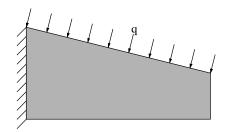
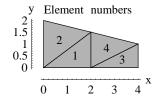
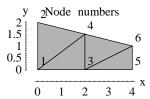
Stress analysis of a bracket: Examples 1.6 p. 32, 1.9 p. 46, and 1.12 p. 55

Top surface of a thin cantilever bracket is subjected to normal pressure $q = 20 \, \text{lb/in}^2$ as shown in Figure. The bracket is 4 in long and is 2 in wide at the base and 1 in wide at the free end. The thickness of the bracket perpendicular to the plane of paper is 1/4 in. The material properties are $E = 10^4 \, \text{lb/in}^2$ and v = 0.2.







Global equations at start of the element assembly process

Equations for element 1

h = 0.25; E = 10000;
$$v = 0.2$$

Plane stress constitutive matrix, $C = \begin{pmatrix} 10416.7 & 2083.33 & 0 \\ 2083.33 & 10416.7 & 0 \\ 0 & 0 & 4166.67 \end{pmatrix}$

Nodal coordinates

$$x_1 = 0.$$
 $x_2 = 2.$ $x_3 = 2.$ $y_1 = 0.$ $y_2 = 0.$ $y_3 = 1.5$

Using these values we get

$$b_1 = -1.5 \qquad b_2 = 1.5 \qquad b_3 = 0.$$

$$c_1 = 0. \qquad c_2 = -2. \qquad c_3 = 2.$$

$$f_1 = 3. \qquad f_2 = 0. \qquad f_3 = 0.$$

Element area, A = 1.5

$$\boldsymbol{B}^{\mathrm{T}} = \begin{pmatrix} -0.5 & 0 & 0.5 & 0 & 0. & 0\\ 0 & 0. & 0 & -0.666667 & 0 & 0.666667\\ 0. & -0.5 & -0.666667 & 0.5 & 0.666667 & 0. \end{pmatrix}$$

Thus the element stiffness matrix is

$$\mathbf{k} = \mathbf{h} \mathbf{A} \mathbf{B} \mathbf{C} \mathbf{B}^{\mathrm{T}} = \begin{pmatrix} 976.563 & 0 & -976.563 & 260.417 & 0 & -260.417 \\ 0 & 390.625 & 520.833 & -390.625 & -520.833 & 0 \\ -976.563 & 520.833 & 1671.01 & -781.25 & -694.444 & 260.417 \\ 260.417 & -390.625 & -781.25 & 2126.74 & 520.833 & -1736.11 \\ 0 & -520.833 & -694.444 & 520.833 & 694.444 & 0 \\ -260.417 & 0 & 260.417 & -1736.11 & 0 & 1736.11 \end{pmatrix}$$

Complete equations for element 1

$$\begin{pmatrix} 976.563 & 0 & -976.563 & 260.417 & 0 & -260.417 \\ 0 & 390.625 & 520.833 & -390.625 & -520.833 & 0 \\ -976.563 & 520.833 & 1671.01 & -781.25 & -694.444 & 260.417 \\ 260.417 & -390.625 & -781.25 & 2126.74 & 520.833 & -1736.11 \\ 0 & -520.833 & -694.444 & 520.833 & 694.444 & 0 \\ -260.417 & 0 & 260.417 & -1736.11 & 0 & 1736.11 \end{pmatrix} \begin{pmatrix} u_1 \\ v_1 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \end{pmatrix} = \begin{pmatrix} 0.0 \\ 0$$

The element contributes to {1, 2, 5, 6, 7, 8} global degrees of freedom.

Locations for element contributions to a global vector: $\begin{bmatrix}
1 \\
2 \\
5 \\
6 \\
7 \\
8
\end{bmatrix}$

and to a global matrix:
$$\begin{bmatrix} [1, 1] & [1, 2] & [1, 5] & [1, 6] & [1, 7] & [1, 8] \\ [2, 1] & [2, 2] & [2, 5] & [2, 6] & [2, 7] & [2, 8] \\ [5, 1] & [5, 2] & [5, 5] & [5, 6] & [5, 7] & [5, 8] \\ [6, 1] & [6, 2] & [6, 5] & [6, 6] & [6, 7] & [6, 8] \\ [7, 1] & [7, 2] & [7, 5] & [7, 6] & [7, 7] & [7, 8] \\ [8, 1] & [8, 2] & [8, 5] & [8, 6] & [8, 7] & [8, 8] \\ \end{bmatrix}$$

Adding element equations into appropriate locations we have

Equations for element 2

$$h = 0.25;$$
 $E = 10000;$ $v = 0.2$

Plane stress constitutive matrix,
$$C = \begin{pmatrix} 10416.7 & 2083.33 & 0 \\ 2083.33 & 10416.7 & 0 \\ 0 & 0 & 4166.67 \end{pmatrix}$$

Nodal coordinates

$$x_1 = 2.$$
 $x_2 = 0.$ $x_3 = 0.$ $y_1 = 1.5$ $y_2 = 2.$ $y_3 = 0.$

Using these values we get

$$b_1 = 2.$$
 $b_2 = -1.5$ $b_3 = -0.5$

$$c_1 = 0.$$
 $c_2 = 2.$ $c_3 = -2.$

$$f_1 = 0.$$
 $f_2 = 0.$ $f_3 = 4.$

Element area, A = 2.

