355.3 & 213819. & 0 \\ 35355.3 & -35355.3 & 0 & 106488. \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ u_5 \\ v_5 \end{pmatrix} = \begin{pmatrix} 10000. \\ 17320.5 \\ 0 \\ 0 \end{pmatrix}$$

Solving the final system of global equations we get

$$\{u_2=0.213105,\ v_2=0.249979,\ u_5=-0.00609705,\ v_5=0.0122424\}$$

Complete table of nodal values

	u	\mathbf{v}
1	0	0
2	0.213105	0.249979
3	0	0
4	0	0
5	-0.00609705	0.0122424

Computation of reactions

Equation numbers of dof with specified values: {1, 2, 5, 6, 7, 8}

Extracting equations {1, 2, 5, 6, 7, 8} from the global system we have

$$\begin{pmatrix} 85355.3 & 35355.3 & -50000. & 0 & 0 & 0 & 0 & -35355.3 & -35355.3 \\ 35355.3 & 35355.3 & 0 & 0 & 0 & 0 & 0 & 0 & -35355.3 & -35355.3 \\ 0 & 0 & 0 & 0 & 71554.2 & -35777.1 & 0 & 0 & -71554.2 & 35777.1 \\ 0 & 0 & 0 & 0 & -35777.1 & 17888.5 & 0 & 0 & 35777.1 & -17888.5 \\ 0 & 0 & 0 & 0 & 0 & 0 & 71554.2 & 35777.1 & -71554.2 & -35777.1 \\ 0 & 0 & 0 & -66666.7 & 0 & 0 & 35777.1 & 84555.2 & -35777.1 & -17888.5 \end{pmatrix}$$

$$\begin{pmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \\ v_4 \\ u_5 \\ v_5 \end{pmatrix} = \begin{pmatrix} R_1 + 0. \\ R_2 + 0. \\ R_3 + 0. \\ R_4 + 0. \\ R_5 + 0. \\ R_6 + 0. \end{pmatrix}$$

Substituting the nodal values and re-arranging

$$\begin{pmatrix} R_1 \\ R_2 \\ R_3 \\ R_4 \\ R_5 \\ R_6 \end{pmatrix} =$$

$$\begin{pmatrix} 85355.3 & 35355.3 & -50000. & 0 & 0 & 0 & 0 & 0 & -35355.3 & -35355.3 \\ 35355.3 & 35355.3 & 0 & 0 & 0 & 0 & 0 & 0 & -35355.3 & -35355.3 \\ 0 & 0 & 0 & 0 & 71554.2 & -35777.1 & 0 & 0 & -71554.2 & 35777.1 \\ 0 & 0 & 0 & 0 & -35777.1 & 17888.5 & 0 & 0 & 35777.1 & -17888.5 \\ 0 & 0 & 0 & 0 & 0 & 0 & 71554.2 & 35777.1 & -71554.2 & -35777.1 \\ 0 & 0 & 0 & -66666.7 & 0 & 0 & 35777.1 & 84555.2 & -35777.1 & -17888.5 \end{pmatrix}$$

$$\begin{pmatrix} 0\\ 0\\ 0.213105\\ 0.249979\\ 0\\ 0\\ 0\\ -0.00609705\\ 0.0122424\\ \end{pmatrix}$$

Carrying out computations, the reactions are as follows.

Label	dof	Reaction
R_1	\mathbf{u}_1	-10872.5
R_2	\mathbf{v}_1	-217.271
R_3	\mathbf{u}_3	874.267
R_4	\mathbf{v}_3	-437.133
R_5	$\mathbf{u_4}$	-1.72786
R_6	$\mathbf{v_4}$	-16666.1

Sum of Reactions

dof: u
$$-10000$$
.
dof: v -17320.5

Solution for element 1

Nodal coordinates

Eler	nent node	Global n	ode number	X	y
	1		1	0	0
	2		2	4000.	0
\mathbf{x}_1	= 0	$y_1 = 0$	$x_2 = 4000.$	$y_2 = 0$	
$L = \sqrt{(x_2 - x_2)^2}$	$(-x_1)^2 + (y_2)^2$	$-y_1)^2 = 4000.$			

$$L = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = 4000.$$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = 1$$
. $m_s = \frac{y_2 - y_1}{L} = 0$

Global to local transformation matrix, $T = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{pmatrix}$

Element nodal displacements in global coordinates, $\mathbf{d} = \begin{pmatrix} \mathbf{u}_1 \\ \mathbf{v}_1 \\ \mathbf{u}_2 \end{pmatrix} = \begin{pmatrix} \mathbf{0} \\ \mathbf{0} \\ 0.213105 \end{pmatrix}$

Element nodal displacements in local coordinates, $d_{\ell} = T d = \begin{pmatrix} 0. \\ 0.213105 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0$. $d_2 = 0.213105$

E = 200000A = 1000.

Axial strain, $\epsilon = (d_2 - d_1)/L = 0.0000532763$

Axial stress, $\sigma = \text{E}\epsilon = 10.6553$ Axial force = σ A = 10655.3

Solution for element 2

Nodal coordinates

Global to local transformation matrix,
$$T = \begin{pmatrix} -0.707107 & 0.707107 & 0 & 0 \\ 0 & 0 & -0.707107 & 0.707107 \end{pmatrix}$$

Element nodal displacements in global coordinates,
$$\emph{\textbf{d}} = \begin{pmatrix} u_2 \\ v_2 \\ u_5 \\ v_5 \end{pmatrix} = \begin{pmatrix} 0.213105 \\ 0.249979 \\ -0.00609705 \\ 0.0122424 \end{pmatrix}$$

Element nodal displacements in local coordinates, $\mathbf{d}_{\ell} = \mathbf{T} \mathbf{d} = \begin{pmatrix} 0.0260733 \\ 0.0129679 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0.0260733$ $d_2 = 0.0129679$

$$E = 200000$$
 $A = 1000$.

Axial strain,
$$\epsilon = (d_2 - d_1)/L = -4.63345 \times 10^{-6}$$

Axial stress,
$$\sigma = \text{E}\epsilon = -0.926689$$
 Axial force = $\sigma A = -926.689$

Solution for element 3

Nodal coordinates

Element node	Global node nui	nber	X	y
1	5		2000.	2000.
2	3		0	3000.
$x_1 = 2000.$	$y_1 = 2000.$	$x_2 = 0$	y ₂ =	3000.

$$L = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = 2236.07$$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = -0.894427$$
 $m_s = \frac{y_2 - y_1}{L} = 0.447214$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = -0.894427$$
 $m_s = \frac{y_2 - y_1}{L} = 0.447214$ Global to local transformation matrix, $T = \begin{pmatrix} -0.894427 & 0.447214 & 0 & 0 \\ 0 & 0 & -0.894427 & 0.447214 \end{pmatrix}$

Element nodal displacements in global coordinates,
$$\mathbf{d} = \begin{pmatrix} u_5 \\ v_5 \\ u_3 \\ v_3 \end{pmatrix} = \begin{pmatrix} -0.00609705 \\ 0.0122424 \\ 0 \\ 0 \end{pmatrix}$$

Element nodal displacements in local coordinates, $d_{\ell} = T d = \begin{pmatrix} 0.0109283 \\ 0. \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0.0109283$ $d_2 = 0$.

$$E = 200000$$
 $A = 1000$.

Axial strain, $\epsilon = (d_2 - d_1)/L = -4.8873 \times 10^{-6}$

Axial stress,
$$\sigma = \text{E}\epsilon = -0.97746$$

Axial force =
$$\sigma A = -977.46$$

Solution for element 4

Nodal coordinates

Element node	Global no	de number	X	y
1	2		4000.	0
2	•	4	4000.	3000.
$x_1 = 4000.$	$y_1 = 0$	$x_2 = 4000.$	y ₂ =	= 3000.

$$L = \sqrt{\left(x_2 - x_1\right)^2 + \left(y_2 - y_1\right)^2} \ = 3000.$$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = 0.$$

$$m_s = \frac{y_2 - y_1}{L} = 1.$$

Global to local transformation matrix, $T = \begin{pmatrix} 0. & 1. & 0 & 0 \\ 0 & 0 & 0. & 1. \end{pmatrix}$

Element nodal displacements in global coordinates, $\mathbf{d} = \begin{pmatrix} u_2 \\ v_2 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} 0.213105 \\ 0.249979 \\ 0 \\ 0 \end{pmatrix}$

Element nodal displacements in local coordinates, $d_{\ell} = T d = \begin{pmatrix} 0.249979 \\ 0. \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0.249979$ $d_2 = 0$.

$$E = 200000$$
 $A = 1000$.

Axial strain, $\epsilon = (d_2 - d_1)/L = -0.0000833262$

Axial stress, $\sigma = \text{E}\epsilon = -16.6652$ Axial force = $\sigma A = -16665.2$

Solution for element 5

Nodal coordinates

Element node Global node number
$$x$$
 y
$$1 \qquad 1 \qquad 0 \qquad 0$$

$$2 \qquad 5 \qquad 2000. \qquad 2000.$$

$$x_1=0 \qquad y_1=0 \qquad x_2=2000. \qquad y_2=2000.$$

$$L=\sqrt{(x_2-x_1)^2+(y_2-y_1)^2}=2828.43$$

$$\text{Direction cosines: } \ell_s=\frac{x_2-x_1}{L}=0.707107 \qquad m_s=\frac{y_2-y_1}{L}=0.707107$$

Global to local transformation matrix,
$$T = \begin{pmatrix} 0.707107 & 0.707107 & 0 & 0 \\ 0 & 0 & 0.707107 & 0.707107 \end{pmatrix}$$

Element nodal displacements in global coordinates,
$$\boldsymbol{d} = \begin{pmatrix} u_1 \\ v_1 \\ u_5 \\ v_5 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ -0.00609705 \\ 0.0122424 \end{pmatrix}$$

Element nodal displacements in local coordinates, $\mathbf{d}_{\ell} = \mathbf{T} \mathbf{d} = \begin{pmatrix} 0.\\ 0.00434542 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0$. $d_2 = 0.00434542$

$$E = 200000$$
 $A = 1000$.

Axial strain,
$$\epsilon = (d_2 - d_1)/L = 1.53634 \times 10^{-6}$$

Axial stress,
$$\sigma = \text{E}\epsilon = 0.307267$$
 Axial force = $\sigma A = 307.267$

Solution for element 6

Nodal coordinates

Element node Global node number
$$x$$
 y 1 5 2000 . 2000 . 2 4 4000 . 3000 . $x_1 = 2000$. $y_1 = 2000$. $x_2 = 4000$. $y_2 = 3000$.

$$L = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = 2236.07$$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = 0.894427$$
 $m_s = \frac{y_2 - y_1}{L} = 0.447214$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = 0.894427$$
 $m_s = \frac{y_2 - y_1}{L} = 0.447214$ Global to local transformation matrix, $T = \begin{pmatrix} 0.894427 & 0.447214 & 0 & 0 \\ 0 & 0 & 0.894427 & 0.447214 \end{pmatrix}$

Element nodal displacements in global coordinates,
$$\mathbf{d} = \begin{pmatrix} u_5 \\ v_5 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} -0.00609705 \\ 0.0122424 \\ 0 \\ 0 \end{pmatrix}$$

Element nodal displacements in local coordinates,
$$\mathbf{d}_{\ell} = \mathbf{T} \mathbf{d} = \begin{pmatrix} 0.0000215983 \\ 0. \end{pmatrix}$$

Axial displacements at element ends, $d_1 = 0.0000215983$ $d_2 = 0$.

$$E = 200000$$
 $A = 1000$.

Axial strain,
$$\epsilon = (d_2 - d_1)/L = -9.65904 \times 10^{-9}$$

Axial stress,
$$\sigma = \text{E}\epsilon = -0.00193181$$

Axial force = σ A = -1.93181

Solution summary

Nodal solution

	x-coord	y-coord	u	\mathbf{v}
1	0	0	0	0
2	4000.	0	0.213105	0.249979
3	0	3000.	0	0
4	4000.	3000.	0	0
5	2000.	2000.	-0.00609705	0.0122424

Element solution

	Stress	Axial force
1	10.6553	10655.3
2	-0.926689	-926.689
3	-0.97746	-977.46
4	-16.6652	-16665.2
5	0.307267	307.267
6	-0.00193181	-1.93181

Support reactions

Node	dof	Reaction
1	$\mathbf{u_1}$	-10872.5
1	\mathbf{v}_1	-217.271
3	\mathbf{u}_3	874.267
3	\mathbf{v}_3	-437.133
4	u_4	-1.72786
4	v_4	-16666.1

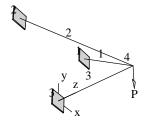
Sum of applied loads \rightarrow (10000. 17320.5)

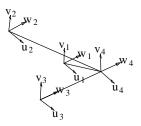
Sum of support reactions \rightarrow (-10000. -17320.5)

Example 4.2: Three-bar truss (p. 230)

The cross-sectional areas of elements 1 and 2 is 200 mm² and that of element 3 is 600 mm². All elements are made of the same material with E = 200 GPa. The applied load is P = 20 kN. The nodal coordinates are as follows.

