# Appendix: noise

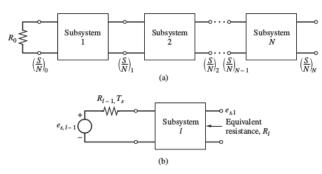
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#### Characterization of noise in systems

- Noise can be modeled and characterized on a subsystem-basis
- Each subsystem can be analyzed separately and optimized for low noise performances



#### Noise Figure of a System

- Noise figure  $F_l$ : ratio between SNR at subsystem input and output:  $\left(\frac{S}{N}\right)_l = \frac{1}{F_l} \left(\frac{S}{N}\right)_{l-1}$
- Ideally,  $F_l=1$  (no additional noise introduced), tipically between 2 and 8 dB
- Without having to calculate the signal power:

$$F_l = 1 + \frac{P_{int,l}}{G_a k T_0 B}$$

 $P_{int,l}$  Available, internally-generated noise power

 $G_a$  Available power gain

k Boltzmann's constant

 $T_0$  Standardized temperature, 290K

B Frequency band

■ For high gains,  $F_l$  approaches 1



#### Noise Temperature

- Power produced by a noisy resistor:  $P_{a,R} = kTB$ 
  - k Boltzmann's constant,  $1.38 \times 10^{-23} J/K$
  - T Temperature of the resistor, in Kelvin
  - B Frequency band, in Hertz
    Noise power independent on the resistor value
- $\blacksquare$  Equivalent noise temperature:  $T_n = \frac{P_{n,max}}{kB}$

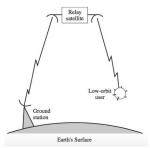


# Free Space Propagation Example

- As a final work for the noise calculation, we will investigate the "free-space electromagnetic-wave propagation channel.
- To understand it fully on a practical example, we will investigate the communication tie between a synchronous-orbit relay satellite and a low-orbit satellite.

# Free Space Propagation Example

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# Investigating the Free-Space Propagation Example

- We made some assumptions in regard to the example.
  - 1 We have assumed that relay satellite transmitted signal power  $P_t$
  - 2 It radiated isotropically
- Power density at a distance will be given by;  $P_t = \frac{P_t}{4\pi d^2} W/m^2$
- If the satellite antenna has directivity, with the radiated power being directed toward low-orbit vehicle, antenna can be explained by the antenna power gain  $G_T$  over the isotropic radiation level.

# Aperture-Type Antennas with Aperture Area $A_t$

- For aperture-type antennas with aperture area  $A_T$  large compared with the square of the transmitted wavelength  $\lambda^2$ .
- We can show that maximum gain will become:
  - 1  $G_T = \frac{4\pi A_T}{\lambda^2}$
  - 2 Also the power  $P_R$  intercepted by the receiving antenna is given by the product of the receiving aperture area  $A_R$  and the power density at the aperture. Thi will give us:  $p_R = p_t A_R = \frac{P_T G_T}{4\pi d^2} A_R$
- If we also include other loses and use maximum gain  $G_R$ , it will yield into this formula:  $P_R = (\frac{\lambda}{4\pi d})^2 \frac{P_T G_T G_R}{L_0}$
- The factor  $(\frac{4\pi d}{\lambda})^2$  is referred as the "free-space loss"



#### Receiver Power

- It is easier to work with decibels when we calculate the receiver power.
- If we take the  $10\log_{10}P_R$ , than we obtain :  $10\log_{10}P_R = 20\log_{10}(\frac{\lambda}{4\pi d}) + 10\log_{10}P_T + 10\log_{10}G_T + 10\log_{10}G_R 10\log_{10}L_0$
- $10 \log_{10} P_R$  can be interpreted as receiver power in decibels referenced to  $1 \ W$
- lacksquare Also  $10\log_{10}P_T$  is referred as the transmitted signal in dbW

