ABSTRACT

CALDERON, VICTOR ALEJANDRO. Time Dependent Performance Based Design. (Under the direction of Dr. Mervyn Kowalsky.)

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Time Dependent Performance Based Design

by
Victor Alejandro Calderon

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DEDICATION

To my parents. To God.

BIOGRAPHY

The author was born in land far away where the earth rocks like a hammock. That land name is El Salvador. . . .

ACKNOWLEDGEMENTS

I would like to thank Dr. Kowalsky for his help. The Staff and Students at The Constructed Facilities Lab of NC State. The Alaska Department of Transportation. . . .

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Chapter 1

INTRODUCTION

Bridges are designed based on discrete events with minimal consideration of interactions between hazards/loading, material aging (or more accurately condition) and bridge performance. The purpose of the research described is to study Time Dependent Performance Based Design that considers the effects of cumulative damage on the properties of the materials both as a function of time and current condition. Specific items of interest include corrosion, strain aging, low cycle fatigue and strength aging. In addition, since there is a high likelihood for a structure in a high seismic region to be subjected to more than one main shock throughout its life, it is deemed important to consider the effects of multiple earthquakes. As a consequence, the effects of repairs on the structural response are also of great importance. An analytical procedure is implemented such that it considers the effect of aging on structures, more specifically this study starts by evaluating an RC bridge Column. A series of condition dependent nonlinear time history analysis are performed assuming that a series of earthquakes occurs throughout the lifetime of the structure while at the same time changing the properties of the structure as time progresses. To achieve this a library of time dependent materials are developed. At the end of each series the main variables of study are the the limit state that was reached, the controlling mode of response (flexural or shear controlled), Equivalent Viscous Damping and the accumulated deformations. The series of earthquake proposed consists of (1) equally spaced main shocks only, (2) main shock-aftershocks series and (3) main shock-aftershock-repair series. At the end of the presentation recommendations on design of new structures and assessment of existing structures will be provided.

1.1 Properties that change with time

- Corrosion
- Strain Aging
- Concrete Strength
- Creep
- Low-cycle Fatigue
- Repairs

Chapter 2

LITERATURE REVIEW

In Chapter 1 we did some typesetting and equations; now let's look at tables, figures, and matrices.

2.1 Corrosion

A structure that is originally designed to meet code specifications may not have the same margin of safety once the structure has undergone significant corrosion.

Research on the cyclic behavior of Corroded RC Columns [7] have shown that at high corrosion levels as high as 35% the yield strength of the columns decreased by 28% and the ultimate strength decreased by 30%, also the ductility is reduced by as much as 18%. This research was performed by fixing the percentage of corrosion and then physical tests were performed; the properties of the materials are modified using empirical equations developed from the tests. While the results appear to correlate well with the tests, this model is not time dependent.

There are time dependent models which first determine the time at which corrosion starts and then a time dependent function in which the diameter of the bar is simulated to reduce its section with time [6], [1], [4], [5].

2.1.1 Time to Corrosion

Christensen Model

Christensen model is based on a probabilistic approach to determine the time to corrosion based on the likelihood of the phenomenon to occur at a certain time in the life of a structure.

$$T_{corr} = X_I \left[\frac{d_c^2}{4k_e k_t k_c D_0 (t_0)^n} \left[erf^{-1} \left(1 - \frac{C_c r}{C_s} \right) \right]^{-2} \right]^{\frac{1}{1-n}} \tag{2.1}$$

X_I: Model Uncertainty

d_c: Depth of reinforcement

k_e k_t k_c: Factors that take into account test methods, curing and environment

D_0: Diffusion

C_s: Water to binder ratio $C_s = A_{cs} \frac{w}{b} + \varepsilon_c s$

Gosh & Padgett Model

Ghosh et al calculate time to corrosion based on Thoft-Christensen model, considering in-field corrosion related studies of existing bridge components in the United States exposed to deicing salts to obtain mean values of chlorides concentration and put them in a modified version of the Thoft-Christensen Model.

$$T_{corr} = \frac{x^2}{4D_c} \left[erf^{-1} \left(\frac{C_0 - C_c r}{C_0} \right) \right]^{-2} \tag{2.2}$$

D_c 1.29 $fraccm^2 year$ Diffusion Coefficient

C_0 0.10 Surface Chloride Concentration

C_r 0.04 Critical Chloride Concentration

While this model provides mean values for the time of initiation of corrosion, it is limited to environments that are controlled by dicing salts only

Life 365 Is a software developed by a consortium of companies of the cementitious materials industries and academic institutions. This software relies on the studies summarized above, mainly using the Thoft-Christensen model, but as opposed to assuming dicing environments only, this software uses a database of chlorides concentration for different location in the USA and Canada, which gives more accurate results depending on the location and environment in which the structure is located.

