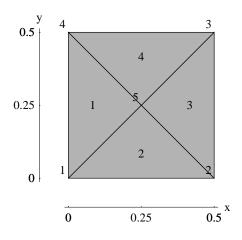
## CHAPTER SIX

## **Plates and Shells**

## Example 6.3 (p. 302): Using Triangles from SHELL63



 $1 \times 1$  plate h = 0.1 E = 10920 v = 0.3 q = 1

#### Essential boundary conditions:

$$w_1 = \theta_{x1} = \theta_{y1} = 0.$$
  
 $w_2 = \theta_{y2} = 0.$   
 $\theta_{x3} = \theta_{y3} = 0.$   
 $w_4 = \theta_{x4} = \theta_{y4} = 0.$ 

#### $An sysFiles \\ \ \ Chap 06 \\ \ \ \ Plate Ex 63.txt$

```
!* Example 6.3 Square plate subjected to a distributed load
!* 4 triangular plate element model
/PREP7
!*
ET,1,SHELL63
KEYOPT,1,1,0
KEYOPT,1,2,0
KEYOPT,1,3,1
KEYOPT,1,5,0
KEYOPT,1,6,0
KEYOPT,1,7,0
KEYOPT,1,8,0
KEYOPT,1,9,0
KEYOPT,1,11,0
R,1,0.1, , , , , ,
\mathsf{RMORE},\,,\,,\,,\,
RMORE
RMORE,,
!*
MPTEMP,,,,,,
MPTEMP,1,0
MPDATA,EX,1,,10920
MPDATA.PRXY.1..0.3
```

```
.... D....,. 1001,1,000
N,1,,,,,
N,2,.5,,,,,
N,3,0.5,.5,,,,
N,4,0,0.5,,,,
N,5,0.25,0.25,,,,
e,4,1,5,5
e,1,2,5,5
e,2,3,5,5
e,3,4,5,5
D,1, , , , , , ,UZ,ROTX,ROTY, , ,
D,2, , , , , , ,UZ,ROTY, , , ,
D,3, , , , , ,ROTX,ROTY, , , ,
D,4, , , , , , ,UZ,ROTX,ROTY, , ,
SFE,1,1,PRES, ,1, , ,
SFE,2,1,PRES, ,1, , ,
SFE,3,1,PRES, ,1, , ,
SFE,4,1,PRES, ,1, , ,
FINISH
/SOL
/STATUS,SOLU
SOLVE
FINISH
/POST1
!*
PRNSOL,U,Z
 PRINT U NODAL SOLUTION PER NODE
  ***** POST1 NODAL DEGREE OF FREEDOM LISTING *****
  LOAD STEP=
                 1 SUBSTEP=
   TIME= 1.0000 LOAD CASE=
  THE FOLLOWING DEGREE OF FREEDOM RESULTS ARE IN GLOBAL COORDINATES
     NODE
                UZ
           0.0000
        1
           0.0000
        3 0.19973E-02
           0.0000
        5 0.95695E-03
```

MAXIMUM ABSOLUTE VALUES

NODE 3 VALUE 0.19973E-02

#### PRINT S ELEMENT SOLUTION PER ELEMENT

#### \*\*\*\*\* POST1 ELEMENT NODAL STRESS LISTING \*\*\*\*\*

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

ELEMENT	'= 1	SHELL			
NODE	SX	SY	SZ	SXY	SYZ
SXZ 4 0.0000	-31.411	-9.4233	0.0000	6.2911	0.0000
0.0000	-15.558	-4.6673	0.0000	-4.4416	0.0000
5	11.780	17.486	0.0000	-7.3982	0.0000
5	11.780	17.486	0.0000	-7.3982	0.0000
0.0000	31.411	9.4233	-1.0000	-6.2911	0.0000
1	15.558	4.6673	-1.0000	4.4416	0.0000
5	-11.780	-17.486	-1.0000	7.3982	0.0000
5	-11.780	-17.486	-1.0000	7.3982	0.0000
0.0000					
0.0000					
ELEMENT		SHELL		QVV.	OV.
ELEMENT NODE	'= 2 SX	SHELL6 SY	53 SZ	SXY	SYZ
ELEMENT	SX			SXY -8.1132	SYZ 0.0000
ELEMENT NODE SXZ 1 0.0000	SX	SY	SZ		
ELEMENT NODE SXZ 1	SX -1.5201	SY -5.0671	SZ 0.0000	-8.1132	0.0000
ELEMENT NODE SXZ 1 0.0000 2 0.0000 5 0.0000	SX -1.5201 -1.9962	SY -5.0671 -6.6540	SZ 0.0000 0.0000	-8.1132 -2.3738	0.0000
ELEMENT NODE SXZ  1 0.0000 2 0.0000 5 0.0000 5 0.0000	SX -1.5201 -1.9962 11.360	SY -5.0671 -6.6540 12.997	SZ 0.0000 0.0000 0.0000	-8.1132 -2.3738 -6.0766	0.0000
ELEMENT NODE SXZ  1 0.0000 2 0.0000 5 0.0000	SX -1.5201 -1.9962 11.360 11.360	SY -5.0671 -6.6540 12.997	SZ 0.0000 0.0000 0.0000	-8.1132 -2.3738 -6.0766 -6.0766	0.0000 0.0000 0.0000

