# Technical University of Košice Faculty of Mining, Ecology, Process Control and Geotechnologies

# Design and implementation of modern methods of modeling and control of technological objects and processes

**Dissertation Thesis** 

2020 Michal Takáč

## Technical University of Košice Faculty of Mining, Ecology, Process Control and Geotechnologies

# Design and implementation of modern methods of modeling and control of technological objects and processes

#### **Dissertation Thesis**

Study Programme: Cybernetics

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#### Abstract

Text abstraktu v svetovom jazyku je potrebný pre integráciu do medzinárodných informačných systémov. Ak nie je možné cudzojazyčnú verziu abstraktu umiestniť na jednej strane so slovenským abstraktom, je potrebné umiestniť ju na samostatnú stranu (cudzojazyčný abstrakt nemožno deliť a uvádzať na dvoch strabách).

#### Keywords

Steelmaking, Visualization, Virtual Reality, Mathematical modeling

#### **Abstrakt**

Abstrakt je povinnou súčasťou každej práce. Je výstižnou charakteristikou obsahu dokumentu. Nevyjadruje hodnotiace stanovisko autora. Má byť taký informatívny, ako to povoľuje podstata práce. Text abstraktu sa píše ako jeden odstavec. Abstrakt neobsahuje odkazy na samotný text práce. Mal by mať rozsah 250 až 500 slov. Pri štylizácii sa používajú celé vety, slovesá v činnom rode a tretej osobe. Používa sa odborná terminológia, menej zvyčajné termíny, skratky a symboly sa pri prvom výskyte v texte definujú.

### Kľúčové slová

Oceliarstvo, Vizualizácia, Virtuálna realita, Matematické modelovanie

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## Introduction

- Popisat o com je process control (vo vseobecnosti) - Popisat v strucnosti ako sa vyvija kybernetika - Popisat v strucnosti ako sa vyvija automatizacia - Spomenut nove trendy - Industry 4.0, IoT, Industrial IoT, Edge computing - Softverova podpora process control a kybernetiky na baze AI, deep learning a machine learning - ake metody, ake modely, co sa pouziva u nas na ustave

The objective of process control is to keep key process-operating parameters within narrow bounds of the reference value or setpoint. This chapter describes the theory behind control circuits to maintain automatic control over a process. The basis of automatic control is the control loop. A control loop for a given process must have at least one sensor, a controller, and a control element to which the results are applied. A good example of automatic control is electric heating of a house in a cold environment, a process where a single variable is controlled. A thermostat (sensor) monitors the temperature. When the temperature drops below the setpoint, a switch is closed and the heater comes on. When the temperature rises above the setpoint, the switch opens and the heater is turned off. The difference between the actual value and the setpoint is called the error. The controller reads the error and makes a decision. The action taken can be very simple to very complicated, depending on the system and the size of the acceptable error.

Process industries have developed along similar lines with control systems. To answer the question of what process control is exactly, we have to go back to the earliest introductions of control mechanisms, where first-generation electro-pneumatic-mechanical loop controllers replaced people doing tasks such as manually adjusting valves in response to some local indicator like a pressure gauge.

Although a device was used to automate a human function in an effort to control a variable, there was no sense of what the process was doing overall. A basic controller could keep an individual loop on an even keel, more or less, so long as there was not too

much disruption. Complex processes might employ dozens or even hundreds of such controllers, each with its performance displayed on a panel board, but keeping an eye on the big picture was still a human process.

When distributed control system (DCS) platforms were introduced in the 1970s, they simplified the mechanics of the panel board, but did not do much to improve its capabilities. Big-picture analysis was still largely a human responsibility. Sure, getting beyond the technical constraints of pneumatic field devices with their troublesome compressed air tubing made it easier to install more instruments and actuators, but the basic control concepts did not really change. Any movement to advanced process control (APC) and other forms of control optimization were still in their infancy. Process automation capable of supporting APC had to encompass many technologies and techniques. It was characterized by incorporating many more input data points into algorithms and orchestrating more complex sequences.

The transition to process automation and APC was empowered by being able to create an all-encompassing platform capable of coordinating more than single loops or small cascade groups. One major advantage of newer platforms is the ability to optimize a process to suit the owner's specific economic goals based on any number of desired outcomes. The process automation system can operate the plant to minimize energy consumption, maximize output, and deliver specific product quality attributes.

Implementing such systems is challenging. During the initial design phase of a control system upgrade or a new installation, it is far too easy to focus just on process fundamentals, and never get beyond considering desired steady-state conditions. Automation system upgrades and new installations can therefore miss opportunities to engage with process and automation technology experts capable of uncovering better ways of doing things.

Many capabilities of modern process automation systems are still underutilized in most process plants, even among companies most people would consider sophisticated. Far

fewer companies use APC as effectively as they could, even though basic APC technologies have been around for decades. —— Even the most modern process plants typically do not take full advantage of the capabilities of their control systems. ————

Peter Drucker, a well-known management thinker, who has been quoted multiple times over the years by various people, has famously said: "If you can't measure it, you can't manage it. If you can't manage it, you can't improve it." His words are now resonating more than ever with the push towards Industry 4.0.

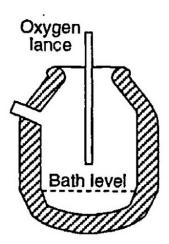
Big Data means the analysis of large amounts of data coming from different sources with high speed and with the aim to create economic benefit.

The oxygen converter process (LD/BOF and its derivatives) is a refinement step in the production of steel from ore. The main purpose of the process is to remove excess carbon from the pig iron produced in the blast furnace. The main feature of the process is to add oxygen through a top lance, in order to remove unwanted impurities through oxidation. It is the main method of carbon and low alloy steelmaking, annual production approaching to 60% of total crude steel production (Jalkanen; 2006). BOF is a widely preferred and effective steelmaking method due to its high productivity and considerably low production cost (Wang, Han and Wang; 2010).

