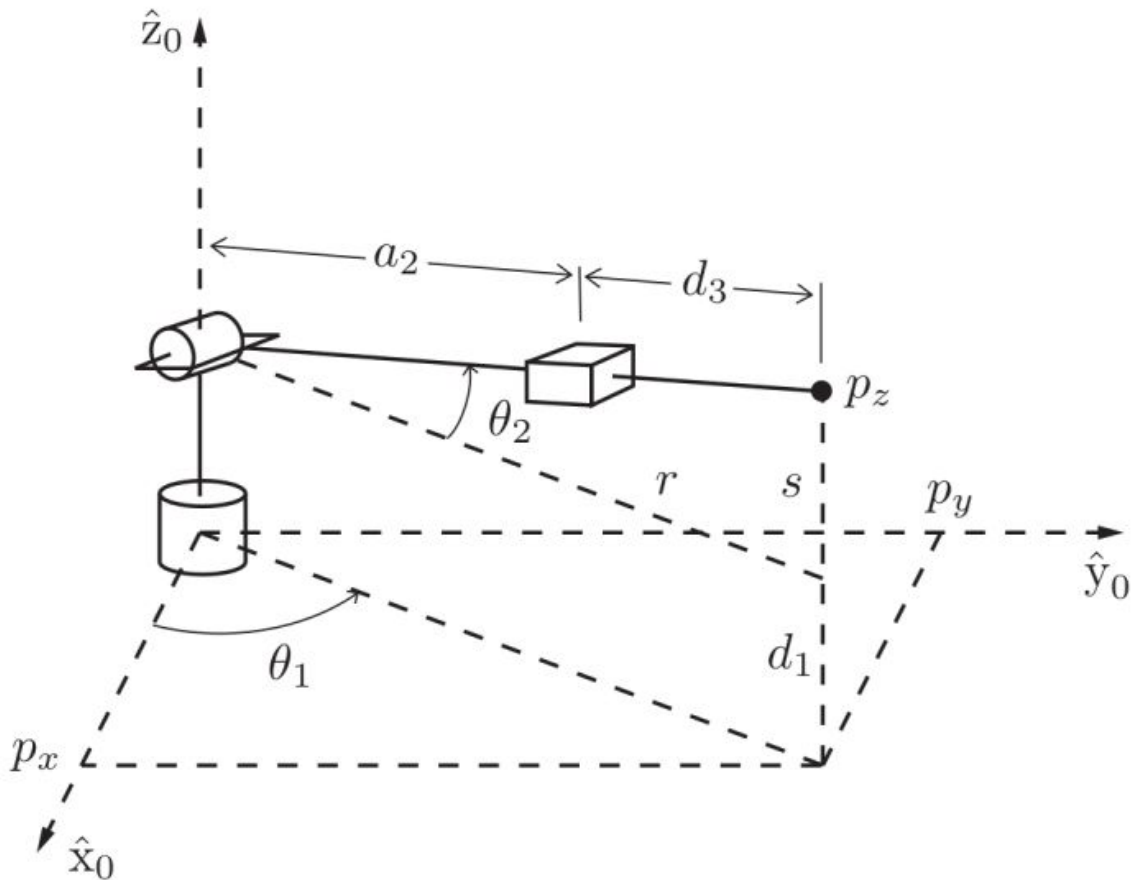


Homework Assignment 3

GitHub link: https://github.com/mhd-medfa/RRP_Robot_Study



Tasks:

1. Derive FK equations for the robot depicted in Fig. 1. Use θ_1 , θ_2 , d_3 as joint space variables, p_x , p_y , p_z as operational space variables. Parameters d_1 , a_2 are known (assign them some positive values for succeeding tasks).

$$p_x = r \cdot \cos(\theta_1) \dots (1)$$

$$p_y = r \cdot \sin(\theta_1) \dots (2)$$

Where:

$$r = (a_2 + d_3) \cdot \cos(\theta_2) \dots (3)$$

$$p_z = d_1 + s \dots (4)$$

Where:

$$s = (a_2 + d_3) \cdot \sin(\theta_2) \dots (5)$$

As a result the position of the end-effector can be described by the vector:

$$O = [px \ py \ pz]^T \dots (6)$$

Where:

$$px = r \cdot \cos(\theta_1) = (a_2 + d_3) \cdot \cos(\theta_1) \cdot \cos(\theta_2)$$

$$py = r \cdot \sin(\theta_1) = (a_2 + d_3) \cdot \sin(\theta_1) \cdot \cos(\theta_2) \dots (7)$$

$$pz = d_1 + s = d_1 + (a_2 + d_3) \cdot \sin(\theta_2)$$

$$\begin{bmatrix} px \\ py \\ pz \end{bmatrix} = \begin{bmatrix} (a_2 + d_3) \cdot \cos(\theta_1) \cdot \cos(\theta_2) \\ (a_2 + d_3) \cdot \sin(\theta_1) \cdot \cos(\theta_2) \\ d_1 + (a_2 + d_3) \cdot \sin(\theta_2) \end{bmatrix}$$

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2. Derive IK equations (closed form solution). How many IK solutions does this robot have? Show all of them.