$$\boldsymbol{B}^{\mathrm{T}} = \begin{pmatrix} 0.5 & 0 & -0.375 & 0 & -0.125 & 0 \\ 0 & 0. & 0 & 0.5 & 0 & -0.5 \\ 0. & 0.5 & 0.5 & -0.375 & -0.5 & -0.125 \end{pmatrix}$$

Thus the element stiffness matrix is

$$\mathbf{k} = \mathbf{h} \mathbf{A} \mathbf{B} \mathbf{C} \mathbf{B}^{\mathrm{T}} = \begin{pmatrix} 1302.08 & 0 & -976.563 & 260.417 & -325.521 & -260.417 \\ 0 & 520.833 & 520.833 & -390.625 & -520.833 & -130.208 \\ -976.563 & 520.833 & 1253.26 & -585.938 & -276.693 & 65.1042 \\ 260.417 & -390.625 & -585.938 & 1595.05 & 325.521 & -1204.43 \\ -325.521 & -520.833 & -276.693 & 325.521 & 602.214 & 195.313 \\ -260.417 & -130.208 & 65.1042 & -1204.43 & 195.313 & 1334.64 \end{pmatrix}$$

Load vector due to distributed load on side 1 (nodes {4, 2})

Specified load components: $q_n = -20$; $q_t = 0$

End nodal coordinates: ($\{2., 1.5\}$ $\{0., 2.\}$) giving side length, L = 2.06155

Components of unit normal to the side:

$$n_x = 0.242536;$$

 $n_y = 0.970143$

Using these values we get

$$\mathbf{r}_{q}^{T} = (-1.25 -5. -1.25 -5. 0 0)$$

Complete equations for element 2

$$\begin{pmatrix} 1302.08 & 0 & -976.563 & 260.417 & -325.521 & -260.417 \\ 0 & 520.833 & 520.833 & -390.625 & -520.833 & -130.208 \\ -976.563 & 520.833 & 1253.26 & -585.938 & -276.693 & 65.1042 \\ 260.417 & -390.625 & -585.938 & 1595.05 & 325.521 & -1204.43 \\ -325.521 & -520.833 & -276.693 & 325.521 & 602.214 & 195.313 \\ -260.417 & -130.208 & 65.1042 & -1204.43 & 195.313 & 1334.64 \end{pmatrix} \begin{pmatrix} u_4 \\ v_4 \\ u_2 \\ v_2 \\ u_1 \\ v_1 \end{pmatrix} = \begin{pmatrix} -1.25 \\ -5. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {7, 8, 3, 4, 1, 2} global degrees of freedom.

Locations for element contributions to a global vector:
$$\begin{bmatrix} 7 \\ 8 \\ 3 \\ 4 \\ 1 \\ 2 \end{bmatrix}$$

and to a global matrix:
$$\begin{bmatrix} [7,7] & [7,8] & [7,3] & [7,4] & [7,1] & [7,2] \\ [8,7] & [8,8] & [8,3] & [8,4] & [8,1] & [8,2] \\ [3,7] & [3,8] & [3,3] & [3,4] & [3,1] & [3,2] \\ [4,7] & [4,8] & [4,3] & [4,4] & [4,1] & [4,2] \\ [1,7] & [1,8] & [1,3] & [1,4] & [1,1] & [1,2] \\ [2,7] & [2,8] & [2,3] & [2,4] & [2,1] & [2,2] \\ \end{bmatrix}$$

Adding element equations into appropriate locations we have

$$\begin{pmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \\ v_5 \\ v_5 \\ u_6 \\ v_6 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ -1.25 \\ -5. \\ 0 \\ 0 \\ -1.25 \\ -5. \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

Equations for element 3

$$h = 0.25;$$
 $E = 10000;$ $v = 0.2$

Plane stress constitutive matrix,
$$C = \begin{pmatrix} 10416.7 & 2083.33 & 0 \\ 2083.33 & 10416.7 & 0 \\ 0 & 0 & 4166.67 \end{pmatrix}$$

Nodal coordinates

Element node	Global node number	X	у
1	3	2.	0.
2	5	4.	0.
3	6	4.	1.

$$x_1 = 2.$$
 $x_2 = 4.$ $x_3 = 4.$ $y_1 = 0.$ $y_2 = 0.$ $y_3 = 1.$

Using these values we get

$$b_1 = -1. \qquad b_2 = 1. \qquad b_3 = 0.$$

$$c_1 = 0. \qquad c_2 = -2. \qquad c_3 = 2.$$

$$f_1 = 4. \qquad f_2 = -2. \qquad f_3 = 0.$$

Element area, A = 1.

$$\boldsymbol{B}^{\mathrm{T}} = \left(\begin{array}{cccccc} -0.5 & 0 & 0.5 & 0 & 0. & 0 \\ 0 & 0. & 0 & -1. & 0 & 1. \\ 0. & -0.5 & -1. & 0.5 & 1. & 0. \end{array} \right)$$

