

Chapters 9.3-9

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Modulation Schemes not Requiring Coherent References

- In this section, now we consider two modulation schemes that you do not need to require the acquisition of a local reference signal in phase coherence with the received carrier.

Differential Phase-Shift Keying (DPSK)

- The implementation of a such a scheme presupposes two things;
 - 1 The unknown phase perturbation on the signal varies slowly that the phase is constant from one signalling interval to next.
 - 2 The phase during a given signalling interval bears a known relationship to the phase during the preceding signalling interval bears a known relationship to the phase during the preceding signalling interval.

Table 9.3 Differential Encoding Example

Message sequence:		1	0	0	1	1	1	0	0	0
Encoded sequence:	1	1	0	1	1	1	1	0	1	0
Reference digit:	↑									
Transmitted phase:	0	0	π	0	0	0	0	π	0	π

Differential Encoding Message Sequence

- An arbitrary reference binary digit is being selected as an initial digit of the sequence
- For each digit, the present digit used as a reference
- 0 in the message sequence is encoded as a transition from state of reference digit to the opposite state in the encoded message sequence
- 1 encoded as no change of state

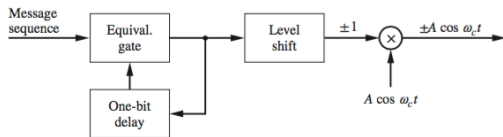
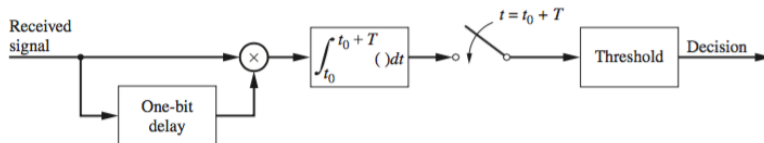


Figure 9.16
Block diagram of a DPSK modulator.

Figure for Differential Encoding Message Sequence

Table 9.4 Truth Table for the Equivalence Operation

Input 1 (Message)	Input 2 (Reference)	Output
0	0	1
0	1	0
1	0	0
1	1	1



Differential Encoding Message Sequence

- After the reference bit and plus the first encoded bit, signal input become $S_1 = A \cos(\omega_c)t$ and $R_1 = A * \cos(\omega_c) * t$
- Than the output correlator is; $v_1 = \int_0^T A^2 \cos^2(\omega_c t) dt$ which eventually become $\frac{1}{2} A^2 T$
- The optimum detector for binary will become
$$l = x_k x_k - 1 + y_k y_k - 1$$
- Without a loss of of generality, we can choose $\theta = 0$; we found outputs at $t = 0$ to be:
 - $x_0 = \frac{AT}{2} + n_1$ and $y_0 = n_3$ and where
$$n_1 = \int_{-T}^0 n(t) \cos^2(\omega_c t) dt$$
 - $n_3 = \int_{-T}^0 n(t) \sin^2(\omega_c t) dt$. Similarly, at the time $t = T$, the outputs are ; $x_1 = \frac{AT}{2} + n_2$ and $y_1 = n_4$
 - $n_2 = \int_0^T n(t) \cos^2(\omega_c t) dt$
 - $n_4 = \int_0^T n(t) \sin^2(\omega_c t) dt$

Important Figure for Differential Encoding

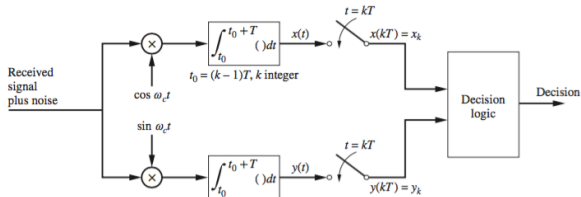


Figure 9.18
Optimum receiver for binary differential phase-shift keying.

If $\ell > 0$, the receiver chooses the signal sequence

$$s_1(t) = \begin{cases} A \cos(\omega_c t + \theta), & -T \leq t < 0 \\ A \cos(\omega_c t + \theta), & 0 \leq t < T \end{cases} \quad (9.95)$$

as having been sent. If $\ell < 0$, the receiver chooses the signal sequence

$$s_2(t) = \begin{cases} A \cos(\omega_c t + \theta), & -T \leq t < 0 \\ -A \cos(\omega_c t + \theta), & 0 \leq t < T \end{cases} \quad (9.96)$$

- It follows as n_1, n_2, n_3 and n_4 are uncorrelated and zero-mean Gaussian random variables with variances $\frac{N_0 T}{4}$ and they are independent.
- Expression for Probability error
- We can define new gaussian random variables such as:

$$\omega_1 = \frac{n_1}{2} + \frac{n_2}{2}$$

$$\omega_2 = \frac{n_1}{2} - \frac{n_2}{2}$$

$$\omega_3 = \frac{n_3}{2} + \frac{n_4}{2}$$

$$\omega_4 = \frac{n_3}{2} - \frac{n_4}{2}$$

- Probability can be written in terms of Gaussian variables:

$$P_E = Pr[(\frac{AT}{2} + \omega_1)^2 + (\omega_3)^2 < (\omega_2^2 + \omega_4^2)]$$

