

Summary

$$\mathcal{L}\{y(t)\} = Y(s)$$

$$\mathcal{L}\{u(t)\} = U(s)$$

$$\mathcal{L}\{\dot{y}(t)\} = s\tilde{Y}(s) - y(0^-)$$

$$\mathcal{L}\{\ddot{y}(t)\} = s^2 Y(s) - sy(0^-) - \dot{y}(0^-)$$

$$\mathcal{L}\{\ddot{y}(t)\} = s^2 Y(s) - sy(0^-) - \dot{y}(0^-)$$

$$y^{(n)} + a_{n-1}y^{(n-1)} + a_{n-2}y^{(n-2)} + \dots + a_0y = b_0u + b_1\dot{u} + \dots + b_m\ddot{u}$$

Called an input-output system because only inputs $u(t)$ and outputs $y(t)$ appear in the model

Let the I.C.'s be $y(0^-), \dots, y^{(n-1)}(0^-)$, then

$Y(s) = Y_{\text{forced}}(s) + Y_{\text{IC}}(s)$ called the
superposition ("superstition") principle

$Y_{\text{forced}}(s)$ = Solution with all I.C. = 0

$Y_{\text{IC}}(s)$ = Solution with input = 0

Let r_1, r_2, \dots, r_n be the roots of the denominator of $Y(s)$, assumed distinct. Then the PFE is

$$Y(s) = \frac{k_1}{s-r_1} + \frac{k_2}{s-r_2} + \dots + \frac{k_n}{s-r_n} \quad \text{where}$$

$k_j = \lim_{s \rightarrow r_j} Y(s)(s - r_j)$ and if $r_{j+1} = r_j^*$ complex

conjugate ($r_j = a_j + i w_j \Rightarrow r_j^* = a_j - i w_j$) then

$$k_{j+1} = \lim_{s \rightarrow r_j^*} Y(s)(s - r_j^*) = k_j^*$$

$e^{r_j t} = e^{a_j t} \cdot e^{i w_j t} = e^{a_j t} [\cos(w_j t) + i \sin(w_j t)]$

$$\frac{1}{s - r_j} \longleftrightarrow e^{r_j t} u_s(t) \xrightarrow[t \rightarrow 0]{\text{Re}} 0 \Leftrightarrow \text{Re}\{r_j\} < 0$$

(associated with "stability")

