ECE307-11

Active Filter Circuits

Higher Order Op Amp Filter

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Higher Order Op Amp Filter

Cascading Identical Filter

To obtain a sharper transition between the pass-band and stopband, we can add more identical filter in cascade.

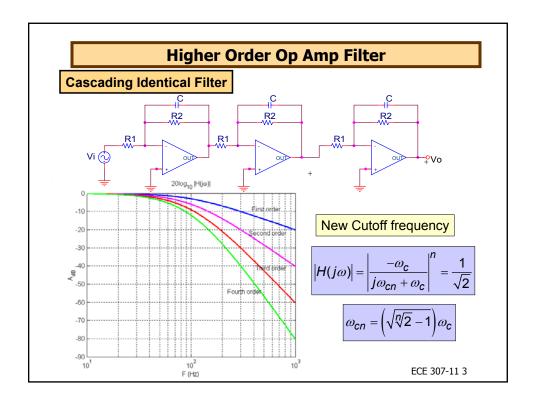
One filter gives us 20dB/dec slope, two identical cascade filters give us 40 dB/dec slope transition.

n identical cascade low-pas filters give us from the corner frequency *n*20dB/dec slope

Transfer function

$$H(s) = \left(\frac{-\omega_{c}}{s + \omega_{c}}\right) \left(\frac{-\omega_{c}}{s + \omega_{c}}\right) \dots \left(\frac{-\omega_{c}}{s + \omega_{c}}\right)$$

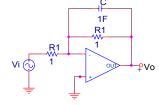
$$H(s) = \left(\frac{-\omega_{\rm c}}{s + \omega_{\rm c}}\right)^n$$



Higher Order Op Amp Filter

Example

 Design 4 order low-pass filter with cut-off frequency is 500Hz and a pass-band gain is 10. Use capacitor 1μF capacitors



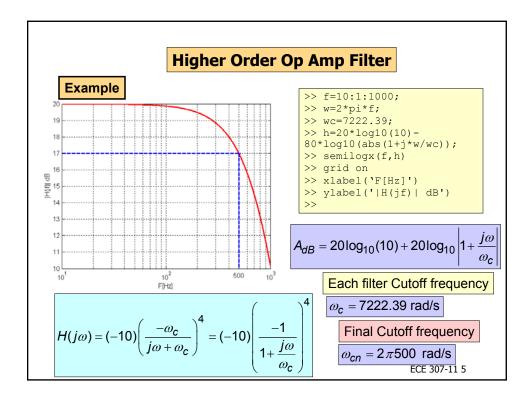
From the cutoff frequency

$$\omega_{cn} = \frac{\omega_{cn}}{\sqrt{\sqrt[4]{2} - 1}} = \frac{2\pi 500}{0.435} = 7222.39 \text{ rad/s}$$

$$\omega_c = \frac{1}{RC}$$
 $R = \frac{1}{\omega_c C} = \frac{1}{7222.39(10^{-6})} = 138.45\Omega$

For gain specification, we need to change R_f

$$R_f = GR_2 = 10(138.45) = 1383.5 \Omega$$



Butterworth Filters

A unity gain Butterworth Filter Transfer function

$$|H(j\omega)| = \frac{1}{\sqrt{1 + (\frac{\omega}{\omega_c})^{2n}}}$$

N is integer and denotes the order of the filter

The cutoff frequency is ω_c for all values of n If n is large enough, the denominator is always close to unity when $\omega < \omega_c$

The exponent of ω/ω_c is always even

We can set ω_c equal to 1 rad/s in the transfer function, then we use scaling transform

Butterworth Filters

• We know that
$$\left|H(j\omega)\right|^2 = H(j\omega)H(-j\omega) \left|\left|H(j\omega)\right|^2\right|_{j\omega=s} = H(s)H(-s)$$

So we observe that $s^2 = -\omega^2$

Then

$$\overline{\left|H(j\omega)\right|^2 = \frac{1}{1 + (\omega)^{2n}} = \frac{1}{1 + (\omega^2)^n} = \frac{1}{1 + (-s^2)^n} = \frac{1}{1 + (-1^n)s^{2n}}$$

$$Hs)H(-s) = \frac{1}{1+(-1^n)s^{2n}}$$

Given value of a

- Find the roots of the polynomial $1+(-1^n)s^{2n}=0$
- Assign the left-half plane roots to H(s) and the right-half plane roots to H(-s)
- Combine terms in the denominator of H(s) to form first and second order factors.