Node
$$x(m)$$
 $y(m)$ $z(m)$
1 0.96 1.92 0
2 -1.44 1.44 0
3 0 0 0
4 0 0 2





The complete computations are as follows. The numerical values are in the $N-\min$ units. The computed displacements are in mm and the stresses in MPa.

Specified nodal loads

$$\begin{array}{cccc} Node & dof & Value \\ & u_4 & 0 \\ 4 & v_4 & -20000 \\ & w_4 & 0 \end{array}$$

Global equations at start of the element assembly process

$$E = 210000$$
 $A = 200$

Element node	Global node number	x	y	z
1	1	960.	1920.	0
2	4	0	0	2000.
Direction cosines, $\ell_s = -0.3$	$m_s = -0.6$	35441	$n_{s} = 0.6$	81677

Substituting into the truss element equations we get

The element contributes to {1, 2, 3, 10, 11, 12} global degrees of freedom.

$$E = 210000$$
 $A = 200$

Element node	Global node number	X	y	Z
1	2	-1440.	1440.	0
2	4	0	0	2000.

Direction cosines, $\ell_s = 0.504497$ $m_s = -0.504497$

Substituting into the truss element equations we get

$$\begin{pmatrix} 3745.09 & -3745.09 & 5201.51 & -3745.09 & 3745.09 & -5201.51 \\ -3745.09 & 3745.09 & -5201.51 & 3745.09 & -3745.09 & 5201.51 \\ 5201.51 & -5201.51 & 7224.32 & -5201.51 & 5201.51 & -7224.32 \\ -3745.09 & 3745.09 & -5201.51 & 3745.09 & -3745.09 & 5201.51 \\ 3745.09 & -3745.09 & 5201.51 & -3745.09 & 3745.09 & -5201.51 \\ -5201.51 & 5201.51 & -7224.32 & 5201.51 & -5201.51 & 7224.32 \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ w_2 \\ u_4 \\ v_4 \\ w_4 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

 $n_s = 0.70069$

The element contributes to {4, 5, 6, 10, 11, 12} global degrees of freedom.

$$E = 210000$$
 $A = 600$

Element node	Global node number	X	y	Z
1	3	0	0	0
2	4	0	0	2000.

Direction cosines, $\ell_s = 0$ $m_s = 0$ $n_s = 1$.

Substituting into the truss element equations we get

The element contributes to {7, 8, 9, 10, 11, 12} global degrees of freedom.

1532.63	3065.27	-3192.99	0	0	0	0	0	0	-1532.63	-3065.27	
3065.27	6130.53	-6385.97	0	0	0	0	0	0	-3065.27	-6130.53	
-3192.99	-6385.97	6652.06	0	0	0	0	0	0	3192.99	6385.97	
0	0	0	3745.09	-3745.09	5201.51	0	0	0	-3745.09	3745.09	
0	0	0	-3745.09	3745.09	-5201.51	0	0	0	3745.09	-3745.09	
0	0	0	5201.51	-5201.51	7224.32	0	0	0	-5201.51	5201.51	
0	0	0	0	0	0	0	0	0	0	0	
0	0	0	0	0	0	0	0	0	0	0	
0	0	0	0	0	0	0	0	63000.	0	0	
-1532.63	-3065.27	3192.99	-3745.09	3745.09	-5201.51	0	0	0	5277.72	-679.818	
-3065.27	-6130.53	6385.97	3745.09	-3745.09	5201.51	0	0	0	-679.818	9875.62	
3192.99	6385.97	-6652.06	-5201.51	5201.51	-7224.32	0	0	-63000.	2008.52	-11587.5	

Essential boundary conditions

Node	dof	Value
	\mathbf{u}_1	0
1	$\mathbf{v_1}$ $\mathbf{w_1}$	0 0
	$\mathbf{u_2}$	0
2	\mathbf{v}_2	0
	\mathbf{w}_2	0
0	\mathbf{u}_3	0
3	$\mathbf{v_3}$ $\mathbf{w_3}$	0 0
	**3	U

Remove $\{1, 2, 3, 4, 5, 6, 7, 8, 9\}$ rows and columns.

After adjusting for essential boundary conditions we have

$$\begin{pmatrix} 5277.72 & -679.818 & 2008.52 \\ -679.818 & 9875.62 & -11587.5 \\ 2008.52 & -11587.5 & 76876.4 \end{pmatrix} \begin{pmatrix} u_4 \\ v_4 \\ w_4 \end{pmatrix} = \begin{pmatrix} 0 \\ -20000. \\ 0 \end{pmatrix}$$

Solving the final system of global equations we get

$$\{u_4=-0.178143,\,v_4=-2.46857,\,w_4=-0.367431\}$$

Complete table of nodal values

	u	V	W
1	0	0	0
2	0	0	0
3	0	0	0
4	-0.178143	-2.46857	-0.367431

Computation of reactions

Equation numbers of dof with specified values: {1, 2, 3, 4, 5, 6, 7, 8, 9}

Extracting equations {1, 2, 3, 4, 5, 6, 7, 8, 9} from the global system we have

1532.63	3065.27	-3192.99	0	0	0	0	0	0	-1532.63	-3065.27	3
3065.27	6130.53	-6385.97	0	0	0	0	0	0	-3065.27	-6130.53	6:
-3192.99	-6385.97	6652.06	0	0	0	0	0	0	3192.99	6385.97	-6
0	0	0	3745.09	-3745.09	5201.51	0	0	0	-3745.09	3745.09	-5
0	0	0	-3745.09	3745.09	-5201.51	0	0	0	3745.09	-3745.09	5:
0	0	0	5201.51	-5201.51	7224.32	0	0	0	-5201.51	5201.51	-7:
0	0	0	0	0	0	0	0	0	0	0	
0	0	0	0	0	0	0	0	0	0	0	
0	0	0	0	0	0	0	0	63000.	0	0	-630

Substituting the nodal values and re-arranging

R_1)	1532.63	3065.27	-3192.99	0	0	0	0	0	0	-1532.63	-3065.1
R_2		3065.27	6130.53	-6385.97	0	0	0	0	0	0	-3065.27	-6130 .
R_3		-3192.99	-6385.97	6652.06	0	0	0	0	0	0	3192.99	6385.
R ₄		0	0	0	3745.09	-3745.09	5201.51	0	0	0	-3745.09	3745.
R ₅	=	0	0	0	-3745.09	3745.09	-5201.51	0	0	0	3745.09	-3745.0
R ₆		0	0	0	5201.51	-5201.51	7224.32	0	0	0	-5201.51	5201.
R ₇		0	0	0	0	0	0	0	0	0	0	0
R ₈		0	0	0	0	0	0	0	0	0	0	0
R_9		0	0	0	0	0	0	0	0	63000.	0	0

Carrying out computations, the reactions are as follows.

Label	dof	Reaction
R_1	\mathbf{u}_1	6666.67
R_2	\mathbf{v}_1	13333.3
R_3	\mathbf{w}_1	-13888.9
R_4	\mathbf{u}_2	-6666.67
R_5	\mathbf{v}_2	6666.67
R_6	\mathbf{w}_2	-9259.26
R_7	\mathbf{u}_3	0
R_8	\mathbf{v}_3	0
R_9	\mathbf{w}_3	23148.1

Sum of Reactions

Solution for element 1

Nodal coordinates

Element node	Global node number	X	y	Z
1	1	960.	1920.	0
2	4	0	0	2000.

Direction cosines, $\ell_s = -0.327205$

$$m_s = -0.65441$$

$$n_s = 0.681677$$

Global to local transformation matrix, T =

$$\begin{pmatrix} -0.327205 & -0.65441 & 0.681677 & 0 & 0 & 0 \\ 0 & 0 & 0 & -0.327205 & -0.65441 & 0.681677 \end{pmatrix}$$

Element nodal displacements in global coordinates, $\mathbf{d} = \begin{pmatrix} u_1 \\ v_1 \\ w_1 \\ u_4 \\ v_4 \\ w_4 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ -0.178143 \\ -2.46857 \\ -0.367431 \end{pmatrix}$

Element nodal displacements in local coordinates, $d_{\ell} = T \ d = \begin{pmatrix} 0. \\ 1.42328 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0$. $d_2 = 1.42328$

$$E = 210000$$
 $A = 200$

Axial strain, $\epsilon = (d_2 - d_1)/L = 0.000485109$

Axial stress,
$$\sigma = \text{E}\epsilon = 101.873$$

Axial force =
$$\sigma A = 20374.6$$

Solution for element 2

Nodal coordinates

Element node	Global node number	X	y	Z
1	2	-1440.	1440.	0
2	4	0	0	2000.

Direction cosines, $\ell_s = 0.504497$

$$m_s = -0.504497$$

$$n_s = 0.70069$$

Global to local transformation matrix, T =

$$\left(egin{array}{ccccccccc} 0.504497 & -0.504497 & 0.70069 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.504497 & -0.504497 & 0.70069 & 0 & 0 & 0 \end{array} \right)$$

Element nodal displacements in global coordinates, $\mathbf{d} = \begin{pmatrix} u_2 \\ v_2 \\ u_4 \\ v_4 \\ w_4 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ -0.178143 \\ -2.46857 \\ -0.367431 \end{pmatrix}$

Element nodal displacements in local coordinates, $d_{\ell} = T d = \begin{pmatrix} 0. \\ 0.89806 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0$.

$$d_2 = 0.89806$$

$$E = 210000$$

$$A = 200$$

Axial strain, $\epsilon = (d_2 - d_1)/L = 0.000314631$

Axial stress, $\sigma = \text{E}\epsilon = 66.0725$

Axial force = σ A = 13214.5

Solution for element 3

Nodal coordinates

Element node Global node number
$$x$$
 y z 1 3 0 0 0 0 $2000.$

Direction cosines, $\ell_s = 0$

$$m_s = 0$$
 $n_s = 1$.

Global to local transformation matrix,
$$T = \begin{pmatrix} 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

Element nodal displacements in global coordinates, $\mathbf{d} = \begin{pmatrix} u_3 \\ v_3 \\ w_3 \\ v_4 \\ v_4 \\ w_4 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ -0.178143 \\ -2.46857 \\ -0.367431 \end{pmatrix}$

Element nodal displacements in local coordinates, $d_{\ell} = T d = \begin{pmatrix} 0. \\ -0.367431 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0$.

 $d_2 = -0.367431$

E = 210000

A = 600

Axial strain, $\epsilon = (d_2 - d_1)/L = -0.000183715$

Axial stress, $\sigma = \text{E}\epsilon = -38.5802$

Axial force = $\sigma A = -23148.1$

Solution summary

Nodal solution

	x-coord	y-coord	z-coord	u	v	W
1	960.	1920.	0	0	0	0
2	-1440 .	1440.	0	0	0	0
3	0	0	0	0	0	0
4	0	0	2000.	-0.178143	-2.46857	-0.367431

Element solution

	Stress	Axial force
1	101.873	20374.6
2	66.0725	13214.5
3	-38.5802	-23148.1

Support reactions

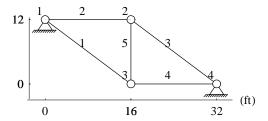
Node	dof	Reaction		
1	$\mathbf{u_1}$	6666.67		
1	\mathbf{v}_1	13333.3		
1	\mathbf{w}_1	-13888.9		
2	\mathbf{u}_2	-6666.67		
2	\mathbf{v}_2	6666.67		
2	\mathbf{w}_2	-9259.26		
3	\mathbf{u}_3	0.		
3	\mathbf{v}_3	0.		
3	\mathbf{w}_3	23148.1		

Sum of applied loads \rightarrow (0 -20000. 0)

Sum of support reactions \rightarrow (0 20000. 0)

Example 4.3: Plane truss with temperature change (p. 233)

All members have the same cross-sectional area A = 1/2 in² and are of the same material E = 29, 000 ksi and $\alpha = 6.5 \times 10^{-6}$ /°F. The first element undergoes a temperature rise of 100°F. The dimensions are shown in the figure.



For numerical calculations the k – in units are used.