Left off: Laplace applied to a state-variable model

$$\dot{x}_1 = -5x_1 + x_2 + 7u$$

$$x_1(0^-) = 2$$

$$\dot{x}_2 = -6x_1 + u$$

$$x_2(0^-) = 13$$

$$y = x_1$$

$$u(t) = e^{-t} u_s(t)$$

$$S X_1(s) - x_1(0^-) = -5X_1(s) + X_2(s) + 7U(s)$$

$$S X_2(s) - x_2(0^-) = -6X_1(s) + U(s)$$

$$Y(s) = X_1(s)$$

Solve linear equations to obtain

$Y(s)$ in terms of $U(s)$, $x_1(0^-)$, $x_2(0^-)$

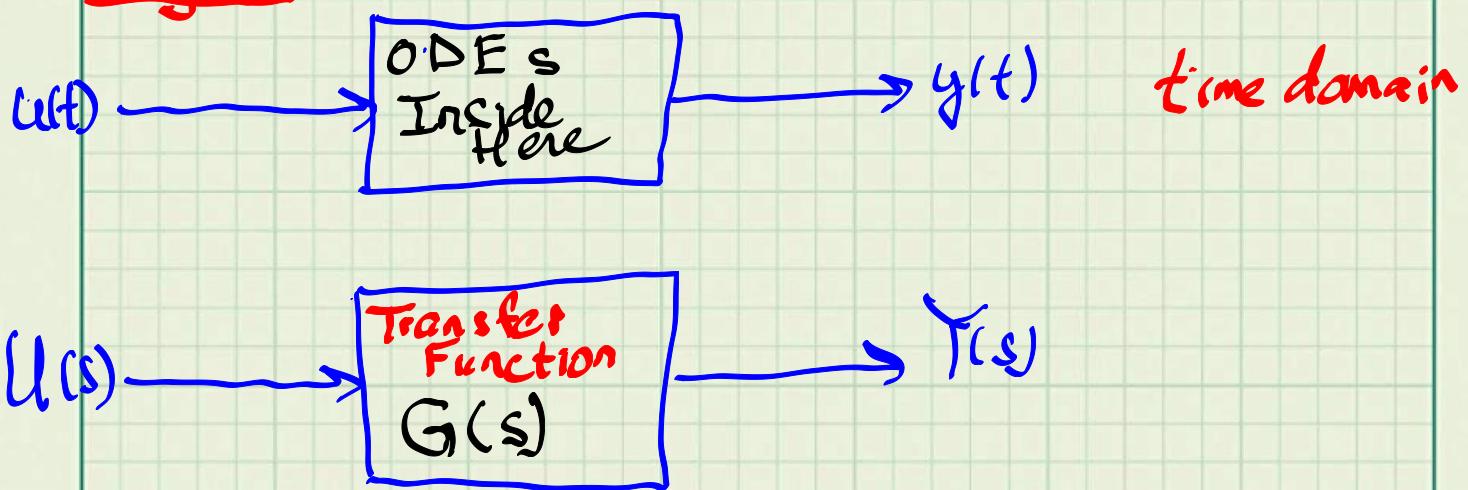
[We'll instead use vectors & matrices]

Today

$$\begin{aligned} \dot{x} &= Ax + Bu \quad \longleftrightarrow \quad Y(s) = C(sI - A)^{-1}Bu(s) + \\ y &= Cx \end{aligned}$$

- Transfer Functions
- Poles & Zeros
- BIBO Stability

Systems



- Transfer function maps $U(s)$ [input in the Laplace domain] to $Y(s)$ [output in the Laplace domain]

Def. The transfer function of the input-output model

$$(*) \quad y^{(n)} + a_{n-1}y^{(n-1)} + \dots + a_1y + a_0y = b_0u(t) + b_1u'(t) + \dots + b_m u^{(m)}(t)$$

(should be t's everywhere or nowhere)

is the rational function

$$G(s) := \frac{Y(s)}{U(s)} = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_1 s + b_0}{s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}$$

Obtained by taking the Laplace transform of (*) with all I.C. = 0.

Note: $Y(s) = G(s) \cdot U(s)$

\uparrow
multiplication of
"rational" functions

Example Compute the transfer function

for $\ddot{y} + 7\dot{y} - 6y = 3u - 4\dot{u}$

$$G(s) = \frac{3-4s}{s^2 + 7s - 6} = \frac{-4s+3}{s^2+7s-6}$$

$G(s) = \frac{Y(s)}{U(s)}$ or $\frac{U(s)}{Y(s)}$?

$$(s^2 + 7s - 6)Y(s) = (3 - 4s)U(s)$$

$$Y(s) = \boxed{\frac{(-4s+3)}{s^2+7s-6}U(s)}$$

$G(s)$

$$\therefore \frac{Y(s)}{U(s)} = \frac{-4s+3}{s^2+7s+6} =: G(s)$$

Def. The transfer function of

$$\begin{aligned}\dot{x} &= Ax + bu & u \in \mathbb{R} & , x \in \mathbb{R} \\ y &= cx & y \in \mathbb{R}\end{aligned}$$

is the Laplace transform, $\tilde{Y}(s)$, divided by the Laplace transform, $\tilde{U}(s)$, when all I.C. are zero ($x(0^-) = 0_{n \times 1}$).

$$Y(s) = \underbrace{c(sI - A)^{-1} b}_{G(s)} U(s)$$

$$\therefore \frac{Y(s)}{U(s)} = c(sI - A)^{-1} b$$

Cannot compute by inspection. Use software.