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Butterworth Filters

Example

Find Butterworth filter transfer function for n=2 and n=3

For n=2
$$1+(-1^2)s^4=0$$
 $s^4=-1$ $s^4=1\angle 180^\circ$

Therefore the four roots

$$s_1 = 1 \angle 45^\circ = \frac{1}{\sqrt{2}} + \frac{j}{\sqrt{2}}$$
 $s_2 = 1 \angle 135^\circ = -\frac{1}{\sqrt{2}} + \frac{j}{\sqrt{2}}$

$$s_1 = 1 \angle 225^\circ = -\frac{1}{\sqrt{2}} - \frac{j}{\sqrt{2}}$$
 $s_1 = 1 \angle 315^\circ = \frac{1}{\sqrt{2}} - \frac{j}{\sqrt{2}}$

Roots s2 and s3 in the left-half plane

$$H(s) = \frac{1}{(s + \frac{1}{\sqrt{2}} - \frac{j}{\sqrt{2}})(s + \frac{1}{\sqrt{2}} + \frac{j}{\sqrt{2}})}$$

$$H(s) = \frac{1}{(s^2 + \sqrt{2}s + \frac{j}{\sqrt{2}})}$$
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For n=3
$$1+(-1^3)s^6=0$$
 $s^6=1$ $s^6=1\angle 360^\circ$

Therefore the four roots

$$s_1 = 1 \angle 0^\circ = 1$$
 $s_2 = 1 \angle 60^\circ = \frac{1}{2} + j\frac{\sqrt{3}}{2}$ $s_3 = 1 \angle 120^\circ = -\frac{1}{2} + j\frac{\sqrt{3}}{2}$

$$\boxed{s_4 = 1 \angle 180^\circ = -1} \quad \boxed{s_5 = 1 \angle 240^\circ = -\frac{1}{2} - j\frac{\sqrt{3}}{2}} \quad \boxed{s_6 = 1 \angle 300^\circ = \frac{1}{2} - j\frac{\sqrt{3}}{2}}$$

Roots s_3 , s_4 and s_5 in the left-half plane

$$Hs) = \frac{1}{(s+1)(s+\frac{1}{2}-j\frac{\sqrt{3}}{2})(s+\frac{1}{2}+j\frac{\sqrt{3}}{2})}$$

$$Hs$$
) = $\frac{1}{(s+1)(s^2+s+1)}$

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Butterworth Filters

Butterworth Polynomials (ω_c =1rad/s)

n	Nth order Butterworth polynomials
1	(s+1)
2	$(s^2 + \sqrt{2}s + 1)$
3	$(s+1)(s^2+s+1)$
4	$(s^2 + 0.765s + 1)(s^2 + 1.848s + 1)$
5	$(s+1)(s^2+0.618s+1)(s^2+1.618s+1)$
6	$(s^2 + 0.518s + 1)(s^2 + \sqrt{2}s + 1)(s^2 + 1.932s + 1)$

 A circuit can be scaled in both magnitude and frequency in simultaneously

$$R' = k_m R$$

$$C' = \frac{C}{k_m k_f}$$

Butterworth Filter Circuit

Fifth order Butterworth filter block diagram is shown in the following figure.

$$V_i$$
 $\frac{1}{s+1}$ $\frac{1}{s^2+0.618s+1}$ $\frac{1}{s^2+1.618s+1}$ V_i

Each block indicates the transfer function. Buterworth filter cutoff frequency is ω_c =1rad/s

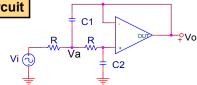
He have designed first order active filter in the previous classes. Now, we need to design second order active filter, which is

$$H(s) = \frac{1}{s^2 + bs + 1}$$

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Butterworth Filters

Butterworth Low-Pass Filter Circuit



Node equations

$$\frac{\overline{V_a - V_i}}{R} + (V_a - V_0)sC_1 + \frac{(V_a - V_0)}{R} = 0$$

$$2 + RC_1V_a - (1 + RC_1s)V_0 = V_i$$

$$V_0 s C_2 + \frac{(V_0 - V_a)}{R} = 0$$

$$-V_a + (1 + RC_2 s)V_0 = 0$$

$$V_0 = \frac{Vi}{R^2 C_1 C_2 s^2 + 2RC_2 s + 1}$$

$$V_0 s C_2 + \frac{(v_0 - v_a)}{R} = 0$$

$$V_0 = \frac{V_i}{R^2 C_1 C_2 s^2 + 2R C_2 s + 1}$$

$$H(s) = \frac{V_0}{V_i} = \frac{\frac{1}{R^2 C_1 C_2}}{s^2 + \frac{2}{R C_1} s + \frac{1}{R^2 C_1 C_2}}$$

Butterworth Filter Circuit

• Set R=1 Ω , then

$$H(s) = \frac{V_0}{Vi} \frac{\frac{1}{C_1 C_2}}{s^2 + \frac{2}{C_1} s + \frac{1}{C_1 C_2}}$$

· Second order circuit in Butterworth filter

$$H(s) = \frac{1}{s^2 + bs + 1}$$

$$b_1 = \frac{2}{C_1}$$

$$1 = \frac{1}{C_1 C_2}$$

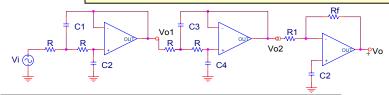
- Second order Butterworth filter with cutoff frequency of ω_c =1 rad/s and gain is 1.
- Use frequency scaling to calculate revised capacitor values for the wanted cutoff frequency
- Use magnitude scaling to provide more realistic component value

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Butterworth Filters

Example

 Design a fourth order Butterworth low-pass filter with a cutoff frequency 500Hz and passband gain of 10.



