Lecture 13: Cauchy-Green Strain Tensos Logistics: - HW 5 due - Itw 4 had issue with fault image - HU6 will be posked Last time: Analysis of local deformation - Changes in surface area; ndAz = I FTN dAx - Polar Decomposition: E=RY=VR R= rotation M=VFTF V=VFFT streches - Strech-rotation decomp.: $q = ros_1 = s_2 o r$ Today: - Cauchy-Green strain tensor [- Interpretation of G - Cauchy-Green strain relations

- Components of [

Canoly - Green Strain Tensor

$$\varphi: \mathcal{B} \to \mathcal{B}_{\epsilon} \simeq = \varphi \mathcal{C} + \underline{F} \mathcal{X}$$

$$\underline{F} = \nabla \varphi$$

(right) Cauchy-Greu strain kusat

$$\subseteq = F^T F = y^2$$

ouly contains in formaiton about streches

Can get & from E but not the other way

Uhy not use 1 ? E is much simply to work

To get $U = \sqrt{c} \Rightarrow \text{need to solve eigen value}$ problem:

eigen vechoss:
$$u_1 = \begin{bmatrix} 1 - \lambda_1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 - \lambda$$

$$\Rightarrow \overline{N} = \sqrt{\overline{C}} = \frac{3}{2} \sqrt{\overline{A_1}} \, \overline{n} \cdot \otimes \overline{n} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 1 \end{pmatrix}$$

Note: F=4 because thre is no robation. Here µ are eigenvalues of ⊆

$$U = \sum_{i=1}^{3} \lambda_i$$
 $U_i \otimes U_i$
 λ_i 's principal efreches

 $C = U^2 = \sum_{i=1}^{3} \lambda_i^2$ $U_i \otimes U_i$
 $\mu_i = \lambda_i^2$ eigen values of C are

squares of principal stackes

 $C = C = C = C$

GL= FikFiL "material strain tensor"

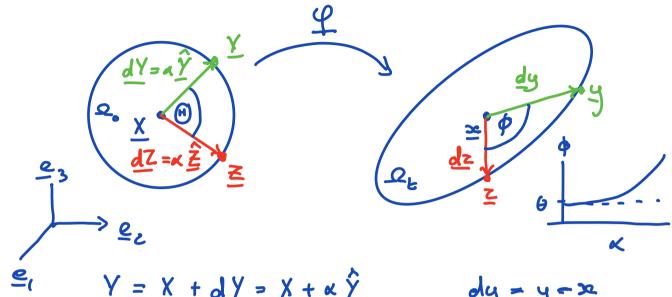
Other strain tensors

I) $E = \frac{1}{2}(C - I)$ Green - Lagrange strain kust $E_{KL} = \frac{1}{2}(C_{KL} - g_{KL})$ material tensor \Rightarrow linear theory

I) $b = FF^{\dagger} = V^{2}$ lest Cauchy Green strain ten. $b_{kl} = FFF$ "spahial tensor"

III) $\underline{e} = \frac{1}{2} (\underline{I} - \underline{F}^{-1} \underline{F}^{-1})$ Full - Almansi kusor ekl = $\frac{1}{2} (S_{kl} - F_{Ik}^{-1} F_{Il})$ "spahial kusor"

luter prefation of =



$$\underline{Y} = \underline{X} + \underline{d}\underline{Y} = \underline{X} + \alpha \underline{\hat{Y}}$$

$$\underline{Z} = \underline{X} + \underline{d}\underline{Z} = \underline{X} + \alpha \underline{\hat{Z}}$$

$$\underline{d}\underline{z} = \underline{Z} - \underline{z}$$

lu limit $\alpha \to 0$ cos $\phi \to \cos \theta(\hat{Y}, \hat{Z})$

Cauchy-Green Strain Relations

$$\lambda(\hat{\underline{Y}}) = \sqrt{\hat{\underline{Y}} \cdot \underline{\underline{C}}}$$

$$\Rightarrow$$
 streck at $\frac{x}{2}$ in direction \hat{y}

$$\cos \Theta(\hat{Y}, \hat{\Xi}) = \frac{\hat{Y} \cdot \hat{Z} \hat{\Xi}}{|\hat{Y} \cdot \hat{Z}|}$$

$$\lambda(\hat{Y}) \quad \lambda(\hat{\Xi})$$

I. Strectus

In the limit
$$\alpha \rightarrow 0$$

$$\frac{|dy|}{|dy|} \rightarrow \lambda(\hat{y}) \quad \text{and} \quad \frac{|dz|}{|d\bar{z}|} \rightarrow \lambda(\hat{z})$$