Thus the element stiffness matrix is

$$\mathbf{k} = \mathbf{h} \mathbf{A} \mathbf{B} \mathbf{C} \mathbf{B}^{\mathrm{T}} = \begin{pmatrix} 651.042 & 0 & -651.042 & 260.417 & 0 & -260.417 \\ 0 & 260.417 & 520.833 & -260.417 & -520.833 & 0 \\ -651.042 & 520.833 & 1692.71 & -781.25 & -1041.67 & 260.417 \\ 260.417 & -260.417 & -781.25 & 2864.58 & 520.833 & -2604.17 \\ 0 & -520.833 & -1041.67 & 520.833 & 1041.67 & 0 \\ -260.417 & 0 & 260.417 & -2604.17 & 0 & 2604.17 \end{pmatrix}$$

Complete equations for element 3

$$\begin{pmatrix} 651.042 & 0 & -651.042 & 260.417 & 0 & -260.417 \\ 0 & 260.417 & 520.833 & -260.417 & -520.833 & 0 \\ -651.042 & 520.833 & 1692.71 & -781.25 & -1041.67 & 260.417 \\ 260.417 & -260.417 & -781.25 & 2864.58 & 520.833 & -2604.17 \\ 0 & -520.833 & -1041.67 & 520.833 & 1041.67 & 0 \\ -260.417 & 0 & 260.417 & -2604.17 & 0 & 2604.17 \end{pmatrix} \begin{pmatrix} u_3 \\ v_3 \\ u_5 \\ v_5 \\ u_6 \\ v_6 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

The element contributes to {5, 6, 9, 10, 11, 12} global degrees of freedom.

Locations for element contributions to a global vector:
$$\begin{bmatrix} 5 \\ 6 \\ 9 \\ 10 \\ 11 \\ 12 \end{bmatrix}$$

and to a global matrix:
$$\begin{bmatrix} [5,5] & [5,6] & [5,9] & [5,10] & [5,11] & [5,12] \\ [6,5] & [6,6] & [6,9] & [6,10] & [6,11] & [6,12] \\ [9,5] & [9,6] & [9,9] & [9,10] & [9,11] & [9,12] \\ [10,5] & [10,6] & [10,9] & [10,10] & [10,11] & [10,12] \\ [11,5] & [11,6] & [11,9] & [11,10] & [11,11] & [11,12] \\ [12,5] & [12,6] & [12,9] & [12,10] & [12,11] & [12,12] \\ \end{bmatrix}$$

Adding element equations into appropriate locations we have

(1	578.78	195.313	-276.693	325.521	-976.563	260.417	-325.521	-781.25	0	0
	195.313	1725.26	65.1042	-1204.43	520.833	-390.625	-781.25	-130.208	0	0
-	276.693	65.1042	1253.26	-585.938	0	0	-976.563	520.833	0	0
	325.521	-1204.43	-585.938	1595.05	0	0	260.417	-390.625	0	0
-	976.563	520.833	0	0	2322.05	-781.25	-694.444	260.417	-651.042	260.
	260.417	-390.625	0	0	-781.25	2387.15	520.833	-1736.11	520.833	-260.
-	325.521	-781.25	-976.563	260.417	-694.444	520.833	1996.53	0	0	0
-	781.25	-130.208	520.833	-390.625	260.417	-1736.11	0	2256.94	0	0
	0	0	0	0	-651.042	520.833	0	0	1692.71	-781.
	0	0	0	0	260.417	-260.417	0	0	-781.25	2864.
	0	0	0	0	0	-520.833	0	0	-1041.67	520.
	0	0	0	0	-260.417	0	0	0	260.417	-2604.

Equations for element 4

$$h = 0.25;$$
 $E = 10000;$ $v = 0.2$

Plane stress constitutive matrix,
$$C = \begin{pmatrix} 10416.7 & 2083.33 & 0 \\ 2083.33 & 10416.7 & 0 \\ 0 & 0 & 4166.67 \end{pmatrix}$$

Nodal coordinates

$$x_1 = 4.$$
 $x_2 = 2.$ $x_3 = 2.$ $y_1 = 1.$ $y_2 = 1.5$ $y_3 = 0.$

Using these values we get

$$b_1 = 1.5$$
 $b_2 = -1.$ $b_3 = -0.5$ $c_1 = 0.$ $c_2 = 2.$ $c_3 = -2.$ $f_1 = -3.$ $f_2 = 2.$ $f_3 = 4.$

Element area, A = 1.5

$$\boldsymbol{B}^{\mathrm{T}} = \begin{pmatrix} 0.5 & 0 & -0.333333 & 0 & -0.166667 & 0 \\ 0 & 0. & 0 & 0.666667 & 0 & -0.666667 \\ 0. & 0.5 & 0.666667 & -0.333333 & -0.666667 & -0.166667 \end{pmatrix}$$

Thus the element stiffness matrix is

$$\mathbf{k} = \mathrm{hA} \mathbf{B} \mathbf{C} \mathbf{B}^{\mathrm{T}} = \begin{pmatrix} 976.563 & 0 & -651.042 & 260.417 & -325.521 & -260.417 \\ 0 & 390.625 & 520.833 & -260.417 & -520.833 & -130.208 \\ -651.042 & 520.833 & 1128.47 & -520.833 & -477.431 & 0 \\ 260.417 & -260.417 & -520.833 & 1909.72 & 260.417 & -1649.31 \\ -325.521 & -520.833 & -477.431 & 260.417 & 802.951 & 260.417 \\ -260.417 & -130.208 & 0 & -1649.31 & 260.417 & 1779.51 \end{pmatrix}$$