Global equations at start of the element assembly process

$$\begin{split} E &= 29000 & A = \frac{1}{2} \\ \alpha &= 6.5 \times 10^{-6} & \Delta T = 100 & \epsilon_0 = 0.00065 \\ & Element \ node & Global \ node \ number & x & y \\ & 1 & 1 & 0 & 144. \\ & 2 & 3 & 192. & 0 \\ & x_1 &= 0 & y_1 &= 144. & x_2 &= 192. & y_2 &= 0 \\ & L &= \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} &= 240. \\ & Direction \ cosines: \ell_s &= \frac{x_2 - x_1}{L} &= 0.8 & m_s &= \frac{y_2 - y_1}{L} &= -0.6 \end{split}$$

Substituting into the truss element equations we get

$$\begin{pmatrix} 38.6667 & -29. & -38.6667 & 29. \\ -29. & 21.75 & 29. & -21.75 \\ -38.6667 & 29. & 38.6667 & -29. \\ 29. & -21.75 & -29. & 21.75 \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ u_3 \\ v_3 \end{pmatrix} = \begin{pmatrix} -7.54 \\ 5.655 \\ 7.54 \\ -5.655 \end{pmatrix}$$

The element contributes to {1, 2, 5, 6} global degrees of freedom.

$$\begin{split} E &= 29000 \qquad A = \frac{1}{2} \\ & & \text{Element node} \qquad \text{Global node number} \qquad x \qquad y \\ & 1 \qquad \qquad 1 \qquad \qquad 0 \qquad 144. \\ & 2 \qquad \qquad 2 \qquad \qquad 192. \qquad 144. \\ & x_1 &= 0 \qquad y_1 &= 144. \qquad x_2 &= 192. \qquad y_2 &= 144. \\ & L &= \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} \ = 192. \\ & \text{Direction cosines:} \ \ell_s &= \frac{x_2 - x_1}{L} = 1. \qquad m_s &= \frac{y_2 - y_1}{L} = 0. \end{split}$$

Substituting into the truss element equations we get

$$\begin{pmatrix} 75.5208 & 0. & -75.5208 & 0. \\ 0. & 0. & 0. & 0. \\ -75.5208 & 0. & 75.5208 & 0. \\ 0. & 0. & 0. & 0. \end{pmatrix} \begin{pmatrix} \mathbf{u}_1 \\ \mathbf{v}_1 \\ \mathbf{u}_2 \\ \mathbf{v}_2 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {1, 2, 3, 4} global degrees of freedom.

Adding element equations into appropriate locations we have

Equations for element 3

$$\begin{split} E &= 29000 & A = \frac{1}{2} \\ & & \text{Element node} & \text{Global node number} & x & y \\ & 1 & 2 & 192. & 144. \\ & 2 & 4 & 384. & 0 \\ & x_1 &= 192. & y_1 &= 144. & x_2 &= 384. & y_2 &= 0 \\ & L &= \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} &= 240. \end{split}$$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = 0.8$$
 $m_s = \frac{y_2 - y_1}{L} = -0.6$

Substituting into the truss element equations we get

$$\begin{pmatrix} 38.6667 & -29. & -38.6667 & 29. \\ -29. & 21.75 & 29. & -21.75 \\ -38.6667 & 29. & 38.6667 & -29. \\ 29. & -21.75 & -29. & 21.75 \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {3, 4, 7, 8} global degrees of freedom.

Adding element equations into appropriate locations we have

$$\begin{pmatrix} 114.188 & -29. & -75.5208 & 0 & -38.6667 & 29. & 0 & 0 \\ -29. & 21.75 & 0 & 0 & 29. & -21.75 & 0 & 0 \\ -75.5208 & 0 & 114.188 & -29. & 0 & 0 & -38.6667 & 29. \\ 0 & 0 & -29. & 21.75 & 0 & 0 & 29. & -21.75 \\ -38.6667 & 29. & 0 & 0 & 38.6667 & -29. & 0 & 0 \\ 29. & -21.75 & 0 & 0 & -29. & 21.75 & 0 & 0 \\ 0 & 0 & -38.6667 & 29. & 0 & 0 & 38.6667 & -29. \\ 0 & 0 & 29. & -21.75 & 0 & 0 & -29. & 21.75 \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} -7.54 \\ 5.655 \\ 0 \\ 0 \\ 7.54 \\ -5.655 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

0

Equations for element 4

$$\begin{split} E &= 29000 \qquad A = \frac{1}{2} \\ & & \text{Element node} \qquad \text{Global node number} \qquad x \\ & 1 \qquad \qquad 3 \qquad \qquad 192. \\ & 2 \qquad \qquad 4 \qquad \qquad 384. \\ & x_1 &= 192. \qquad y_1 &= 0 \qquad \qquad x_2 &= 384. \qquad y_2 &= 0 \\ & L &= \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} &= 192. \\ & \text{Direction cosines: } \ell_s &= \frac{x_2 - x_1}{L} &= 1. \qquad \qquad m_s &= \frac{y_2 - y_1}{L} &= 0 \end{split}$$

Substituting into the truss element equations we get

$$\begin{pmatrix} 75.5208 & 0. & -75.5208 & 0. \\ 0. & 0. & 0. & 0. \\ -75.5208 & 0. & 75.5208 & 0. \\ 0. & 0. & 0. & 0. \end{pmatrix} \begin{pmatrix} u_3 \\ v_3 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {5, 6, 7, 8} global degrees of freedom.

$$\begin{pmatrix} 114.188 & -29. & -75.5208 & 0 & -38.6667 & 29. & 0 & 0 \\ -29. & 21.75 & 0 & 0 & 29. & -21.75 & 0 & 0 \\ -75.5208 & 0 & 114.188 & -29. & 0 & 0 & -38.6667 & 29. \\ 0 & 0 & -29. & 21.75 & 0 & 0 & 29. & -21.75 \\ -38.6667 & 29. & 0 & 0 & 114.188 & -29. & -75.5208 & 0 \\ 29. & -21.75 & 0 & 0 & -29. & 21.75 & 0 & 0 \\ 0 & 0 & -38.6667 & 29. & -75.5208 & 0 & 114.188 & -29. \\ 0 & 0 & 29. & -21.75 & 0 & 0 & -29. & 21.75 \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} -7.54 \\ 5.655 \\ 0 \\ 0 \\ 7.54 \\ -5.655 \\ 0 \\ 0 \end{pmatrix}$$

$$\begin{split} E &= 29000 \qquad A = \frac{1}{2} \\ & & \text{Element node} \qquad \text{Global node number} \qquad x \qquad y \\ & 1 \qquad \qquad 2 \qquad \qquad 192. \qquad 144. \\ & 2 \qquad \qquad 3 \qquad \qquad 192. \qquad 0 \\ & x_1 &= 192. \qquad y_1 &= 144. \qquad x_2 &= 192. \qquad y_2 &= 0 \\ & L &= \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} \\ &= 144. \\ & \text{Direction cosines: } \ell_s &= \frac{x_2 - x_1}{L} &= 0. \qquad m_s &= \frac{y_2 - y_1}{L} &= -1. \end{split}$$

Substituting into the truss element equations we get

$$\begin{pmatrix} 0. & 0. & 0. & 0. \\ 0. & 100.694 & 0. & -100.694 \\ 0. & 0. & 0. & 0. \\ 0. & -100.694 & 0. & 100.694 \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ u_3 \\ v_2 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to $\{3,\,4,\,5,\,6\}$ global degrees of freedom.

Adding element equations into appropriate locations we have

$$\begin{pmatrix} 114.188 & -29. & -75.5208 & 0 & -38.6667 & 29. & 0 & 0 \\ -29. & 21.75 & 0 & 0 & 29. & -21.75 & 0 & 0 \\ -75.5208 & 0 & 114.188 & -29. & 0 & 0 & -38.6667 & 29. \\ 0 & 0 & -29. & 122.444 & 0 & -100.694 & 29. & -21.75 \\ -38.6667 & 29. & 0 & 0 & 114.188 & -29. & -75.5208 & 0 \\ 29. & -21.75 & 0 & -100.694 & -29. & 122.444 & 0 & 0 \\ 0 & 0 & -38.6667 & 29. & -75.5208 & 0 & 114.188 & -29. \\ 0 & 0 & 29. & -21.75 & 0 & 0 & -29. & 21.75 \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} -7.54 \\ 5.655 \\ 0 \\ 0 \\ 7.54 \\ -5.655 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

Essential boundary conditions

$$\begin{array}{cccc} Node & dof & Value \\ 1 & u_1 & 0 \\ v_1 & 0 \\ & u_4 & 0 \\ v_4 & 0 \end{array}$$

Remove {1, 2, 7, 8} rows and columns.

After adjusting for essential boundary conditions we have

$$\begin{pmatrix} 114.188 & -29. & 0 & 0 \\ -29. & 122.444 & 0 & -100.694 \\ 0 & 0 & 114.188 & -29. \\ 0 & -100.694 & -29. & 122.444 \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ u_3 \\ v_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 7.54 \\ -5.655 \end{pmatrix}$$

Solving the final system of global equations we get

$$\{u_2=-0.0308148,\ v_2=-0.121333,\ u_3=0.0308148,\ v_3=-0.138667\}$$

Complete table of nodal values

Computation of reactions

Equation numbers of dof with specified values: {1, 2, 7, 8}

Extracting equations $\{1, 2, 7, 8\}$ from the global system we have

$$\begin{pmatrix} 114.188 & -29. & -75.5208 & 0 & -38.6667 & 29. & 0 & 0 \\ -29. & 21.75 & 0 & 0 & 29. & -21.75 & 0 & 0 \\ 0 & 0 & -38.6667 & 29. & -75.5208 & 0 & 114.188 & -29. \\ 0 & 0 & 29. & -21.75 & 0 & 0 & -29. & 21.75 \end{pmatrix} \begin{pmatrix} u_1 \\ v_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} R_1 - 7.54 \\ R_2 + 5.655 \\ R_3 + 0. \\ R_4 + 0. \end{pmatrix}$$

Substituting the nodal values and re-arranging

$$\begin{pmatrix} R_1 \\ R_2 \\ R_3 \\ R_4 \end{pmatrix} =$$

$$\begin{pmatrix} 114.188 & -29. & -75.5208 & 0 & -38.6667 & 29. & 0 & 0 \\ -29. & 21.75 & 0 & 0 & 29. & -21.75 & 0 & 0 \\ 0 & 0 & -38.6667 & 29. & -75.5208 & 0 & 114.188 & -29. \\ 0 & 0 & 29. & -21.75 & 0 & 0 & -29. & 21.75 \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ -0.0308148 \\ -0.121333 \\ 0.0308148 \\ -0.138667 \\ 0 \\ 0 \end{pmatrix} - \begin{pmatrix} -7.54 \\ 5.655 \\ 0. \\ 0 \\ 0 \end{pmatrix}$$

Carrying out computations, the reactions are as follows.

Label	dof	Reaction		
R_1	\mathbf{u}_1	4.65432		
R_2	\mathbf{v}_1	-1.74537		
R_3	$\mathbf{u_4}$	-4.65432		
R_4	V_4	1.74537		

Sum of Reactions

$$\begin{array}{ll} dof: u & 0 \\ dof: v & 0 \end{array}$$

Solution for element 1

Nodal coordinates

Element nodal displacements in global coordinates,
$$\mathbf{d} = \begin{pmatrix} u_1 \\ v_1 \\ u_3 \\ v_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0.0308148 \\ -0.138667 \end{pmatrix}$$

Element nodal displacements in local coordinates, $\mathbf{d}_{\ell} = \mathbf{T} \mathbf{d} = \begin{pmatrix} 0.\\ 0.107852 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0$. $d_2 = 0.107852$

Axial strain, $\epsilon = (d_2 - d_1)/L - \epsilon_0 = 0.000449383$

Axial stress, $\sigma = \text{E}\epsilon = -5.8179$ Axial force = σ A = -2.90895

Solution for element 2

Nodal coordinates

Element node Global node number
$$x$$
 y
$$1 \qquad 1 \qquad 0 \qquad 144.$$

$$2 \qquad 2 \qquad 192. \qquad 144.$$

$$x_1=0 \qquad y_1=144. \qquad x_2=192. \qquad y_2=144.$$

$$L=\sqrt{(x_2-x_1)^2+(y_2-y_1)^2}=192.$$

$$L = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = 192.$$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = 1.$$

$$m_s = \frac{y_2 - y_1}{L} = 0.$$

Global to local transformation matrix, $T = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{pmatrix}$

Element nodal displacements in global coordinates, $\mathbf{d} = \begin{pmatrix} \mathbf{u}_1 \\ \mathbf{v}_1 \\ \mathbf{u}_2 \\ \mathbf{v}_2 \end{pmatrix} = \begin{pmatrix} \mathbf{0} \\ \mathbf{0} \\ -0.0308148 \\ -0.121333 \end{pmatrix}$