LD/BOF process consists of these subprocesses:

- 1. Charging slag
- 2. Charging hot metal
- 3. Oxygen blowing and addition of slagging and alloying additives
- 4. Measurement of steel temperature and composition
- 5. Tapping of steel
- 6. Tapping of slag

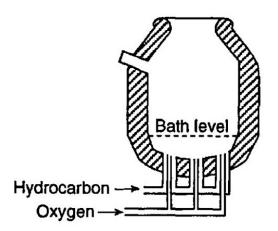
The first commercial operation of steelmaking with oxygen top blowing in the converter was in the early 1950s at Linz and Donawitz (Austria). This manner of steelmaking became known as Linz-Donawitz or LD process. For many years now, most of the steel has been made by top oxygen blowing for which different names are given. For example, in European steel plants the process is still called LD; in the UK, BOS (basic oxygen steelmaking); in the Far East and America, BOF (basic oxygen furnace), with the exception of U.S. Steel where it is called BOP (basic oxygen process) (Turkdogan; 1996).



**Fig. 0–1**: Production of steel in the converter with top-blown oxygen (LD/BOF) (Turkdogan; 1996).

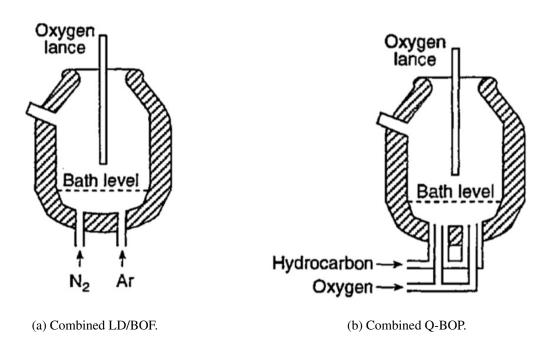
In the early 1970s, a bottom-blown oxygen steelmaking process was developed in Canada and Germany. This process, known as OBM in Europe and Q-BOP elsewhere, was in full size commercial operation by the mid 1970s in U.S. Steel plants followed by several plants in Europe and Japan. The tuyeres, mounted in a removable bottom, consist of a central pipe for blowing oxygen together with burnt lime, and an annular gap around the central pipe for the passage of gaseous hydrocarbon, e.g. propane or natural gas (Turkdogan; 1996).

Further developments in oxygen steelmaking led to the present practices of various types of top and bottom blowing known as combined blowing, as illustrated schematically in



**Fig. 0–2**: Production of steel in the converter with bottom-blown oxygen (Q-BOP) (Turkdogan; 1996).

Fig. 8.1 for BOF and Q-BOP processes. There is also post combustion of CO in the upper part of the vessel to generate additional heat for steelmaking (Turkdogan; 1996).



**Fig. 0 − 3**: LD/BOF a Q-BOP processes in oxygen convertor with combined blowing.

In modern steel mills about 300 tons of steel are produced within a 30-40 minute cycle.

Various additives are added during the process to adapt the steel quality and slag formation. The converter furnace is inclined during charging and tapping. The converter has a vertical position during oxygen blowing. The changes in the position of the converter during the individual elementary processes are shown in the figure 0-4.



Fig. 0 – 4: Representation of elementary processes in LD converter.

Depending on local operating conditions, availability of scrap, blast furnace iron and the extent of hot metal pretreatment, the metallic charge (LD/BOF, Q-BOP) is 75 to 95 % pig iron and the remainder is steel scrap. The types of scrap used are usually those produced in a steel mill: sheet scrap, damaged molds, bimetallic cans etc Turkdogan (1996).

Oxygen is blown at a high speed (up to twice the speed of sound) on the surface of the metal bath in the converter and so-called hot area is formed in the region where the oxygen stream hits the surface. The oxidation products dissolve in the slag, with the exception of carbon monoxide, which passes through the slag layer and forms the major component

of the converted gas. The oxidation intensity of the individual elements depends on their chemical affinity for oxygen. Carbon oxidation is one of the most important processes. Carbon is oxidized in the metal during the steelmaking process by the influence of oxygen, in particular on CO and partly on  $CO_2$ , depending on the reactions

$$C + \frac{1}{2}O_2 \longrightarrow CO \tag{0.1}$$

$$C + O_2 \longrightarrow CO_2 \tag{0.2}$$

Manganese is oxidized to MnO

$$Mn + \frac{1}{2}O_2 \longrightarrow MnO$$
 (0.3)

Phosphorus is undesirable in steel and oxidizes to P<sub>2</sub>O<sub>5</sub>

$$2P + \frac{5}{2}O_2 \longrightarrow P_2O_5 \tag{0.4}$$

Sulphur is a harmful element and passes into the slag in the form of CaS based on the reaction of CaO

$$CaO + MnS \longrightarrow CaS + MnO$$
 (0.5)

whereby MnS is formed by reaction

$$Mn + S \longrightarrow MnS$$
 (0.6)

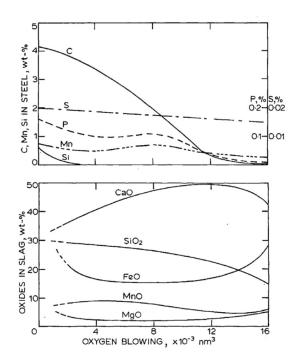
and sulphur also goes out in the form of gas as SO<sub>2</sub>

$$S + O_2 \longrightarrow SO_2$$
 (0.7)

Silicon has a high affinity for oxygen, so it is easily oxidized to form SiO<sub>2</sub>

$$Si + O_2 \longrightarrow SiO_2$$
 (0.8)

In the initial stages of blowing, most of the silicon oxidizes to form a slag of low basicity - the composition of the metal and slag changes, as shown in the figure 0-5.