Load vector due to distributed load on side 1 (nodes {6, 4})

Specified load components: $q_n = -20$; $q_t = 0$

End nodal coordinates: ($\{4., 1.\}$ $\{2., 1.5\}$) giving side length, L = 2.06155

Components of unit normal to the side: $n_x = 0.242536$; $n_y = 0.970143$

Using these values we get $r_q^T = (-1.25 -5. -1.25 -5. 0 \ 0)$

Complete equations for element 4

$$\begin{pmatrix} 976.563 & 0 & -651.042 & 260.417 & -325.521 & -260.417 \\ 0 & 390.625 & 520.833 & -260.417 & -520.833 & -130.208 \\ -651.042 & 520.833 & 1128.47 & -520.833 & -477.431 & 0 \\ 260.417 & -260.417 & -520.833 & 1909.72 & 260.417 & -1649.31 \\ -325.521 & -520.833 & -477.431 & 260.417 & 802.951 & 260.417 \\ -260.417 & -130.208 & 0 & -1649.31 & 260.417 & 1779.51 \end{pmatrix} \begin{pmatrix} u_6 \\ v_6 \\ u_4 \\ v_4 \\ u_3 \\ v_3 \end{pmatrix} = \begin{pmatrix} -1.25 \\ -5. \\ 0. \\ 0. \\ 0. \end{pmatrix}$$

The element contributes to {11, 12, 7, 8, 5, 6} global degrees of freedom.

Locations for element contributions to a global vector:
$$\begin{bmatrix}
11 \\
12 \\
7 \\
8 \\
5 \\
6
\end{bmatrix}$$

and to a global matrix:
$$\begin{bmatrix} [11,11] & [11,12] & [11,7] & [11,8] & [11,5] & [11,6] \\ [12,11] & [12,12] & [12,7] & [12,8] & [12,5] & [12,6] \\ [7,11] & [7,12] & [7,7] & [7,8] & [7,5] & [7,6] \\ [8,11] & [8,12] & [8,7] & [8,8] & [8,5] & [8,6] \\ [5,11] & [5,12] & [5,7] & [5,8] & [5,5] & [5,6] \\ [6,11] & [6,12] & [6,7] & [6,8] & [6,5] & [6,6] \\ \end{bmatrix}$$

Adding element equations into appropriate locations we have

-325.521 -781.25 -976.563 260.417 -1171.88 520.833 3125. -520.833 0 -781.25 -130.208 520.833 -390.625 520.833 -3385.42 -520.833 4166.67 0 0 0 0 0 -651.042 520.833 0 0 1692.71 0 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67										
-276.693 65.1042 1253.26 -585.938 0 0 -976.563 520.833 0 325.521 -1204.43 -585.938 1595.05 0 0 260.417 -390.625 0 -976.563 520.833 0 0 3125. -520.833 -1171.88 520.833 -651.042 260.417 -390.625 0 0 -520.833 4166.67 520.833 -3385.42 520.833 -325.521 -781.25 -976.563 260.417 -1171.88 520.833 3125. -520.833 0 -781.25 -130.208 520.833 -390.625 520.833 -3385.42 -520.833 4166.67 0 0 0 0 -651.042 520.833 0 0 1692.71 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	(1578.78	195.313	-276.693	325.521	-976.563	260.417	-325.521	-781.25	0	
325.521 -1204.43 -585.938 1595.05 0 0 260.417 -390.625 0 -976.563 520.833 0 0 3125. -520.833 -1171.88 520.833 -651.042 260.417 -390.625 0 0 -520.833 4166.67 520.833 -3385.42 520.833 -325.521 -781.25 -976.563 260.417 -1171.88 520.833 3125. -520.833 0 -781.25 -130.208 520.833 -390.625 520.833 -3385.42 -520.833 4166.67 0 0 0 0 0 -651.042 520.833 0 0 1692.71 0 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	195.313	1725.26	65.1042	-1204.43	520.833	-390.625	-781.25	-130.208	0	
-976.563 520.833 0 0 3125. -520.833 -1171.88 520.833 -651.042 260.417 -390.625 0 0 -520.833 4166.67 520.833 -3385.42 520.833 -325.521 -781.25 -976.563 260.417 -1171.88 520.833 3125. -520.833 0 -781.25 -130.208 520.833 -390.625 520.833 -3385.42 -520.833 4166.67 0 0 0 0 -651.042 520.833 0 0 1692.71 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	-276.693	65.1042	1253.26	-585.938	0	0	-976.563	520.833	0	
260.417 -390.625 0 0 -520.833 4166.67 520.833 -3385.42 520.833 -325.521 -781.25 -976.563 260.417 -1171.88 520.833 3125. -520.833 0 -781.25 -130.208 520.833 -390.625 520.833 -3385.42 -520.833 4166.67 0 0 0 0 0 -651.042 520.833 0 0 1692.71 0 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	325.521	-1204.43	-585.938	1595.05	0	0	260.417	-390.625	0	
-325.521 -781.25 -976.563 260.417 -1171.88 520.833 3125. -520.833 0 -781.25 -130.208 520.833 -390.625 520.833 -3385.42 -520.833 4166.67 0 0 0 0 0 -651.042 520.833 0 0 1692.71 0 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	-976.563	520.833	0	0	3125.	-520.833	-1171.88	520.833	-651.042	2
-781.25 -130.208 520.833 -390.625 520.833 -3385.42 -520.833 4166.67 0 0 0 0 0 -651.042 520.833 0 0 1692.71 0 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	260.417	-390.625	0	0	-520.833	4166.67	520.833	-3385.42	520.833	-2
0 0 0 0 -651.042 520.833 0 0 1692.71 0 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	-325.521	-781.25	-976.563	260.417	-1171.88	520.833	3125.	-520.833	0	
0 0 0 0 260.417 -260.417 0 0 -781.25 0 0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	-781.25	-130.208	520.833	-390.625	520.833	-3385.42	-520.833	4166.67	0	
0 0 0 -325.521 -781.25 -651.042 260.417 -1041.67	0	0	0	0	-651.042	520.833	0	0	1692.71	-7
	0	0	0	0	260.417	-260.417	0	0	-781.25	28
.	0	0	0	0	-325.521	-781.25	-651.042	260.417	-1041.67	5
$\begin{pmatrix} 0 & 0 & 0 & 0 & -781.25 & -130.208 & 520.833 & -260.417 & 260.417 & -120.208 & -120.$	(0	0	0	0	-781.25	-130.208	520.833	-260.417	260.417	-26

