

Predicting Resonant Behaviour of Undamped Multipendulums by Perturbing Normal Modes With Respect to Constraint Forces

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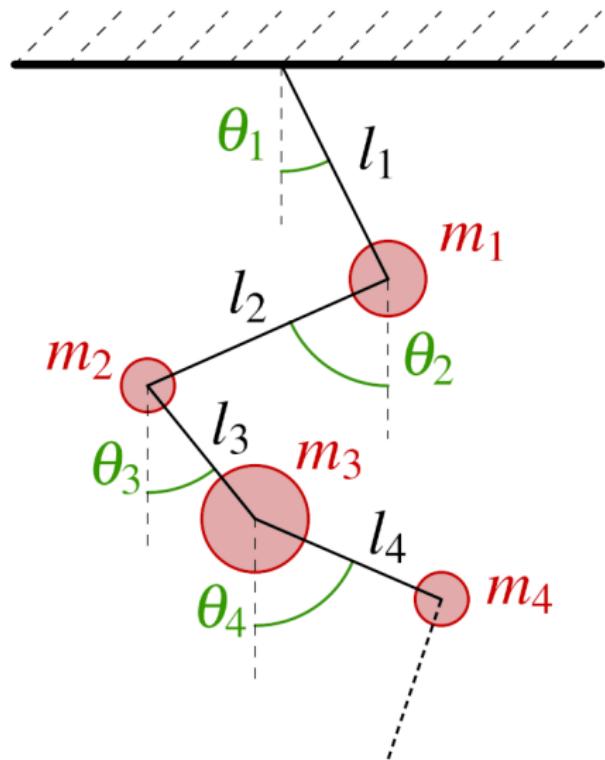
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Introduction and Motivation

Every pendulum has its mode.

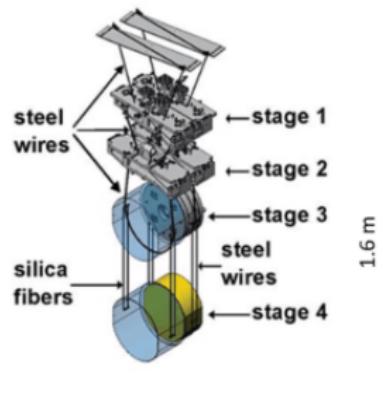
Jacob J. Edginton, 2023



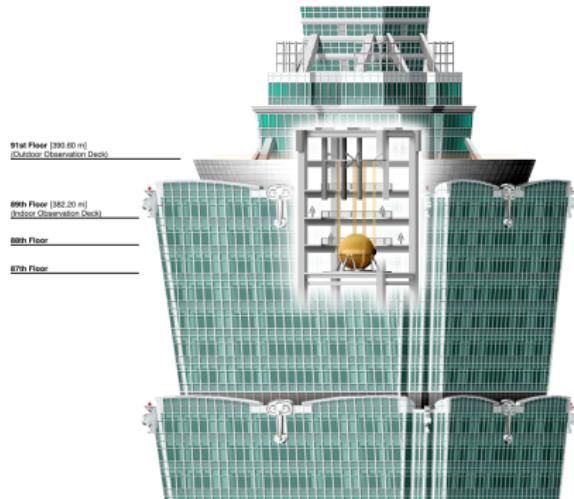
Introduction and Motivation

Real-life Examples of a Multipendulum

LIGO's Quadruple Pendulum



The top two masses of the LIGO pendulum are 20 kg and the lower two masses 40 kg.



Images credit: LIGO/Caltech; Wikimedia/Someformofhuman

Motion of a Multipendulum

Physical Descriptors

1. The potential energy:

$$U = - \sum_{i=1}^N \tau_i(t) \theta_i - \sum_{i=1}^N m_i g \sum_{j=1}^i l_j \cos \theta_j$$

where $\tau_i(t)$ is the external torque acting on the i -th segment

2. The kinetic energy

$$T = \sum_{i=1}^N \frac{1}{2} m_i \left(\left(\sum_{j=1}^i \dot{\theta}_j l_j \cos \theta_j \right)^2 + \left(\sum_{j=1}^i \dot{\theta}_j l_j \sin \theta_j \right)^2 \right)$$