While this is a more robust model to obtain the initiation of corrosion since it considers the location and environment of the structure and it also has the ability to include other durability issues, it is difficult to implement in a batch run format since the program is in a closed format.

Liu & Weyers Model

$$T_{cr} = \frac{W_{crit}^2}{2k_p} \tag{2.3}$$

$$W_{crit} = \rho_{rust}\left[\pi\left[\frac{Cf_t'}{E_{ef}}\left(\frac{a^2+b^2}{a^2-b^2}+\nu_c\right)+d_o\right]D+\frac{W_{st}}{\rho_{st}}\right] \tag{2.4}$$

$$k_p = 0.098(\frac{1}{\alpha})\pi D i_{corr} \tag{2.5}$$

W_{crit}: Critical amount of corrosion needed to induce cracking.
W_{st}: Mass of corroded steel.
ρ_{rust}: Density of rust material.
ρ_{st}: Density of steel.
f_t': Tensile strength of the concrete.
E_{ef}: Effective elastic modulus of concrete $E_{ef} = \frac{E_c}{1+\phi_{crit}}$
ϕ_{crit} Creep coefficient of the concrete.
D: Diameter of bar.
d_o: Thickness of pore band around the steel/concrete interface.
ν_c: Poisson's ratio of concrete.
C: Cover depth
$a = \frac{D+2d_o}{2}$
$b = C + \frac{D+2d_o}{2}$

2.1.2 Rate of corrosion

Vu et al. Model To estimate the loss of steel cross section due to corrosion a time dependent corrosion rate model was developed by [5], this model implies that corrosion diminishes with time since as corrosion accumulates with time around the steel, it precludes uncorroded steel to react with the environment. The model is shown in Eq. 2.6.

$$i_{corr} = \frac{37.5(1-w/c)}{d_c} \tag{2.6}$$

w/c: Water Cement ratio d_c: Cover depth

In Fig. 2.1 the behavior of this model for different values of w/c ratios is shown. It can be seen that at larger values of cover depth the rate of corrosion decreases rapidly and as the water cement ratio increases the rate of corrosion decreases.

From the Vu et al model the diamater degradation is calculated according to Choe et al as:

$$d_{corr} = d_{bi} - \frac{1.0508(1-w/c)}{d_c}(t-t_{corr})^{0.71} \tag{2.7}$$

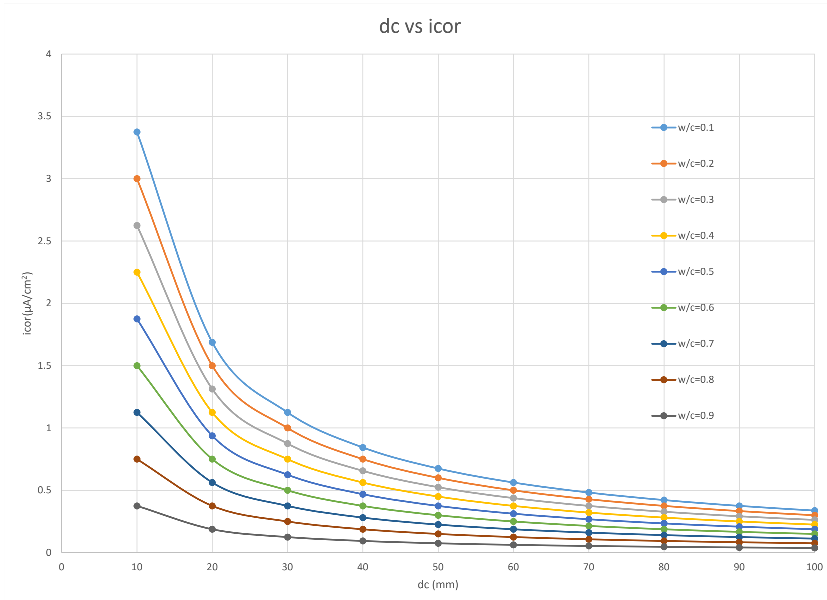

Figure 2.1 Concrete cover depth vs rate of corrosion

d_{bi}: Is the initial diameter of the bar

The diameter is plotted in Fig. 2.2.