Element nodal displacements in local coordinates, $\mathbf{d}_{\ell} = \mathbf{T} \mathbf{d} = \begin{pmatrix} 0. \\ -0.0308148 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0$. $d_2 = -0.0308148$

$$E = 29000$$
 $A = \frac{1}{2}$

Axial strain, $\epsilon = (d_2 - d_1)/L = -0.000160494$

Axial stress,
$$\sigma = \text{E}\epsilon = -4.65432$$

Axial force =
$$\sigma A = -2.32716$$

Solution for element 3

Nodal coordinates

Element node	Global node number		X	y
1	2		192.	144.
2	4		384.	0
$x_1 = 192.$	$y_1 = 144.$	$x_2 = 384.$	y_2	= 0

$$L = \sqrt{\left(x_2 - x_1\right)^2 + \left(y_2 - y_1\right)^2} \ = 240.$$

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = 0.8$$

$$m_s = \frac{y_2 - y_1}{L} = -0.6$$

Global to local transformation matrix,
$$T = \begin{pmatrix} 0.8 & -0.6 & 0 & 0 \\ 0 & 0 & 0.8 & -0.6 \end{pmatrix}$$

Element nodal displacements in global coordinates,
$$\mathbf{d} = \begin{pmatrix} \mathbf{u}_2 \\ \mathbf{v}_2 \\ \mathbf{u}_4 \\ \mathbf{v}_4 \end{pmatrix} = \begin{pmatrix} -0.0308148 \\ -0.121333 \\ 0 \\ 0 \end{pmatrix}$$

Element nodal displacements in local coordinates, $d_{\ell} = T d = \begin{pmatrix} 0.0481481 \\ 0. \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0.0481481$ $d_2 = 0.0481481$

$$E = 29000$$
 $A = \frac{1}{2}$

Axial strain, $\epsilon = (d_2 - d_1)/L = -0.000200617$

Axial stress,
$$\sigma = \text{E}\epsilon = -5.8179$$
 Axial force = $\sigma A = -2.90895$

Solution for element 4

Nodal coordinates

Element node Global node number
$$x$$
 1 3 192. 2 4 384.
$$x_1 = 192. \quad y_1 = 0 \quad x_2 = 384. \quad y_2 = 0$$

$$L = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = 192.$$
 Direction cosines: $\ell_s = \frac{x_2 - x_1}{L} = 1$.
$$m_s = \frac{y_2 - y_1}{L} = 0$$

Global to local transformation matrix, $T = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{pmatrix}$

Element nodal displacements in global coordinates, $\mathbf{d} = \begin{pmatrix} \mathbf{u}_3 \\ \mathbf{v}_3 \\ \mathbf{u}_4 \\ \mathbf{v}_4 \end{pmatrix} = \begin{pmatrix} 0.0308148 \\ -0.138667 \\ 0 \\ 0 \end{pmatrix}$

Element nodal displacements in local coordinates, $d_{\ell} = T d = \begin{pmatrix} 0.0308148 \\ 0. \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0.0308148$

$$E = 29000$$
 $A = \frac{1}{2}$

Axial strain, $\epsilon = (d_2 - d_1)/L = -0.000160494$

Axial stress,
$$\sigma = \text{E}\epsilon = -4.65432$$
 Axial force = $\sigma A = -2.32716$

Solution for element 5

Nodal coordinates

Element node Global node number
$$x$$
 y
$$1 \qquad 2 \qquad 192. \qquad 144$$

$$2 \qquad 3 \qquad 192. \qquad 0$$

$$x_1 = 192. \qquad y_1 = 144. \qquad x_2 = 192. \qquad y_2 = 0$$

$$L = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2} = 144.$$
 Direction cosines: $\ell_s = \frac{x_2 - x_1}{1} = 0$.
$$m_s = \frac{y_2 - y_1}{1} = -1$$
.

Direction cosines:
$$\ell_s = \frac{x_2 - x_1}{L} = 0.$$

$$m_s = \frac{y_2 - y_1}{L} = -1.$$

Global to local transformation matrix, $T = \begin{pmatrix} 0. & -1. & 0 & 0 \\ 0 & 0 & 0. & -1. \end{pmatrix}$

Element nodal displacements in global coordinates, $\mathbf{d} = \begin{pmatrix} u_2 \\ v_2 \\ u_3 \end{pmatrix} = \begin{pmatrix} -0.0308148 \\ -0.121333 \\ 0.0308148 \\ 0.120067 \end{pmatrix}$

Element nodal displacements in local coordinates, $\mathbf{d}_{\ell} = \mathbf{T} \mathbf{d} = \begin{pmatrix} 0.121333 \\ 0.138667 \end{pmatrix}$

Axial displacements at element ends, $d_1 = 0.121333$ $d_2 = 0.138667$

$$E = 29000$$
 $A = \frac{1}{2}$

Axial strain, $\epsilon = (d_2 - d_1)/L = 0.00012037$

Axial stress, $\sigma = \text{E}\epsilon = 3.49074$

Axial force = σ A = 1.74537

Solution summary

Nodal solution

	x-coord	y-coord	u	v
1	0	144.	0	0
2	192.	144.	-0.0308148	-0.121333
3	192.	0	0.0308148	-0.138667
4	384.	0	0	0

Element solution

	Stress	Axial force
1	-5.8179	-2.90895
2	-4.65432	-2.32716
3	-5.8179	-2.90895
4	-4.65432	-2.32716
5	3.49074	1.74537

Support reactions

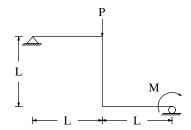
Node	dof	Reaction
1	$\mathbf{u_1}$	4.65432
1	\mathbf{v}_1	-1.74537
4	$\mathbf{u_4}$	-4.65432
4	V₄	1.74537

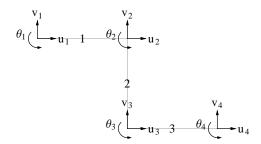
Sum of applied loads \rightarrow (0 0)

Sum of support reactions \rightarrow (0 0)

Example 4.10 Three element frame (p. 270)

$$M = 20 \text{ kN} - m$$
; $P = 10 \text{ kN}$; $L = 1 \text{ m}$; $E = 210 \text{ GPa}$; $A = 4 \times 10^{-2} \text{ m}^2$; $I = 4 \times 10^{-4} \text{ m}^4$





Use kN-m units for numerical computations. The computed displacements will be in m and stresses in kN/m^2 .

Specified nodal loads

Node	dof	Value
2	\mathbf{v}_2	-10
4	$ heta_{4}$	-20

Global equations at start of the element assembly process

Equations for element 1

$$E = 2.1 \times 10^8; \hspace{1cm} I = 0.0004; \hspace{1cm} A = 0.04; \hspace{1cm} q = \{0., \, 0.\}$$

Nodal coordinates

Element node	Global node number	X	y
1	1	0	0
2	2	1	0

Length = 1; Direction cosines:
$$\ell_s = 1$$
 $m_s = 0$

Element equations in local coordinates

$$10^{6} \begin{pmatrix} 8.4 & 0 & 0 & -8.4 & 0 & 0 \\ 0 & 1.008 & 0.504 & 0 & -1.008 & 0.504 \\ 0 & 0.504 & 0.336 & 0 & -0.504 & 0.168 \\ -8.4 & 0 & 0 & 8.4 & 0 & 0 \\ 0 & -1.008 & -0.504 & 0 & 1.008 & -0.504 \\ 0 & 0.504 & 0.168 & 0 & -0.504 & 0.336 \end{pmatrix} \begin{pmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

Global to local transformation,
$$T = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

Element equations in global coordinates

$$10^{6} \begin{pmatrix} 8.4 & 0 & 0 & -8.4 & 0 & 0 \\ 0 & 1.008 & 0.504 & 0 & -1.008 & 0.504 \\ 0 & 0.504 & 0.336 & 0 & -0.504 & 0.168 \\ -8.4 & 0 & 0 & 8.4 & 0 & 0 \\ 0 & -1.008 & -0.504 & 0 & 1.008 & -0.504 \\ 0 & 0.504 & 0.168 & 0 & -0.504 & 0.336 \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ \theta_1 \\ u_2 \\ v_2 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {1, 2, 3, 4, 5, 6} global degrees of freedom.

Adding element equations into appropriate locations we have

Equations for element 2

$$E = 2.1 \times 10^8; \hspace{1cm} I = 0.0004; \hspace{1cm} A = 0.04; \hspace{1cm} q = \{0., \, 0.\}$$

Nodal coordinates

Element node	Global node number	X	y
1	2	1	0
2	3	1	-1

Length = 1; Direction cosines:
$$\ell_s = 0$$
 $m_s = -1$

Element equations in local coordinates

$$10^{6}. \begin{pmatrix} 8.4 & 0 & 0 & -8.4 & 0 & 0 \\ 0 & 1.008 & 0.504 & 0 & -1.008 & 0.504 \\ 0 & 0.504 & 0.336 & 0 & -0.504 & 0.168 \\ -8.4 & 0 & 0 & 8.4 & 0 & 0 \\ 0 & -1.008 & -0.504 & 0 & 1.008 & -0.504 \\ 0 & 0.504 & 0.168 & 0 & -0.504 & 0.336 \end{pmatrix} \begin{pmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

Global to local transformation,
$$T = \begin{pmatrix} 0 & -1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

Element equations in global coordinates

The element contributes to {4, 5, 6, 7, 8, 9} global degrees of freedom.

Adding element equations into appropriate locations we have

Equations for element 3

$$E = 2.1 \times 10^8$$
; $I = 0.0004$; $A = 0.04$; $q = \{0., 0.\}$

Nodal coordinates

Element node	Global node number	X	y
1	3	1	-1
2	4	2	-1

Length = 1; Direction cosines:
$$\ell_s = 1$$
 $m_s = 0$

Element equations in local coordinates

$$10^{6} \begin{pmatrix} 8.4 & 0 & 0 & -8.4 & 0 & 0 \\ 0 & 1.008 & 0.504 & 0 & -1.008 & 0.504 \\ 0 & 0.504 & 0.336 & 0 & -0.504 & 0.168 \\ -8.4 & 0 & 0 & 8.4 & 0 & 0 \\ 0 & -1.008 & -0.504 & 0 & 1.008 & -0.504 \\ 0 & 0.504 & 0.168 & 0 & -0.504 & 0.336 \end{pmatrix} \begin{pmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{pmatrix} = \begin{pmatrix} 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

Global to local transformation,
$$T = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

Element equations in global coordinates

The element contributes to {7, 8, 9, 10, 11, 12} global degrees of freedom.

Adding element equations into appropriate locations we have

$$10^{6} \begin{pmatrix} 8.4 & 0 & 0 & -8.4 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1.008 & 0.504 & 0 & -1.008 & 0.504 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0.504 & 0.336 & 0 & -0.504 & 0.168 & 0 & 0 & 0 & 0 & 0 & 0 \\ -8.4 & 0 & 0 & 9.408 & 0 & 0.504 & -1.008 & 0 & 0.504 & 0 & 0 & 0 \\ 0 & -1.008 & -0.504 & 0 & 9.408 & -0.504 & 0 & -8.4 & 0 & 0 & 0 & 0 \\ 0 & 0.504 & 0.168 & 0.504 & -0.504 & 0.672 & -0.504 & 0 & 0.168 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1.008 & 0 & -0.504 & 9.408 & 0 & -0.504 & -8.4 & 0 & 0 \\ 0 & 0 & 0 & 0 & -8.4 & 0 & 0 & 9.408 & 0.504 & 0 & -1.008 & 0.504 \\ 0 & 0 & 0 & 0.504 & 0 & 0.168 & -0.504 & 0.504 & 0.672 & 0 & -0.504 & 0.168 \\ 0 & 0 & 0 & 0 & 0 & 0 & -8.4 & 0 & 0 & 8.4 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -8.4 & 0 & 0 & 8.4 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1.008 & -0.504 & 0 & 1.008 & -0.504 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0.504 & 0.168 & 0 & -0.504 & 0.336 \end{pmatrix}$$

$$\begin{pmatrix} u_1 \\ v_1 \\ \theta_1 \\ u_2 \\ v_2 \\ \theta_2 \\ u_3 \\ v_3 \\ \theta_3 \\ u_4 \\ v_4 \\ \theta_4 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ -10. \\ 0 \\ 0 \\ 0 \\ 0 \\ -20. \end{pmatrix}$$

Essential boundary conditions

Node	dof	Value
1	$\mathbf{u_1}$	0
4	V ₄	0

Remove {1, 2, 11} rows and columns.