3. The Lagrangian

$$L = T - U$$

Motion of a Multipendulum

Euler-Lagrange Equations and RK-Compatible Formulation

1. The Euler-Lagrange equations:

$$\sum_{i=n}^N m_i \left[g \sin \theta_n + \sum_{j=1}^i l_j \left[\ddot{\theta}_j \cos(\theta_n - \theta_j) + \dot{\theta}_j^2 \sin(\theta_n - \theta_j) \right] \right] = F_n(t)$$

for $n = 1, 2, \dots, N$, where $F_n(t) = l_n^{-1} \tau_n(t)$

2. We define the following quantities:

$$S_a = F_a(t) - \sum_{i=a}^N m_i \left[g \sin \theta_a + \sum_{j=1}^i l_j \dot{\theta}_j^2 \sin(\theta_a - \theta_j) \right]$$

$$M_{ab}^* = \cos(\theta_a - \theta_b) \mu_{ab}, \quad M_n^* \text{ being } M^* \text{ with } n\text{-th col. set to } \vec{S}$$

$$\text{then } \ddot{\theta}_n(\vec{\theta}, \dot{\vec{\theta}}, t) = \frac{\det(M_n^*)}{l_n \det(M^*)}$$

Normal Modes of a Multipendulum Under Free Conditions

Why Care About Normal Modes?

1. Mode: all components have the same frequency.
2. **Normal modes** - emerge by perturbing around an equilibrium
3. Normal modes *tend* to match resonant frequencies
4. System with many coordinates: ambiguous definition of resonance.
5. Maximised mechanical energy

Normal Modes of a Multipendulum Under Free Conditions

Finding the Normal Modes - The Natural Lagrangian

1. The only stable equilibrium: $\theta_i = 0, i = 1, 2 \dots N$
2. The Lagrangian perturber to the 2nd order about the equilibrium:

$$L = \frac{1}{2} \sum_{i=1}^N m_i \left(\sum_{j=1}^i \dot{\theta}_j l_j \right)^2 - \frac{1}{2} g \sum_{i=1}^N l_i \theta_i^2 \mu_i$$

3. We find the natural coordinates as:

$$\begin{aligned} q_1 &= \sqrt{m_1} l_1 \theta_1 & \theta_1 &= \frac{q_1}{l_1 \sqrt{m_1}} \\ q_n &= \sqrt{\frac{m_n}{m_{n-1}}} q_{n-1} + \sqrt{m_n} l_n \theta_n & \theta_n &= \frac{1}{l_n} \left(\frac{q_n}{\sqrt{m_n}} - \frac{q_{n-1}}{\sqrt{m_{n-1}}} \right) \end{aligned}$$

Normal Modes of a Multipendulum Under Free Conditions

Finding the Normal Modes - The k -matrix

1. The k -matrix elements are now found to be

$$k_{ij} = \frac{\partial^2 V}{\partial q^i \partial q^j} = \begin{cases} \frac{g}{l_N} & i = j = N \\ -\frac{g}{l_N} \sqrt{\frac{m_N}{m_{N-1}}} & i = N-1, j = N \\ -\frac{g}{l_{j+1}} \frac{\mu_{j+1}}{\sqrt{m_j m_{j+1}}} & i = j+1, j \neq N \\ \frac{g}{m_j} \left(\frac{\mu_j}{l_j} + \frac{\mu_{j+1}}{l_{j+1}} \right) & i = j \neq N \\ -\frac{g}{l_j} \frac{\mu_j}{\sqrt{m_{j-1} m_j}} & i = j-1, j \neq N \\ 0 & \text{otherwise} \end{cases}$$

