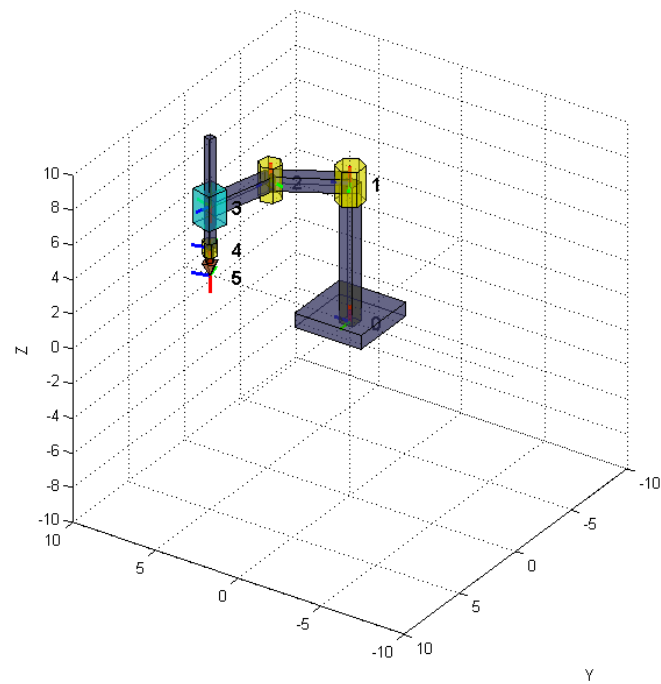


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# FORWARD AND INVERSE KINEMATICS

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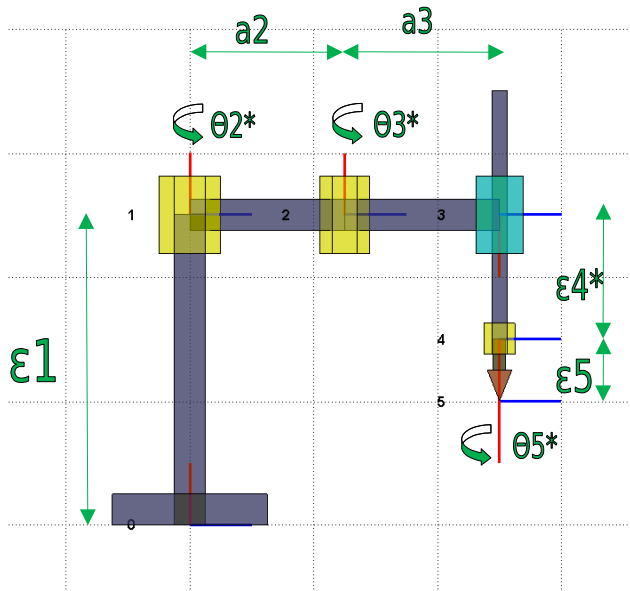
## SCARA ROBOT



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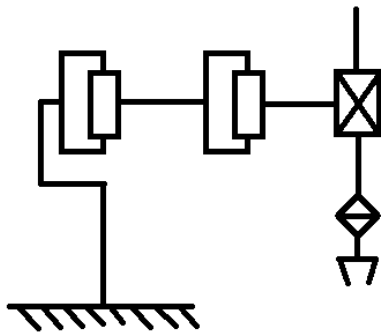
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## SCHEMATIC, D-H TABLE



	$\Theta_i$	$\epsilon_i$	$a_i$	$\alpha_i$
H01	$0^\circ$	$\epsilon_1$	0	$0^\circ$
H12	$\Theta_2^*$	0	$a_2$	$0^\circ$
H23	$\Theta_3^*$	0	$a_3$	$180^\circ$
H34	$0^\circ$	$\epsilon_4^*$	0	$0^\circ$
H45	$\Theta_5^*$	$\epsilon_5$	0	$0^\circ$

**SCARA schematic with coordinate systems**  
(red lines – Z axis, blue lines – X axis ; numbers near coordinate systems)



**SCARA kinematic diagram**

## HOMOGENEOUS MATRICES

Homogeneous matrices were created with use of the D-H tables (previous page). They describe positions and orientations of subsequent coordinate systems attached to the robot's joints and links – each relative to previous coordinate systems. Last matrix describes position and orientation of the end-effector, relative to the base coordinate system {0}.