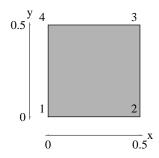
0.0000 5 -11.360 0.0000	-12.997	-1.0000	6.0766	0.0000
ELEMENT= 3 NODE SX	SHELL6 SY	SZ	SXY	SYZ
2 -0.32122	1.4791	0.0000	0.26681	0.0000
0.0000 3 22.013 0.0000	18.902	0.0000	0.55170	0.0000
5 9.9098 0.0000	9.5395	0.0000	-7.3982	0.0000
5 9.9098 0.0000	9.5395	0.0000	-7.3982	0.0000
2 0.32122 0.0000	-1.4791	-1.0000	-0.26681	0.0000
3 -22.013 0.0000	-18.902	-1.0000	-0.55170	0.0000
5 -9.9098 0.0000	-9.5395	-1.0000	7.3982	0.0000
5 -9.9098 0.0000	-9.5395	-1.0000	7.3982	0.0000

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

ELEMEN	T= 4	SHEL	L63		
NODE	SX	SY	SZ	SXY	SYZ
SXZ					
3	33.288	23.719	0.0000	-3.7808	0.0000
0.0000					
4	-34.153	-26.603	0.0000	0.92759	0.0000
0.0000					
5	10.329	14.029	0.0000	-8.7198	0.0000
0.0000					
5	10.329	14.029	0.0000	-8.7198	0.0000
0.0000					
3	-33.288	-23.719	-1.0000	3.7808	0.0000
0.0000					
4	34.153	26.603	-1.0000	-0.92759	0.0000
0.0000					
5	-10.329	-14.029	-1.0000	8.7198	0.0000
0.0000					

# Example 6.4 (p. 321): Square plate subjected to distributed load using quadrilateral element — SHELL43

#### ■ One element solution



 $1 \times 1$  plate h = 0.1 E = 10920 v = 0.3 q = 1

Essential boundary conditions  $w_1 = \theta_{x1} = \theta_{y1} = w_2 = \theta_{y2} = \theta_{x3} = \theta_{y3} = w_4 = \theta_{x4} = \theta_{y4} = 0$ .

AnsysFiles\\Chap06\\PlateEx64.txt

- !\* Example 6.4 Square plate subjected to a distributed load
- !\* One plate element model

/PREP7

۱\*

ET,1,SHELL43

!\*

KEYOPT,1,1,0

KEYOPT,1,2,0

KEYOPT,1,3,1

KEYOPT,1,5,0

KFYOPT 160

```
KEYOPT,1,7,0
KEYOPT,1,8,0
KEYOPT,1,9,0
KEYOPT,1,11,0
!*
R,1,0.1,\,,\,,\,,\,,\,
RMORE, , , ,
RMORE
RMORE,,
!*
!*
MPTEMP,,,,,,
MPTEMP,1,0
MPDATA,EX,1,,10920
MPDATA,PRXY,1,,0.3
k,1,,,,,,
k,2,.5,,,,,
k,3,0.5,.5,,,,
k,4,0,0.5,,,,
a,1,2,3,4
esize,.5
amesh,1
DL,1, ,UZ,
DL,1, ,ROTY,
DL,2, ,ROTY,
DL,3, ,ROTX,
DL,4, ,UZ,
DL,4, ,ROTY,
DL,4, ,ROTX,
SFA,1,1,PRES,1
FINISH
/SOL
/STATUS,SOLU
SOLVE
FINISH
/POST1
!*
PRNSOL,U,Z
```

#### PRINT U NODAL SOLUTION PER NODE

\*\*\*\*\* POST1 NODAL DEGREE OF FREEDOM LISTING \*\*\*\*\*

LOAD STEP= 1 SUBSTEP= 1 TIME= 1.0000 LOAD CASE= 0

THE FOLLOWING DEGREE OF FREEDOM RESULTS ARE IN GLOBAL COORDINATES

NODE UZ

1 0.0000

2 0.0000

3 0.50629E-03

4 0.0000

MAXIMUM ABSOLUTE VALUES

NODE 3

VALUE 0.50629E-03

PRINT S ELEMENT SOLUTION PER ELEMENT

\*\*\*\*\* POST1 ELEMENT NODAL STRESS LISTING \*\*\*\*\*

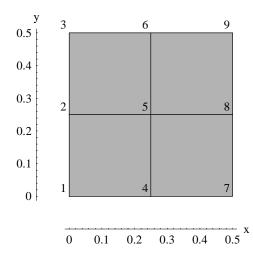
LOAD STEP= 1 SUBSTEP= 1

TIME= 1.0000 LOAD CASE= 0

SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

ELEMENT	= 1	SHELL43			
NODE	SX	SY	SZ	SXY	SYZ
SXZ					
1	0.15266E-13	0.50626E-13	0.0000	-0.80112	
-0.83267E	-16-0.11102E	-14			
2	0.68667	2.2889	0.0000	-0.80112	0.20600
-0.11102E	-14				
3	0.68667	2.2889	0.0000	-0.17708E-13	0.20600
3.5440					
4	0.15266E-13	0.50626E-13	0.0000	-0.17708E-13	-0.27756E-15
3.5440					
1	-0.15266E-13	-0.50626E-13	-1.0000	0.80112	
-0.16653E	-15-0.11102E	-14			
2	-0.68667	-2.2889	-1.0000	0.80112	0.20600
-0.11102E	-14				
3	-0.68667	-2.2889	-1.0000	0.17708E-13	0.20600
3.5440					
4	-0.15266E-13	-0.50626E-13	-1.0000	0.17708E-13	0.27756E-16
3.5440					