Normal Modes of a Multipendulum Under Free Conditions

Finding the Normal Modes - Back to Original Coordinates

1. The normal modes are formed from the eigenvectors v_n of k and their associated eigenvalues λ_n like so:

$$\vec{q}_n(t) = \vec{v}_n e^{i\omega_n t}, \omega_n = \sqrt{\lambda_n}$$

2. Changing back to θ coordinates:

$$\begin{aligned}\theta_{n,1}(t) &= \frac{v_{n,1}}{l_1 \sqrt{m_1}} e^{i\omega_n t} \\ \theta_{n,i}(t) &= \frac{1}{l_i} \left(\frac{v_{n,i}}{\sqrt{m_i}} - \frac{v_{n,i-1}}{\sqrt{m_{i-1}}} \right) e^{i\omega_n t}\end{aligned}$$

where n is the index of the normal mode and i is the index of the segment

Normal Modes of a Multipendulum Under Free Conditions

Comparison of Normal Mode Frequencies to Resonant Frequencies

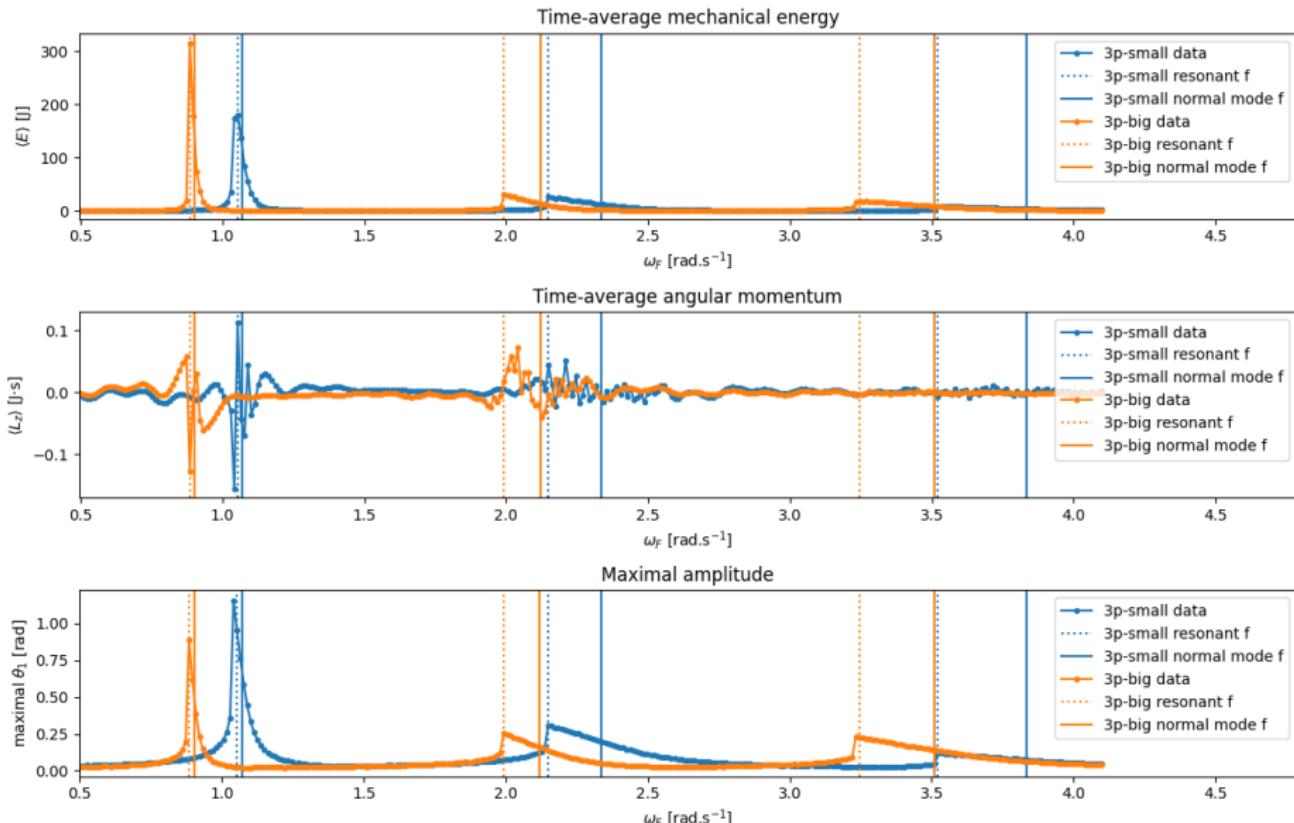
1. We choose a random small driving force mode - qualitative picture
2. Two triple pendulums:

$$3p - \text{small} : \vec{m} = \begin{pmatrix} 5 \\ 3 \\ 3 \end{pmatrix} \text{kg}, \vec{l} = \begin{pmatrix} 5 \\ 3 \\ 3 \end{pmatrix} \text{m}$$

$$3p - \text{big} : \vec{m} = \begin{pmatrix} 5 \\ 5 \\ 5 \end{pmatrix} \text{kg}, \vec{l} = \begin{pmatrix} 5 \\ 5 \\ 5 \end{pmatrix} \text{m}$$