$$H_{01} = \text{Trans}(0,0, \epsilon_1) =$$

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & \epsilon_1 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$H_{12} = \text{Rot}(Z, \Theta_2^*) \cdot \text{Trans}(a_2, 0, 0) =$$

$$\begin{pmatrix} \cos(\theta_2) & -\sin(\theta_2) & 0 & a_2 \cos(\theta_2) \\ \sin(\theta_2) & \cos(\theta_2) & 0 & a_2 \sin(\theta_2) \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$H_{23} = \text{Rot}(Z, \Theta_3^*) \cdot \text{Trans}(a_3, 0, 0) \cdot \text{Rot}(X, 180^\circ) =$$

$$\begin{pmatrix} \cos(\theta_3) & \sin(\theta_3) & 0 & a_3 \cos(\theta_3) \\ \sin(\theta_3) & -\cos(\theta_3) & 0 & a_3 \sin(\theta_3) \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$H_{05} = H_{01} \cdot H_{12} \cdot H_{23} \cdot H_{34} \cdot H_{45} =$$

$$\begin{pmatrix} \cos(\theta_2 + \theta_3 - \theta_5) & \sin(\theta_2 + \theta_3 - \theta_5) & 0 & a_3 \cos(\theta_2 + \theta_3) + a_2 \cos(\theta_2) \\ \sin(\theta_2 + \theta_3 - \theta_5) & -\cos(\theta_2 + \theta_3 - \theta_5) & 0 & a_3 \sin(\theta_2 + \theta_3) + a_2 \sin(\theta_2) \\ 0 & 0 & -1 & \epsilon_1 - \epsilon_4 - \epsilon_5 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

**D-H Table** (joint variable marked with star \*)

$\Theta_2^*$  - rotation angle - joint 1.

$\Theta_3^*$  - rotation angle - joint 2.

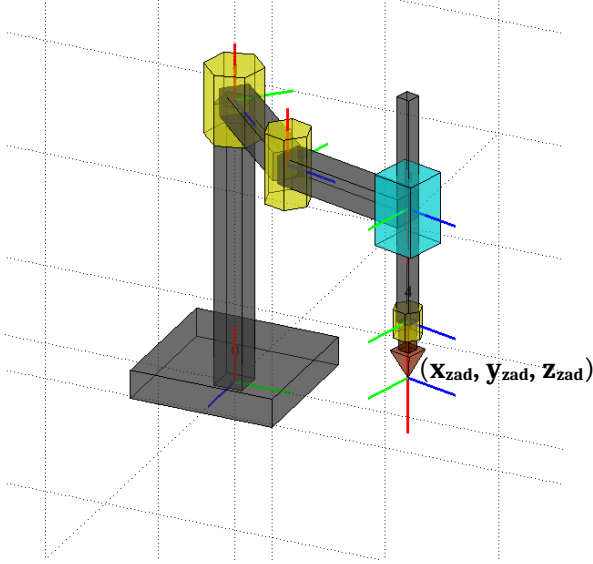
$\epsilon_4^*$  - rotation angle - joint 3.

$\Theta_5^*$  - rotation angle - joint 4.  
(end-effector orientation)

$$\begin{pmatrix} \cos(\theta_5) & -\sin(\theta_5) & 0 & 0 \\ \sin(\theta_5) & \cos(\theta_5) & 0 & 0 \\ 0 & 0 & 1 & \epsilon_5 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

## INVERSE KINEMATICS

To solve the inverse kinematics we need to find relation between joint variables  $(\Theta_2^*, \Theta_3^*, \Theta_4^*, \Theta_5^*)$  and variables describing desired position of the robot's end effector  $(x_{zad}, y_{zad}, z_{zad})$ . Below a geometric approach is described to find target variables:



The Law of cosines in  $\triangle ADC$  gives:

$$\left(\sqrt{x_{zad}^2 + y_{zad}^2}\right)^2 = l_{L2}^2 + l_{L3}^2 - 2l_{L2}l_{L3}\cos(\pi - \theta_3)$$

$$x_{zad}^2 + y_{zad}^2 = l_{L2}^2 + l_{L3}^2 + 2l_{L2}l_{L3}\cos(\theta_3)$$

$$\cos(\theta_3) = \frac{x_{zad}^2 + y_{zad}^2 - l_{L2}^2 - l_{L3}^2}{2l_{L2}l_{L3}} := D$$

Utilizing the Pythagorean trigonometric identity:

$$\cos^2(\theta_3) + \sin^2(\theta_3) = 1$$

leads to:

$$\sin(\theta_3) = \pm \sqrt{1 - D^2}$$

Thus:

$$\theta_3 = \arctg\left(\pm \frac{\sqrt{1 - D^2}}{D}\right)$$

There are two possible robot's elbow configurations, depending on a choice of a sign above. In the MATLAB visualisation code „+” sign was chosen. That implies „elbow down” configuration.