### ■ Four element solution (p. 323)



 $1 \times 1$  plate h = 0.1 E = 10920 v = 0.3 q = 1

 $An sysFiles \verb|\Chap06| \verb|\PlateEx64FourElem.txt|$ 

```
!* Example 6.4 Square plate subjected to a distributed load
!* Four plate element model
/PREP7
!*
ET,1,SHELL43
!*
KEYOPT,1,1,0
KEYOPT,1,2,0
KEYOPT,1,3,1
KEYOPT,1,5,0
KEYOPT,1,6,0
KEYOPT,1,6,0
KEYOPT,1,7,0
KEYOPT,1,7,0
KEYOPT,1,9,0
KEYOPT,1,9,0
KEYOPT,1,11,0
!*
```

```
R,1,0.1, , , , , ,
RMORE, , , ,
RMORE
RMORE,,
!*
!*
\mathsf{MPTEMP},,,,,,
MPTEMP,1,0
MPDATA,EX,1,,10920
MPDATA,PRXY,1,,0.3
k,1,,,,,,
k,2,.5,,,,,
k,3,0.5,.5,,,,
k,4,0,0.5,,,,
a,1,2,3,4
esize,.25
amesh,1
DL,1, ,UZ,
DL,1, ,ROTY,
DL,2, ,ROTY,
DL,3, ,ROTX,
DL,4, ,UZ,
DL,4, ,ROTY,
DL,4, ,ROTX,
SFA,1,1,PRES,1
FINISH
/SOL
/STATUS,SOLU
SOLVE
FINISH
/POST1
PRNSOL,U,Z
 PRINT U
             NODAL SOLUTION PER NODE
   ***** POST1 NODAL DEGREE OF FREEDOM LISTING *****
  LOAD STEP= 1 SUBSTEP=
   TIME= 1.0000 LOAD CASE=
```

#### THE FOLLOWING DEGREE OF FREEDOM RESULTS ARE IN GLOBAL COORDINATES

NODE UZ

1 0.0000
2 0.0000
3 0.0000
4 0.20405E-02
5 0.14762E-02
6 0.0000
7 0.11192E-02
8 0.0000
9 0.81890E-03

MAXIMUM ABSOLUTE VALUES

NODE 4 VALUE 0.20405E-02

PRINT S ELEMENT SOLUTION PER ELEMENT

\*\*\*\*\* POST1 ELEMENT NODAL STRESS LISTING \*\*\*\*\*

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

	ELEMENT:	= 1	SHELL43			
	NODE	SX	SY	SZ	SXY	SYZ
S	XZ					
	1 .	-0.23448E-	-12-0.24147E-14	0.0000	-3.2821	
-	0.33307E	-15-0.8881	L8E-15			
	3	1.0061	3.3536	0.0000	-7.3449	0.23464
-	0.88818E	-15				
	-	-10.602	-0.12877	0.0000	-6.1711	0.23464
3	.0004					
	-	-11.608	-3.4824	0.0000	-2.1083	-0.49960E-15
3	.0004					
	1		-12 0.24147E-14	-1.0000	3.2821	
-		-15-0.1554				
			-3.3536	-1.0000	7.3449	0.23464
-	0.11102E	-14				
	9	10.602	0.12877	-1.0000	6.1711	0.23464
3	.0004					
	8	11.608	3.4824	-1.0000	2.1083	0.47184E-15
3	.0004					
		_				
	ELEMENT:	_	SHELL43			
	NODE	SX	SY	SZ	SXY	SYZ
S.	XZ					