After adjusting for essential boundary conditions we have

$$\begin{pmatrix} 0.336 & 0 & -0.504 & 0.168 & 0 & 0 & 0 & 0 & 0 \\ 0 & 9.408 & 0 & 0.504 & -1.008 & 0 & 0.504 & 0 & 0 \\ -0.504 & 0 & 9.408 & -0.504 & 0 & -8.4 & 0 & 0 & 0 \\ 0.168 & 0.504 & -0.504 & 0.672 & -0.504 & 0 & 0.168 & 0 & 0 \\ 0 & -1.008 & 0 & -0.504 & 9.408 & 0 & -0.504 & -8.4 & 0 \\ 0 & 0 & -8.4 & 0 & 0 & 9.408 & 0.504 & 0 & 0.504 \\ 0 & 0 & 0.504 & 0 & 0.168 & -0.504 & 0.504 & 0.672 & 0 & 0.168 \\ 0 & 0 & 0 & 0 & -8.4 & 0 & 0 & 8.4 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0.504 & 0.168 & 0 & 0.336 \end{pmatrix} \begin{pmatrix} \theta_1 \\ u_2 \\ v_2 \\ \theta_2 \\ u_3 \\ v_3 \\ \theta_3 \\ u_4 \\ \theta_4 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ -10. \\ 0 \\ 0 \\ 0 \\ -20. \end{pmatrix}$$

Solving the final system of global equations we get

$$\{\theta_1=0.0000784722,\ u_2=0,\ v_2=0.0000685516,\ \theta_2=0.0000487103,\ u_3=0.0000189484,\ v_3=0.0000703373,\ \theta_3=-0.0000108135,\ u_4=0.0000189484,\ \theta_4=-0.000159623\}$$

Complete table of nodal values

	u	V	θ
1	0	0	0.0000784722
2	0	0.0000685516	0.0000487103
3	0.0000189484	0.0000703373	-0.0000108135
4	0.0000189484	0	-0.000159623

Computation of reactions

Equation numbers of dof with specified values: {1, 2, 11}

Extracting equations {1, 2, 11} from the global system we have

Substituting the nodal values and re-arranging

$$\begin{pmatrix} R_1 \\ R_2 \\ R_3 \end{pmatrix} = 10^6$$

Carrying out computations, the reactions are as follows.

Sum of Reactions

$$\begin{array}{ll} \text{dof: u} & 0 \\ \text{dof: v} & 10. \\ \text{dof: } \theta & 0 \end{array}$$

Solution for element 1

$$E = 2.1 \times 10^8; \hspace{1.5cm} I = 0.0004; \hspace{1.5cm} A = 0.04; \hspace{1.5cm} q = \{0., \, 0.\}$$

Length = 1; Direction cosines:
$$\ell_s = 1$$
 $m_s = 0$

Nodal values in global coordinates, $d^{T} = (0 \ 0 \ 0.0000784722 \ 0 \ 0.0000685516 \ 0.0000487103)$

Global to local transformation,
$$T = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

Nodal values in local coordinates, $\mathbf{d}_{\ell}^{T} = T\mathbf{d} = (0 \ 0 \ 0.0000784722 \ 0 \ 0.0000685516 \ 0.0000487103)$

Axial displacement interpolation functions, $N_u^T = \{1 - s, s\}$

Axial displacement,
$$u(s) = N_u^T \begin{pmatrix} d_1 \\ d_4 \end{pmatrix} = 0$$

Axial force, EA du(s)/ds = 0

Beam bending interpolation functions, $N_{v}^{T} = \left\{2\,s^{3} - 3\,s^{2} + 1,\,s^{3} - 2\,s^{2} + s,\,3\,s^{2} - 2\,s^{3},\,s^{3} - s^{2}\right\}$

$$Transverse \ displacement, \ v(s) = \textbf{\textit{N}}_{v}^{T} \begin{pmatrix} d_{2} \\ d_{3} \\ d_{5} \\ d_{6} \end{pmatrix} = 0.0000784722 \, s - 9.92063 \times 10^{-6} \, s^{3}$$

Fixed-end displacement solution, = $0.(1-s)^2 s^2$

Total transverse displacement, $v(s) = 0.0000784722 s - 9.92063 \times 10^{-6} s^3$

Bending moment, $M = EI d^2v(s)/ds^2 = -5. s$

Shear force, V(s) = dM/ds = -5.

Solution for element 2

$$E = 2.1 \times 10^8; \hspace{1cm} I = 0.0004; \hspace{1cm} A = 0.04; \hspace{1cm} q = \{0., \ 0.\}$$

Length = 1; Direction cosines:
$$\ell_s = 0$$
 $m_s = -1$

Nodal values in global coordinates, $d^{T} =$

 $(0\ 0.0000685516\ 0.0000487103\ 0.0000189484\ 0.0000703373\ -0.0000108135)$

Global to local transformation,
$$T = \begin{pmatrix} 0 & -1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

Nodal values in local coordinates, $d_{\ell}^{T} = Td =$

 $(-0.0000685516\ 0\ 0.0000487103\ -0.0000703373\ 0.0000189484\ -0.0000108135)$

Axial displacement interpolation functions, $N_{u}^{T} = \{1 - s, s\}$

Axial displacement,
$$u(s) = N_u^T \begin{pmatrix} d_1 \\ d_4 \end{pmatrix} = -1.78571 \times 10^{-6} \text{ s} - 0.0000685516$$

Axial force, EA du(s)/ds = -15.

Beam bending interpolation functions, $\textit{N}_{v}^{T} = \left\{2\,s^{3}\,-3\,s^{2}\,+\,1,\,s^{3}\,-\,2\,s^{2}\,+\,s,\,3\,s^{2}\,-\,2\,s^{3},\,s^{3}\,-\,s^{2}\right\}$

$$\text{Transverse displacement, } \mathbf{v}(s) = \textbf{\textit{N}}_{v}^{T} \begin{pmatrix} d_{2} \\ d_{3} \\ d_{5} \\ d_{6} \end{pmatrix} = 0.0000487103\,s - 0.0000297619\,s^{2}$$

Fixed-end displacement solution, = $0.(1-s)^2 s^2$

Total transverse displacement, $v(s) = 0.0000487103 s - 0.0000297619 s^2$

Bending moment, $M = EI d^2v(s)/ds^2 = -5$.

Shear force, V(s) = dM/ds = 0

Solution for element 3

$$E = 2.1 \times 10^8$$
; $I = 0.0004$; $A = 0.04$; $q = \{0., 0.\}$

$$q = \{0., 0.\}$$

Length = 1;

Direction cosines: $\ell_s = 1$ $m_s = 0$

Nodal values in global coordinates, $\mathbf{d}^{\mathrm{T}} =$

 $(0.0000189484 \ 0.0000703373 \ -0.0000108135 \ 0.0000189484 \ 0 \ -0.000159623)$

Global to local transformation, $T = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$

Nodal values in local coordinates, $\mathbf{d}_{\ell}^{\mathrm{T}} = T\mathbf{d} =$

 $(\ 0.0000189484 \ \ 0.0000703373 \ \ -0.0000108135 \ \ 0.0000189484 \ \ 0 \ \ -0.000159623 \,)$

Axial displacement interpolation functions, $N_{u}^{T} = \{1 - s, s\}$

Axial displacement, $\mathbf{u}(s) = \mathbf{N}_{\mathbf{u}}^{T} \begin{pmatrix} \mathbf{d}_{1} \\ \mathbf{d}_{4} \end{pmatrix} = 0.0000189484$

Axial force, EA du(s)/ds = 0

Beam bending interpolation functions, $N_v^T = \left\{2\,s^3 - 3\,s^2 + 1,\,s^3 - 2\,s^2 + s,\,3\,s^2 - 2\,s^3,\,s^3 - s^2\right\}$

Transverse displacement,
$$\mathbf{v}(s) = \textbf{N}_{\mathbf{v}}^T \begin{pmatrix} d_2 \\ d_3 \\ d_5 \\ d_6 \end{pmatrix} =$$

 $-0.0000297619 s^3 - 0.0000297619 s^2 - 0.0000108135 s + 0.0000703373$

Fixed-end displacement solution, = $0.(1-s)^2 s^2$

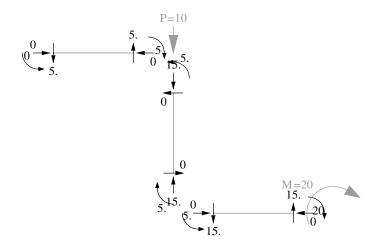
 $Total\ transverse\ displacement,\ v(s) = -0.0000297619\,s^3 - 0.0000297619\,s^2 - 0.0000108135\,s + 0.0000703373\,s + 0.000070373\,s + 0.0000703\,s + 0.00000703\,s + 0.$

Bending moment, $M = EI d^2v(s)/ds^2 = -15. s - 5.$

Shear force, V(s) = dM/ds = -15.

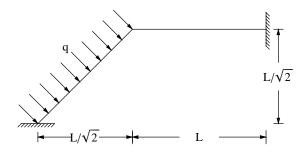
Forces at element ends

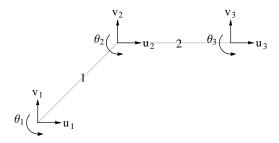
	X	\mathbf{y}	Axial force	Bending moment	Shear force
1	0	0	0	0	-5.
1	1	0	0	−5 .	-5.
9	1	0 -1	-15 .	-5.	0
۷	1	-1	-15. $-15.$	−5 .	0
9	1	-1	0	-5 .	-15 .
3	2	-1	0	-20.	-15.



Example 4.11 Frame with distributed load (p. 274)

$$q = 1 k/\text{ft}; \ L = 15 \text{ ft}; \ E = 30 \times 10^3 k/\text{in}^2; \ A = 100 \text{in}^2; \ I = 1000 \text{in}^4$$





Use k-in units

Global equations at start of the element assembly process

Equations for element 1

$$E = 30000; \hspace{1cm} I = 1000; \hspace{1cm} A = 100; \hspace{1cm} q = \{0., \, -0.0833333\}$$

Nodal coordinates

Length = 180.; Direction cosines:
$$\ell_s = 0.707107$$
 $m_s = 0.707107$

Element equations in local coordinates

$$\begin{pmatrix} 16666.7 & 0 & 0 & -16666.7 & 0 & 0 \\ 0 & 61.7284 & 5555.56 & 0 & -61.7284 & 5555.56 \\ 0 & 5555.56 & 666667. & 0 & -5555.56 & 333333. \\ -16666.7 & 0 & 0 & 16666.7 & 0 & 0 \\ 0 & -61.7284 & -5555.56 & 0 & 61.7284 & -5555.56 \\ 0 & 5555.56 & 333333. & 0 & -5555.56 & 666667. \end{pmatrix} \begin{pmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{pmatrix} = \begin{pmatrix} 0 & 0 & 0 & 0 \\ -7.5 & 0 & 0 \\ -7.5 & 0 & 0 \\ -7.5 & 0 & 0 \end{pmatrix}$$

Global to local transformation,
$$T = \begin{pmatrix} 0.707107 & 0.707107 & 0 & 0 & 0 & 0 \\ -0.707107 & 0.707107 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.707107 & 0.707107 & 0 \\ 0 & 0 & 0 & 0 & -0.707107 & 0.707107 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

Element equations in global coordinates

$$\begin{pmatrix} 8364.2 & 8302.47 & -3928.37 & -8364.2 & -8302.47 & -3928.37 \\ 8302.47 & 8364.2 & 3928.37 & -8302.47 & -8364.2 & 3928.37 \\ -3928.37 & 3928.37 & 666667. & 3928.37 & -3928.37 & 333333. \\ -8302.47 & -8302.47 & 3928.37 & 8364.2 & 8302.47 & 3928.37 \\ -8302.47 & -8364.2 & -3928.37 & 8302.47 & 8364.2 & -3928.37 \\ -3928.37 & 3928.37 & 333333. & 3928.37 & -3928.37 & 666667. \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ \theta_1 \\ u_2 \\ v_2 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} 5.3033 \\ -5.3033 \\ -5.3033 \\ -5.3033 \\ 225. \end{pmatrix}$$

The element contributes to {1, 2, 3, 4, 5, 6} global degrees of freedom.

Adding element equations into appropriate locations we have

Equations for element 2

$$E = 30000; \hspace{1cm} I = 1000; \hspace{1cm} A = 100; \hspace{1cm} q = \{0, \, 0\}$$

Nodal coordinates

Element node	Global node number	X	y
1	2	127.279	127.279
2	3	307.279	127.279

Length = 180.; Direction cosines:
$$\ell_s = 1$$
. $m_s = 0$.

Element equations in local coordinates

$$\begin{pmatrix} 16666.7 & 0 & 0 & -16666.7 & 0 & 0 \\ 0 & 61.7284 & 5555.56 & 0 & -61.7284 & 5555.56 \\ 0 & 5555.56 & 666667. & 0 & -5555.56 & 333333. \\ -16666.7 & 0 & 0 & 16666.7 & 0 & 0 \\ 0 & -61.7284 & -5555.56 & 0 & 61.7284 & -5555.56 \\ 0 & 5555.56 & 333333. & 0 & -5555.56 & 666667. \end{pmatrix} \begin{pmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

Global to local transformation,
$$T = \begin{pmatrix} 1. & 0. & 0 & 0 & 0 & 0 \\ 0. & 1. & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1. & 0. & 0 \\ 0 & 0 & 0 & 0. & 1. & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

Element equations in global coordinates

$$\begin{pmatrix} 16666.7 & 0 & 0 & -16666.7 & 0 & 0 \\ 0 & 61.7284 & 5555.56 & 0 & -61.7284 & 5555.56 \\ 0 & 5555.56 & 666667. & 0 & -5555.56 & 333333. \\ -16666.7 & 0 & 0 & 16666.7 & 0 & 0 \\ 0 & -61.7284 & -5555.56 & 0 & 61.7284 & -5555.56 \\ 0 & 5555.56 & 333333. & 0 & -5555.56 & 666667. \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ \theta_2 \\ u_3 \\ v_3 \\ \theta_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

The element contributes to {4, 5, 6, 7, 8, 9} global degrees of freedom.