Essential boundary conditions

Node	dof	Value
1	$egin{array}{c} u_1 \\ v_1 \end{array}$	$0 \\ 0$
2	$\mathbf{u_2}$ $\mathbf{v_2}$	0 0

Remove {1, 2, 3, 4} rows and columns.

After adjusting for essential boundary conditions we have

$$\begin{pmatrix} u_3 \\ v_3 \\ u_4 \\ v_4 \\ u_5 \\ v_5 \\ u_6 \\ v_6 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ -2.5 \\ -10. \\ 0 \\ 0 \\ -1.25 \\ -5. \end{pmatrix}$$

Solving the final system of global equations we get

$$\begin{aligned} \{u_3 = -0.0103553, \, v_3 = -0.0255297, \, u_4 = 0.00472765, \, v_4 = -0.0247357, \\ u_5 = -0.0131394, \, v_5 = -0.0554931, \, u_6 = 0.0000838902, \, v_6 = -0.0555664 \} \end{aligned}$$

Complete table of nodal values

	u	v
1	0	0
2	0	0
3	-0.0103553	-0.0255297
4	0.00472765	-0.0247357
5	-0.0131394	-0.0554931
6	0.0000838902	-0.0555664

Computation of reactions

Equation numbers of dof with specified values: {1, 2, 3, 4}

Extracting equations {1, 2, 3, 4} from the global system we have

$$\begin{pmatrix} 1578.78 & 195.313 & -276.693 & 325.521 & -976.563 & 260.417 & -325.521 & -781.25 & 0 & 0 & 0 & 0 \\ 195.313 & 1725.26 & 65.1042 & -1204.43 & 520.833 & -390.625 & -781.25 & -130.208 & 0 & 0 & 0 & 0 \\ -276.693 & 65.1042 & 1253.26 & -585.938 & 0 & 0 & -976.563 & 520.833 & 0 & 0 & 0 & 0 \\ 325.521 & -1204.43 & -585.938 & 1595.05 & 0 & 0 & 260.417 & -390.625 & 0 & 0 & 0 & 0 \\ \end{pmatrix} \begin{bmatrix} u_1 \\ v_1 \\ u_2 \\ v_2 \\ u_3 \\ v_3 \\ u_4 \\ v_4 \\ u_5 \\ v_5 \\ u_6 \\ v_6 \end{pmatrix}$$

$$\begin{pmatrix} R_1 + 0. \\ R_2 + 0. \\ R_3 - 1.25 \\ R_4 - 5. \end{pmatrix}$$

Substituting the nodal values and re-arranging

$$\begin{pmatrix} R_1 \\ R_2 \\ R_3 \\ R_4 \end{pmatrix} = \begin{pmatrix} 1578.78 & 195.313 & -276.693 & 325.521 & -976.563 & 260.417 & -325.521 & -781.25 & 0 & 0 & 0 & 0 \\ 195.313 & 1725.26 & 65.1042 & -1204.43 & 520.833 & -390.625 & -781.25 & -130.208 & 0 & 0 & 0 \\ -276.693 & 65.1042 & 1253.26 & -585.938 & 0 & 0 & -976.563 & 520.833 & 0 & 0 & 0 \\ 325.521 & -1204.43 & -585.938 & 1595.05 & 0 & 0 & 260.417 & -390.625 & 0 & 0 & 0 \\ \end{pmatrix}$$

$$\begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -0.0103553 \\ -0.0255297 \\ 0.00472765 \\ -0.0247357 \\ -0.0131394 \\ -0.0554931 \\ 0.0000838902 \\ -0.0555664 \end{pmatrix} - \begin{pmatrix} 0 \\ 0 \\ -1.25 \\ -5 \\ \end{pmatrix}$$

Carrying out computations, the reactions are as follows.