$\triangle ADC$  angles analysis gives:

$$\alpha = \beta + \theta_2 \rightarrow \theta_2 = \alpha - \beta$$

$$\alpha = \arctan\left(\frac{y_{zad}}{x_{zad}}\right)$$

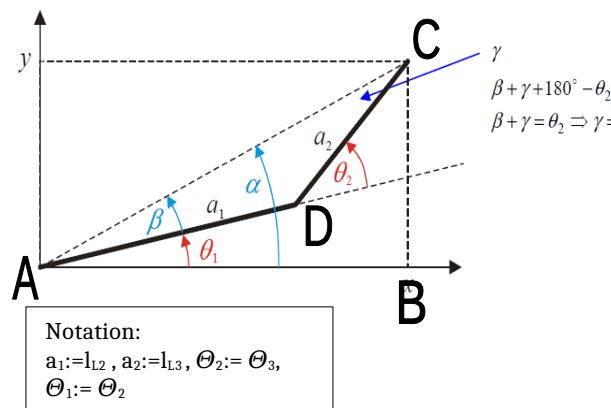
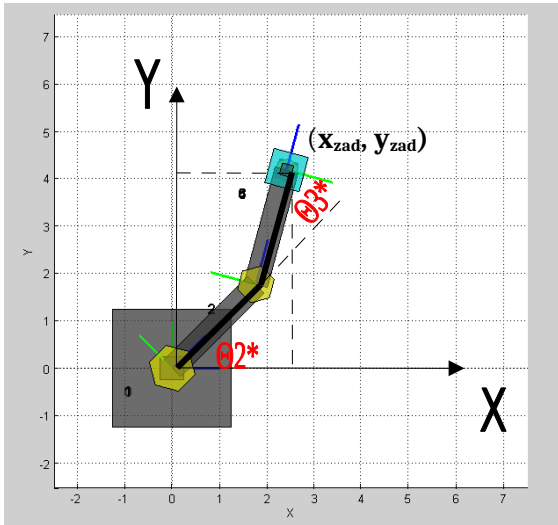
$$\gamma + \beta + (\pi - \theta_3) = \pi \rightarrow \gamma = \beta - \theta_3$$

From the Law of sines in  $\triangle ADC$ :

$$\frac{l_{L3}}{\sin\beta} = \frac{l_{L2}}{\sin\gamma}$$

$$\frac{l_{L3}}{\sin\beta} = \frac{l_{L2}}{\sin(\beta - \theta_3)}$$

$$\frac{l_{L3}}{\sin\beta} = \frac{l_{L2}}{\sin\theta_3 \cos\beta - \sin\beta \cos\theta_3}$$



$$l_{L3} \sin \theta_3 \cos \beta - l_{L3} \sin \beta \cos \theta_3 = l_{L2} \sin \beta$$

$$l_{L3} \sin \theta_3 \cos \beta = l_{L3} \sin \beta \cos \theta_3 + l_{L2} \sin \beta$$

$$(l_{L3} \sin \theta_3) \cos \beta = (l_{L3} \cos \theta_3 + l_{L2}) \sin \beta$$

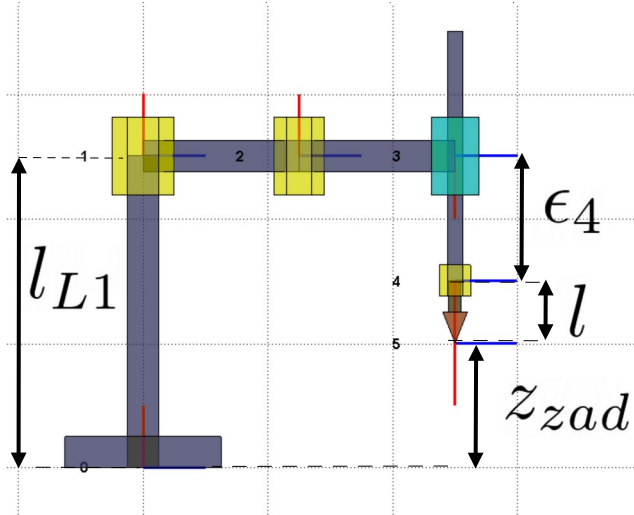
To get tangent of  $\beta$  angle :

$$\frac{\sin \beta}{\cos \beta} = \frac{l_{L3} \sin \theta_3}{l_{L3} \cos \theta_3 + l_{L2}}$$

$$\tan \beta = \frac{l_{L3} \sin \theta_3}{l_{L3} \cos \theta_3 + l_{L2}}$$

$$\beta = \arctg \left( \frac{l_{L3} \sin \theta_3}{l_{L3} \cos \theta_3 + l_{L2}} \right)$$