**Fig. 0−5**: Changes in metal and slag composition during steel production in LD/BOF process (Turkdogan; 1996).

An intense oxygen flow induces fluid flows in the iron bath, forcing the highly oxidized metal and the molten oxidation products from the iron bath surface to penetrate into the bath, where they react with the "fresh" hot metal with a high content of impurities and therefore loss of iron in the form of FeO and Fe<sub>2</sub>O<sub>3</sub> should also be considered:

$$Fe + \frac{1}{2}O_2 \longrightarrow FeO \tag{0.9}$$

$$2Fe + \frac{3}{2}O_2 \longrightarrow Fe_2O_3 \tag{0.10}$$

.

This oxygen stream and gas bubbles generated in the bath bring portions of the iron melt to the slag. The heat generated by the highly exothermic oxidation reactions is consumed by heating and melting the feed materials, heating the iron bath, slag and carbon oxides that are formed during the oxidation of the carbon and are partially lost to the environment during the blowing process.

The resulting  $SiO_2$  passes into the slag as  $2CaO \cdot SiO_2$  according to the equation

$$SiO_2 + 2CaO \longrightarrow 2CaO \cdot SiO_2$$
 (0.11)

and additionally,  $P_2O_5$  passes into the slag as  $3 \, \text{CaO} \cdot P_2O_5$  according to the equation Laciak et al. (2017)

$$P_2O_5 + 3CaO = 3CaO \cdot P_2O_5.$$
 (0.12)

Circulation in the iron bath caused by the flow of oxygen, rising gas bubbles and purging of inert gas through the lower tubes in converters with combined blowing type transports minor iron melt components (C, Si, Ti, Mn, P, V, etc.) to the upper bath layers Jalkanen (2006).

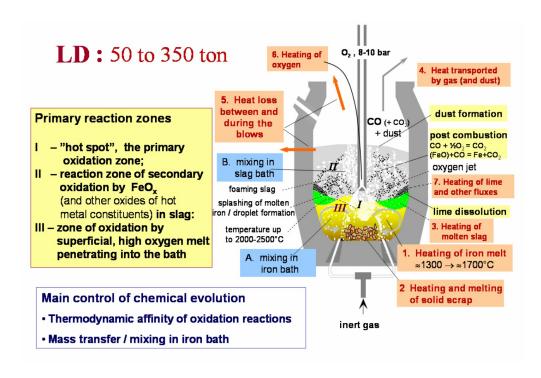
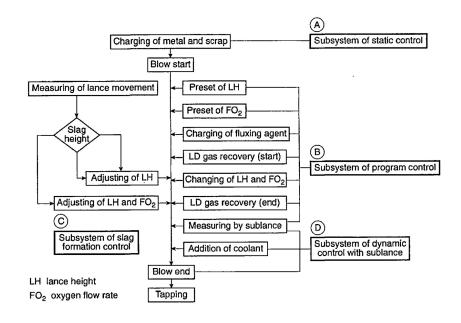


Fig. 0 – 6: Chemical and thermal processes in LD converter (Jalkanen; 2006).



**Fig. 0−7**: Schematic representation of the system and function of fully automatic LD/BOF process (Turkdogan; 1996).

### 1 State of art

In this section we deal with the current state of the art of process theory, simulation and visualization of elementary processes in the oxygen converter used in steelmaking. There have been tremendous improvements in iron and steelmaking processes in the past twenty years. Productivity and coke rates in the blast furnace and the ability to refine steel to demanding specifications have been improved significantly. Much of this improvement is based on the application of fundamental principles and thermodynamic and kinetic parameters which have been determined (Turkdogan and Fruehan; 1999).

#### 1.1 Process control

The need for developing improved control systems has traditionally been powered by the demand for more accurate and cost efficient production. This is still a major driving force but environmental issues do also have a profound influence on this development today (Widlund et al.; 1998).

The main objective of controlling oxygen converter steelmaking is to obtain prescribed parameters for the steel when it is tapped from the furnace, including weight, temperature, and each element content. In practical steelmaking process, the criterion whether the molten steel is acceptable or not is often decided by the endpoint carbon content and temperature (Wang, Han and Wang; 2010).

The fast dynamics of the LD converter steelmaking process or the BOF process, as it is commonly known, often makes it a challenge to obtain stable blowing conditions and to achieve the required steel composition and temperature simultaneously at the end point. For this reason, process control becomes very necessary and attempts had started as early as in the 1970s (Fritz and Gebert; 2005). Out of the originally very simple LD process have grown the modern process-controlled and automated production systems that enable present-day adaptations to meet today's economic and ecological demands (Sarkar et al.; 2015).

Generally, the BOF steelmaking process with sub-lance system can be divided into two stages: static control and dynamic control. Static models include oxygen supplying model, slaging model and bottom blowing model; dynamic models include decarburization speed model, molten steel warming model and the model for the amount of coolant. (Wang, Han and Wang; 2010).

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Deviations from the desired process course can be caused by several factors. These factors may be described in four different categories; process, hardware, operator induced irregularities and production disturbances (Widlund et al.; 1998).

Process irregularities. There is a contradiction between the need to obtain high slag levels to provide good refining conditions and the desire to minimise uncontrolled slag overflow, "slopping". All events of slopping result in severe dust emissions and iron yield losses affecting the mass and heat balance computations by the control system. FW'thermore, production must be stopped to allow for cleaning of the vessel mouth and the area below the vessel (Widlund et al.; 1998).

Unknown scrap dissolution rate may also interfere with process performance. Late melting of high-carbon scrap can cause uncertain composition of sample taken with a sub lance resulting in erratic feed-back to the control system (Widlund et al.; 1998).