These values would correspond to a level of corrosion that varies from 7% corrosion to 21% of corrosion for w/c ratios that ranges from 0.4 to 0.6 The level of corrosion is calculated as:

$$C = \frac{G_o - G}{g_o l_o} * 100 \tag{2.8}$$

Then the Corrosion level is plotted as a function of time in Fig. 2.3

2.1.3 Corrosion modified properties of reinforcing steel bars

In a study presented by Yuan et al [7] it was shown from experimental results that the mechanical properties of steel for different levels of corrosion could be modified for analysis as follows:

$$f_{y,C} = f_{yo}(1 - 0.021C) \tag{2.9}$$

$$f_{u,C} = f_{yo}(1.018 - 0.019C)$$

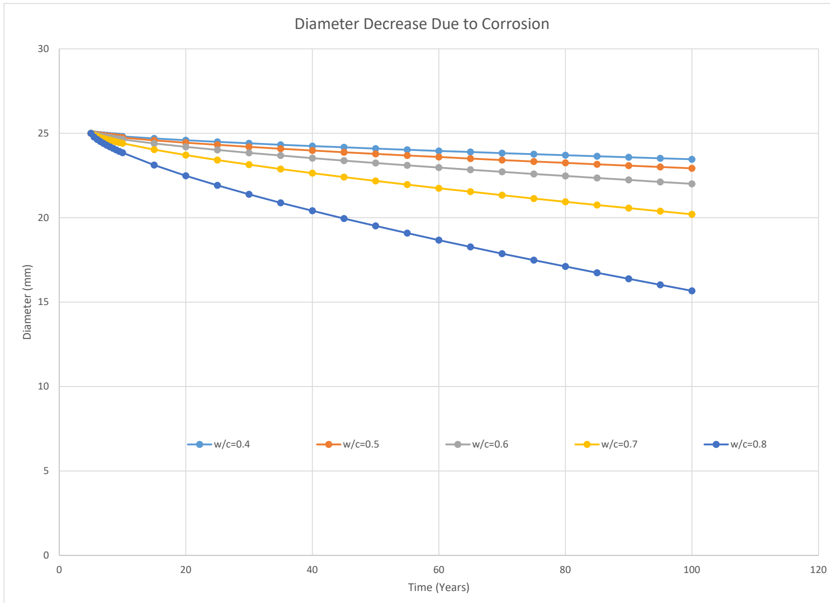

Figure 2.2 Diameter decrease due to corrosion

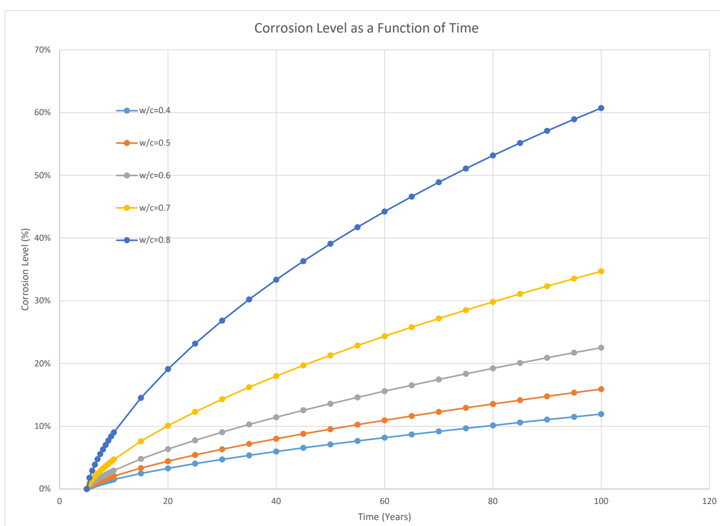

Figure 2.3 Corrosion Level vs Time (years)

$$\delta_{s,C} = \delta_{so}(1 - 0.021C)$$

$$\varepsilon_{y,C} = \varepsilon_{yo}(1 - 0.021C)$$

Choe et al. Model Choe et al research is a seismic fragility estimates for RC columns subjected to corrosion, while the study is probabilistic in nature it defines the reduction in rebar cross section as:

$$d_b(t) = d_{bi} - 2\int_{T_{corr}}^{t} \lambda(t)dt \tag{2.10}$$

Considering the model proposed by Vu et al the bar diameter degradation can be expressed as:

$$d_b(t) = d_{bi} - \frac{1.508(1-\frac{w}{c})^{-}1.64}{d}(t - T_{corr})^{0}.71 \tag{2.11}$$

Where the diameter of the bar and the cover is in (mm). Pros: Easy way to calculate the reduction of bar diameter. Cons: The model carries out the assumptions made by Vu et al. concerning concentration of chlorides assumed and the diffusion assumed.