- Gaussian variables will also let us define the Ricean random variables. Ricean random variable will become:

$$R_1 = \sqrt{(\frac{AT}{2} + \omega_1)^2 + \omega_3^2}$$

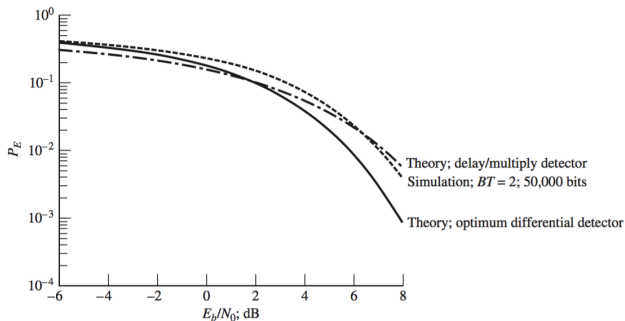
- Also Rayleigh random variable will become $R_2 = \sqrt{\frac{\omega_2^2}{\omega_4^2}}$

- If we also define the bit energy E_b as $A^2 \frac{A^2 T}{2}$ will give;

$$P_E = \frac{1}{2} e^{(\frac{-E_b}{N_0})} \text{ for the optimum DPSK receiver.}$$

- At the large values $\frac{-E_b}{N_0}$ values of ; $P_E = Q[\sqrt{\frac{-E_b}{N_0}}] = Q[\sqrt{z}]$

- Following result obtained by using the asymptotic approximation; $P_E = \frac{e^{(-E_b/N_0)}}{2\sqrt{\pi \frac{E_b}{N_0}}}$



Comparison of Digital Modulation Systems

- Bit error probabilities are compared in Figure 9.22 for the modulation schemes that considered in this chapter. Note that the curve for antipodal binary PAM is identical to BPSK
- Also bit error probability of antipodal PAM becomes worse the larger M . Curves move more to the right as M gets larger

Important figure for Chapter 9

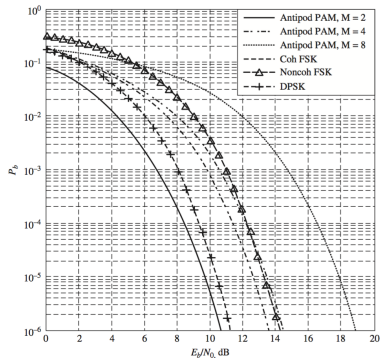


Figure 9.22
Error probabilities for several binary digital signaling schemes.

- Non-coherent binary FSK and PAM with $M=4$ have almost identical performance at large signal-to-noise ratios.
- In addition to cost and complexity implementation, there are many other considerations in choosing one type of digital data system over another.
- Some channels, where the channel gain, phase or when both are in effect, we use a noncoherent system may be dictated because of impossibility of establishing a coherent reference at the receiver under such conditions. They will be referred as "fading".

Multipath Interference (1)

- Additive Gaussian noise is not sufficient to accurately model the transmission channel
- Other sources of degradation:
 - bandwidth limiting by the channel
 - impulse noise (lightnings, switching)
 - RF interference from other transmitters
 - *multipath interference* from signal reflections and scattering

Multipath Interference (2)

- Two-way multipath model: $y(t) = s_d(t) + \beta s_d(t - \tau_m) + n(t)$
 - $n(t)$ Gaussian noise component
 - $s_d(t)$ Signal from the direct path
 - β Gain of secondary path component
 - τ_m Time delay of secondary path component
- For binary phase-shift keying signals: $s_d(t) = A d(t) \cos(\omega_c t)$
 - $d(t)$ Data stream (sequence of ± 1 rectangular pulses) of width T
 - ω_c Carrier frequency

Multipath Interference (3)

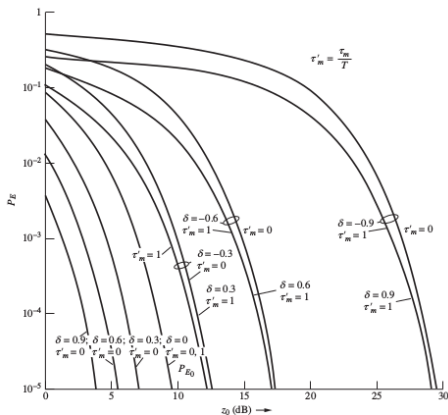
- Input of the integrator at the receiving end: $x(t) = LP\{2y(t) \cos(\omega_c t)\} = Ad(t) + \beta Ad(t - \tau_m) \cos(\omega_c \tau_m) + n_c(t)$
- Two scenarios:
 - $\tau_m/T \cong 0$ The original and reflected signals are almost congruent, so $\omega_c \tau_m$ is uniformly distributed in $[-\pi, \pi]$. When many reflection components are considered, the envelope of the signal assumes a Rayleigh or Rician distribution
 - $0 < \tau_m/T \leq 1$ Adjacent bits in the original and reflected signals overlap; inter-symbol interference appears