$$|\overrightarrow{q\lambda}| = |\cancel{\lambda} \cdot \overrightarrow{\zeta}| = \sqrt{(\cancel{\lambda})}$$

$$|\overrightarrow{q\lambda}| = |\cancel{\gamma} \cdot \cancel{\zeta}| = \sqrt{\cancel{\lambda}}$$

$$= \cancel{\gamma} \cdot \cancel{\zeta} \cdot \overrightarrow{\zeta}$$

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If
$$(\lambda_i, \hat{\underline{U}}_i)$$
 are earn pair of $\underline{\underline{U}}$

$$(\subseteq -\lambda_i^* \underline{\underline{I}}) \hat{\underline{U}}_i = \underline{\underline{0}} \quad \text{eigen problem for } \subseteq$$

$$\subseteq \hat{\underline{U}}_i - \lambda_i^* \hat{\underline{U}}_i = \underline{\underline{0}}$$

$$\hat{\underline{U}}_i \cdot \subseteq \hat{\underline{U}}_i - \lambda_i^* \hat{\underline{U}}_i \cdot \hat{\underline{U}}_i = \underline{\underline{0}}$$

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=> proves that is ore principal shockers

Use argument similer to max/min normal stresses to show that his correspond to the max/min strectus.

II, Shear

The shear $f(\hat{Y}, \hat{Z})$ at \hat{Y} is the deauge in angle between the two directions $\hat{Y} \& \hat{Z}$ $f(\hat{Y}, \hat{Z}) = \Theta(\hat{Y}, \hat{Z}) - \Theta(\hat{Y}, \hat{Z})$

where $\lim_{\alpha \to 0} \cos \phi = \cos \theta(\hat{\Sigma}, \hat{\Xi})$

$$\frac{dy \cdot dz}{dy \cdot dz} = \frac{dy \cdot dz}{dy \cdot dz}$$

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$$\frac{dy}{dz} \cdot \frac{dz}{dz} = (\underbrace{F}_{d}\underline{Y}) \cdot (\underbrace{F}_{d}\underline{Z}) = \underline{d}\underline{Y} \cdot \underbrace{F}_{f}_{d}\underline{Z}$$

$$= \underline{d}\underline{Y} \cdot \underline{C}_{d}\underline{Z} = \underline{\alpha}^{2} \hat{Y} \cdot \underline{C}_{d}\underline{Z}$$

$$|\underline{d}\underline{y}| = \underline{\alpha} \lambda(\hat{Y}) = \underline{\lambda}(\underline{Y} \cdot \underline{C}_{f})$$

$$|\underline{d}\underline{z}| = \underline{\alpha} \lambda(\hat{Z} \cdot \underline{C}_{f})$$

$$\cos \phi = \frac{\hat{Y} \cdot \hat{\zeta} \hat{Z}}{|\hat{Y} \cdot \hat{\zeta} \hat{Y}| \sqrt{\hat{Z} \cdot \hat{\zeta} \hat{Z}}} \longrightarrow \cos \theta(\hat{Y}, \hat{Z})$$

Components of
$$\subseteq$$

For frame $\{e_{\underline{I}}\}$
 $C_{\underline{II}} = \lambda^2(e_{\underline{I}})$
 $C_{\underline{IJ}} = \lambda(e_{\underline{I}}) \lambda(e_{\underline{J}}) \sin \gamma(e_{\underline{I}}, e_{\underline{J}})$

diagonal eoup. are squered strectus in coardinate altrebions

off-diagonal components are related to shear between associated coor. dir.

Diagonal components:

$$\lambda(\hat{Y}) - \sqrt{\hat{Y} \cdot \hat{\subseteq} \hat{Y}}$$

$$\Rightarrow$$
 $C_{II} = \underline{e}_{I} \cdot \underline{c} \underline{e}_{I} = \lambda^{2}(\underline{e}_{I})$

Off diagonal components:
$$C_{IJ} = C_{IJ} = C_{$$

$$C_{IJ} = \lambda(\underline{e}_{I}) \lambda(\underline{e}_{J}) \cos\theta(\underline{e}_{I},\underline{e}_{J})$$

shew between two basis vectors

$$\gamma(e_{I},e_{J})=\Theta(e_{I},e_{J})-\theta(e_{I},e_{J})$$

$$O(s^{1/3} = y(s^{1/3}) + y(s^{1/3}) + y(s^{1/3}) + y(s^{1/3}) + y(s^{1/3}) + y(s^{1/3}) + y(s^{1/3})$$

$$O(s^{1/3} = y(s^{1/3}) + y(s^{$$

⇒ Components of ⊆ directly quantity

streck and shear unlike components

of E.