Adding element equations into appropriate locations we have

8364.2	8302.47	-3928.37	-8364.2	-8302.47	-3928.37	0	0	
8302.47	8364.2	3928.37	-8302.47	-8364.2	3928.37	0	0	
-3928.37	3928.37	666667.	3928.37	-3928.37	333333.	0	0	
-8364.2	-8302.47	3928.37	25030.9	8302.47	3928.37	-16666.7	0	
-8302.47	-8364.2	-3928.37	8302.47	8425.93	1627.18	0	-61.7284	÷
-3928.37	3928.37	333333.	3928.37	1627.18	1.33333×10^{6}	0	-5555.56	33
0	0	0	-16666.7	0	0	16666.7	0	
0	0	0	0	-61.7284	-5555.56	0	61.7284	-:
0	0	0	0	5555.56	333333.	0	-5555.56	66

Essential boundary conditions

Node	dof	Value
1	$\mathbf{u_1}\\ \mathbf{v_1}\\ \mathbf{\theta_1}$	0 0 0
3	$\mathbf{u_3}\\ \mathbf{v_3}\\ \mathbf{\theta_3}$	0 0 0

Remove {1, 2, 3, 7, 8, 9} rows and columns.

After adjusting for essential boundary conditions we have

$$\begin{pmatrix} 25030.9 & 8302.47 & 3928.37 \\ 8302.47 & 8425.93 & 1627.18 \\ 3928.37 & 1627.18 & 1.33333 \times 10^6 \end{pmatrix} \begin{pmatrix} u_2 \\ v_2 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} 5.3033 \\ -5.3033 \\ 225. \end{pmatrix}$$

Solving the final system of global equations we get

$$\{u_2=0.000601607,\ v_2=-0.00125474,\ \theta_2=0.000168509\}$$

Complete table of nodal values

Computation of reactions

Equation numbers of dof with specified values: {1, 2, 3, 7, 8, 9}

Extracting equations {1, 2, 3, 7, 8, 9} from the global system we have

$$\begin{pmatrix} 8364.2 & 8302.47 & -3928.37 & -8364.2 & -8302.47 & -3928.37 & 0 & 0 & 0 \\ 8302.47 & 8364.2 & 3928.37 & -8302.47 & -8364.2 & 3928.37 & 0 & 0 & 0 \\ -3928.37 & 3928.37 & 666667. & 3928.37 & -3928.37 & 333333. & 0 & 0 & 0 \\ 0 & 0 & 0 & -16666.7 & 0 & 0 & 16666.7 & 0 & 0 \\ 0 & 0 & 0 & 0 & -61.7284 & -5555.56 & 0 & 61.7284 & -5555.56 \\ 0 & 0 & 0 & 0 & 5555.56 & 333333. & 0 & -5555.56 & 666667. \end{pmatrix}$$

$$\begin{pmatrix} u_1 \\ v_1 \\ \theta_1 \\ u_2 \\ v_2 \\ \theta_2 \\ u_3 \\ v_3 \\ \theta_3 \end{pmatrix} = \begin{pmatrix} R_1 + 5.3033 \\ R_2 - 5.3033 \\ R_3 - 225. \\ R_4 \\ R_5 \\ R_6 \end{pmatrix}$$

Substituting the nodal values and re-arranging

$$\begin{pmatrix} R_1 \\ R_2 \\ R_3 \\ R_4 \\ R_5 \\ R_6 \end{pmatrix} = \begin{pmatrix} 8364.2 & 8302.47 & -3928.37 & -8364.2 & -8302.47 & -3928.37 & 0 & 0 & 0 \\ 8302.47 & 8364.2 & 3928.37 & -8302.47 & -8364.2 & 3928.37 & 0 & 0 & 0 \\ -3928.37 & 3928.37 & 666667. & 3928.37 & -3928.37 & 333333. & 0 & 0 & 0 \\ 0 & 0 & 0 & -16666.7 & 0 & 0 & 16666.7 & 0 & 0 \\ 0 & 0 & 0 & 0 & -61.7284 & -5555.56 & 0 & 61.7284 & -5555.56 \\ 0 & 0 & 0 & 0 & 5555.56 & 333333. & 0 & -5555.56 & 666667. \end{pmatrix}$$

Carrying out computations, the reactions are as follows.

Label	dof	Reaction
R_1	\mathbf{u}_1	-0.579812
R_2	\mathbf{v}_1	11.4653
R_3	$ heta_1$	288.462
R_4	\mathbf{u}_3	-10.0268
R_5	\mathbf{v}_3	-0.858707
R_6	$ heta_3$	49.1988

Sum of Reactions

dof: u -10.6066dof: v 10.6066dof: θ 337.661

Solution for element 1

 $E = 30000; \hspace{1cm} I = 1000; \hspace{1cm} A = 100; \hspace{1cm} q = \{0., \, -0.0833333\}$

Length = 180.; Direction cosines: $\ell_s = 0.707107$ $m_s = 0.707107$

Nodal values in global coordinates, $\mathbf{d}^{T} = (0 \ 0 \ 0 \ 0.000601607 \ -0.00125474 \ 0.000168509)$

Global to local transformation, $T = \begin{pmatrix} 0.707107 & 0.707107 & 0 & 0 & 0 & 0 \\ -0.707107 & 0.707107 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.707107 & 0.707107 & 0 \\ 0 & 0 & 0 & 0 & -0.707107 & 0.707107 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$

Nodal values in local coordinates, $\mathbf{d}_{t}^{T} = T\mathbf{d} = (0 \ 0 \ 0 \ -0.000461833 \ -0.00131263 \ 0.000168509)$

Axial displacement interpolation functions, $N_u^T = \{1. -0.00555556 \text{ s}, 0.00555556 \text{ s}\}$

Axial displacement,
$$u(s) = \textbf{\textit{N}}_{u}^{T}\!\!\left(\begin{array}{c}d_{1}\\d_{4}\end{array}\right) = -2.56574 \times 10^{-6}~s$$

Axial force, EA du(s)/ds = -7.69721

Beam bending interpolation functions, $N_v^T =$

$$\left\{ 3.42936 \times 10^{-7} \text{ s}^3 - 0.0000925926 \text{ s}^2 + 1, \ 0.0000308642 \text{ s}^3 - 0.0111111 \text{ s}^2 + \text{s}, \\ 0.0000925926 \text{ s}^2 - 3.42936 \times 10^{-7} \text{ s}^3, \ 0.0000308642 \text{ s}^3 - 0.00555556 \text{ s}^2 \right\}$$

Transverse displacement,
$$\mathbf{v}(s) = \mathbf{N}_{\mathbf{v}}^{T} \begin{pmatrix} d_2 \\ d_3 \\ d_5 \\ d_6 \end{pmatrix} = 5.65104 \times 10^{-9} \ s^3 - 1.0577 \times 10^{-6} \ s^2$$

Fixed-end displacement solution, =
$$-1.15741 \times 10^{-10} (180. - s)^2 s^2$$

Total transverse displacement, $v(s) = -1.15741 \times 10^{-10} \text{ s}^4 + 4.73177 \times 10^{-8} \text{ s}^3 - 4.8077 \times 10^{-6} \text{ s}^2$

Bending moment, $M = EI d^2v(s)/ds^2 = -0.0416667 s^2 + 8.51719 s - 288.462$

Shear force, V(s) = dM/ds = 8.51719 - 0.0833333 s

Solution for element 2

E = 30000;

I = 1000;

A = 100;

 $q = \{0, 0\}$

Length = 180.;

Direction cosines: $\ell_s = 1$.

 $m_{\rm s}=0.$

Nodal values in global coordinates, $\mathbf{d}^{T} = (0.000601607 - 0.00125474 \ 0.000168509 \ 0 \ 0)$

Global to local transformation, $T = \begin{pmatrix} 1. & 0. & 0 & 0 & 0 & 0 \\ 0. & 1. & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1. & 0. & 0 \\ 0 & 0 & 0 & 0. & 1. & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$

Nodal values in local coordinates, $\mathbf{d}_{\ell}^{T} = T\mathbf{d} = (0.000601607 - 0.00125474 \ 0.000168509 \ 0 \ 0 \ 0)$

Axial displacement interpolation functions, $\textbf{\textit{N}}_{u}^{T} = \{1.-0.00555556\,\text{s},\,0.00555556\,\text{s}\}$

Axial displacement, $u(s) = \textit{N}_u^T\!\!\left(\begin{array}{c} d_1 \\ d_4 \end{array}\right) = 0.000601607 - 3.34226 \times 10^{-6} \, s$

Axial force, EA du(s)/ds = -10.0268

Beam bending interpolation functions, $N_v^T =$

 $\left\{ 3.42936 \times 10^{-7} \, s^3 - 0.0000925926 \, s^2 + 1, \, 0.0000308642 \, s^3 - 0.01111111 \, s^2 + s, \\ 0.0000925926 \, s^2 - 3.42936 \times 10^{-7} \, s^3, \, 0.0000308642 \, s^3 - 0.00555556 \, s^2 \right\}$

Transverse displacement, $\nu(s) = \textbf{\textit{N}}_{\nu}^T\!\!\left(\!\!\!\begin{array}{c} d_2 \\ d_3 \\ d_5 \\ d_6 \end{array}\!\!\right) =$

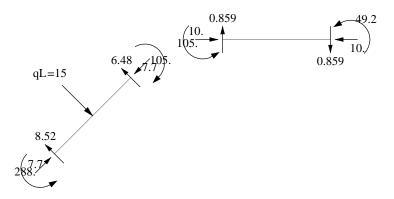
 $4.77059 \times 10^{-9} \text{ s}^3 - 1.75614 \times 10^{-6} \text{ s}^2 + 0.000168509 \text{ s} - 0.00125474$

Bending moment, $M=EI\ d^2v(s)/ds^2=0.858707\ s-105.368$

Shear force, V(s) = dM/ds = 0.858707

Forces at element ends

	X	y	Axial force	Bending moment	Shear force
1	0 127.279	0 127.279	-7.69721 -7.69721	$-288.462 \\ -105.368$	8.51719 -6.48281
2	127.279	127.279	-10.0268	-105.368	0.858707
~	307.279	127.279	-10.0268	49.1988	0.858707



Example 4.14: Three dimensional frame (p. 290)

Analyze one story three dimensional frame shown in Figure. The height of the columns is 12 ft and the length of the beams is 10 ft. Each beam is subjected to a uniformly distributed load of 2 kip/ft in the downward direction. I-shape sections are used for both columns and beams with the arrangement as shown in the figure. The columns are connected to the foundation through simple connections that do not resist moments. The material is steel with $E = 29000 \, \text{kip/in}^2$ and $G = 11200 \, \text{kip/in}^2$. The section properties are as follows.

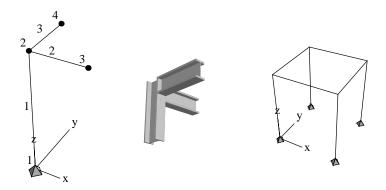
Beams:
$$A = 3.2 \text{ in}^2$$
; $J = 43 \text{ in}^4$; $I_{\text{max}} = I_r = 450 \text{ in}^4$; $I_{\text{min}} = I_s = 32 \text{ in}^2$

Columns:
$$A = 4 \text{ in}^2$$
; $J = 60 \text{ in}^4$; $I_{\text{max}} = I_r = 650 \text{ in}^4$; $I_{\text{min}} = I_s = 54 \text{ in}^2$

Taking advantage of symmetry we model a quarter of the frame using three elements. Because of symmetry, the boundary conditions at nodes 3 and 4 are as follows.

Node 3:
$$u = 0$$
; $\theta_y = 0$; $\theta_z = 0$

Node 4:
$$v = 0$$
; $\theta_x = 0$; $\theta_z = 0$



The distributed load is applied to the elements in their local coordinates. Therefore to assign proper direction and sign to the distributed loads we must carefully establish the local coordinates for the elements as follows.