- For now, invite you to read about
 - 1) Segway model
 - 2) Linear Approximations of NL ODEs

Poles-Zeros- BIBO Stability

Def. For a rational transfer function $G(s) = \frac{N(s)}{D(s)}$ with all common factors **REMOVED**, the

Poles of $G(s)$ = roots of $D(s)$

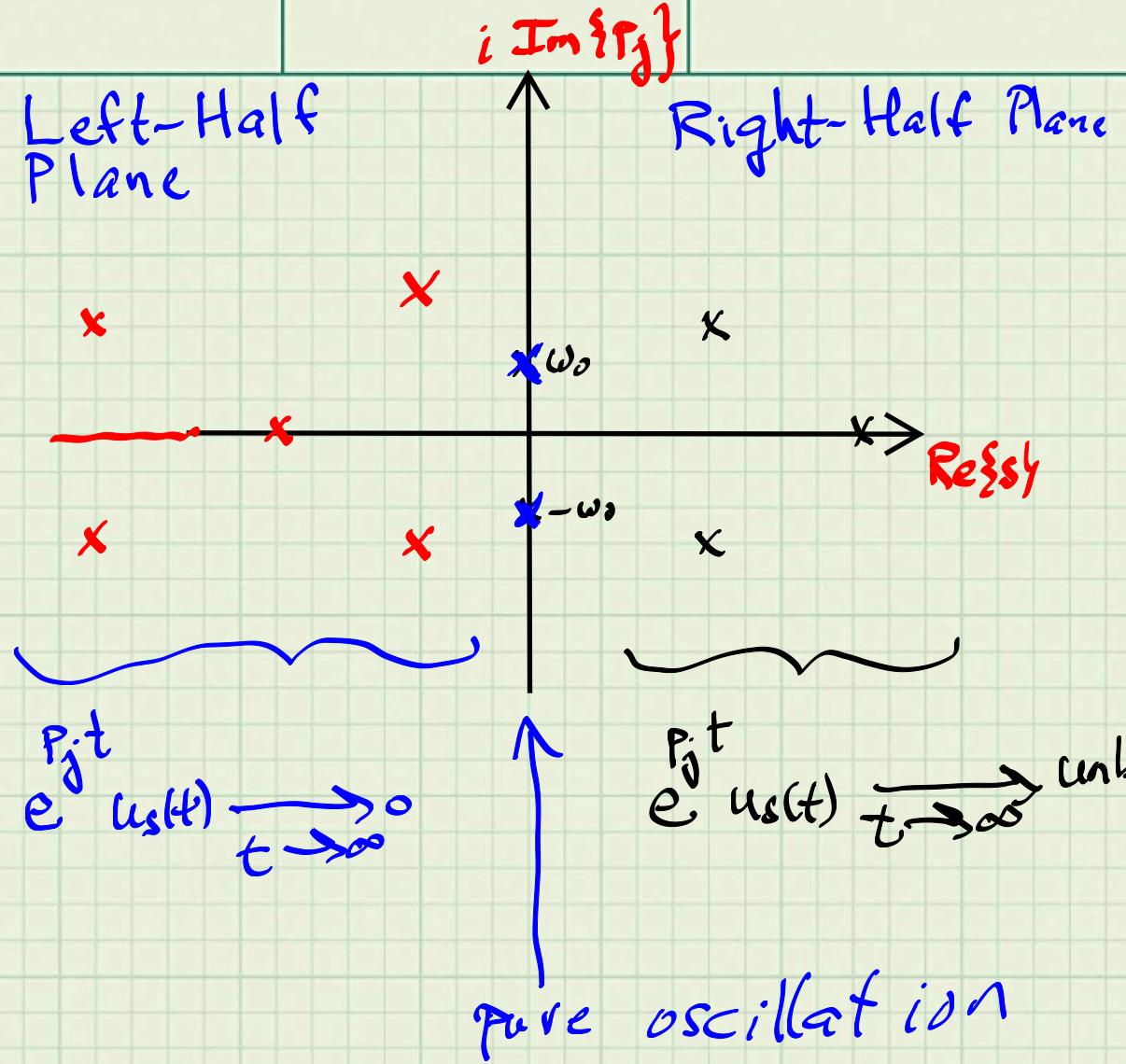
Zeros of $G(s)$ = roots of $N(s)$

$$Y(s) = G(s) \cdot U(s), \quad U(s) = \frac{1}{s} \quad \leftrightarrow u(t) = u(st)$$

$$Y(s) = \frac{k_0}{s} + \frac{k_1}{s-p_1} + \frac{k_2}{s-p_2} + \dots + \frac{k_n}{s-p_n} \quad \text{PFE}$$

as long as the poles are distinct. Note that p_1, p_2, \dots, p_n are the poles of $G(s)$

$$y(t) = \underbrace{k_0 u(st)}_{\text{Bounded}} + \sum_{j=1}^n k_j e^{p_j t} \underbrace{u(st)}_{\substack{\rightarrow \infty \\ \text{Re}\{p_j\} < 0}}$$