Having  $\alpha$  and  $\beta$  and using  $\theta_2 = \alpha - \beta$  leads to :



$$\theta_2 = \arctg \left( \frac{y_{zad}}{x_{zad}} \right) - \arctg \left( \frac{l_{L3} \sin \theta_3}{l_{L3} \cos \theta_3 + l_{L2}} \right)$$

After analysis of the schematic one can write:

$$\epsilon_4 = l_{L1} - l - z_{zad}$$

Last joint variable  $\Theta_5$  orients the end-effector in space. It is a rotation angle (Z axis) of the local coordinate system {5}. By fixing  $\Theta_5$  angle as 0, end-effector rotation angle with respect to coordinate system {0} equals  $\Theta_2 + \Theta_3$ .

If one want to control a global rotation angle of the end-effector, following formula shall be used:

$$\theta_5 = \theta_{5glob.} + \theta_2 + \theta_3$$

where :  $\theta_{5glob.}$  - desired angle of the end-effector relative to global coordinate system {1},  
(  $\theta_2 + \theta_3$  ) - compensation term

The use of „+“ sign in the compensation term should be clarified . Coordinate system {5} is oriented „upside-down“ relative to a global coordinate system {0}, thus positive local angle of the end-effector implies negative global rotation angle of the end-effector. This concludes to:

$$\theta_5 \neq \theta_{5glob.} - (\theta_2 + \theta_3)$$

## SCARA ROBOT SIMULATION PROGRAM DESCRIPTION

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### OUTLINE

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Simulation program is divided into following main parts:

1. **Init the workspace (function: *InitSpace*)**
2. **Load robot's dimensions, scale factor and robot's global orientation**
3. **Choice of one of the demo trajectories (variable: *mode*):**
  - 3.1. Static configuration (*mode*=0)
  - 3.2. Trajectory 1: Circle (*mode*=1)
  - 3.3. Trajectory 2: Line (*mode*=2)
  - 3.4. Trajectory 3: „Fish” (*mode*=3)
  - 3.5. Trajectory 4: Quadrifolium (*mode*=4)
  - 3.6. Trajectory 5: Archimedean spiral (*mode*=5)
4. **Model animation, trajectory trace drawing, coordination system assignment (functions: *SCARA\_3Dmodel* and *plot3*)**

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### MODEL DRAWING FUNCTION

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**SCARA\_3Dmodel ( $H_{loc}$ ,  $Q$ ,  $s$ )** – inputs  $H_{loc}$  homogeneous matrix (which places the robot in desired position and with desired orientation), vector of joint variables  $Q$  and scale factor  $s$ . In the code user can define joints and links dimensions and their orientation in space defining forward kinematics (homogeneous matrices). *SCARA\_3Dmodel* function calls four subfunctions: two for drawing linear and rotational joints ( *J\_ROT3D* and *J\_TRANS3D* ), one for drawing links ( *L\_BOX3D* ) and one responsible for drawing the end-effector ( *L\_TOOL3D* ).

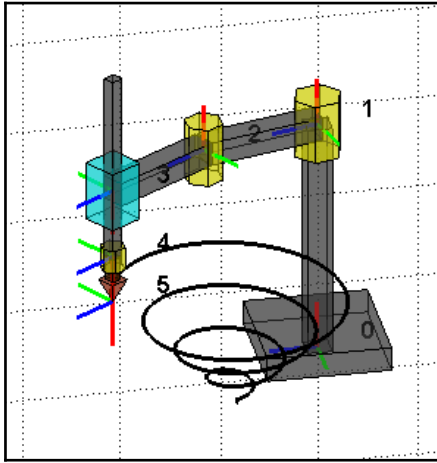
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### TRAJECTORY GENERATION FUNCTION (MODE\_XXX FILES)

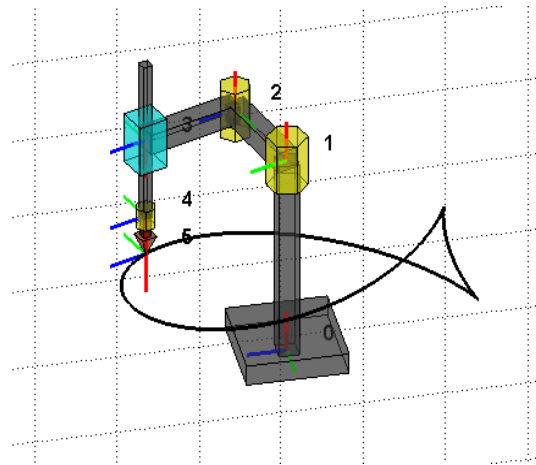
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In each for loop iteration current trajectory point in space is computed and joint variable recalculated via inverse kinematics.