Normal Modes of a Multipendulum Under Free Conditions

Comparison of Normal Mode Frequencies to Resonant Frequencies - Motional Spectrum



A Driven Multipendulum

Driving Force Equations - The Impact on Resonance

1. Driving force in the form

$$\vec{\tau}(t) = \vec{Q}e^{-i\omega_\tau t}$$

where \vec{Q} is the "force mode"

2. Separate the potential term
3. Updated E-L equation:

$$\tau_i(t) = \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\theta}_i} \right) - \frac{\partial L}{\partial \theta_i}$$

4. Resonant frequencies depend on the driving force

A Driven Multipendulum

The Mode Hypothesis

THE MODE HYPOTHESIS

The trajectory of a driven multipendulum at resonance is a mode, which is perturbed from an associated normal mode.

1. We can take an arbitrary mode trajectory and interpret the driving force as a constraint force
2. The holonomic mode constraint:

$$\vec{\theta}(t) = \vec{u} e^{i\omega(\vec{u})t}$$

3. Does the system possess a scale?

Mode Space

Definition of Mode Space - Natural Modal Frequency - Isofrequents

1. Space \mathbb{R}^N spanning all possible \vec{u} modes
2. Every mode has its natural frequency (scalar field $\omega_0(\vec{u})$) and constraint force (vector field $\vec{Q}(\vec{u})$)
3. By reducing the perturbed Lagrangian to θ_1 we get

$$\omega_0(\vec{u}) = \left[\frac{g \sum_{i=1}^N l_i u_i^2 \mu_i}{\sum_{i=1}^N m_i \left(\sum_{j=1}^i u_j l_j \right)^2} \right]^{\frac{1}{2}}$$

4. For a normal mode \vec{v}_n with an associated frequency ω_n , we recover $\omega_0(\vec{v}_n) = \omega_n$
5. $\omega_0(\vec{u})$ is *scale-invariant* ($\omega_0(c\vec{u}) = \omega(\vec{u})$), hence isofrequents are lines passing through the origin

Mode Space

Constraint Force Modes

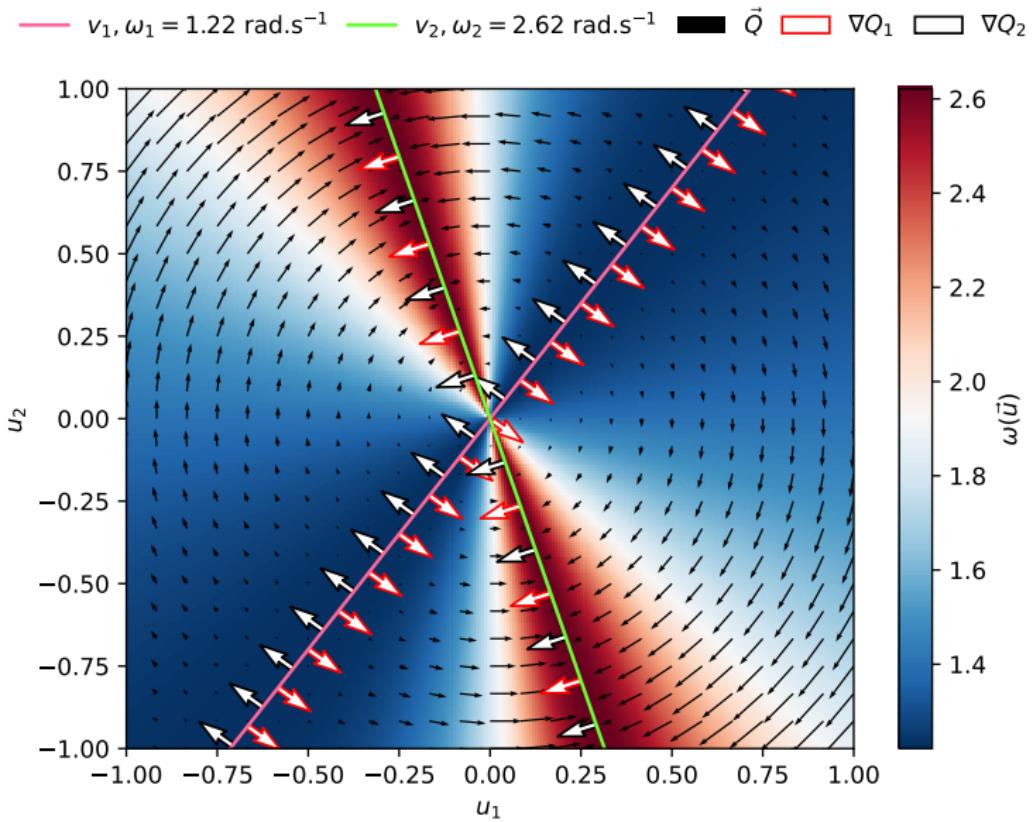
1. *Constraint force*: a force needed to be introduced for a specific trajectory (given by constraints) to be allowed
2. By equating it to the driving force, we can directly search for steady-state solutions to the E-L equations
3. From the E-L equation for a mode:

$$Q_i(\omega, \vec{u}) = l_i \left[g u_i \mu_i - \omega(\vec{u})^2 \sum_{x=1}^N u_x l_x \mu_{\max(i,x)} \right]$$

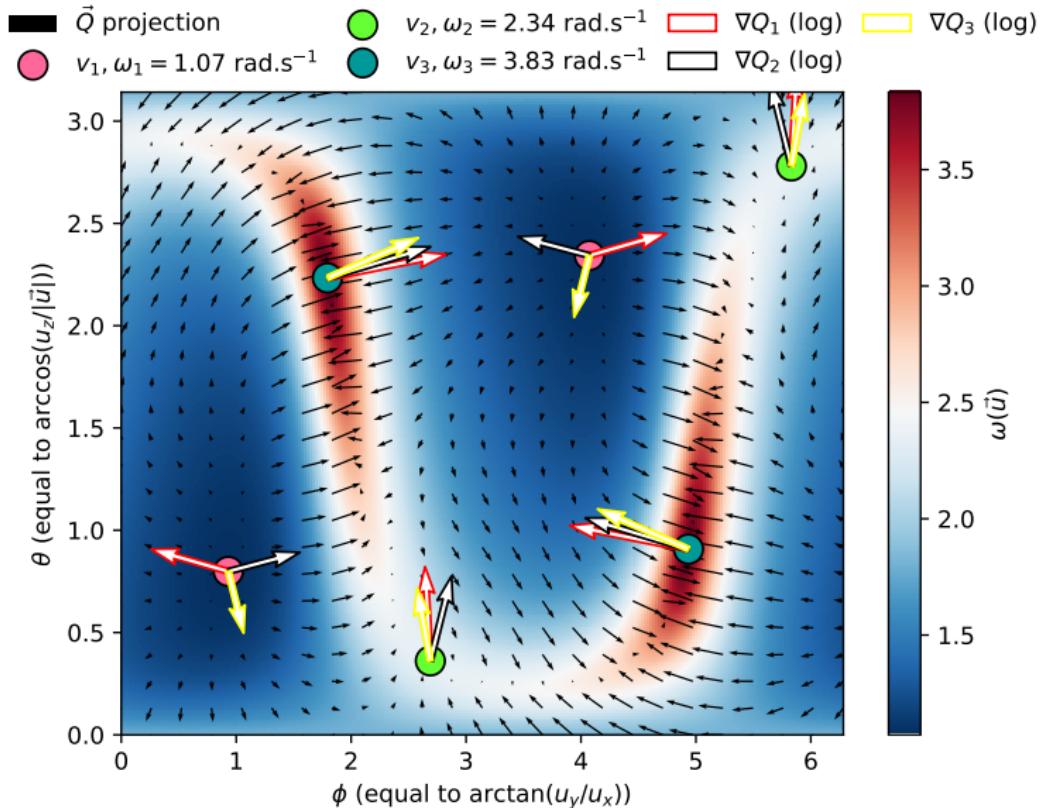
We can check numerically this satisfies $\vec{Q}(\omega_n, \vec{v}_n) = 0$