Hardware irregularities. Hot metal temperature measurements in the transfer ladle are made by means of a thennocouple and believed to be reliable. However, it remains unclear whether the measW'ement is representative for the total amount of the hot metal to be charged to the converter. Weighing equipment for hot metal, scrap and other additions is regularly calibrated but still has an insufficient accuracy. This influences the reliability of the model computations and estimations in the control system. The use of gas analysis in a control system is hindered by the presence of long time delays (up to 25 seconds) in the measuring system. Unknown and inconsistent wear of the fiunace lining as well as the lance nozzles will also introduce uncertainties in the control system since these

parameters influence the iron oxidation (Widlund et al.; 1998).

Operator induced irregularities. Most of the existing systems require control actions from the operator and therefore to some extent depend on the operator's experience and personal preferences. For instance, it is a common practice that operators add other material amotmts than those recommended by the control system. It is not uncommon that the pre-set lance programs are shifted up- or downwards according to the operator's interpretation of previous heats. Furthermore, since reliable real-time measurements of the carbon content are not presently available, different operators apply different rules for deciding when to stop the blow. These operator induced irregularities make it difficult to achieve Production disturbances. The converter process is only one link in a chain of unit operations from raw materials 10 fmal product. Therefore, production disturbances can change process conditions. For example, poor blast furnace performance might lead to insufficient hot metal supply or even production disruptions. Under these circumstances, more metal scrap and fuel should be used instead of hot metal to uphold production volumes. Logically, this implies changes in blowing practice (Widlund et al.; 1998).

In order to monitor and/or control the process, different measuring systems can be employed to give feedback to either the operator or directly to existing system for automated control. These measurements can be either direct or indirect as well as with or without time delays (Widlund et al.; 1998).

The real-time information on the process state can be obtained from a number of sensors (Widlund et al.; 1998).

Sensor: Flow rate measurement with venturi Information obtained: Off-gas flow rate. Sound level measurement with microphone Indication of changes in slag level. Load cell or accelerometer on lance or vessel Indication of changes in slag level. Temperature measurement Off-gas temperature. Lance elongation Hood pressure Indication of changes in slag level. Pressure difference with ambient pressure.

All these signals can, in principle, be used for closed-loop control (Widlund et al.; 1998).

There are only a few process variables that can be manipulated by the control system or the operator - lance height, oxygen gas flow rate and purge gas flow rate. Naturally, changes in lance height are easier to measure as well as set and therefore preferable to use in a closed-loop control system. Oxygen gas flow rate should not be changed more than approximately  $\pm 5\%$  since the nozzle is designed for a specific flow rate (Widlund et al.; 1998).

Two basic approaches to control the process are; open-loop control and closed-loop control. The former assumes availability of a pre-defined control signal trajectory bringing the process to a desired state. Using the latter, measurements of the process output signals are fed back to the actuators via a controller. An obvious shortcaning of the open-loop strategy is a high sensitivity to process disturbances. Thus, a closed-loop control system of the BOS converter is sought. A major difficulty in designing such a system would be the necessity to analyse stability and performance of the closed-loop system (Widlund et al.; 1998).

## 1.2 Computer-aided Mathematical Modeling and Numerical Simulation

The motivation for using computer simulations to investigate metallurgical processes is two-fold. First, it enables design changes to be tested before building a prototype, which naturally leads to a lower total design cost. Second, it makes it possible to investigate phenomena that cannot easily be measured or observed in the process. Even a seemingly simple operation such as the continuous measurement of the temperature during the decarburization process is difficult due to the very high temperatures in the process and generally harsh conditions prevailing in the steel plants (Ersson and Tilliander; 2018).

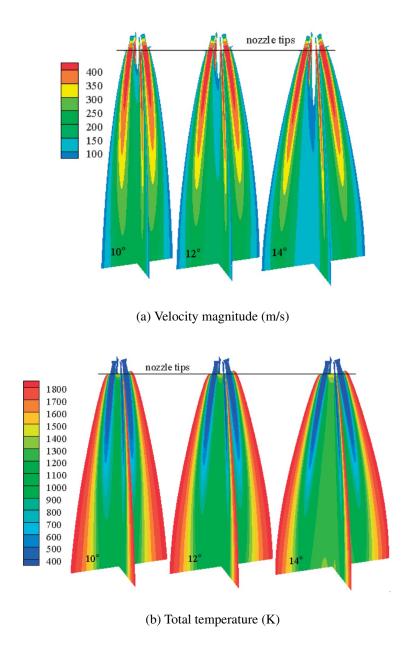
In metallurgy, simulating linear and non-linear processes that we encounter in steelmaking by creating mathematical models is of great importance. Since first attempts to use

mathematical techniques for the simulation and optimization of large scale metallurgical operations (Ray et al.; 1973), various numerical methods were implemented as algorithms and used to simulate phenomena in steelmaking processes. One class of such methods is called Monte Carlo, which is useful for simulating systems with many coupled degrees of freedom such as fluids.

Modern fluid mechanics problems would be impossible to solve without use of Computational Fluid Dynamics (CFD), since the scope of analytical solutions to fundamental equations of fluid mechanics is very limited and, once a more difficult geometry is encountered, we usually have to choose a given numerical method for obtaining a solution. CFD encompasses a wide spectrum of numerical methods used for solving complex threedimensional (3D) and time-dependent flow problems (Rapp; 2017). Since early pioneering work in the metallurgical field done by Szekely et al. (1977), the cost of performing computer simulations has decreased over the last few decades, while the available processing power has increased. Most of the processors and processing units that are currently developed and produced have several cores that can execute instructions in parallel. Thus, the processing power available to a CFD software also depends on the capability of the software to execute in parallel. A study by Ersson and Tilliander (2018) of the last two decades of metallurgical CFD simulations reveals huge improvements on the type of phenomena that can be explored and we will see this trend is continuing thanks to improvements in both the available processing power and the available algorithms. Therefore CFD found its way into numerous studies in steelmaking, where these methods proved useful in demonstrating the hidden and significant properties. However, its use in the steel industry may not be as integrated as in the aero and automotive industries, in which the development of new designs is of key importance. The major difference between aero and metallurgical industries is that the metallurgical industries almost always deal with multiphase systems at elevated temperatures and that the motivation of modeling is mainly process optimization. With a continuing development in multiphase models as well as in reacting flow modeling, the continued usefulness of CFD in metallurgy remains clear.