Element 1: Nodes 1, 2, and 4

 \implies t – axis along global z; s – axis along global x; r – axis along global y

Element 2: Nodes 2, 3, and 4

 \implies t – axis along global x; s – axis along global (–z); r – axis along global y

Distributed load: $q_r = 0$; $q_s = 2/12 \text{ kip/in}$

Element 3: Nodes 2, 4, and 3

 $\implies t$ – axis along global y; s – axis along global z; r – axis along global x

Distributed load: $q_r = 0$; $q_s = -2/12 \text{ kip/in}$

Global equations at start of the element assembly process

Equations for element 1

$$\begin{array}{lll} q_s=0; & q_r=0; & E=29000.; & G=11200. \\ A=4; & J=60; & I_r=650; & I_s=54 \end{array}$$
 Element nodal coordinates:
$$\begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 144. \\ 0 & 60. & 144. \end{pmatrix}$$

Element length, L = 144.

Direction cosines:
$$\mathbf{H} = \begin{pmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix}$$

Element equations in local coordinates

(75.7539	0.	0.	0.	5454.28	0.	-75.7539	0.	0.	
0.	6.2934	0.	-453.125	0.	0.	0.	-6.2934	0.	-4
0.	0.	805.556	0.	0.	0.	0.	0.	-805.556	
0.	-453.125	0.	43500.	0.	0.	0.	453.125	0.	217
5454.28	0.	0.	0.	523611.	0.	-5454.28	0.	0.	
0.	0.	0.	0.	0.	4666.67	0.	0.	0.	
-75.7539	0.	0.	0.	-5454.28	0.	75.7539	0.	0.	
0.	-6.2934	0.	453.125	0.	0.	0.	6.2934	0.	4
0.	0.	-805.556	0.	0.	0.	0.	0.	805.556	
0.	-453.125	0.	21750.	0.	0.	0.	453.125	0.	435
5454.28	0.	0.	0.	261806.	0.	-5454.28	0.	0.	
0.	0.	0.	0.	0.	-4666.67	0.	0.	0.	

Element equations in global coordinates

75.7539	0	0	0	5454.28	0	-75.7539	0	0	
0	6.2934	0	-453.125	0	0	0	-6.2934	0	-4
0	0	805.556	0	0	0	0	0	-805.556	
0	-453.125	0	43500.	0	0	0	453.125	0	217
5454.28	0	0	0	523611.	0	-5454.28	0	0	
0	0	0	0	0	4666.67	0	0	0	
-75.7539	0	0	0	-5454.28	0	75.7539	0	0	
0	-6.2934	0	453.125	0	0	0	6.2934	0	4
0	0	-805.556	0	0	0	0	0	805.556	
0	-453.125	0	21750.	0	0	0	453.125	0	435
5454.28	0	0	0	261806.	0	-5454.28	0	0	
0	0	0	0	0	-4666.67	0	0	0	

The element contributes to {1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12} global degrees of freedom.

Adding element equations into appropriate locations we have

	_	=	_							
1	75.7539	0	0	0	5454.28	0	-75.7539	0	0	
l	0	6.2934	0	-453.125	0	0	0	-6.2934	0	-4
l	0	0	805.556	0	0	0	0	0	-805.556	
	0	-453.125	0	43500.	0	0	0	453.125	0	217
	5454.28	0	0	0	523611.	0	-5454.28	0	0	
	0	0	0	0	0	4666.67	0	0	0	
l	-75.7539	0	0	0	-5454.28	0	75.7539	0	0	
	0	-6.2934	0	453.125	0	0	0	6.2934	0	4
	0	0	-805.556	0	0	0	0	0	805.556	
	0	-453.125	0	21750.	0	0	0	453.125	0	435
	5454.28	0	0	0	261806.	0	-5454.28	0	0	
	0	0	0	0	0	-4666.67	0	0	0	
	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	
l	0	0	0	0	0	0	0	0	0	
l	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	
l	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	

Equations for element 2

$$\begin{array}{lll} q_s = 0.166667; & q_r = 0; & E = 29000.; & G = 11200. \\ A = 3.2; & J = 43; & I_r = 450; & I_s = 32 \\ \\ Element \ nodal \ coordinates: \left(\begin{array}{lll} 0 & 0 & 144. \\ 60. & 0 & 144. \\ 0 & 60. & 144. \\ \end{array} \right) \end{array}$$

Element length, L = 60.

Direction cosines:
$$H = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{pmatrix}$$

Element equations in local coordinates

0

0 0 0

1. 0

0. 0 0

Element equations in global coordinates

1	1546.67	0	0	0	0	0	-1546.67	0	0	0
	0	51.5556	0	0	0	1546.67	0	-51.5556	0	0
	0	0	725.	0	-21750.	0	0	0	-725.	0
	0	0	0	8026.67	0	0	0	0	0	-8026.67
	0	0	-21750.	0	870000.	0	0	0	21750.	0
	0	1546.67	0	0	0	61866.7	0	-1546.67	0	0
	-1546.67	0	0	0	0	0	1546.67	0	0	0
	0	-51.5556	0	0	0	-1546.67	0	51.5556	0	0
	0	0	-725.	0	21750.	0	0	0	725.	0
	0	0	0	-8026.67	0	0	0	0	0	8026.67
	0	0	-21750.	0	435000.	0	0	0	21750.	0
	0	1546.67	0	0	0	30933.3	0	-1546.67	0	0

The element contributes to {7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18} global degrees of freedom.

Adding element equations into appropriate locations we have

(75.7539	0	0	0	5454.28	0	-75.7539	0	0
0			-453.125		0	0	-6.2934	0
0	0	805.556	0	0	0	0	0	-805.556
0	-453.125	0	43500.	0	0	0	453.125	0
5454.28	0	0	0	523611.	0	-5454.28	0	0
0	0	0	0	0	4666.67	0	0	0
-75.7539	0	0	0	-5454.28	0	1622.42	0	0
0	-6.2934	0	453.125	0	0	0	57.849	0
0	0	-805.556	0	0	0	0	0	1530.56
0	-453.125	0	21750.	0	0	0	453.125	0
5454.28	0	0	0	261806.	0	-5454.28	0	-21750.
0	0	0	0	0	-4666.67	0	1546.67	0
0	0	0	0	0	0	-1546.67	0	0
0	0	0	0	0	0	0	-51.5556	0
0	0	0	0	0	0	0	0	-725.
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	-21750.
0	0	0	0	0	0	0	1546.67	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0

Equations for element 3

$$\begin{split} q_s &= -0.166667; & q_r = 0; & E = 29000.; & G = 11200. \\ A &= 3.2; & J = 43; & I_r = 450; & I_s = 32 \end{split}$$
 Element nodal coordinates:
$$\begin{pmatrix} 0 & 0 & 144. \\ 0 & 60. & 144. \\ 60. & 0 & 144. \end{pmatrix}$$

Element length, L = 60.

Direction cosines:
$$\mathbf{H} = \begin{pmatrix} 0 & 1. & 0. \\ 0. & 0. & 1. \\ 1. & 0. & 0. \end{pmatrix}$$

Element equations in local coordinates

(51.5556	0.	0.	0.	0.	-1546.67	-51.5556	0.	0.	0.
0.	1546.67	0.	0.	0.	0.	0.	-1546.67	0.	0.
0.	0.	725.	21750.	0.	0.	0.	0.	-725.	21750.
0.	0.	21750.	870000.	0.	0.	0.	0.	-21750.	435000.
0.	0.	0.	0.	8026.67	0.	0.	0.	0.	0.
-1546.67	0.	0.	0.	0.	61866.7	1546.67	0.	0.	0.
-51.5556	0.	0.	0.	0.	1546.67	51.5556	0.	0.	0.
0.	-1546.67	0.	0.	0.	0.	0.	1546.67	0.	0.
0.	0.	-725.	-21750.	0.	0.	0.	0.	725.	-21750.
0.	0.	21750.	435000.	0.	0.	0.	0.	-21750.	870000.
0.	0.	0.	0.	-8026.67	0.	0.	0.	0.	0.
-1546.67	0.	0.	0.	0.	30933.3	1546.67	0.	0.	0.

Element equations in global coordinates

1	51.5556	0	0	0	0	-1546.67	-51.5556	0	0	0
	0	1546.67	0	0	0	0	0	-1546.67	0	0
	0	0	725.	21750.	0	0	0	0	-725.	21750.
	0	0	21750.	870000.	0	0	0	0	-21750.	435000.
	0	0	0	0	8026.67	0	0	0	0	0
	-1546.67	0	0	0	0	61866.7	1546.67	0	0	0
	-51.5556	0	0	0	0	1546.67	51.5556	0	0	0
	0	-1546.67	0	0	0	0	0	1546.67	0	0
	0	0	-725.	-21750.	0	0	0	0	725.	-21750.
	0	0	21750.	435000.	0	0	0	0	-21750.	870000.
	0	0	0	0	-8026.67	0	0	0	0	0
	-1546.67	0	0	0	0	30933.3	1546.67	0	0	0

The element contributes to {7, 8, 9, 10, 11, 12, 19, 20, 21, 22, 23, 24} global degrees of freedom.

Adding element equations into appropriate locations we have

1	75.7539	0	0	0	5454.28	0	-75.7539	0	0
	0	6.2934	0	-453.125	0	0	0	-6.2934	0
I	0	0	805.556	0	0	0	0	0	-805.556
	0	-453.125	0	43500.	0	0	0	453.125	0
	5454.28	0	0	0	523611.	0	-5454.28	0	0
İ	0	0	0	0	0	4666.67	0	0	0
	-75.7539	0	0	0	-5454.28	0	1673.98	0	0
	0	-6.2934	0	453.125	0	0	0	1604.52	0
l	0	0	-805.556	0	0	0	0	0	2255.56
	0	-453.125	0	21750.	0	0	0	453.125	21750.
	5454.28	0	0	0	261806.	0	-5454.28	0	-21750.
	0	0	0	0	0	-4666.67	-1546.67	1546.67	0
	0	0	0	0	0	0	-1546.67	0	0
	0	0	0	0	0	0	0	-51.5556	0
l	0	0	0	0	0	0	0	0	-725.
I	0	0	0	0	0	0	0	0	0
	0	0	0	0	0	0	0	0	-21750.
	0	0	0	0	0	0	0	1546.67	0
	0	0	0	0	0	0	-51.5556	0	0
ı	0	0	0	0	0	0	0	-1546.67	0
	0	0	0	0	0	0	0	0	-725.
	0	0	0	0	0	0	0	0	21750.
	0	0	0	0	0	0	0	0	0
	0	0	0	0	0	0	-1546.67	0	0

Essential boundary conditions

Node	dof	Value
1	\mathbf{u}_1	0
1	\mathbf{v}_1	0
1	\mathbf{w}_1	0
3	\mathbf{u}_3	0
3	$ heta \mathbf{y_3}$	0
3	$\theta \mathbf{z}_3$	0
4	$\mathbf{v_4}$	0
4	$\theta \mathbf{x_4}$	0
4	θz_4	0

Remove {1, 2, 3, 13, 17, 18, 20, 22, 24} rows and columns.

After adjusting for essential boundary conditions we have

43500.	0	0	0	453.125	0	21750.	0	
0	523611.	0	-5454.28	0	0	0	261806.	
0	0	4666.67	0	0	0	0	0	
0	-5454.28	0	1673.98	0	0	0	-5454.28	
453.125	0	0	0	1604.52	0	453.125	0	
0	0	0	0	0	2255.56	21750.	-21750.	
21750.	0	0	0	453.125	21750.	921527.	0	
0	261806.	0	-5454.28	0	-21750.	0	1.40164×10^{6}	3
0	0	-4666.67	-1546.67	1546.67	0	0	0	1
0	0	0	0	-51.5556	0	0	0	
0	0	0	0	0	-725.	0	21750.	
0	0	0	0	0	0	-8026.67	0	
0	0	0	-51.5556	0	0	0	0	
0	0	0	0	0	-725.	-21750.	0	
0	0	0	0	0	0	0	-8026.67	

Solving the final system of global equations we get

```
\begin{split} \{\theta x_1 &= 0.000398634, \ \theta y_1 = -0.00015917, \ \theta z_1 = 0, \ u_2 = 0.000575402, \ v_2 = 0.000117025, \\ w_2 &= -0.0248276, \ \theta x_2 = -0.000799706, \ \theta y_2 = 0.000330328, \ \theta z_2 = 0, \ v_3 = 0.000117025, \\ w_3 &= -0.041634, \ \theta x_3 = -0.000799706, \ u_4 = 0.000575402, \ w_4 = -0.0557153, \ \theta y_4 = 0.000330328 \} \end{split}
```

Complete table of nodal values

	u	v	W	$\theta \mathbf{x}$	$ heta \mathbf{y}$	$\theta \mathbf{z}$
1	0	0	0	0.000398634	-0.00015917	0
2	0.000575402	0.000117025	-0.0248276	-0.000799706	0.000330328	0
3	0	0.000117025	-0.041634	-0.000799706	0	0
4	0.000575402	0	-0.0557153	0	0.000330328	0

Computation of reactions

Equation numbers of dof with specified values: {1, 2, 3, 13, 17, 18, 20, 22, 24}

Extracting equations {1, 2, 3, 13, 17, 18, 20, 22, 24} from the global system we have

75.7539	0	0	0	5454.28	0	-75.7539	0	0	0	5
0	6.2934	0	-453.125	0	0	0	-6.2934	0	-453.125	
0	0	805.556	0	0	0	0	0	-805.556	0	
0	0	0	0	0	0	-1546.67	0	0	0	
0	0	0	0	0	0	0	0	-21750.	0	435
0	0	0	0	0	0	0	1546.67	0	0	
0	0	0	0	0	0	0	-1546.67	0	0	
0	0	0	0	0	0	0	0	21750.	435000.	
0	0	0	0	0	0	-1546.67	0	0	0	

Substituting the nodal values and re-arranging

R_1)	75.7539	0	0	0	5454.28	0	-75.7539	0	0	0
R_2		0	6.2934	0	-453.125	0	0	0	-6.2934	0	-453. 1
R_3		0	0	805.556	0	0	0	0	0	-805.556	0
R ₄		0	0	0	0	0	0	-1546.67	0	0	0
R_5	=	0	0	0	0	0	0	0	0	-21750.	0
R ₆		0	0	0	0	0	0	0	1546.67	0	0
R ₇		0	0	0	0	0	0	0	-1546.67	0	0
R ₈		0	0	0	0	0	0	0	0	21750.	435000.
R_9)	(0	0	0	0	0	0	-1546.67	0	0	0

Carrying out computations, the reactions are as follows.