4. $\vec{Q}(\vec{u})$ scales linearly: $\vec{Q}(c\vec{u}) = c\vec{Q}(\vec{u})$

Mode Space - Double Pendulum



Mode Space - Triple Pendulum (Projection Onto a Sphere)



Frequency-Mode Space

Definition of Frequency-Mode Space - Motivation - Scaling Convention

1. Space \mathbb{R}^{N+1} in which a vector \vec{s} represents

$$\vec{s} = \begin{pmatrix} \omega \\ \vec{u} \end{pmatrix} = \begin{pmatrix} \omega \\ u_1 \\ u_2 \\ \vdots \\ u_N \end{pmatrix}$$

2. It gives us one more degree of freedom in reference to \vec{Q}
3. The constraint force vector field translates well

$$\vec{Q}(\omega, \vec{u}) = \vec{Q}(\vec{s}) \quad \text{where} \quad s_\omega = \omega, \vec{s}_{\vec{u}} = \vec{u}$$

4. Scaling convention

$$c\vec{s} = \begin{pmatrix} \omega \\ c\vec{u} \end{pmatrix} \quad \text{for} \quad c \neq 0$$

preserves mode scaling properties and isofrequenths

Perturbation of Normal Modes in Frequency-Mode Space

A General Perturbation - Linear Dependence of Elements

1. Normal mode in F-M space = \vec{w}_n . For a perturbation $\delta\vec{s}$:

$$Q_i(c\vec{w}_n + \delta\vec{s}) = Q_i(c\vec{w}_n) + \delta\vec{s} \cdot \nabla Q_i \Big|_{c\vec{w}_n} = \delta\vec{s} \cdot \nabla Q_i \Big|_{c\vec{w}_n}$$

2. We control c , so we choose $\delta\vec{s}_{\vec{u}} \perp \vec{v}_n$, from which we have

$$\delta s_{\vec{u}N} = \sum_{i=1}^{N-1} d_i \delta s_{\vec{u}i} \quad \text{where} \quad d_i = -\frac{v_{ni}}{v_{nN}}$$

We define a reduced displacement

$$\delta\vec{s}^* = \begin{pmatrix} \delta\omega \\ \delta u_1 \\ \delta u_2 \\ \vdots \\ \delta u_{N-1} \end{pmatrix}$$

3. $\delta\vec{s}^*$ has N dimensions, which gives us N degrees of freedom plus the scale c .

Perturbation of Normal Modes in Frequency-Mode Space

Force Mode Gradient

1. We see the gradient is

$$\nabla Q_i(\vec{s}) = \begin{pmatrix} \frac{\partial Q_i}{\partial \omega} \\ \nabla_u Q_i \end{pmatrix} = \begin{pmatrix} \frac{\partial Q_i}{\partial \omega} \\ \frac{\partial Q_i}{\partial u_1} \\ \frac{\partial Q_i}{\partial u_2} \\ \vdots \\ \frac{\partial Q_i}{\partial u_N} \end{pmatrix}$$

2. By direct differentiation:

$$\frac{\partial Q_i}{\partial \omega} = -2l_i \omega \sum_{x=1}^N u_x l_x \mu_{\max(i,x)}$$

$$\frac{\partial Q_i}{\partial u_j} = l_i (g \mu_i \delta_{ij} - \omega(\vec{u})^2 l_j \mu_{\max(i,j)})$$

3. Since $\nabla_u Q_i \perp \vec{v}_n$, we need δs_ω to span all possible \vec{Q}

Perturbation of Normal Modes in Frequency-Mode Space

The Displacement for an Arbitrary Force Mode

1. Consider a matrix $R_{(N) \times (N)}$ defined like so:

$$R_{ij}(\vec{s}) = \begin{cases} \frac{\partial Q_i}{\partial \omega}(\vec{s}) & j = 1 \\ \frac{\partial Q_i}{\partial u_{j-1}}(\vec{s}) + d_{j-1} \frac{\partial Q_i}{\partial u_N}(\vec{s}) & \text{otherwise} \end{cases}$$