Label	dof	Reaction
R_1	\mathbf{u}_1	21.25
R_2	\mathbf{v}_1	4.10648
R_3	u_2	-16.25
R_4	v_2	15.8935

Sum of Reactions

Solution for element 1

$$h = 0.25$$
; $E = 10000$; $v = 0.2$

Plane stress constitutive matrix,
$$C = \begin{pmatrix} 10416.7 & 2083.33 & 0 \\ 2083.33 & 10416.7 & 0 \\ 0 & 0 & 4166.67 \end{pmatrix}$$

Element nodes: First node (node # 1): $\{0., 0.\}$

Second node (node # 3): {2., 0.} Third node (node # 4): {2., 1.5}

$$x_1 = 0.$$
 $x_2 = 2.$ $x_3 = 2.$ $y_1 = 0.$ $y_2 = 0.$ $y_3 = 1.5$

Using these values we get

$$b_1 = -1.5$$
 $b_2 = 1.5$ $b_3 = 0.$

$$c_1 = 0.$$
 $c_2 = -2.$ $c_3 = 2.$

$$f_1 = 3.$$
 $f_2 = 0.$ $f_3 = 0.$

Element area, A = 1.5

$$\boldsymbol{B}^{\mathrm{T}} = \left(\begin{array}{ccccc} -0.5 & 0 & 0.5 & 0 & 0. & 0 \\ 0 & 0. & 0 & -0.666667 & 0 & 0.666667 \\ 0. & -0.5 & -0.666667 & 0.5 & 0.666667 & 0. \end{array} \right)$$

Substituting these into the formulas for triangle interpolation functions we get

Interpolation functions, $\{1. - 0.5 \text{ x}, 0.5 \text{ x} - 0.666667 \text{ y}, 0.666667 \text{ y}\}\$

$$\boldsymbol{N}^{\mathrm{T}} = \begin{pmatrix} 1. - 0.5 \, \mathrm{x} & 0 & 0.5 \, \mathrm{x} - 0.666667 \, \mathrm{y} & 0 & 0.666667 \, \mathrm{y} & 0 \\ 0 & 1. - 0.5 \, \mathrm{x} & 0 & 0.5 \, \mathrm{x} - 0.666667 \, \mathrm{y} & 0 & 0.666667 \, \mathrm{y} \end{pmatrix}$$

From global solution the displacements at the element nodes are

(displacements at nodes {1, 3, 4}):

$$d^{T} = \{0, 0, -0.0103553, -0.0255297, 0.00472765, -0.0247357\}$$

The displacement distribution over the element is

$$\begin{pmatrix} \mathbf{u}(\mathbf{x}, \mathbf{y}) \\ \mathbf{v}(\mathbf{x}, \mathbf{y}) \end{pmatrix} = \mathbf{N}^{\mathrm{T}} \mathbf{d} = \begin{pmatrix} 0.0100553 \,\mathrm{y} - 0.00517764 \,\mathrm{x} \\ 0.000529362 \,\mathrm{y} - 0.0127648 \,\mathrm{x} \end{pmatrix}$$

In-plane strain components, $\epsilon = \mathbf{B}^{\mathrm{T}} \mathbf{d} = (-0.00517764 \ 0.000529362 \ -0.00270956)$

In-plane stress components,
$$\sigma = C\epsilon = (-52.8309 -5.27256 -11.2898)$$

Computing out-of-plane strain and stress components

using appropriate formulas, the complete strain and stress vectors are as follows.

$$\boldsymbol{\epsilon}^{\mathrm{T}} = (-0.00517764 \ 0.000529362 \ 0.00116207 \ -0.00270956 \ 0 \ 0)$$

$$\sigma^{\mathrm{T}} = (-52.8309 -5.27256 \ 0 \ -11.2898 \ 0 \ 0)$$

Substituting these stress components into appropriate formulas

Principal stresses =
$$(0 -2.72856 -55.3749)$$

Effective stress (von Mises) =
$$54.0623$$

Solution for element 2

$$h = 0.25;$$
 $E = 10000;$ $v = 0.2$

Plane stress constitutive matrix,
$$C = \begin{pmatrix} 10416.7 & 2083.33 & 0 \\ 2083.33 & 10416.7 & 0 \\ 0 & 0 & 4166.67 \end{pmatrix}$$

Element nodes: First node (node # 4): {2., 1.5}

Second node (node # 2): {0., 2.} Third node (node # 1): {0., 0.}

$$x_1 = 2.$$
 $x_2 = 0.$ $x_3 = 0.$ $y_1 = 1.5$ $y_2 = 2.$ $y_3 = 0.$

Using these values we get

$$b_1 = 2.$$
 $b_2 = -1.5$ $b_3 = -0.5$

$$c_1 = 0.$$
 $c_2 = 2.$ $c_3 = -2.$

$$f_1 = 0.$$
 $f_2 = 0.$ $f_3 = 4.$

Element area, A = 2.

$$\boldsymbol{B}^{\mathrm{T}} = \begin{pmatrix} 0.5 & 0 & -0.375 & 0 & -0.125 & 0 \\ 0 & 0. & 0 & 0.5 & 0 & -0.5 \\ 0. & 0.5 & 0.5 & -0.375 & -0.5 & -0.125 \end{pmatrix}$$

