Electrical Engineering 141, Homework 6

Michael Wu UID: 404751542

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Problem 1

The open loop transfer function is the following.

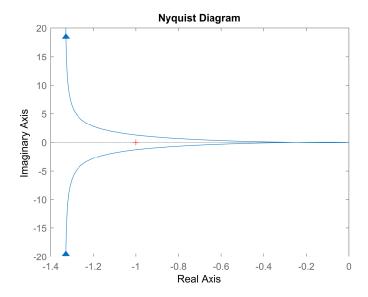
$$\frac{K}{(s+1)^3}$$

This crosses the real axis when $1+j\omega$ has a phase of $\pm \frac{\pi}{3}$ or 0. This occurs at $\omega=0,\pm\sqrt{3}$. The magnitude of the open loop transfer function at these points are K and $-\frac{K}{8}$, respectively. The open loop transfer function has no poles in the right half plane, so we should have no encirclements around -1 in order to have a stable system. Since we know that the value of the transfer function goes to zero as ω goes to ∞ , we know that we will have an encirclement if $-\frac{K}{8} < -1$. On the positive side we also know we will have an encirclement if K < -1. Thus we want the following inequality to hold in order to have a stable system.

$$-1 < K < 8$$

Problem 2

a) The Nyquist diagram is shown below.



The plot goes to infinity, and since we choose to not include the open loop pole at s=0, we determine that the loop connects on the right half plane. Thus the critical point is not contained within a loop, and there are no unstable poles in the closed loop transfer function since the contour does not circle any open loop poles.

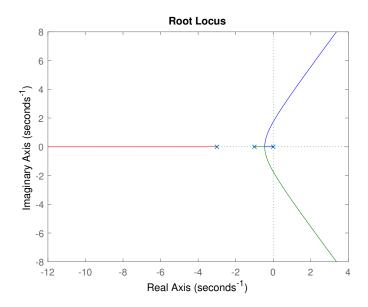
b) The Nyquist plot crosses the real axis when $j\omega(1+j\omega)(3+j\omega)$ is real. This can be rewritten as the following expression.

$$-4\omega^2 + i(3\omega - \omega^3)$$

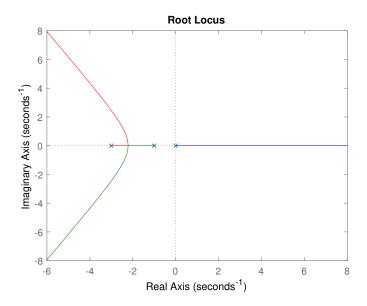
This occurs when $\omega = 0, \pm \sqrt{3}$ and the corresponding magnitude of the transfer function is $K\infty$ and $-\frac{K}{4}$. Thus we must have 0 < K < 4 in order to have a stable closed loop system.

c) If we have K > 4, then the critical point will have two clockwise loops around it. Then the Nyquist stability criterion indicates that there will be two more closed loop poles than open loop poles in the right half plane. Since we have zero open loop poles in the right half plane, this means there will be two closed loop poles in the right half plane. If we have K < 0, then the critical point will have one clockwise loop around it. This corresponds to one closed loop pole in the right half plane.

d) The root locus plot is shown below.



The complementary root locus plot is shown below.

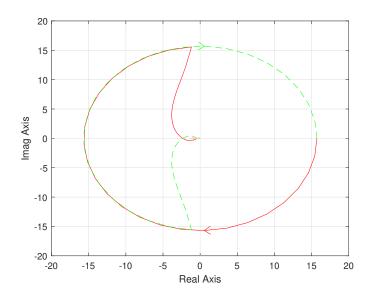


This confirms that there will be two unstable poles as K increases above

4. Clearly the complementary root locus plot indicates that there will be one unstable real pole if K is negative.

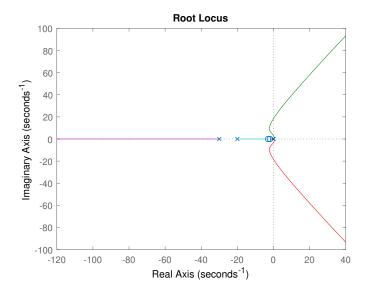
Problem 3

a) The shape of the Nyquist diagram is shown below.