2. Multiply R by the reduced displacement:

$$(R\delta\vec{s}^*)_i = \delta\omega \frac{\partial Q_i}{\partial \omega} + \sum_{j=2}^N \delta u_{j-1} \left(\frac{\partial Q_i}{\partial u_{j-1}} + d_{j-1} \frac{\partial Q_i}{\partial u_N} \right) = \delta\vec{s} \cdot \nabla Q_i$$

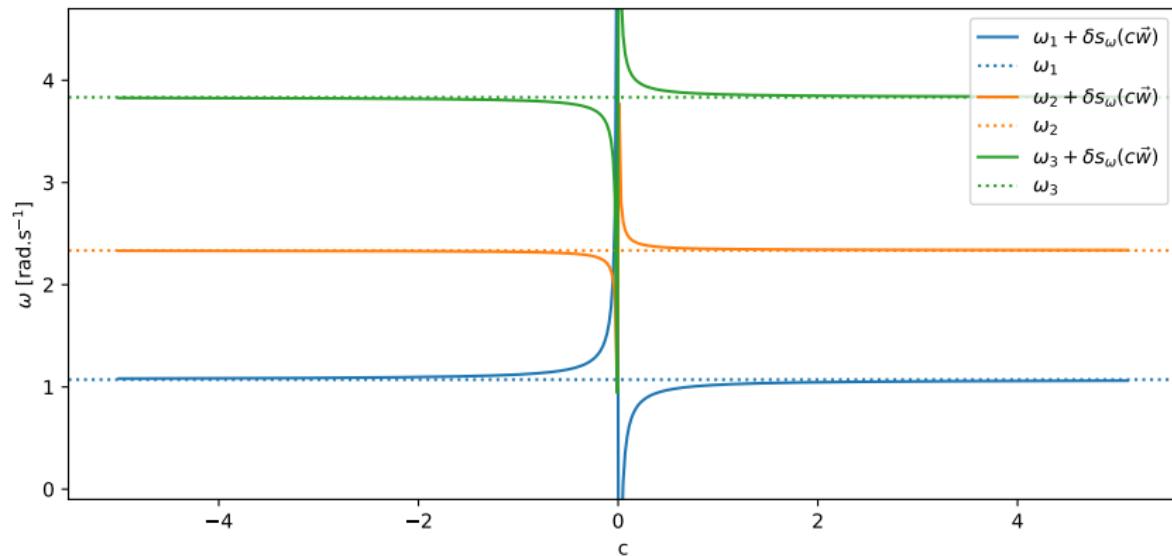
3. By equating the perturbed constraint force mode to our imposed force mode, we get:

$$\delta\vec{s}^*(\vec{Q}) = R^{-1}\vec{Q}(c\vec{w}_n + \delta\vec{s})$$

and the corrected frequency is $\omega(\vec{Q}) = \omega_n + \delta\vec{s}_\omega^*(\vec{Q})$

Perturbation of Normal Modes in Frequency-Mode Space

Perturbed Modal Frequency Scale Variance - *C the Scaleless?*



1. The problem of c : if $\omega(\vec{Q})$ isn't scale-invariant, how do we choose the value of modal frequency?
2. As of now, we aren't able to predict the resonant frequency using this model

Conclusions and Further Research

1. We can calculate the normal modes to approximate resonance without considering the specific force mode
2. For a given force mode, we can find allowed mode trajectories in the vicinities of normal mode isofrequenth
3. *Either* the system **possesses a scale**, or the mode hypothesis is **false** (as not all allowed modes are resonant)
4. Immediate directions of further research:
 - 4.1 Find the scale of the perturbed mode trajectory whose frequency matches resonance - is it somehow special?
 - 4.2 Can we derive the scale theoretically? Maybe only one scale satisfies a certain condition (average work done on the steady state...)
 - 4.3 Maybe *all* measured trajectories around the normal mode are modes? Is mechanical energy maximised for a certain scale?
 - 4.4 Empirically search for mode behaviour in simulation (problem with slowly decaying transient)

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Thank you for your attention