	3.3536	0.0000	-6.1937	0.23464
15				
1.5759	5.2529	0.0000	-2.1309	1.9430
-15				
	0 7252	0 0000	1 4661	1.9430
13.104	0.7333	0.0000	-1.4001	1.9430
12.614	6.8360	0.0000	-5.5289	0.23464
-1.0061	-3.3536	-1.0000	6.1937	0.23464
	3.3333	2.0000	0.1337	0.20101
	F 0F00	1 0000	0 1200	1 0420
	-5.2529	-1.0000	2.1309	1.9430
-15				
-13.184	-8.7353	-1.0000	1.4661	1.9430
-12 614	-6 8360	-1 0000	5 5289	0 23464
-12.014	-0.0300	-1.0000	3.3209	0.23404
2	SHELL4	2		
= 3	SUPTIT	: 3		
= 3 SX	SY	sz	SXY	SYZ
			SXY	SYZ
SX	SY	SZ		
SX		SZ		SYZ 0.10825E-14
SX -11.608	SY -3.4824	SZ		0.10825E-14
SX -11.608	SY	SZ		0.10825E-14
SX -11.608	SY -3.4824	SZ 0.0000	-2.1083	0.10825E-14
SX -11.608 -9.8009	SY -3.4824 2.5413	SZ 0.0000 0.0000	-2.1083 -3.6869	0.10825E-14 -0.18856
SX -11.608 -9.8009	SY -3.4824	SZ 0.0000 0.0000	-2.1083	0.10825E-14 -0.18856
SX -11.608 -9.8009 -14.311	SY -3.4824 2.5413 1.1882	SZ 0.0000 0.0000 0.0000	-2.1083 -3.6869 -1.5786	0.10825E-14 -0.18856 -0.18856
SX -11.608 -9.8009 -14.311	SY -3.4824 2.5413 1.1882	SZ 0.0000 0.0000 0.0000	-2.1083 -3.6869 -1.5786	0.10825E-14 -0.18856
SX -11.608 -9.8009 -14.311	SY -3.4824 2.5413 1.1882	SZ 0.0000 0.0000 0.0000	-2.1083 -3.6869 -1.5786	0.10825E-14 -0.18856 -0.18856
SX -11.608 -9.8009 -14.311 -16.118	SY -3.4824 2.5413 1.1882	SZ 0.0000 0.0000 0.0000	-2.1083 -3.6869 -1.5786 -0.81268E-1	0.10825E-14 -0.18856 -0.18856
SX -11.608 -9.8009 -14.311 -16.118	SY -3.4824 2.5413 1.1882 -4.8355	SZ 0.0000 0.0000 0.0000	-2.1083 -3.6869 -1.5786 -0.81268E-1	0.10825E-14 -0.18856 -0.18856 13-0.11657E-14
SX -11.608 -9.8009 -14.311 -16.118 11.608	SY -3.4824 2.5413 1.1882 -4.8355 3.4824	SZ 0.0000 0.0000 0.0000 -1.0000	-2.1083 -3.6869 -1.5786 -0.81268E-3	0.10825E-14 -0.18856 -0.18856 13-0.11657E-14 -0.24980E-15
SX -11.608 -9.8009 -14.311 -16.118 11.608	SY -3.4824 2.5413 1.1882 -4.8355	SZ 0.0000 0.0000 0.0000 -1.0000	-2.1083 -3.6869 -1.5786 -0.81268E-1	0.10825E-14 -0.18856 -0.18856 13-0.11657E-14 -0.24980E-15
SX -11.608 -9.8009 -14.311 -16.118 11.608	SY -3.4824 2.5413 1.1882 -4.8355 3.4824	SZ 0.0000 0.0000 0.0000 -1.0000	-2.1083 -3.6869 -1.5786 -0.81268E-3	0.10825E-14 -0.18856 -0.18856 13-0.11657E-14 -0.24980E-15
SX -11.608 -9.8009 -14.311 -16.118 11.608 9.8009	SY -3.4824 2.5413 1.1882 -4.8355 3.4824	SZ 0.0000 0.0000 0.0000 -1.0000	-2.1083 -3.6869 -1.5786 -0.81268E-3	0.10825E-14 -0.18856 -0.18856 13-0.11657E-14 -0.24980E-15 -0.18856
SX -11.608 -9.8009 -14.311 -16.118 11.608 9.8009	SY -3.4824 2.5413 1.1882 -4.8355 3.4824 -2.5413	SZ 0.0000 0.0000 0.0000 -1.0000	-2.1083 -3.6869 -1.5786 -0.81268E-2 2.1083 3.6869	0.10825E-14 -0.18856 -0.18856 13-0.11657E-14 -0.24980E-15 -0.18856
SX -11.608 -9.8009 -14.311 -16.118 11.608 9.8009 14.311	SY -3.4824 2.5413 1.1882 -4.8355 3.4824 -2.5413 -1.1882	SZ 0.0000 0.0000 0.0000 -1.0000 -1.0000	-2.1083 -3.6869 -1.5786 -0.81268E-2.1083 3.6869 1.5786	0.10825E-14 -0.18856 -0.18856 13-0.11657E-14 -0.24980E-15 -0.18856 -0.18856
SX -11.608 -9.8009 -14.311 -16.118 11.608 9.8009 14.311	SY -3.4824 2.5413 1.1882 -4.8355 3.4824 -2.5413 -1.1882	SZ 0.0000 0.0000 0.0000 -1.0000 -1.0000	-2.1083 -3.6869 -1.5786 -0.81268E-2.1083 3.6869 1.5786	0.10825E-14 -0.18856 -0.18856 13-0.11657E-14 -0.24980E-15 -0.18856
	15 1.5759 -15 13.184 12.614 -1.0061 -15 -1.5759 -15 -13.184 -12.614	15 1.5759 5.2529 -15 13.184 8.7353 12.614 6.8360 -1.0061 -3.3536 -15 -1.5759 -5.2529 -15 -13.184 -8.7353 -12.614 -6.8360	15 1.5759 5.2529 0.0000 -15 13.184 8.7353 0.0000 12.614 6.8360 0.0000 -1.0061 -3.3536 -1.0000 -1.5759 -5.2529 -1.0000 -15 -13.184 -8.7353 -1.0000 -12.614 -6.8360 -1.0000	1.5759 5.2529 0.0000 -2.1309 -15

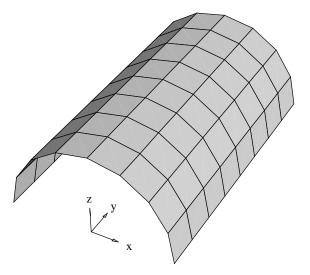
LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

ELEMENT=	= 4	SHELL4	3		
NODE	SX	SY	SZ	SXY	SYZ
SXZ					
9	13.415	9.5061	0.0000	-3.0448	-0.18856

0.73810					
5	14.672	13.695	0.0000	-1.4661	0.45397
0.73810					
4	19.182	15.048	0.0000	-0.67502E-13	0.45397
1.1463					
7	17.926	10.859	0.0000	-1.5786	-0.18856
1.1463					
9	-13.415	-9.5061	-1.0000	3.0448	-0.18856
0.73810					
5	-14.672	-13.695	-1.0000	1.4661	0.45397
0.73810					
4	-19.182	-15.048	-1.0000	0.67502E-13	0.45397
1.1463					
7	-17.926	-10.859	-1.0000	1.5786	-0.18856
1.1463					

## Shell analysis example

This example is not included in the printed book.



Cylinderical barrel shell. Arc angle = 80 °, symmetric about y-z plane. Radius = 25 m. Length = 50 m. Thickness = 0.25m.  $E = 4.32 \times 10^8~N/m^2$  and v = 0. Load due to gravity. Mass density =  $36.7347~kg/m^3$ . Acceleration due to gravity =  $9.8~m/s^2$ .

The shell is supported (u, w,  $\theta_z$  = 0) along the two curved sides only. The sides along the y-direction are free

Taking advantage of symmetry we can model a 1/4 of the shell.

The following analytical solution of the problem is available.