With this information, the corrosion level is calculated as:

$$CL = \frac{d_i - d(t)}{d_i} \tag{2.12}$$

2.1.4 Corrosion modified properties of reinforcing steel bars

Yuan et al. 2017 Yuan et al performed full-scale tests on columns with corroded longitudinal reinforcement, with which they proposed the following equation to characterize the effects of corrosion in reinforcing steel.

$$f_y(t) = f_{y0}(1 + 0.021CL) \tag{2.13}$$

While the equation showed, agreement with the test results that they performed it has not been corroborated by other researchers. In the current consensus, the model used is the one proposed by Du et al.

Du et al. 2005

Du et al investigated the effect of corrosion on the mechanical properties of steel using corrosion levels of 5

$$f_y(t) = f_{y0}(1 + 0.021CL) \tag{2.14}$$

2.2 Steel Strain Aging

2.2.1 Metallurgical Process

It is generally accepted that strain aging is due to the diffusion of carbon and/or nitrogen atoms in solution to dislocations that have been generated by plastic deformation. Initially, an atmosphere of carbon and nitrogen atoms is formed along the length of a dislocation, immobilizing it. Extended aging, however, results in sufficient carbon and nitrogen atoms for precipitates to form along the length of the dislocation.

These precipitates impede the motion of subsequent dislocations, and result in some hardening and loss in ductility. The extent of strain aging, which is a thermally activated process, depends primarily on aging time and temperature. In general, extended aging results in a saturation value above which further aging has no effect.

A second strengthening mechanism occurs when cold deformation (alone) is applied to steels. When dislocations break away for their pinning interstitial atoms and begin the movement causing slip they begin to intersect with each other. A complex series of interactions between the dislocations occurs, causing them to pin each other, decreasing their mobility. The decreased mobility also results in higher strength, lower ductility and lower toughness. As a result, cold deformed steels already have lowered ductility and toughness before any strain aging occurs and when heating follows cold deformation, the loss in ductility and toughness is greater. It is this combination of events that is the most damaging to the toughness of structural steels.

2.2.2 Strain aging effects in structures

Since it has already been established that strain aging is the process in which steel after being subjected to large strains develops an increased strength and reduced ductility with time and therefore important to include it in a time dependent analysis, considering the fact that plastic hinges will form in a ductile structure and the steel could reach high strains in this regions of the structure. Furthermore strain aging will cause an increased in the strength of the plastic hinge and as a consequence plastic hinges might be formed in regions of the structures that have not been designed for such demands. The effects of strain aging may also alter the transverse reinforcement due to both cold bending, making them susceptible to brittle failure.

According to [3] most strain aging occurs in the first 37 days. Also [2] studied strain aging effects with respect to time for different levels of pre-strains that ranged from $2\varepsilon_y - 10\varepsilon_y$ and for a time frame of 3 days to 50 days, from this study it was determined that a significant effect of strain aging took place from pre-strains $5\varepsilon_y$ and on. Strains higher than $15\varepsilon_y$ indicate a performance level in which substantial damage has been induced in the structure such that it is deemed unrepairable and therefore pre-strains higher that $15\varepsilon_y$ are unpractical and not studied by Montahan et al[2].

Momtahan et al Strain Aging Effects in Yield Strength of Steel

Momtahan et al was able to correlate the increase in yield strength as a function of time and the pre-strain in reinforcing steel bars. The proposed equations are shown below:

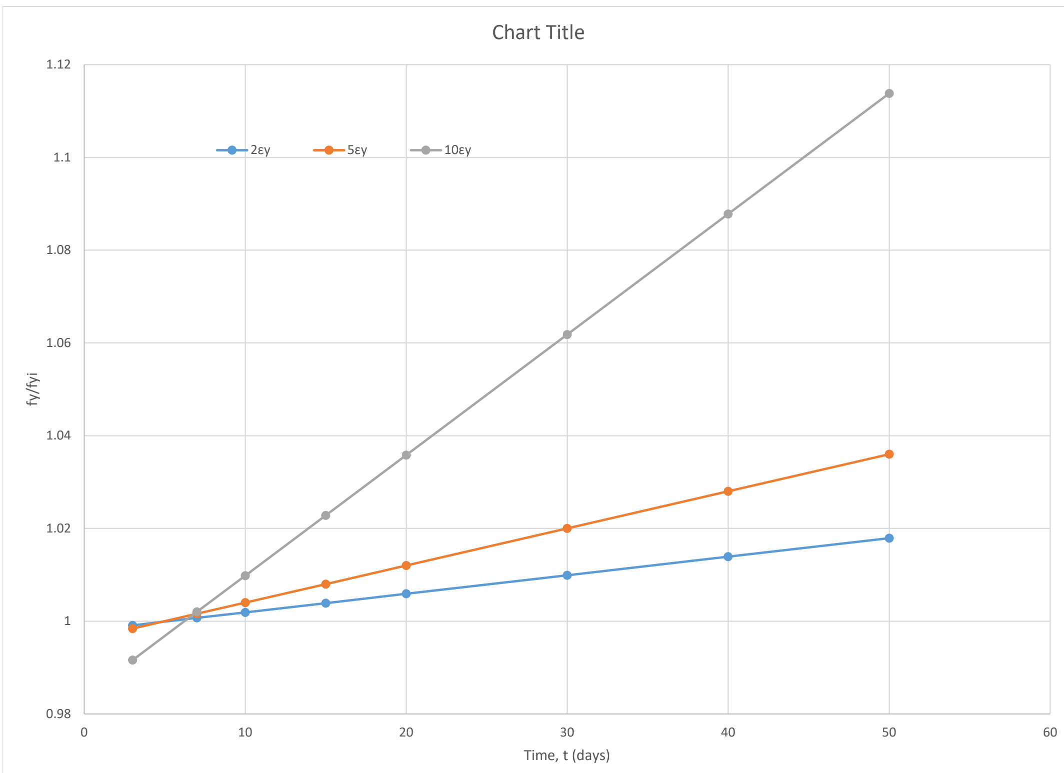

Figure 2.4 Strain Aging effect on Yield Strength vs Time (days)

For $10\varepsilon_y$

$$\frac{f_y}{f_{yi}} = 0.0026t + 0.9838 \tag{2.15}$$

For $5\varepsilon_y$

$$\frac{f_y}{f_{yi}} = 0.0008t + 0.996 \tag{2.16}$$

For $2\varepsilon_y$

$$\frac{f_y}{f_{yi}} = 0.0004t + 0.9979 \tag{2.17}$$

It is proposed to limit the increase in yield strength to the one obtained at 50 days. These equations are plotted in Fig. 2.4

2.3 Concrete Strength

2.4 Welding and Fatigue in Steel Structures

2.5 Repair Effects

2.6 Multiple Seismic Events

2.6.1 Main Shock Series

2.6.2 Main Shock - After Shock Series

2.6.3 Main Shock - After Shock Series - Repair Series

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APPENDIX

Appendix A

LOREM IPSUM

A.1 A First Section

A.1.0.0.1 Filler Text

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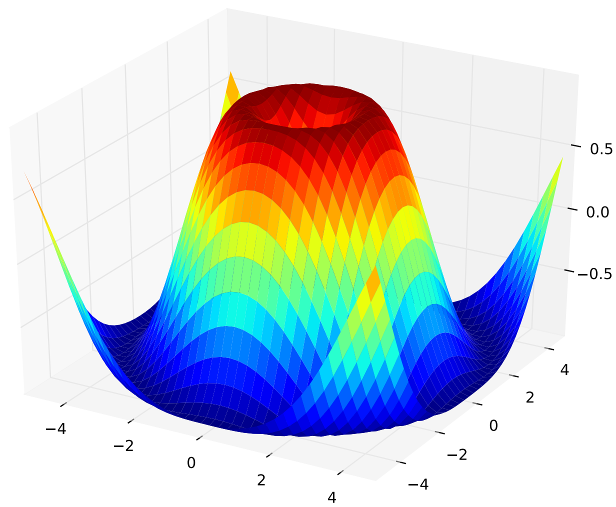

Figure A.1 A figure in the appendix.

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Table A.1 A table in the appendix.

System	Author
TeX	Donald Knuth
LaTeX	Leslie Lamport

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A.2 A Second Section

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