Label	dof	Reaction
R_1	\mathbf{u}_1	0.889955
R_2	\mathbf{v}_1	0.180999
R_3	\mathbf{w}_1	20.
R_4	\mathbf{u}_3	-0.889955
R_5	$ heta \mathbf{y_3}$	-171.846
R_6	$ heta \mathbf{z}_3$	0
R_7	\mathbf{v}_4	-0.180999
R_8	$\theta \mathbf{x_4}$	273.936
R_9	$ heta \mathbf{z_4}$	0

Sum of Reactions

dof: u
 0

 dof: v
 0

 dof: w
 20.

 dof:
$$\theta x$$
 273.936

 dof: θy
 -171.846

 dof: θz
 0

Solution for element 1

Nodal values in global coordinates, $\mathbf{d}^{T} = \{0, 0, 0, 0.000398634,$

-0.00015917, 0, 0.000575402, 0.000117025, -0.0248276, -0.000799706, 0.000330328, 0

Nodal values in local coordinates, $d_{\ell}^{T} = Td = \{0., 0., 0., 0., 0.000398634,$

-0.00015917, -0.0248276, 0.000575402, 0.000117025, 0., -0.000799706, 0.000330328

Axial effects:

Interpolation functions, $N_{ij}^{T} = \{1. -0.00694444t, 0.00694444t\}$

Axial displacement,
$$u(t) = N_u^T \begin{pmatrix} d_1 \\ d_7 \end{pmatrix} = -0.000172414 t$$

Axial force, EA du(t)/dt = -20.

Torsional effects:

Twist angle,
$$\psi(t) = N_u^T \begin{pmatrix} d_4 \\ d_{10} \end{pmatrix} = 0$$

Twisting moment, GJ $d\psi(t)/dt = 0$.

Bending about r-axis:

$$\begin{aligned} \boldsymbol{N}_{v}^{T} &= \left\{6.69796 \times 10^{-7} \ t^{3} - 0.000144676 \ t^{2} + 1, \ 0.0000482253 \ t^{3} - 0.0138889 \ t^{2} + t, \right. \\ &0.000144676 \ t^{2} - 6.69796 \times 10^{-7} \ t^{3}, \ 0.0000482253 \ t^{3} - 0.00694444 \ t^{2} \right\} \end{aligned}$$

$$\mathbf{v}(t) = \mathbf{N}_{\mathbf{v}}^{T} \begin{pmatrix} \mathbf{d}_{2} \\ \mathbf{d}_{6} \\ \mathbf{d}_{8} \\ \mathbf{d}_{12} \end{pmatrix} = 7.86875 \times 10^{-9} \ t^{3} - 0.00015917 \ t$$

Bending moment, $M_r = E I_r d^2 v(t)/dt^2 = 0.889955 t$

Shear force, $V_s = dM_r/dt = 0.889955$

Bending about s-axis:

$$\begin{aligned} \boldsymbol{N}_{w}^{T} &= \left\{6.69796 \times 10^{-7} \ t^{3} - 0.000144676 \ t^{2} + 1, \ -0.0000482253 \ t^{3} + 0.0138889 \ t^{2} - t, \right. \\ &\left. 0.000144676 \ t^{2} - 6.69796 \times 10^{-7} \ t^{3}, \ 0.00694444 \ t^{2} - 0.0000482253 \ t^{3} \right\} \end{aligned}$$

$$w(t) = \textbf{\textit{N}}_{w}^{T} \begin{pmatrix} d_{3} \\ d_{5} \\ d_{9} \\ d_{11} \end{pmatrix} = -1.94202 \times 10^{-8} \, t^{3} + 3.38615 \times 10^{-8} \, t^{2} + 0.000398634 \, t$$

Bending moment, $M_s = -EI_s d^2w(t)/dt^2 = -0.180999 t$

Shear force, $V_r = -dM_s/dt = 0.180999$

Solution for element 2

Nodal values in global coordinates, $\mathbf{d}^{T} = \{0.000575402, 0.000117025, -0.0248276, -0.000799706, 0.000330328, 0, 0, 0.000117025, -0.041634, -0.000799706, 0, 0\}$

Nodal values in local coordinates, $\boldsymbol{d}_{\ell}^{\mathrm{T}} = \boldsymbol{T}\boldsymbol{d} = \{0.000575402, 0.0248276, 0.000117025, -0.000799706, 0., 0.000330328, 0., 0.041634, 0.000117025, -0.000799706, 0., 0.\}$

Axial effects:

Interpolation functions, $N_{ij}^{T} = \{1. -0.0166667 t, 0.0166667 t\}$

Axial displacement,
$$u(t) = N_u^T \begin{pmatrix} d_1 \\ d_2 \end{pmatrix} = 0.000575402 - 9.59003 \times 10^{-6} t$$

Axial force, EA du(t)/dt = -0.889955

Torsional effects:

Twist angle,
$$\psi(t) = N_u^T \begin{pmatrix} d_4 \\ d_{10} \end{pmatrix} = -0.000799706$$

Twisting moment, GJ $d\psi(t)/dt = 8.70253 \times 10^{-16}$

Bending about r-axis:

$$N_{v}^{T} = \{9.25926 \times 10^{-6} t^{3} - 0.000833333 t^{2} + 1,$$

$$0.000277778\,t^3 - 0.0333333\,t^2 + t,\ 0.000833333\,t^2 - 9.25926 \times 10^{-6}\,t^3,\ 0.000277778\,t^3 - 0.0166667\,t^2\}$$

$$v(t) = \textbf{\textit{N}}_v^T \left(\begin{array}{c} d_2 \\ d_6 \\ d_8 \\ d_{12} \end{array} \right) = -6.3857 \times 10^{-8} \ t^3 + 2.99439 \times 10^{-6} \ t^2 + 0.000330328 \ t + 0.0248276$$

Fixed-end displacement solution, = $5.32141 \times 10^{-10} (60. - t)^2 t^2$

Transverse displacement, v(t) =

Bending moment, $M_r = E I_r d^2 v(t)/d$

$$t^2 = 1.305 \times 10^7 (6.3857 \times 10^{-9} t^2 - 7.66284 \times 10^{-7} t + 9.8202 \times 10^{-6})$$

Shear force, $V_s = dM_r/dt = 0.166667 t - 10$.

Bending about s-axis:

$$\textbf{\textit{N}}_{w}^{T} = \left\{9.25926 \times 10^{-6} \ t^{3} - 0.000833333 \ t^{2} + 1, \ -0.000277778 \ t^{3} + 0.0333333 \ t^{2} - t, \right. \\ 0.000833333 \ t^{2} - 9.25926 \times 10^{-6} \ t^{3}, \ 0.0166667 \ t^{2} - 0.000277778 \ t^{3} \right\}$$

$$\mathbf{w}(\mathbf{t}) = \mathbf{N}_{\mathbf{w}}^{\mathbf{T}} \begin{pmatrix} \mathbf{d}_3 \\ \mathbf{d}_5 \\ \mathbf{d}_9 \\ \mathbf{d}_{11} \end{pmatrix} = 0.000117025$$

Bending moment, $M_s = -EI_s d^2w(t)/dt^2 = 0$

Shear force,
$$V_r = -dM_s/dt = 0$$

Solution for element 3

Nodal values in global coordinates, $\boldsymbol{d}^T = \{0.000575402,\ 0.000117025,\ -0.0248276,\ -0.000799706,\ 0.000330328,\ 0,\ 0.000575402,\ 0,\ -0.0557153,\ 0,\ 0.000330328,\ 0\}$

Nodal values in local coordinates, $\boldsymbol{d}_{\ell}^{\mathrm{T}} = \boldsymbol{T}\boldsymbol{d} = \{0.000117025, -0.0248276, 0.000575402, 0.000330328, 0., -0.000799706, 0., -0.0557153, 0.000575402, 0.000330328, 0., 0.\}$

Axial effects:

Interpolation functions, $N_u^T = \{1. -0.0166667 t, 0.0166667 t\}$

Axial displacement,
$$u(t) = \textbf{N}_u^T\!\!\left(\!\!\!\begin{array}{c} d_1 \\ d_7 \end{array}\!\!\right) = 0.000117025 - 1.95042 \times 10^{-6} \, t$$

Axial force, EA du(t)/dt = -0.180999

Torsional effects:

Twist angle,
$$\psi(t) = N_{\rm u}^{\rm T} \begin{pmatrix} d_4 \\ d_{10} \end{pmatrix} = 0.000330328$$

Twisting moment, GJ $d\psi(t)/dt = 0$.

Bending about r-axis:

$$\begin{aligned} \textbf{\textit{N}}_{v}^{T} &= \left\{9.25926 \times 10^{-6} \ t^{3} - 0.000833333 \ t^{2} + 1, \right. \\ &0.000277778 \ t^{3} - 0.0333333 \ t^{2} + t, \ 0.000833333 \ t^{2} - 9.25926 \times 10^{-6} \ t^{3}, \ 0.000277778 \ t^{3} - 0.0166667 \ t^{2} \right\} \end{aligned}$$

$$v(t) = N_v^T \begin{pmatrix} d_2 \\ d_6 \\ d_8 \\ d_{12} \end{pmatrix} = 6.3857 \times 10^{-8} t^3 + 9.17092 \times 10^{-7} t^2 - 0.000799706 t - 0.0248276$$

Fixed-end displacement solution, = $-5.32141 \times 10^{-10} (60. - t)^2 t^2$

Transverse displacement, v(t) =

$$-5.32141\times 10^{-10}\,t^4 + 1.27714\times 10^{-7}\,t^3 - 9.98617\times 10^{-7}\,t^2 - 0.000799706\,t - 0.0248276$$

Bending moment,
$$M_r = E I_r d^2 v(t)/d$$

$$t^2 = 1.305 \times 10^7 \left(-6.3857 \times 10^{-9} \ t^2 + 7.66284 \times 10^{-7} \ t - 1.99723 \times 10^{-6} \right)$$

Shear force,
$$V_s = dM_r/dt = 10. - 0.166667 t$$

Bending about s-axis:

$$\begin{aligned} \textbf{\textit{N}}_{w}^{T} &= \left\{9.25926 \times 10^{-6}~t^{3} - 0.000833333~t^{2} + 1,~ -0.000277778~t^{3} + 0.0333333~t^{2} - t, \right. \\ &\left. 0.000833333~t^{2} - 9.25926 \times 10^{-6}~t^{3},~ 0.0166667~t^{2} - 0.000277778~t^{3} \right\} \end{aligned}$$

$$w(t) = \textbf{\textit{N}}_{w}^{T} \begin{pmatrix} d_{3} \\ d_{5} \\ d_{9} \\ d_{11} \end{pmatrix} = 0.000575402$$

Bending moment, $M_s = -EI_s d^2w(t)/dt^2 = 0$

Shear force, $V_r = -dM_s/dt = 0$

Forces & Moments at element ends

	X	y	Z	Axial force	V_s	$V_{\rm r}$	$M_{ m r}$	M_s	M_t
1	0	0	0	-20.	0.889955	0.180999	0	0	0
1	0	0	144.	-20.	0.889955	0.180999	128.154	-26.0639	0
0	0	0	144.	-0.889955	-10 .	0	128.154	0	0
۷	60.	0	144.	-0.889955	0	0	-171.846	0	0
9	0	0	144.	-0.180999	10.	0	-26.0639	0	0
3	0	60.	144.	-0.180999	0	0	273.936	0	0