Maximum deflection (at the center of longitudinal edge) = 0.3024 m (Cook et al, Concepts and Applications of finite element analysis, 4th Edition p. 584, Wiley 2002)

#### ■ 2×2 Mesh

AnsysFiles\\Chap06\\ShellEx4Elem.txt

```
!* Shell analysis example. p. 331
!* 2x2 Mesh
/PREP7
ET,1,SHELL143
KEYOPT,1,2,0
KEYOPT,1,3,1
KEYOPT,1,4,0
KEYOPT,1,5,0
KEYOPT,1,6,0
R,1,0.25
MP,EX,1,4.32e8
                ! MATERIAL PROPERTIES
MP,NUXY,1,0.0
MP,DENS,1,36.7347
CSYS,1
K,1,25,50
K,2,25,50,25
               ! DEFINE KEYPOINTS AND AREA
K,3,25,90
K,4,25,90,25
A,1,3,4,2
ESIZE,,2
AMESH,1
CSYS,0
              ! SWITCH BACK TO GLOBAL CARTESIAN C.S.
DL,3, ,UX,
DL,3, ,UY,
DL,3, ,ROTZ,
DL,
      2, ,SYMM
DL,
      1, ,SYMM
ACEL,,9.8
FINISH
/SOLU
SOLVE
FINISH
/POST1
             NODAL SOLUTION PER NODE
 PRINT U
  ***** POST1 NODAL DEGREE OF FREEDOM LISTING *****
```

LOAD STEP= 1 SUBSTEP= 1 TIME= 1.0000 LOAD CASE= 0

THE FOLLOWING DEGREE OF FREEDOM RESULTS ARE IN GLOBAL COORDINATES

NODE UY

1 -0.35763
2 0.52439E-01
3 -0.74481E-01
4 0.0000
5 0.36954E-01
6 0.0000
7 0.0000
8 -0.26099

MAXIMUM ABSOLUTE VALUES

9 -0.53222E-01

NODE 1 VALUE -0.35763

PRINT S ELEMENT SOLUTION PER ELEMENT

\*\*\*\*\* POST1 ELEMENT NODAL STRESS LISTING \*\*\*\*\*

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

1	SHELL143			
I SY		SZ	SXY	SYZ
511. 242	85. 5	561434	40837.	56824.
511. 242	2859	99878	40837.	52360.
46. 193	8869	99878:	32477	3795.5
46. 193	886. 5	56143:	32477.	667.90
82250	013. 0.	.20592E+06	44549.	32064.
82250	)136	59575.	44549.	33837.
11209	9336	59575.	37358	65321.
511209	933. 0.	.20592E+06	37358	67094.
	SY 11. 242 11. 242 46. 193 46. 193 82250 82250	SY  11. 24285. 5  11. 242855  46. 193865  46. 19386. 5  8225013. 0  82250136  11209336	SY SZ  11. 24285. 56143  11. 2428599878  46. 1938699878  46. 19386. 56143  8225013. 0.20592E+06  822501369575.  112093369575.	SY SZ SXY  11. 24285. 5614340837.  11. 242859987840837.  46. 193869987832477  46. 19386. 5614332477.  8225013. 0.20592E+06 44549.  822501369575. 44549.  112093369575. 37358

ELEMENT=	= 2	SHELL143	3		
NODE SXZ	SX	SY	SZ	SXY	SYZ
	0.16916E+06	5271.2	-99948.	-29861.	-4669.2
2 45698.	0.16916E+06	5271.2	48850.	-29861.	-8408.5
5 -59787.	0.11572E+06	3525.8	48850.	-20200.	10191.
9 -78589.	0.11572E+06	3525.8	-99948.	-20200.	13931.
	0.18905E+06	-5866.1	-69505.	33302.	-11102.
2 - 45698.	0.18905E+06	-5866.1	27989.	33302.	-8408.5
	0.13904E+06	-4394.9	27989.	24721.	3778.3
	0.13904E+06	-4394.9	-69505.	24721.	1084.6
373311					
		SHELL143			
NODE SXZ	SX	SY	SZ	SXY	SYZ
8 -0.15179E+	54346.	19386.	3359.7	-32477.	91296.
		19386.	-43932	-32477.	74008.
-0.13221E+		19300.	13332.	32177.	71000.
		-0.77520E-05	-43932.	0.13390E-04	56987.
-0.10272E+		0 775405 05	3359.7	0 13304E 04	74075
-0.12231E+		-U.//548E-U5	3359.7	U.13394E-U4	74275.
		-20933.	0.10842E+06	37358.	-25325.
9	-66611.	-20933.	-28383.	37358.	-14608.
21281.		0 600000 05	00000	0 118545 04	62245
7 - 0.10657E+0		-U.68U/8E-U5	-28383.	U.11/54E-04	-6384/.
6 - 0.13549E+0		-0.68090E-05	0.10842E+06	0.11757E-04	-74565.

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

ELEMENT	Γ=	4		SHELL14	3				
NODE	5	SX	SY	7	SZ		SXY	SYZ	
SXZ									
9	0.1	11572E+	06 352	25.8	-43872		20200.	6563	. 9
-37063.									
5	0.1	11572E+	06 352	25.8	20477		20200.	-1403	. 0
3584.4									
4	-0.2	22700E-	04-0.66	795E-06	20477	. (	).38954E-05	6640	. 7
-42033.									
7	-0.2	22728E-	04-0.66	903E-06	-43872	. (	39009E-05	14608	В.
-82681.									
9	-0.1	13904E+	06 -439	94.9	-28443		24721.	-15693	1.
89148.									
5	-0.1	13904E+	06 -439	94.9	12373		24721.	-7815	. 9
39954.									
4	-0.2	28402E-	04-0.84	1558E-06	12373	. (	.49018E-05	-2714	. 0
11020.									
7	-0.2	28435E-	04-0.84	1643E-06	-28443	. (	0.49072E-05	-10589	9.
60213.									