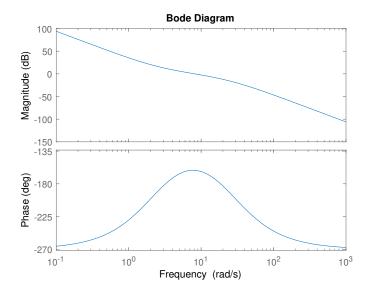
- **b)** The Nyquist diagram encircles the critical point zero times, since it encircles it once in the clockwise direction and once in the counterclockwise direction. This means that our system is stable.
- c) Using a calculator I found that the Nyquist plot crosses the real axis at -0.2843 and -4.0705. This corresponds to the following upward and downward gain margin.

d) The root locus is shown below.



The gain values associated with the $j\omega$ axis crossings are approximately 0.25 and 3.5 which agrees with my earlier results.

e) The bode plot is shown below.



At the crossover frequency of 3.23 radians per second, we have a gain

margin of -12.2 dB which corresponds to the downward gain margin. At the crossover frequency of 18.6 radians per second, we have a gain margin of 10.9 dB which corresponds to the upward gain margin. At the crossover frequency of 8.17 radians per second we have a phase margin of 18.6 degrees.

Problem 4

a) We want the intersection of the Nyquist diagram with the unit circle to be at $-\frac{\sqrt{2}}{2} \pm j\frac{\sqrt{2}}{2}$ in order for the phase margin to be 45 degrees. Then we can solve the following equation.

$$\frac{K_p}{j\omega(j\omega+1)} = -\frac{\sqrt{2}}{2} + j\frac{\sqrt{2}}{2}$$

$$\frac{K_p}{-\omega^2 + j\omega} = -\frac{\sqrt{2}}{2} + j\frac{\sqrt{2}}{2}$$

$$K_p = \frac{\sqrt{2}}{2}(\omega^2 - j\omega - j\omega^2 - \omega)$$

$$K_p = \frac{\sqrt{2}}{2}(\omega(\omega - 1) - j\omega(\omega + 1))$$

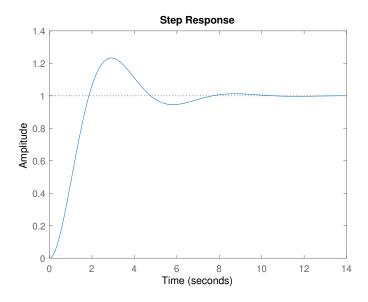
$$K_p = \sqrt{2}$$

We set $\omega = -1$ in order to make the imaginary term zero.

b) Since our phase margin is fairly low, we can use the approximate the damping ratio as $\zeta = 0.45$. Then the approximate percent overshoot is given by the following equation.

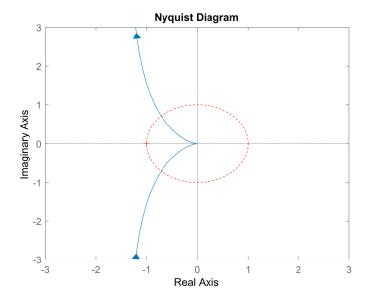
$$e^{-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}} = 0.2053$$

c) The step response is shown below.



The actual percent overshoot was 0.233 and the actual damping ratio is $\frac{1}{2^{1.25}} = 0.42$. This is slightly lower than I predicted, leading to a slightly higher percent overshoot.

d) The Nyquist diagram is shown below.



This does indeed have a 45 degree phase margin since the Nyquist diagram lies on the line y=x when it intersects the unit circle.

Problem 5

- **a**)
- b)
- $\mathbf{c})$
- d)
- **e**)
- f)
- $\mathbf{g})$