Substituting these into the formulas for triangle interpolation functions we get

Interpolation functions, $\{0.5 \text{ x}, \ 0.5 \text{ y} - 0.375 \text{ x}, \ -0.125 \text{ x} - 0.5 \text{ y} + 1.\}$

$$\boldsymbol{N}^{\mathrm{T}} = \left(\begin{array}{cccc} 0.5 \ x & 0 & 0.5 \ y - 0.375 \ x & 0 & -0.125 \ x - 0.5 \ y + 1. \\ 0 & 0.5 \ x & 0 & 0.5 \ y - 0.375 \ x & 0 & -0.125 \ x - 0.5 \ y + 1. \end{array} \right)$$

From global solution the displacements at the element nodes are

(displacements at nodes {4, 2, 1}):

$$\boldsymbol{d}^{\mathrm{T}} = \{0.00472765, -0.0247357, 0, 0, 0, 0\}$$

The displacement distribution over the element is

$$\begin{pmatrix} \mathbf{u}(\mathbf{x}, \mathbf{y}) \\ \mathbf{v}(\mathbf{x}, \mathbf{y}) \end{pmatrix} = \mathbf{N}^{\mathrm{T}} \mathbf{d} = \begin{pmatrix} 0.00236383 \, \mathbf{x} \\ -0.0123678 \, \mathbf{x} \end{pmatrix}$$

In-plane strain components, $\epsilon = \mathbf{B}^{T} \mathbf{d} = (0.00236383 \ 0 \ -0.0123678)$

In-plane stress components, $\sigma = C\epsilon = (24.6232 \ 4.92464 \ -51.5326)$

Computing out-of-plane strain and stress components

using appropriate formulas, the complete strain and stress vectors are as follows.

$$\epsilon^{\mathrm{T}} = (0.00236383 \ 0 \ -0.000590956 \ -0.0123678 \ 0 \ 0)$$

$$\sigma^{T} = (24.6232 \ 4.92464 \ 0 \ -51.5326 \ 0 \ 0)$$

Substituting these stress components into appropriate formulas

Principal stresses =
$$(67.2393 \ 0 \ -37.6915)$$

Effective stress (von Mises) = 92.0659

Solution for element 3

$$h = 0.25$$
; $E = 10000$; $v = 0.2$

Plane stress constitutive matrix,
$$C = \begin{pmatrix} 10416.7 & 2083.33 & 0 \\ 2083.33 & 10416.7 & 0 \\ 0 & 0 & 4166.67 \end{pmatrix}$$

Element nodes: First node (node # 3): {2., 0.}

Second node (node # 5): {4., 0.}

Third node (node # 6): {4., 1.}

 $x_1 = 2.$ $x_2 = 4.$ $x_3 = 4.$ $y_1 = 0.$ $y_2 = 0.$ $y_3 = 1.$

Using these values we get

 $b_1 = -1$. $b_2 = 1$. $b_3 = 0$.

 $c_1 = 0.$ $c_2 = -2.$ $c_3 = 2.$

 $f_1 = 4.$ $f_2 = -2.$ $f_3 = 0.$

Element area, A = 1.

$$\boldsymbol{B}^{\mathrm{T}} = \left(\begin{array}{cccccc} -0.5 & 0 & 0.5 & 0 & 0. & 0 \\ 0 & 0. & 0 & -1. & 0 & 1. \\ 0. & -0.5 & -1. & 0.5 & 1. & 0. \end{array} \right)$$

Substituting these into the formulas for triangle interpolation functions we get

Interpolation functions, $\{2. -0.5 \text{ x}, 0.5 \text{ x} - 1. \text{ y} - 1., 1. \text{ y}\}\$

$$\boldsymbol{N}^{\mathrm{T}} = \begin{pmatrix} 2. - 0.5 \, \mathrm{x} & 0 & 0.5 \, \mathrm{x} - 1. \, \mathrm{y} - 1. & 0 & 1. \, \mathrm{y} & 0 \\ 0 & 2. - 0.5 \, \mathrm{x} & 0 & 0.5 \, \mathrm{x} - 1. \, \mathrm{y} - 1. & 0 & 1. \, \mathrm{y} \end{pmatrix}$$

From global solution the displacements at the element nodes are

(displacements at nodes {3, 5, 6}):

$$\boldsymbol{d}^{\mathrm{T}} = \{-0.0103553, -0.0255297, -0.0131394, -0.0554931, 0.0000838902, -0.0555664\}$$

The displacement distribution over the elemen

$$\begin{pmatrix} \mathbf{u}(\mathbf{x}, \mathbf{y}) \\ \mathbf{v}(\mathbf{x}, \mathbf{y}) \end{pmatrix} = \mathbf{N}^{\mathrm{T}} \mathbf{d} = \begin{pmatrix} -0.00139207 \,\mathbf{x} + 0.0132233 \,\mathbf{y} - 0.00757114 \\ -0.0149817 \,\mathbf{x} - 0.0000732667 \,\mathbf{y} + 0.00443371 \end{pmatrix}$$

In-plane strain components, $\epsilon = \mathbf{B}^{T} \mathbf{d} = (-0.00139207 -0.0000732667 -0.0017584)$

In-plane stress components, $\sigma = C\epsilon = (-14.6533 - 3.66334 - 7.32667)$

Computing out-of-plane strain and stress components

using appropriate formulas, the complete strain and stress vectors are as follows.