#### ■ 4×4 Mesh

 $An sys Files \verb|\Chap06| \verb|\ShellEx16Elem.txt|$ 

```
!* Shell analysis example. p. 331
!* 4x4 Mesh
/PREP7
ET,1,SHELL143
KEYOPT,1,2,0
KEYOPT,1,3,1
KEYOPT,1,4,0
KEYOPT,1,5,0
KEYOPT,1,6,0
R,1,0.25
MP,EX,1,4.32e8
                ! MATERIAL PROPERTIES
MP,NUXY,1,0.0
MP,DENS,1,36.7347
CSYS,1
K,1,25,50
K,2,25,50,25
               ! DEFINE KEYPOINTS AND AREA
K,3,25,90
K,4,25,90,25
A,1,3,4,2
ESIZE,,4
AMESH,1
CSYS,0
              ! SWITCH BACK TO GLOBAL CARTESIAN C.S.
DL,3, ,UX,
DL,3, ,UY,
DL,3, ,ROTZ,
DL,
      2, ,SYMM
DL,
      1, ,SYMM
ACEL,,9.8
FINISH
/SOLU
SOLVE
FINISH
/POST1
             NODAL SOLUTION PER NODE
 PRINT U
  ***** POST1 NODAL DEGREE OF FREEDOM LISTING *****
```

```
LOAD STEP= 1 SUBSTEP=
TIME= 1.0000 LOAD CASE= 0
```

THE FOLLOWING DEGREE OF FREEDOM RESULTS ARE IN GLOBAL COORDINATES

```
NODE
     1 -0.28483
     2 0.42346E-01
     3 -0.17722
     4 -0.69604E-01
      5 0.11965E-01
         0.0000
     7 0.39168E-01
     8 0.29880E-01
     9 0.15866E-01
    10
         0.0000
    11
         0.0000
    12
         0.0000
        0.0000
    13
    14 -0.11710
    15 -0.20878
    16 -0.26549
    17 -0.16472
    18 -0.12832
    19 -0.71072E-01
     20 -0.64348E-01
    21 -0.49446E-01
    22 -0.27056E-01
    23 0.11195E-01
    24 0.86716E-02
    25 0.45164E-02
MAXIMUM ABSOLUTE VALUES
```

NODE VALUE -0.28483

PRINT S ELEMENT SOLUTION PER ELEMENT

\*\*\*\*\* POST1 ELEMENT NODAL STRESS LISTING \*\*\*\*\*

LOAD STEP= 1 SUBSTEP= TIME= 1.0000 LOAD CASE= 0 SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

THE FOLLOWING X,Y,Z VALUES ARE IN GLOBAL COORDINATES

ELEMENT= ELEMENT= 1 SHELL143

NODE SX SY SZ SXY SYZ SXZ

1	4980.6	3033.6	0.17891E+06	-3909.9	62502.
-87973. 3	4980.6	3033.6	-65395.	-3909.9	61516.
-88741. 17	5117.6	3077.6	-65395.	-3989.3	-38970.
54768. 16	5117.6	3077.6	0.17891E+06	-3989.3	-37984.
55536. 1	-8897.9	-3770.9	0.29797E+06	5807.9	52993.
-74392. 3	-8897.9	-3770.9	8021.3	5807.9	52027.
-75190. 17	-8690.5	-3692.3	8021.3	5679.2	-67233.
95132. 16	-8690.5	-3692.3	0.29797E+06	5679.2	-66268.
95930.					
ELEMENT	= 2	SHELL143	3		
	SX	SY	SZ	SXY	SYZ
3	43651.	10421.	-66075.	-21351.	11576.
-24421. 4	43651.	10421.	-84280.	-21351.	11086.
-24071. 20	42445.	10122.	-84280.	-20749.	5569.1
-12239. 17	42445.	10122.	-66075.	-20749.	6058.6
-12589. 3	-57583.	-11592.	8701.4	25855.	4584.6
-9428.3 4	-57583.	-11592.	-53571.	25855.	4686.9
-10347. 20	-55489.	-11174.	-53571.	24918.	-14185.
30125. 17			8701.4	24918.	
31044.	33103.	111/11	0,01.1	21310.	11200.
ELEMENT	= 3	CHETT 1 / 1	2		
NODE	= 3 SX	SHELL143 SY	SZ	SXY	SYZ
	0.11323E+06	8536.1	-84288.	-31098.	-1848.9
6809.5	0.11323E+06	8536.1	-21796.	-31098.	-2637.9
	0.10661E+06	8014.6	-21796.	-29238.	8960.6
-34111. 20	0.10661E+06	8014.6	-84288.	-29238.	9749.6
-36477. 4	-0.13558E+06	-9327.4	-53563.	35569.	-5768.0
21436.					

5	-0.13558E+06	-9327.4	-25510.	35569.	-5117.8
18431.					
23	-0.12732E+06	-8780.5	-25510.	33442.	88.815
-1000.5					
20	-0.12732E+06	-8780.5	-53563.	33442.	-561.36
2004.5					