Def. A system $\xrightarrow{u(t)} \boxed{\text{ODE}} \rightarrow y(t)$
 is BIBO STABLE (Bounded-Input
 Bounded-Output) if bounded inputs
 always produce bounded outputs.

Prop. Suppose the system is defined by a transfer function $G(s) = \frac{N(s)}{D(s)}$ where $\deg(N(s)) \leq \deg(D(s))$. Then, it is

BIBO STABLE \Leftrightarrow all poles of $G(s)$ have negative real parts.

Examples

$$G_a(s) = \frac{s+2}{s^2 - 1} = \frac{s+2}{(s+1)(s-1)}$$

| | |
|-------|----|
| zeros | -2 |
| poles | +1 |

BIBO NO, because of a pole with a positive real part, +1

$$G_b(s) = \frac{s+1}{s^2 - 1} = \frac{s+1}{(s+1)(s-1)}$$

| | |
|-------|-----------------------|
| zeros | None |
| poles | +1 |
| BIBO | No, due to pole at +1 |

$$G_c(s) = \frac{2s-4}{s^2+2s+2} = \frac{2(s-2)}{(s+1+i)(s+1-i)}$$

| | |
|-------|------|
| zeros | +2 |
| poles | -1±i |
| BIBO | YES |

$\operatorname{Re}\{-1\pm i\} = -1 < 0$

$$G(s) = \frac{1}{s^2 + 1}$$

| | |
|-------|--------------------------|
| Zeros | None |
| Poles | $\pm i$ |
| SISO | No? Do we believe it? |

$$u(t) = \underbrace{\sin(t)}_{\text{Bounded}} u_s(t) \longleftrightarrow \frac{s}{s^2 + 1} = U(s)$$

$$Y(s) = G(s)U(s) = \frac{s}{(s^2 + 1)^2} \quad \begin{array}{l} \text{Table} \\ \xrightarrow{\text{Laplace Transform}} \end{array}$$

