# FP2: Torso Pose Estimation on the HRP4 Humanoid Robot

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#### Introduction

Intro.

#### Kinematic Model

#### Extended Kalman Filter

# Accelerometer Integration

# Gyroscope Integration

#### IMU

Experiments (5.1).

# Filtering Linear Velocities

#### Trilateration

## MPC Loop Closure

Regulation

#### Kinematic Model of the Unicycle

Brief description:

$$\dot{x} = v\cos(\theta)$$
$$\dot{y} = v\sin(\theta)$$
$$\dot{\theta} = \omega$$

with v and  $\omega$  respectively linear and angular velocity.

## **Proportional Controller**

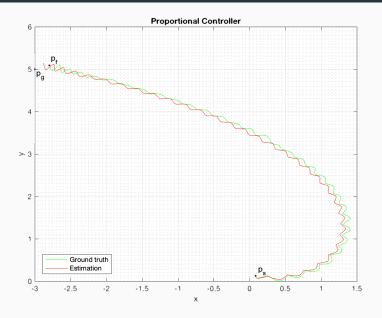
Control law:

$$v = k_1 \| \mathbf{p}_g - \hat{\mathbf{p}}_t \|$$
$$\omega = k_2 e_{\theta}$$

with  $e_{\theta}$  angle between the sagittal vector of the unicycle and the vector pointing from the unicycle towards the goal,  $k_1=0.18$  and  $k_2=0.014$ . Forcing v and  $\omega$  to zero when  $\|\boldsymbol{p}_g-\hat{\boldsymbol{p}}_t\|<0.25$ . Desired and final configuration:

$$\mathbf{q}_g = (-3, 5, \cdot)^T$$
  
 $\mathbf{q}_f = (-2.798, 5.090, 0.98\pi)^T$   
 $\hat{\mathbf{q}}_f = (-2.885, 5.127, 0.979\pi)^T$ 

### Proportional Controller: x-y Plot



#### Cartesian Regulation

Let's express the coordinates of the unicycle in a reference frame  $\mathcal{F}_g$  fixed at a position  $(x_g, y_g)^T$  and rotated by  $\theta_g$  around  $\mathcal{F}_w$ :

$$\begin{pmatrix} g_X \\ g_Y \\ g_\theta \end{pmatrix} = R_Z^{\mathsf{T}}(\theta_g) \begin{pmatrix} x - x_g \\ y - y_g \\ \theta - \theta_g \end{pmatrix}$$

## Cartesian Regulation

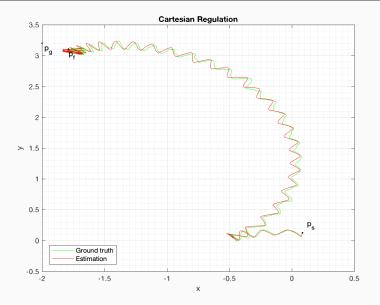
Control law:

$$v = -k_1({}^{g}x\cos({}^{g}\theta) + {}^{g}y\sin({}^{g}\theta))$$
$$\omega = k_2(A\tan({}^{g}y, {}^{g}x) - {}^{g}\theta + \pi)$$

with  $k_1=0.07$  and  $k_2=0.01$ . Forcing v and  $\omega$  to zero when  $\|p_g-\hat{p}_t\|<0.2$ . Desired and final configuration:

$$\mathbf{q}_g = (-2, 3.2, \cdot)^T$$
  
 $\mathbf{q}_f = (-1.788, 3.105, 1.562\pi)^T$   
 $\hat{\mathbf{q}}_f = (-1.823, 3.108, 1.562\pi)^T$ 

#### Cartesian Regulation: x-y Plot



#### Kinematic Model of the Unicycle in Polar Coordinates

Brief description:

$$\dot{\rho}_r = -v\cos(\gamma_r)$$

$$\dot{\gamma}_r = \frac{\sin(\gamma_r)}{\rho_r} v - \omega$$

$$\dot{\delta}_r = \frac{\sin(\gamma_r)}{\rho_r} v$$

Polar coordinates can be obtained from the generalized coordinates of the unicycle  $(x, y, \theta)^T$  by computing:

$$\rho_r = \sqrt{{}^g x^2 + {}^g y^2}$$

$$\gamma_r = \text{Atan2}({}^g y, {}^g x) - {}^g \theta + \pi$$

$$\delta_r = \gamma_r + {}^g \theta$$

#### Posture Regulation

Control law:

$$v = k_1 \rho_r \cos(\gamma_r)$$

$$w = k_2 \gamma_r + k_1 \frac{\sin(\gamma_r) \cos(\gamma_r)}{\gamma_r} (\gamma_r + k_3 \delta_r)$$

with  $k_1=0.1$ ,  $k_2=0.007$   $k_3=0.004$ . Forcing v and  $\omega$  to zero when  $\rho_r<0.2$ . Desired and final configuration:

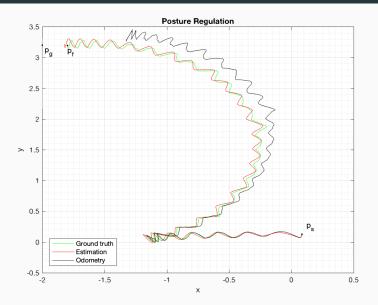
$$\mathbf{q}_g = (-2, 3.2, \pi)^T$$

$$\mathbf{q}_f = (-1.797, 3.194, 1.024\pi)^T$$

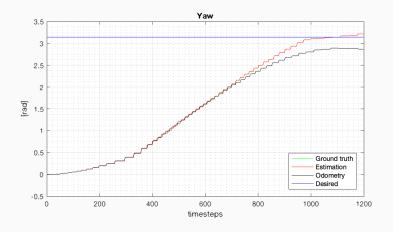
$$\hat{\mathbf{q}}_f = (-1.824, 3.222, 1.024\pi)^T$$

$$\bar{\mathbf{q}}_f = (-1.282, 3.424, 0.912\pi)^T$$

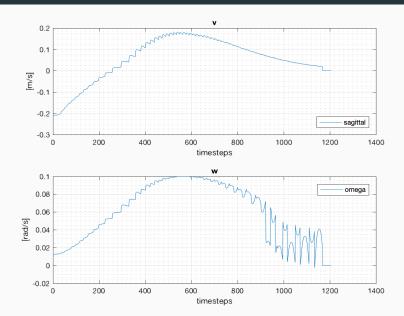
#### Posture Regulation: x-y Plot



## Posture Regulation: Yaw Plot



#### Posture Regulation: Velocity Profile Plots

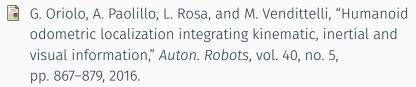


## Conclusion

Conclusion.



#### References



- W. Hereman and J. William S. Murphy, "Determination of a Position in Three Dimensions Using Trilateration and Approximate Distances," 1995.
- B. Siciliano, L. Sciavicco, L. Villani, and G. Oriolo, *Robotics:*Modelling, Planning and Control.

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