In LD/BOF process, different chemical reactions among oxygen, slag, and molten iron in oxygen converter, in combination with vigorous stirring process to promote slagging, dephosphorization, decarbonization, heating of molten steel, and homogenization of steel composition and temperature, determines the final properties of steel. The objective of the oxygen converter is to refine molten iron to crude steel through oxidization to achieve a specified temperature and chemical composition at the end blow. Failure to do this leads to the need to reblow. The impact of oxygen jet into molten bath strongly affects the bath and promotes the three-phase flow among gas, slag, and molten steel in the bath. With the move from old rule-based systems to a model-based, real-time closedloop control of lance movement and oxygen flow, significant drawbacks were eliminated. There have been efforts in developing accurate and efficient numerical models within CFD field to solve the jets flow in the oxygen converter. Peng and Han (1996) established the conditions of optimum nozzles of performance by deriving the system of mathematical equations to simulate the steady, quasi-one-dimensional supersonic flow through a single De Laval nozzle. Tago and Higuchi (2003) analyzed single-nozzle and multi-nozzle lances with the help of two-dimensional simulation based on fluid dynamics and found that higher ambient temperature leads to the lower density and the higher velocity of the gas jets, but does little affect the dynamic pressure. They report that CFD proved useful method to predict the effect of the inclination angle and the number of the nozzles on the jet behavior in the top blown processes. Wang, Yuan, Matsuura, Zhao, Cheng and Tsukihashi (2010) developed a three-dimensional mathematical model to simulate the compressible jets flow from the top-blown lance, taking into consideration variations of fluid density, viscosity, high temperature and Mach number. They demonstrated that  $k-\omega$  turbulence model is superior to the widely used  $k-\varepsilon$  turbulence model to calculate turbulent conditions within multiple jets. Simulation results of final computational flow field distributions of three kinds of multiple jets are shown in Fig (1-1).

CFD models have been also used in developing deeper understanding of the decarburization processes in steelmaking. However, these processes are highly complex with large



**Fig. 1–1**: Simulating results of velocity magnitude and total temperature field distributions of the three kinds of multiple jets: (a) velocity magnitude (m/s) and (b) total temperature (K) (Wang, Yuan, Matsuura, Zhao, Cheng and Tsukihashi; 2010).

variations in time and length, and therefore it makes the systems extremely demanding to simulate. Ersson and Tilliander (2018) reviewed latest research on the subject from 1998 until 2016 and found out that, even though several reports have been published discussing research about modeling parts of the decarburization processes numerically, no models have been presented that can handle the entire complexity of the processes. Many authors had simplified the system in existing models in order to achieve an understanding of particular phenomena rather than of the entire process.

Another important part of the oxygen steelmaking process is keeping the usual balance of 80% hot metal and 20% scrap during charging to regulate the temperature of steel in the vessel. To define the charge conditions and oxygen blowing requirements to achieve the temperature and chemical composition, mathematical and thermodynamic models have been developed (Kačur et al.; 2019; Laciak et al.; 2018). Reactions that take place in LD process can vary significantly from heat to heat, while not many variables involved are not accurately known. Therefore, it is necessary to take into account the uncertainty affecting the whole process reactions. To correct the differences between the theoretical predictions of the process models and the real results, Bouhouche et al. (2012) introduced a random quantity term into their models and improved the prediction model with the use of Support Vector Regression and Monte Carlo Simulation methods in combination. Most of the control schemes rely on an accurate system model. However, as these systems become more complex, writing down the dynamics from the first principles is extremely challenging. In such cases, neural networks are used to approximate the dynamics directly using system data. In this context, neural networks can be thought of as a generalization of linear regression for non-linear dynamics. At the Institute of Control and Informatization of Production Processes at BERG Faculty (TUKE), team around Laciak et al. (2018) built upon Bouhouche's work and started experimenting with machine learning in process control and its application in oxygen steelmaking, precisely in LD converter. They applied Support Vector Machines (SVM) and Support Vector Regression (SVR) to predict the final melt temperature and final carbon concentration based on dynamical data.

Their work also focuses on developing innovative fractional-order mathematical models for indirect measurement of molten steel temperature and concentration of CO and CO<sub>2</sub>. The non-linear nature of these processes presents the opportunity to model them by using derivatives of non-integer order, which in their definition are based on the influence of past data on the present value of derivative.

Control of non-linear systems was the subject of intensive studies in the last few decades.

Fractional-order dynamic systems

fractional-order gradient method for backward propagation of neural networks (Sheng et al.; 2019)

## 1.3 Visualization and Virtual Reality

- O VRku - Immersiveness, immersive, immersivity - Non-immersive vs immersive

Scientific visualization is the use of computer graphics to create visual images that aid in the understanding of complex numerical representations of scientific concepts or results. As discussed in previous chapter, computational fluid dynamics (CFD) based numerical simulations often output massive amounts of data. These simulations often contain high-dimensional data in a three-dimensional volume. The display of phenomena associated with this data may involve complex three-dimensional structures.