From (1) & (2) we can find two solutions for θ_1 :

$$\theta_1 = \text{atan2}(py, px) \dots (8)$$

or

$$\theta_1 = \pi + \text{atan2}(py, px) \dots (9)$$

Now to determine θ_2 we have:

$$r = \sqrt{px^2 + py^2} \dots (10)$$

$$s = pz - d_1 \dots (11)$$

Thus:

In case of (8) \Rightarrow

$$2 = \frac{\pi}{2} + \text{atan2}(s, r) \dots (12)$$

Or

In case of (9) \Rightarrow

$$2 = \frac{3\pi}{2} - \text{atan2}(s, r) \dots (13)$$

Finally, in order to find d_3 we have:

In case of d_3 is positive:

$$a_2 + d_3 = \sqrt{r^2 + s^2}$$

$$\Rightarrow d_3 = \sqrt{r^2 + s^2} - a_2 \quad \dots(14)$$

Or

In case of d_3 is negative:

$$a_2 - d_3 = \sqrt{r^2 + s^2}$$

$$\Rightarrow d_3 = a_2 - \sqrt{r^2 + s^2} \quad \dots(15)$$

As a result, we find that we have four different solutions:

$$q = \begin{bmatrix} \frac{\pi}{2} + \text{atan2}(s, r) \\ \sqrt{r^2 + s^2} - a_2 \end{bmatrix} = \begin{bmatrix} \frac{\pi}{2} + \text{atan2}(p_2 - d_1, \sqrt{p_x^2 + p_y^2}) \\ \sqrt{p_x^2 + p_y^2 + (p_z - d_1)^2} - a_2 \end{bmatrix}$$

Or

$$q = \begin{bmatrix} \frac{3\pi}{2} - \text{atan2}(s, r) \\ \sqrt{r^2 + s^2} - a_2 \end{bmatrix} = \begin{bmatrix} \frac{3\pi}{2} - \text{atan2}(p_2 - d_1, \sqrt{p_x^2 + p_y^2}) \\ \sqrt{p_x^2 + p_y^2 + (p_z - d_1)^2} - a_2 \end{bmatrix}$$

Or

$$q = \begin{bmatrix} \frac{\pi}{2} - \text{atan2}(s, r) \\ a_2 - \sqrt{r^2 + s^2} \end{bmatrix} = \begin{bmatrix} \frac{\pi}{2} - \text{atan2}(p_2 - d_1, \sqrt{p_x^2 + p_y^2}) \\ a_2 - \sqrt{p_x^2 + p_y^2 + (p_z - d_1)^2} \end{bmatrix}$$

Or

$$q = \begin{bmatrix} \text{atan2}(py, px) \\ \frac{3\pi}{2} + \text{atan2}(s, r) \\ a2 - \sqrt{r^2 + s^2} \end{bmatrix} = \begin{bmatrix} \text{atan2}(py, px) \\ \frac{3\pi}{2} + \text{atan2}(p2 - d1, \sqrt{px^2 + py^2}) \\ a2 - \sqrt{px^2 + py^2 + (pz - d1)^2} \end{bmatrix}$$

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3. Compute the manipulator Jacobian for representation of linear and angular velocity of point p.

- Use classical approach (partial derivatives).
- Use geometric approach (cross products).
- Use numerical derivatives approach.

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4. Analyze the Jacobian for singularities. Characterize each singular configuration if any.

Singularities are those manipulator configurations where it loses one or more degrees-of-freedom, i.e., it can not move further in specific direction(s). Physically, it means a manipulator would be in a singular configuration if its end-effector cannot move in one or more directions. In other words, infinite joint velocities are required to move the end-effector in that particular direction(s).