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

	ELEMENT	7= 4	SHELI	143		
				SZ	SXY	SYZ
SX	Z					
	5	0.15932E+06	1262.5	-21591.	-14184.	-467.19
51	.93.7					
٥٦		0.15932E+06	1262.5	12806.	-14184.	-1004.2
95	20.3	0 146025.06	1160 6	12806.	12060	1115 6
_ 1	5052.	0.146926+06	1160.6	12000.	-13060.	1145.6
_		0.14692E+06	1160.6	-21591.	-13060.	1682.6
-1	9378.					
	5	-0.18490E+06	-1372.3	-25716.	15931.	-1302.3
14	739.					
		-0.18490E+06	-1372.3	-4623.8	15931.	-1004.2
	20.3					
			-1265.4	-4623.8	14669.	314.02
	547.2		1065 4	-25716.	14660	15 026
	28.41	-U.1/UUZE+U6	-1265.4	-25/16.	14669.	15.936
J	20.41					
	ELEMENT	C= 5	SHELI	L143		
	NODE	SX	SY	SZ	SXY	SYZ
SX	Z					
	16	5117.6	3077.6	0.15616E+06	-3989.3	81400.
- 0	.11246E					
			3077.6	-62101.	-3989.3	78425.
	.11448E		2060 0	60101	2020 5	11250
	729.	4990.9	3068.8	-62101.	-3938.7	-11350.
		4990.9	3068 8	0.15616E+06	_3938 7	-8375 6
	754.	1990.9	3000.0	0.130101100	3330.7	0373.0
		-8690.5	-3692.3	0.26747E+06	5679.2	34582.
- 4	5596.					
	17	-8690.5	-3692.3	4998.7	5679.2	31304.

-9836.6	-4201.0	4998.7	6443.6	-76657.
06				
-9836.6	-4201.0	0.26747E+0	6 6443.6	-73379.
06				
			~	
SX	SY	SZ	SXY	SYZ
42445.	10122.	-62699.	-20749.	27999.
42445.	10122.	-72690.	-20749.	25983.
35722.	8504.3	-72690.	-17447.	22955.
35722.	8504.3	-62699.	-17447.	24971.
-55489.	-11174.	5596.2	24918.	-6242.0
-55489.	-11174.	-47006.	24918.	-6210.5
-50795.	-10308.	-47006.	22896.	-22152.
-50795.	-10308.	5596.2	22896.	-22184.
	06 -9836.6 06 '= 6 SX 42445. 42445. 35722. -55489. -55489.	06 -9836.6 -9836.6 -4201.0 06  SHELL1 SX SY 42445. 10122. 42445. 10122. 35722. 8504.3 35722. 8504.3 -55489111745548910308.	06 -9836.6 -4201.0 0.26747E+0 06  SHELL143 SX SY SZ 42445. 1012262699. 42445. 1012272690. 35722. 8504.3 -72690. 35722. 8504.3 -626995548911174. 5596.2 -507951030847006.	-9836.6

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

ELEMENT	7= 7	SHEL	L143		
NODE	SX	SY	SZ	SXY	SYZ
SXZ					
20	0.10661E+06	8014.6	-72684.	-29238.	6413.9
-23917.					
23	0.10661E+06	8014.6	-16961.	-29238.	3704.5
-15367.					
24	82738.	6181.6	-16961.	-22620.	14047.
-53965.					
21	82738.	6181.6	-72684.	-22620.	16756.
-62515.					
20	-0.12732E+06	-8780.5	-47011.	33442.	-11515.
42994.					
23	-0.12732E+06	-8780.5	-21985.	33442.	-9651.9
34480.					

24 -0.10391E+06 17145.	-7219.1	-21985.	27392.	-5007.0
21 -0.10391E+06	-7219.1	-47011.	27392.	-6869.8
25659.				
ELEMENT= 8	SHELL14	3		
NODE SX	SY	SZ	SXY	SYZ
SXZ 23 0.14692E+06	1160.6	-16782.	-13060.	911.45
-9962.5 7 0.14692E+06	1160.6	11995.	-13060.	-666.85
3265.4	1160.6	11995.	-13060.	-000.03
8 0.10904E+06	856.14	11995.	-9662.5	1131.7
-17292. 24 0.10904E+06 -30520.	856.14	-16782.	-9662.5	2710.0
23 -0.17002E+06	-1265.4	-22164.	14669.	-2265.4
26349. 7 -0.17002E+06	-1265.4	-4143.6	14669.	-1498.4
12770. 8 -0.13131E+06	-983 56	-4143 6	11365.	-372.11
-103.50	-903.30	-4143.0	11303.	-3/2.11
24 -0.13131E+06 13475.	-983.56	-22164.	11365.	-1139.1
ELEMENT= 9	SHELL14	3		
NODE SX	SY	SZ	SXY	SYZ
SXZ	2060 0	0 100000 06	2020 5	0.10.50
15 4990.9 -0.12916E+06	3068.8	0.10099E+06	-3938.7	94868.
18 4990.9	3068.8	-52874.	-3938.7	89236.
-0.13182E+06 19 3003.6	2036.0	-52874.	2505 4	25949.
-41433.	2036.0	-52674.	-2303.4	23343.
	2036.0	0.10099E+06	-2505.4	31582.
-38775. 15 -9836.6	-4201.0	0.20716E+06	6443.6	9752.3
-7599.2				
18 -9836.6	-4201.0	3270.5	6443.6	4832.3
-11276. 19 -9432.6	-4061.4	3270.5	6202.5	-79030.
0.10849E+06	4061.4	0 000160 06	6000 5	E4110
14 -9432.6 0.11217E+06	-4061.4	0.20716E+06	6202.5	-74110.