Multipath Interference - second scenario (1)

- Four equally likely cases; total probability of error is:
$$P_E = \frac{1}{4}[P(E|++) + P(E| - +) + P(E| + -) + P(E| - -)]$$
- Noise on the integrator integrator out is Gaussian-distributed with $\mu = 0$ and $\sigma_n^2 = N_0 T$
- Due to the symmetric nature of the overlapping bits and Gaussian probability density function, only two cases need to be computed
 - $P(E|++) = P(E|--) = Q\left[\sqrt{\frac{2E_b}{N_0}}(1 + \delta)\right]$
 - $P(E|+-) = P(E|-+) = Q\left[\sqrt{\frac{2E_b}{N_0}}\left((1 + \delta) - \frac{2\delta\tau_m}{T}\right)\right]$
- After substituting the cases above into the matching ones:
$$P_E = \frac{1}{2}Q\left[\sqrt{2z_0}(1 + \delta)\right] + \frac{1}{2}Q\left[\sqrt{2z_0}\left((1 + \delta) - \frac{2\delta\tau_m}{T}\right)\right]$$

Multipath Interference - second scenario (2)

- Overall probability of error changes with $z_0 = \frac{E_b}{N_0} = \frac{A^2 T}{2N_0}$



Equalization

- Equalization is used in telecommunication to reverse the signal degradation caused by multipath propagation and bandwidth limitations
- Simplest form of equalization consists in an inverse filter - *Tapped-delay-line filter*
- Two ways of determining the filter coefficients:
 - zero-forcing
 - mean-square error

Equalization by Zero Forcing

- Impulse response of equalized output:
$$p_{eq}(mT) = \sum_{n=-N}^N \alpha_n p_c((m-n)T) \Rightarrow [P_{eq}] = [P_c][A]$$
- $[P_{eq}]$ is a column vector composed of: N zeros, 1, N zeros
- Equalization filter coefficient matrix: $[A]_{opt} = [P_c]^{-1}[P_{eq}]$
- Multiplying by $[P_{eq}]$ corresponds to picking the middle column of matrix $[P_c]^{-1}$

Equalization by Minimum Mean-Squared Error (1)

- Obtain filter coefficients that minimize the difference between the output of the equalizer and the actual output:

$$\varepsilon = E \{ [z(t) - d(t)]^2 \} = \textit{minimum}$$

- $z(t)$ is the equalizer output response (incl. noise):

$$z(t) = \sum_{n=-N}^N \alpha_n p_c((m-n)T)$$

- $d(t)$ is the desired response

Equalization by Minimum Mean-Squared Error (2)

- ε is concave and can be minimized by derivation:

$$\frac{\delta \varepsilon}{\delta \alpha_m} = 0 = 2E \left\{ [z(t) - d(t)] \frac{\delta z(t)}{\delta \alpha_m} \right\}$$

- Substituting $z(t)$ gives the following conditions (in terms of cross-correlation): $R_{yz}(m\Delta) = R_{yd}(m\Delta) = 0$
 - $R_{yz}(\tau) = E[y(t)z(t + \tau)]$
 - $R_{yd}(\tau) = E[y(t)d(t + \tau)]$
- In terms of matrices: $[R_{yy}][A]_{opt} = [R_{yd}]$
- Solving for the filter taps: $[A]_{opt} = [R_{yy}]^{-1}[R_{yd}]$

Tap Weight Adjustment (LMS Algorithm) (1)

- How to obtain $d(t)$
 - 1 Periodically send known data sequence used for weight adjustment
 - 2 Use method 1 for first guess and then use detected data (*decision-directed* mode)
- Apply gradient descent to initial weight values ($[A]^{(0)}$):
$$[A]^{(k+1)} = [A]^{(k)} + \frac{1}{2}\mu[-\nabla\varepsilon^{(k)}]$$
 - k iteration of weights calculation
 - $\nabla\varepsilon$ slope of error surface
 - μ size of the step

Tap Weight Adjustment (LMS Algorithm) (2)

- Alternative approach (Least-Mean-Square):
$$\alpha_m^{(k+1)} = \alpha_m^{(k)} - \mu y[(k-m)\Delta] \epsilon(k\Delta)$$
- $\epsilon(k\Delta)$ is the error given by $y_{eq}(k\Delta) - d(k\Delta)$
 - $y_{eq}(k\Delta)$ equalization filter output
 - $d(k\Delta)$ data sequence used for training