Such numerical representations, or data sets, may be the output of numerical simulations, as in computational fluid dynamics (CFD) or molecular modeling; recorded data, as in geological or astronomical applications; or constructed shapes, as in visualization of topological arguments. These simulations often contain high-dimensional data in a three-dimensional volume. The display of phenomena associated with this data may involve complex three-dimensional structures. Non-immersive interactive visualization systems implemented for the convention- al desktop and mouse are effective for moderately complex problems. Virtual reality displays aid in the unambiguous display of these structures by providing a rich set of spatial and depth cues. Virtual reality interface concepts al-

low the rapid and intuitive exploration of the volume containing the data, enabling the phenomena at various places in the volume to be explored, as well as provide simple control of the visualization environment through interfaces integrated into the environment (Bryson; 1996).

Luckily for many scientific visualization applications, the graphical rendering is to some extent arbitrary and can be chosen specifically to satisfy the perfor- mance constraints. This situation contrasts with the high-fidelity visual simulation of the real world, which can require time-consuming photo-realistic render- ing techniques. Consider again the example of streamlines in CFD. A streamline is simply an array of points in three dimensions. The array can be simply rendered as lines, allowing very fast rendering. This example can be generalized into a principle for developing real-time interactive visualization systems: Keep the graphical rendering as simple as possible (Bryson; 1996).

Beside mathematical modeling and simulations, creating a graphical representation of environments where particular processes happen is also very important and effective method when designing a future plant or planning upgrades to an already established one. It's important to understand the physical dimensions of is spatially explorable modelling of environment

In some simplified form, the simulation of steelmaking processes can be used as a educational tool in process control courses at technical universities. The aim of the online, webbased interactive simulation of basic oxygen steelmaking at steeluniversity.org shown in Fig. 1-3 is to introduce students to this process in a more fun and engaging way.

A 3-D comprehensive CFD model has been developed, by Zheng and Hu (2014) of Purdue University, specifically for simulating the blast furnace hearth. It includes both the hot metal flow and conjugate heat transfer through the refractories. The model has been extensively validated using measurement data from industry blast furnace. Good agreements between measured and calculated refractory temperature profiles haven been achieved. The virtual reality (VR) visualization technology has been used to analyze the velocity

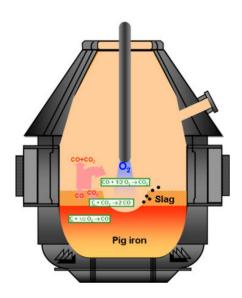


Fig. 1-2: Static representation of basic oxygen furnace (Doh et al.; 2013).

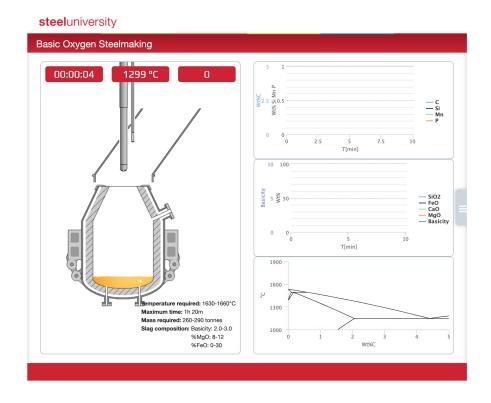
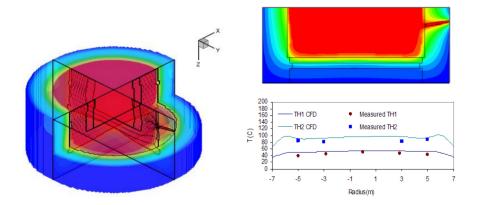
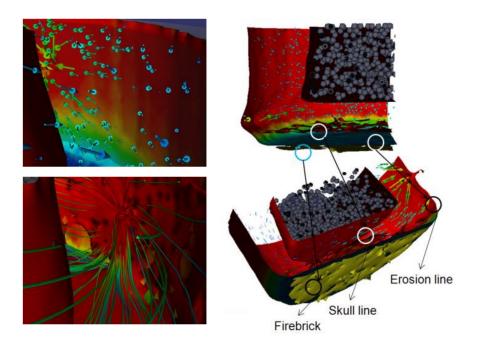


Fig. 1–3: Interactive, educational simulation of basic oxygen steelmaking by steeluniversity.org.

and temperature distributions and wear patterns of different furnaces and operating conditions.



**Fig. 1–4**: Interactive, educational simulation of basic oxygen steelmaking by steeluniversity.org.



**Fig. 1–5**: Interactive, educational simulation of basic oxygen steelmaking by steeluniversity.org.

The campaign life of a blast furnace is highly dependent on residual thickness of refractory lining in the hearth. The progress of hearth lining erosion is greatly affected by hot

metal flow patterns and heat transfer in refractory under different operating conditions. Thus it is of great importance to monitor the hearth erosion and adjust operating conditions accordingly to prevent further erosion. The difficulty of measurement in the hearth makes computational fluid dynamics (CFD) modeling more feasible in hearth erosion prediction.

The CFD model has been applied to predict the hearth inner profiles of the actual blast furnace and understand the effects of operation conditions. The results can be used to predict the inner profile of hearth and to provide guidance for protecting the hearth.

Virtual realia shares many of the same characteristics as VR, while in other ways the two experiences differ substantially. Vr displays, for example, simulate the experiences of manipulating a real object but without the need for the immersive environment characteristic of VR. Following the Extent of Presence Metaphor dimension of Milgram and Kishino's (1994) "virtuality continuum," Vr is essentially a window-on- the-world with a fixed monoscopic viewpoint; changes in the viewer's head position do not result in different perspectives of the object. Immersive virtual environments, by comparison, lie at the other end of the spectrum and permit looking around an object by moving one's head position. Therefore, a fundamental difference between Vr and VR is that the latter is a true 3D representation that may be either viewer or object-centered while the latter is exclusively viewercentered (Kosslyn 1994). In other words, changes in the relative positions of a 2D object's components result from shifts in the viewer's perspective. The same may be true for objects viewed in a three dimensional environment, whether real or virtual. However, in such an environment, an object may also appear to change shape (e.g., through foreshortening), not due to an altered position of the viewer, but because the object itself has moved to a different position (Kealy and Subramaniam; 2006).