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

THE FOLLOWING X,Y,Z VALUES ARE IN GLOBAL COORDINATES

ELEMENT	C= 10	SHELI	L143		
NODE	SX	SY	SZ	SXY	SYZ
SXZ 18	35722.	8504.3	-53270.	-17447.	42656.
-89431. 21	35722.	8504.3	-50363.	-17447.	38384.
-83625. 22	19334.	4619.3	-50363.	-9460.9	39265.
-85514. 19	19334.	4619.3	-53270.	-9460.9	43537.
-91320. 18	-50795.	-10308.	3666.9	22896.	-18570.
41868. 21	-50795.	-10308.	-32075.	22896.	-17336.
35866. 22	-36485.	-7518.2	-32075.	16568.	-28168.
59095. 19	-36485.	-7518.2	3666.9	16568.	-29401.
65097.					
ELEMENT	C= 11	SHELI	L143		
NODE SXZ	SX	SY	SZ	SXY	SYZ
21 -52050.	82738.	6181.6	-50360.	-22620.	13754.
24 -37332.	82738.	6181.6	-10890.	-22620.	9304.6
25 -64672.	41734.	3104.8	-10890.	-11385.	16630.
22 - 79389.	41734.	3104.8	-50360.	-11385.	21080.
	-0.10391E+06	-7219.1	-32078.	27392.	-16371.
	-0.10391E+06	-7219.1	-14079.	27392.	-12938.
25 33209.	-63399.	-4443.5	-14079.	16785.	-9596.8
22 47912.	-63399.	-4443.5	-32078.	16785.	-13030.
ELEMENT	S= 12 SX	SHELI SY	5143 SZ	SXY	SYZ
SXZ 24	0.10904E+06	856.14	-10763.	-9662.5	1944.6
-22665. 8	0.10904E+06	856.14	7828.1	-9662.5	-363.14

-3132.2					
9	53084.	414.87	7828.1	-4693.1	798.82
-16413.					
25	53084.	414.87	-10763.	-4693.1	3106.6
-35946.					
24	-0.13131E+06	-983.56	-14206.	11365.	-2978.2
33602.					
8	-0.13131E+06	-983.56	-1956.7	11365.	-1866.9
14056.					
9	-75596.	-570.08	-1956.7	6564.9	-1101.4
5306.1					
25	-75596.	-570.08	-14206.	6564.9	-2212.6
24852.					

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

ELEM	ENT=		13	SHELL1	43		
NO	DE	SX		SY	SZ	SXY	SYZ
SXZ							
			6	2036.0	31395.	-2505.4	98547.
-0.131		-	_	2026 0	22722	-2505.4	90402.
-0.134			6	2036.0	-23/23.	-2505.4	90402.
		-	34E-04-	0 23015E-0	4 -23723	0.32488E-04	67731
-0.102			712 01	0.230131 0	1 23,23.	0.321002 01	07731.
			6E-04-	0.23028E-0	4 31395.	0.32495E-04	75876.
-99036							
	14 -	9432.	6	-4061.4	84907.	6202.5	-24743.
44664.							
		9432.	6	-4061.4	2534.5	6202.5	-29183.
35812.			CE 04	0 004045 0	4 2524 5	0 217217 04	62064
84200.		.44/4	6E-04-	0.22484E-0	4 2534.5	0.31721E-04	-63064.
		4476	7E-04-	0 22477E-0	4 84907	0.31723E-04	-58624
93051.		.11/0	771 01	0.221776 0	1 01507.	0.317231 01	30021.
ELEM	ENT=		14	SHELL1	43		
NO	DE	SX		SY	SZ	SXY	SYZ
SXZ							
				4619.3	-23852.	-9460.9	53543.
-0.112		-				0.4.5.0.0	
-0.105	22			4619.3	-19329.	-9460.9	48390.
-0.105	∠0Ľ+U	Ö					

12 -0.10820E	-0.46934E-05-	-0.96997E-06	-19329.	0.21343E-05	49760.
	-0.46930E-05-	.0 97244F-06	-23852	0 21369F-05	54914
-0.11501E		-0.97244E-00	-23032.	0.21309E-03	24914.
	-36485.	-7518.2	2662.9	16568.	-30157.
67425.					
	-36485.	-7518.2	-10183.	16568.	-25298.
52764.					
61113.	-0.63352E-05-	-0.13277E-05	-10183.	0.29008E-05	-29191.
	-0.63402E-05-	-0 13271E-05	2662 9	0 29012E-05	-34050
75774.	0.031021 03	0.132711 03	2002.5	0.230121 03	31030.
ELEMENT	7= 15	SHELL143	3		
	SX	SY	SZ	SXY	SYZ
SXZ	41524	2104 0	10227	11205	10000
-71499.	41734.	3104.8	-1933/.	-11385.	18823.
	41734.	3104.8	-5078.1	-11385.	14399.
-56501.					
11	0.21419E-05	0.16946E-06	-5078.1	-0.60317E-06	17046.
-66378.					
	0.21417E-05	0.16964E-06	-19337.	-0.60349E-06	21470.
-81376.	62200	4442 5	10174	16705	10110
70099.	-63399.	-4443.5	-101/4.	16785.	-19118.
	-63399.	-4443.5	-3448.4	16785.	-13374.
47152.					
11	-0.34382E-05-	-0.23133E-06	-3448.4	0.89231E-06	-12126.
42493.					
	-0.34383E-05-	-0.23160E-06	-10174.	0.89281E-06	-17869.
65440.					

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0
SHELL RESULTS FOR TOP/BOTTOM ALSO MID WHERE APPROPRIATE

	ELEMENT	'= 16	SHELL143	3		
	NODE	SX	SY	SZ	SXY	SYZ
S	XZ					
	25	53084.	414.87	-5030.8	-4693.1	2614.9
- :	29380.					
	9	53084.	414.87	1272.2	-4693.1	270.21
- 3	10863.					
	6	-0.67609E-0	5-0.39629E-07	1272.2	0.52223E-06	664.15

-15366.					
11	-0.67851E-05	-0.39928E-07	-5030.8	0.52500E-06	3008.9
-33883.					
25	-75596.	-570.08	-3495.7	6564.9	-3225.1
37372.					
9	-75596.	-570.08	879.20	6564.9	-1630.0
10857.					
6	-0.54305E-05	-0.29656E-07	879.20	0.40704E-06	-1356.6
7731.3					
11	-0.54659E-05	-0.29823E-07	-3495.7	0.40954E-06	-2951.7
34246.					

#### Von Mises Stresses