Mathematically, singularities relate to the manipulator configuration(s) for which its Jacobian matrix becomes singular, i.e.,

$$\det J = 0$$

We need to take the first three rows in the Jacobian which represents the linear part and calculate the determinant:

$$\det J_v = -1.0(a_2 + d_3)^2 \cos(\theta_2)$$

It means that we have a singular case when:

$$1. \quad \theta_2 = \pm \frac{\pi}{2}$$

In this case, either p_x and p_y will be equal to zero. And this means we lost one DoF because the end-effector intersects with the base frame's Z-axis. Thus any rotation around the base frame won't affect the position of the end-effector.

2. $d_3 = -a_2$

In this case and depending on the equation (14):

$$d_3 = \sqrt{r^2 + s^2} - a_2$$

So d_3 will be equal to $(-a_2)$ in case of both r and s are equal to zero.

From (10) we have:

$$r = \sqrt{p_x^2 + p_y^2}$$

So r will be equal to zero if and only if p_x and p_y are both equal to zero which is the same as the first case.

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5. Compute the velocity of the tool frame when joint variables are changing with time as follows:

$\theta_1(t) = \sin(t)$; $\theta_2(t) = \cos(2t)$; $d_3(t) = \sin(3t)$:

Add some fancy graphs showing evolution of all variables.

Formally, a Jacobian is a set of partial differential equations:

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \mathbf{q}}$$

With a bit of manipulation we can get a neat result:

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \mathbf{t}} \frac{\partial \mathbf{t}}{\partial \mathbf{q}} \rightarrow \frac{\partial \mathbf{x}}{\partial \mathbf{t}} = \mathbf{J} \frac{\partial \mathbf{q}}{\partial \mathbf{t}}$$

Or

$$\dot{\mathbf{x}} = \mathbf{J} \dot{\mathbf{q}}$$

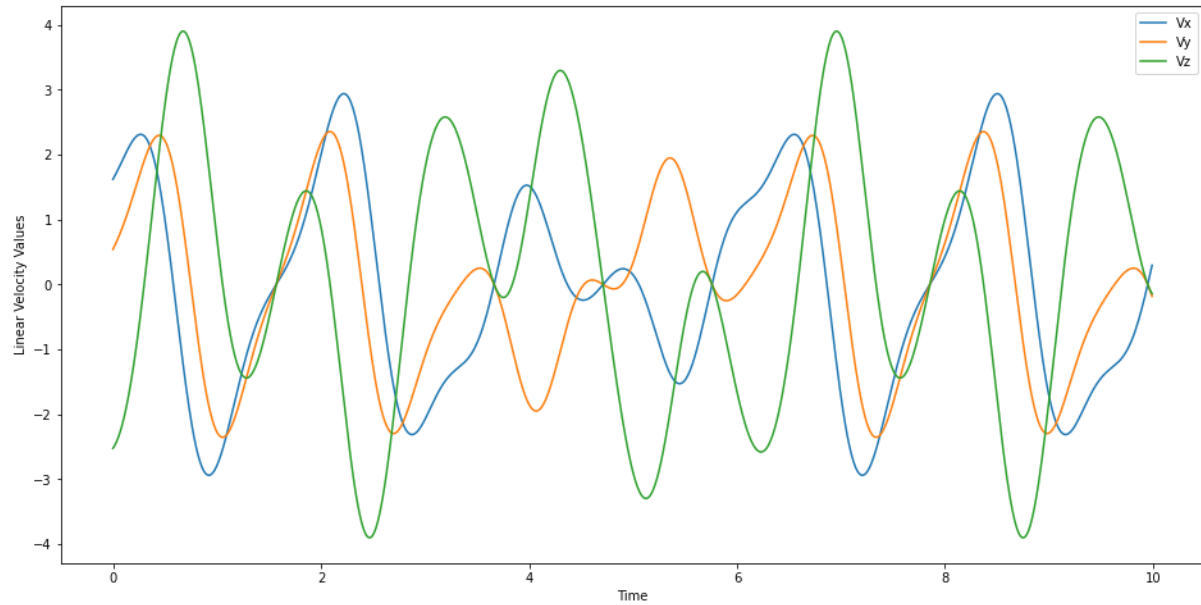
This tells us that the end-effector velocity is equal to the Jacobian \mathbf{J} multiplied by the joint angle velocity.

We can substitute variables into the Jacobian multiplied by joint velocities (*) in order to get the velocities of the tool frame. Joint velocities are, respectively:

$$\begin{bmatrix} \cos(t) \\ -2 \sin(2t) \\ 3 \cos(3t) \end{bmatrix}$$

The following two plots are representing the tool frame velocities where:

1-The first figure shows the linear velocities of the tool frame



2-And the second figure represents the angular velocities