Because, sensory breadth contributes more than sensory depth to the experience of presence, it follows that reproduction fidelity is easier to achieve in Vr versus VR, yet more critical to the success of the latter (Kealy and Subramaniam; 2006).

the advent of commodity-level virtual reality (VR) hardware has made this technology accessible for meaningful applications.

Meaningful applications and techniques are being developed to discern how immersive technology benefits visualization. The medical field provides an especially promising context for this development, as medical practitioners require a thorough understanding of specific 3D structures: human anatomy. The most commonly disseminated visualization tools for learning these complex, 3D relationships rely on 2-dimensional (2D) representations. However, when 2D visualizations are used to represent 3D structures, there is a risk of information loss and important interactions between anatomical structures can be absent.

One of In the simulation, users may interact simultaneously with high resolution computed tomography (CT) scans and their corresponding, 3D anatomical structures.

Virtual reality (VR) applications have great potentials for use in education at all levels. VR interfaces have the potentials to complement existing approaches in education. In virtual worlds, learners can be simultaneously provided with three-dimensional representations, multiple perspectives and frames-of-reference, simultaneous visual and auditory feedbacks. With careful de- sign and implementation, these capabilities can be synthesised to create a profound sense of motivation and concentration conducive to mastering complex materials. However, few educational applications have been developed and reported. Shin has reported a desktop VR system for science education in the areas of earth sciences for middle school students (Shin, 2002). VR simulations were developed to teach science concepts such as radiation balance, earthquakes waves, movement of the ocean and earth crust balance. A virtual instrument of a gas chromatograph-mass spectrometer was set up in a web-based environment to train students in instrument operation (Waller & Foster, 2000). Students learn to operate the virtual instrument via the website outside the laboratory, thus freeing the instrument for use within the laboratory to run meaningful experiments and collect data.

Virtual reality is the use of computers and human-computer interfaces to create the effect of a three-dimensional world containing interactive objects with a strong sense of three-dimensional presence (Bryson; 1996).

Immersing the user in the solution, virtual reality reveals the spatially complex structures in computational science in a way that makes them easy to understand and study. But beyond adding a 3D interface, virtual reality also means greater computational complexity (Bryson; 1996).

The ability to provide real-time interaction can provide strong depth cues, either through allowing interactive rotations or through the use of head-tracked rendering.

There are, of course, visualization techniques that demand considerable graphics performance, such as isosurfaces and volumetric rendering. In a large data set, a typical isosurface may contain tens of thousands of (logically) disconnected polygons. These polygons are difficult to render within real-time performance constraints. Ways of meeting this problem for isosurfaces include subsampling the surface (potentially masking interesting features), rearranging the polygons so they are optimized for the graphics hardware, hashing the polygon list to replace coplanar neighboring polygons with a single polygon, and limiting the spatial extent of the isosurface. Many or all of these techniques may be necessary to achieve real-time performance demands, and even then a limited number of isosurfaces may be practical. Time-intensive methods, such as ray-traced or volumetric rendering, may be impractical in real-time applications.

However, in the section on scientific visualization, we suggested that real-time performance is only one of two requirements of a scientific exploration envi- ronment; the other requirement is a natural, inher- ently three-dimensional, human-conforming interface. By this we mean an interface that is used in as natural a way as possible, that provides as unam- biguous a three-dimensional display as possible, and that requires as little as possible of the user's attention. This approach contrasts with the current interaction paradigm in scientific visualization based on text or two-dimensional input through

graphical user interfaces and two-dimensional projections of three-dimensional scenes. Conventional interfaces make it difficult to specify positions in three dimensions and do not provide unambiguous display of three-dimensional structure.

Virtual reality interfaces attempt to provide the most anthropomorphic interfaces possible. Virtual reality interfaces must include two components: display and user control.

Scientific visualization makes particular demands on virtual reality displays. The phenomena to be displayed in a scientific visualization application often involve delicate and detailed structure, requiring high-quality, high-resolution full-color displays. A wide field of view is often desirable, because it allows the researcher to view how detailed structures are related to larger, more global phenomena.

Historically, the early attempts at using head-mounted virtual reality technologies started with CRT-based Binocular Omni-Oriented Monitor (BOOM) created by Fakespace Systems Inc. BOOM is a stereoscopic display device with screens and optical system housed in a box that is attached to a multi-link arm. The user looks into the box through two holes, sees the virtual world, and can guide the box to any position within the operational volume of the device. Head tracking is accomplished via sensors in the links of the arm that holds the box.

Another frequently used type of immersive, interactive display technology is projection-screen-based Cave Automatic Virtual Environment (CAVE). These systems consists of 3 to 6 large displays positioned into a room-sized cube around the observer. The walls of a CAVE are typically made up of rear-projection screens, but recently the flat panel displays are commonly used. The floor can be a downward-projection screen, a bottom projected screen or a flat panel display. The projection systems are very high-resolution due to the near distance viewing which requires very small pixel sizes to retain the illusion of reality. The user wears 3D glasses inside the CAVE to see 3D graphics generated by the CAVE. People using the CAVE can see objects apparently floating in the air, and can walk around them, getting a proper view of what they would look like in reality. This is made possible

by infrared cameras. Movement of the observer in the CAVE is tracked by the sensors typically attached to the 3D glasses and the video continually adjusts to retain the viewers perspective.