$$\rightarrow y(t) = \underbrace{t \sin(t)}_{\text{unbounded}} u_s(t)$$

"Resonance" yields unbounded behavior

Poles s in the Left Half Plane

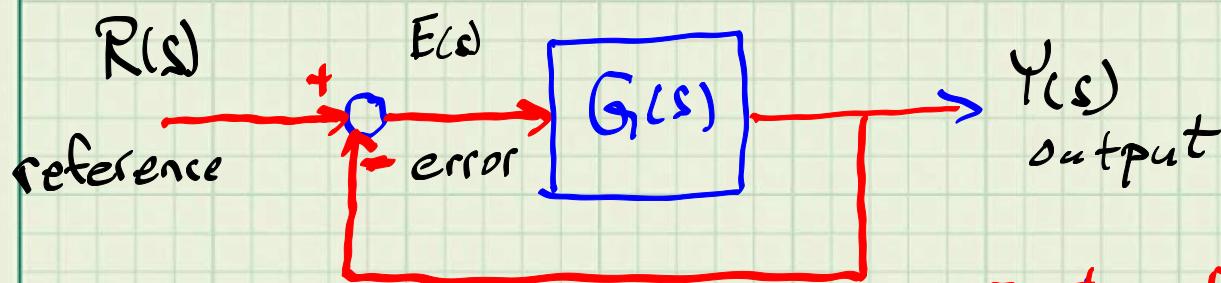


$$\operatorname{Re}\{p_j\} < 0 \quad 1 \leq j \leq n$$

Start Feedback Control

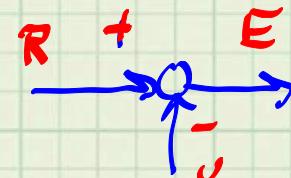
Def.: Block Diagram of a

Unity Feedback System



$$E(s) = R(s) - Y(s)$$

$$Y(s) = G(s) E(s)$$



Summing junction

$$Y(s) = G(s) [R(s) - Y(s)]$$

$$Y(s) = G(s) R(s) - G(s) Y(s)$$

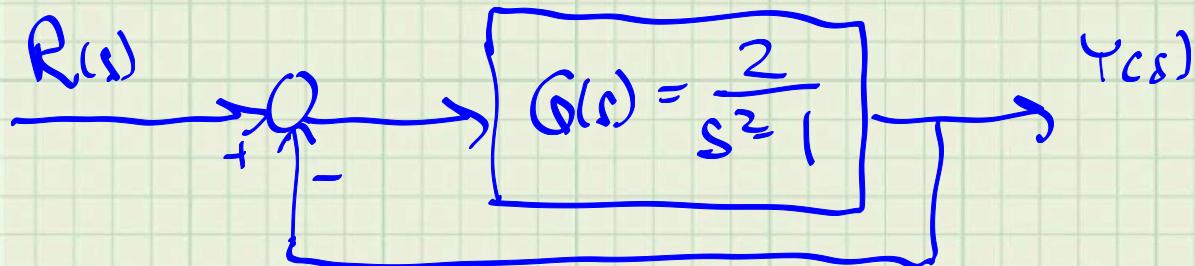
$$Y(s) + G(s) Y(s) = G(s) R(s)$$

$$(1 + G(s)) Y(s) = G(s) R(s)$$

$$\left\{ \frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)} \right\}$$

closed-loop transfer function

Aside: $\frac{\frac{3}{4}}{1 + \frac{3}{4}} = \frac{4}{4+3} = \frac{3}{7}$



$$\frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)} = \frac{\frac{2}{s^2 - 1}}{1 + \frac{2}{s^2 - 1}} = \frac{2}{s^2 - 1 + 2}$$

$$= \frac{2}{s^2 + 1}$$

$$G_2(s) = \frac{s+2}{s^2 - 1}$$

in the unity feedback loop

$$\frac{Y(s)}{R(s)} = \frac{\frac{s+2}{s^2 - 1}}{1 + \frac{s+2}{s^2 - 1}} = \frac{s+2}{s^2 - 1 + s + 2} = \frac{s+2}{s^2 + s + 1}$$

$$G_2(s) = \frac{s+2}{s^2 - 1} \quad \left\{ \begin{array}{l} \text{poles : } \pm 1 \\ \text{BIBO : NO} \end{array} \right.$$

open-loop TF unstable

$$\frac{Y(s)}{R(s)} = \frac{s+2}{s^2+s+1} \quad \left\{ \begin{array}{l} \text{Poles: } -\frac{1}{2} \pm \frac{\sqrt{3}}{2} i \\ \text{BIBO Yes} \end{array} \right.$$

Closed-loop TF
BIBO Stable

Fact 10.33: Simplified Stability Test

For real numbers a_1 and a_0 , the roots of the quadratic equation

$$s^2 + a_1 s + a_0 = 0 \quad (10.49)$$

have negative real parts if, and only if, $a_1 > 0$ and $a_0 > 0$.

Note: To apply the above result to $\bar{a}_2 s^2 + \bar{a}_1 s + \bar{a}_0 = 0$, with $\bar{a}_2 \neq 0$, you simply divide through by \bar{a}_2 , yielding $a_1 = \frac{\bar{a}_1}{\bar{a}_2}$ and $a_0 = \frac{\bar{a}_0}{\bar{a}_2}$.

For a cubic equation, the result is, for real numbers a_2, a_1 , and a_0 , the roots of the equation

$$s^3 + a_2 s^2 + a_1 s + a_0 = 0$$

$$(s+r_1)(s+r_2) = s^2 + (r_1+r_2)s + r_1 r_2$$

$$\rho_1 = -r_1, \quad \rho_2 = -r_2$$

$$\underbrace{(s+r)^2 + \omega^2}_{-r \pm i\omega} = s^2 + 2rs + r^2 + \omega^2$$

See textbook for cubic case