$$\boldsymbol{\epsilon}^{\mathrm{T}} = (-0.00139207 \ -0.0000732667 \ 0.000366334 \ -0.0017584 \ 0 \ 0)$$

$$\boldsymbol{\sigma}^{\mathrm{T}} = (-14.6533 \ -3.66334 \ 0 \ -7.32667 \ 0 \ 0)$$

Substituting these stress components into appropriate formulas

Principal stresses = $(0 \ 0 \ -18.3167)$

Effective stress (von Mises) = 18.3167

Solution for element 4

$$h = 0.25;$$
 $E = 10000;$ $v = 0.2$

Plane stress constitutive matrix,
$$C = \begin{pmatrix} 10416.7 & 2083.33 & 0 \\ 2083.33 & 10416.7 & 0 \\ 0 & 0 & 4166.67 \end{pmatrix}$$

Element nodes: First node (node # 6): {4., 1.}

> Second node (node # 4): {2., 1.5} Third node (node # 3): {2., 0.}

$$x_1 = 4.$$
 $x_2 = 2.$ $x_3 = 2.$ $y_1 = 1.$ $y_2 = 1.5$ $y_3 = 0.$

Using these values we get

$$b_1 = 1.5$$
 $b_2 = -1.$ $b_3 = -0.5$ $c_1 = 0.$ $c_2 = 2.$ $c_3 = -2.$

$$f_1 = -3.$$
 $f_2 = 2.$ $f_3 = 4.$

Element area, A = 1.5

$$\boldsymbol{B}^{\mathrm{T}} = \begin{pmatrix} 0.5 & 0 & -0.333333 & 0 & -0.166667 & 0 \\ 0 & 0. & 0 & 0.666667 & 0 & -0.666667 \\ 0. & 0.5 & 0.666667 & -0.333333 & -0.666667 & -0.166667 \end{pmatrix}$$

Substituting these into the formulas for triangle interpolation functions we get

Interpolation functions, $\{0.5 \text{ x} - 1., -0.3333333 \text{ x} + 0.666667 \text{ y} + 0.666667, -0.1666667 \text{ x} - 0.666667 \text{ y} + 1.33333\}$

$$\boldsymbol{N}^{\mathrm{T}} = \begin{pmatrix} 0.5 \ \mathrm{x} - 1. & 0 & -0.333333 \ \mathrm{x} + 0.6666667 \ \mathrm{y} + 0.6666667 \ \\ 0 & 0.5 \ \mathrm{x} - 1. & 0 & -0.333333 \ \mathrm{x} + 0.6666667 \ \\ 0 & -0.3$$

From global solution the displacements at the element nodes are

(displacements at nodes {6, 4, 3}):

$$\boldsymbol{d}^{\mathrm{T}} = \{0.0000838902, \, -0.0555664, \, 0.00472765, \, -0.0247357, \, -0.0103553, \, -0.0255297\}$$

The displacement distribution over the element is

$$\begin{pmatrix} \mathbf{u}(\mathbf{x}, \mathbf{y}) \\ \mathbf{v}(\mathbf{x}, \mathbf{y}) \end{pmatrix} = \mathbf{N}^{\mathrm{T}} \mathbf{d} = \begin{pmatrix} 0.000191941 \,\mathbf{x} + 0.0100553 \,\mathbf{y} - 0.0107392 \\ -0.015283 \,\mathbf{x} + 0.000529362 \,\mathbf{y} + 0.00503634 \end{pmatrix}$$

In-plane strain components, $\epsilon = \mathbf{B}^{\mathrm{T}} \mathbf{d} = (0.000191941 \ 0.000529362 \ -0.00522773)$

In-plane stress components, $\sigma = C\epsilon = (3.10223 \ 5.91407 \ -21.7822)$

Computing out-of-plane strain and stress components

using appropriate formulas, the complete strain and stress vectors are as follows.

$$\epsilon^{\text{T}} = (0.000191941 \ 0.000529362 \ -0.000180326 \ -0.00522773 \ 0 \ 0)$$

$$\sigma^{\text{T}} = (3.10223 \ 5.91407 \ 0 \ -21.7822 \ 0 \ 0)$$

Substituting these stress components into appropriate formulas

Principal stresses =
$$(26.3357 \ 0 \ -17.3194)$$

Effective stress (von Mises) = 38.0742

Solution summary

Nodal solution

Solution at element centers

	Coord	Disp	Stresses	Principal stresses	Effective Stress
1	1.33333 0.5	-0.00187588 -0.0167551	-52.8309 -5.27256 0 -11.2898 0	0 -2.72856 -55.3749	54.0623
2	0.666667 1.16667	0.00157588 -0.00824522	24.6232 4.92464 0 -51.5326 0	67.2393 0 -37.6915	92.0659
3	3.33333 0.333333	-0.0078036 -0.0455297	-14.6533 -3.66334 0 -7.32667 0	0 0 -18.3167	18.3167
4	2.66667 0.833333	-0.00184791 -0.0352772	3.10223 5.91407 0 -21.7822 0	26.3357 0 -17.3194	38.0742

Support reactions

Node	dof	Reaction
1	1	21.25
1	2	4.10648
2	1	-16.25
2	2	15.8935

Sum of applied loads \rightarrow (-5. -20.)

Sum of support reactions \rightarrow (5. 20.)