Many universities and engineering companies own and use CAVE systems. Researchers can use these systems to conduct their research topic in a more effective and accessible method. Engineers have found them useful in enhancing of a product development through prototyping and testing phases.

## 2 Objectives of the dissertation

This dissertation thesis deals with design and implementation of

## 3 Methodology

## **Bibliography**

Bouhouche, S., Mentouri, Z., Hazem, M. and Yazid, L. (2012). Combined use of support vector regression and monte carlo simulation in quality and process control calibration, *Proceedings of the 2012 international conference on industrial engineering and operations management* pp. 3–6.

- Bryson, S. (1996). Virtual reality in scientific visualization, *Commun. ACM* **39**(5): 62–71. **URL:** http://doi.acm.org/10.1145/229459.229467
- Doh, Y., Chapelle, P., Jardy, A., Djambazov, G., Pericleous, K., Ghazal, G. and Gardin, P. (2013). Toward a full simulation of the basic oxygen furnace: Deformation of the bath free surface and coupled transfer processes associated with the post-combustion in the gas region, *Metallurgical and Materials Transactions B: Process Metallurgy and Materials Processing Science* **44**(3): 653–670.
- Ersson, M. and Tilliander, A. (2018). Review on CFD Simulation and Modeling of Decarburization Processes, *Steel Research International* **89**(1): 1–13.
- Fritz, E. and Gebert, W. (2005). Milestones and challenges in oxygen steelmaking, *Canadian Metallurgical Quarterly* **44**(2): 249–260.
  - **URL:** https://doi.org/10.1179/cmq.2005.44.2.249
- Jalkanen, H. (2006). Experiences in physicochemical modelling of oxygen converter process (BOF), 2006 TMS Fall Extraction and Processing Division: Sohn International Symposium 2: 541–554.
- Kačur, J., Laciak, M., Flegner, P., Terpak, J., Durdan, M. and Trefa, G. (2019). Application of support vector regression for data-driven modeling of melt temperature and carbon content in ld converter, pp. 1–6.
- Kealy, W. A. and Subramaniam, C. P. (2006). Virtual realia: Maneuverable computer 3D models and their use in learning assembly skills, *Virtual Reality* **10**(3-4): 283–292.
- Laciak, M., Petráš, I., Terpák, J., Kačur, J., Flegner, P., Durdán, M. and Tréfa, G. (2018).

Výskum nepriameho merania teploty a uhlíka v procese skujňovania, *Technical report*, Institute of Control and Informatization of Production Processes.

- Laciak, M., Petráš, I., Flegner, P., Durdán, M. and Tréfa, G. (2017). Výskum nepriameho merania teploty a uhlíka v procese skujňovania, *Technical report*, Fakulta BERG Ústav riadenia a informatizácie výrobných procesov.
- Peng, Y. and Han, T. (1996). Gas-particle flow in a de laval nozzle with curved convergent configuration, *ISIJ International* **36**(3): 263–268.
- Rapp, B. E. (2017). Chapter 1 introduction, *in* B. E. Rapp (ed.), *Microfluidics: Modelling, Mechanics and Mathematics*, Micro and Nano Technologies, Elsevier, Oxford, pp. 3 7.
  - URL: http://www.sciencedirect.com/science/article/pii/B9781455731411500010
- Ray, W. H., Szekely, J. and Ajinkya, M. B. (1973). Optimization of the ironmaking-steelmaking sequence in an integrated steel plant having non-linear and distributed elements, *Metallurgical Transactions* **4**(6): 1607–1614.
- Sarkar, R., Gupta, P., Basu, S. and Ballal, N. B. (2015). Dynamic Modeling of LD Converter Steelmaking: Reaction Modeling Using Gibbs' Free Energy Minimization, *Metallurgical and Materials Transactions B: Process Metallurgy and Materials Processing Science* **46**(2): 961–976.
- Sheng, D., Wei, Y., Chen, Y. and Wang, Y. (2019). Convolutional neural networks with fractional order gradient method, *Neurocomputing*.
  - URL: http://www.sciencedirect.com/science/article/pii/S0925231219313918
- Szekely, J., Chang, C. W. and Ryan, R. E. (1977). The measurement and prediction of the melt velocities in aturbulent, electromagnetically driven recirculating low melting alloy system, *Metallurgical Transactions B* **8**(1): 333–338.

URL: https://doi.org/10.1007/BF02657664

Tago, Y. and Higuchi, Y. (2003). Fluid flow analysis of jets from nozzles in top blown process, *ISIJ International* **43**(2): 209–215.

- Turkdogan, E. T. (1996). *Fundamentals of Steelmaking*, The Institute of Materials, London.
- Turkdogan, E. T. and Fruehan, R. J. (1999). Fundamental of Iron and STM (Chapter 2), i.
- Wang, W., Yuan, Z., Matsuura, H., Zhao, H., Cheng, D. A. and Tsukihashi, F. (2010).
  Three-dimensional Compressible Flow Simulation of Top-blown Multiple Jets in Converter, *ISIJ International* 50(4): 491–500.
- Wang, X., Han, M. and Wang, J. (2010). Applying input variables selection technique on input weighted support vector machine modeling for BOF endpoint prediction, *Engineering Applications of Artificial Intelligence* **23**(6): 1012–1018.

**URL:** http://dx.doi.org/10.1016/j.engappai.2009.12.007

Widlund, D., Medvedev, A. and Gyllenram, R. (1998). Towards Model-Based Closed-Loop Control of the Basic Oxygen Steelmaking Process, *IFAC Proceedings Volumes* **31**(23): 69–74.

**URL:** http://dx.doi.org/10.1016/S1474-6670(17)35858-5

Zheng, L. and Hu, Y. (2014). Blast Furnace Hearth Flow and Erosion Model.