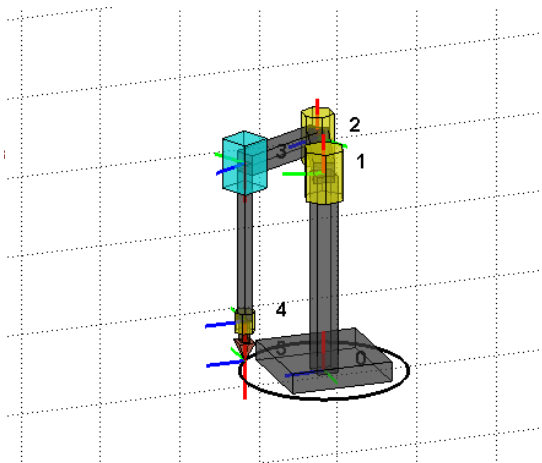
## SCREENSHOTS



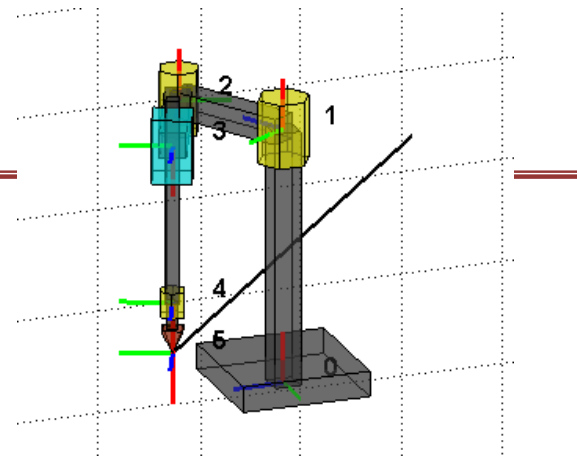
ARCHIMEDEAN SPIRAL (MODE=5)



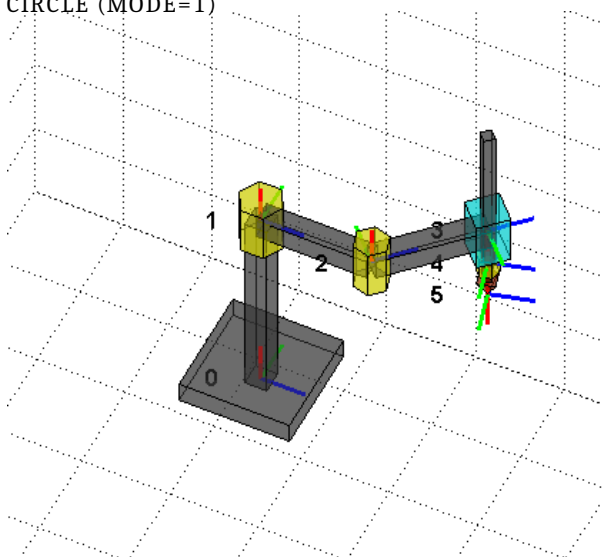
FISH (MODE=3)



CIRCLE (MODE=1)

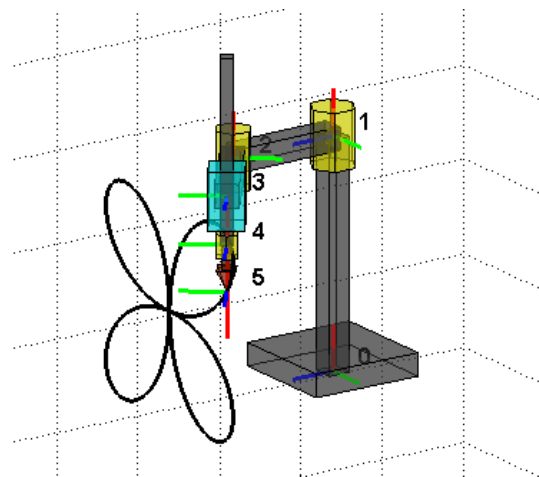


LINE (MODE=2)



ARBITRARY STATIC CONFIGURATION:

$$\Theta_2=0, \Theta_3=45 \text{ } E_4=1 \text{ } \Theta_5=30$$



QUADRIFOLIUM (MODE=4)



## References

- Jezierski E.: *Dynamika robotów*, Wydawnictwa Naukowo-Techniczne, 2006
- <http://www.mathworks.com/help/rptgenext/ug/documentation.html>
- [www.wolframalpha.com](http://www.wolframalpha.com) (parametric curves)