From the Butterworth polynomial table

$$(s^2 + 0.765s + 1)(s^2 + 1.848s + 1)$$

- Thus we need two cascade of two second order filters and inverting amplifier circuit for gain 10
- · First stage of cascade

$$0.765 = \frac{2}{C_1}$$

$$1 = \frac{1}{C_1 C_2}$$

$$C_1 = 2.61 F$$

 $C_2 = 0.38 F$

Example

Second stage of cascade

$$(s^2 + 1.848s + 1)$$

$$1.848 = \frac{2}{C_3}$$

$$1 = \frac{1}{C_3 C_4}$$

$$C_3 = 1.08 F$$

Frequency scaling factor f_c=500 Hz

$$k_f = \frac{\omega_c}{1 \text{rad/s}} = 2\pi 500 = 3141.6$$

To have $R=1K\Omega$, magnitude scaling factor

$$k_m = 1000$$

$$R' = k_m R = 1 K\Omega$$

$$R' = k_m R = 1 K\Omega$$
 $C' = \frac{C}{k_m k_f}$ $C_1 = 831 nF$ $C_3 = 344 nF$ $C_4 = 294 nF$

$$C_1 = 831 \, nF$$

$$C_3 = 344 \ nF$$

$$C_2 = 121 \, nF$$

$$C_4 = 294 \, nR$$

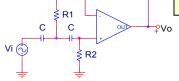
For inverting amplifier stage, let R_i =1K Ω

$$R_f = 10R_i = 10 K\Omega$$

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Butterworth Filters

Butterworth High-Pass Filter



Second order High-pass filter form

$$H(s) = \frac{s^2}{s^2 + b_1 s + 1}$$

The transfer function of the circuit

$$H(s) = \frac{V_0}{Vi} = \frac{s^2}{s^2 + \frac{2}{R_2C}s + \frac{1}{R_1R_2C^2}}$$

$$H(s) = \frac{V_0}{Vi} = \frac{s^2}{s^2 + \frac{2}{R_2}s + \frac{1}{R_1R_2}}$$

$$H(s) = \frac{V_0}{Vi} = \frac{s^2}{s^2 + \frac{2}{R_2}s + \frac{1}{R_1R_2}}$$

$$b_1 = \frac{2}{R_2}$$

$$b_1 = \frac{2}{R_2}$$

$$1 = \frac{1}{R_1 R_2}$$
Example : Second order Butterworth filter
$$R_2 = \frac{2}{\sqrt{2}} = 1.41 \Omega$$

$$R_1 = \frac{1}{R_2} = 0.707 \Omega$$

$$R_1 = \frac{1}{R_2} = 0.707 \Omega$$

Example

Second order Butterworth High-pass filter with cutoff frequency 1KHz gain 10. Use 0.1uF capacitor

From the Butterworth polynomial table

$$(s^2 + \sqrt{2}s + 1)$$

We need a second order filters and an inverting amplifier circuit for gain 10

$$b_1 = \frac{2}{R_2}$$

$$1 = \frac{1}{R_1 R_2}$$

$$R_2 = \frac{2}{\sqrt{2}} = 1.41 \Omega$$

$$R_1 = \frac{1}{R_2} = 0.707 \,\Omega$$

$$b_1 = \frac{2}{R_2} \qquad 1 = \frac{1}{R_1 R_2} \qquad R_2 = \frac{2}{\sqrt{2}} = 1.41 \Omega \qquad R_1 = \frac{1}{R_2} = 0.707 \Omega$$
Frequency scaling factor $f_c = 1000 \text{ Hz}$

$$k_f = \frac{\omega_c}{1 \text{rad/s}} = 2\pi 1000 = 6283.2$$

To have C=0.1uF, magnitude scaling factor

$$k_m = \frac{C}{C'k_f} = \frac{1}{0.1(10^{-6})6283.2} = 1591.5$$
 $R_{1n} = k_m R_1 = 1591.5 (0.707) = 1125 \Omega$

$$R_{1n} = k_m R_1 = 1591.5 (0.707) = 1125 \Omega$$

$$R_{2n} = k_m R_2 = 1591.5 (1.41) = 2244 \Omega$$

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Butterworth Filters

Example (Cont):

For inverting amplifier stage, let R_i =1K Ω

$$R_f = 10R_j = 10 K\Omega$$

Finally, we have

$$H(s) = \frac{V_0}{V_i} = \frac{s^2}{s^2 + \frac{2}{R_2 C} s + \frac{1}{R_1 R_2 C^2}} (-\frac{R_f}{R_i})$$

$$R_1 = 1125 \Omega$$

$$R_2 = 2244 \Omega$$

$$R_f = 10 \text{ K}\Omega$$

$$C = 0.1 \mu F$$

$$R_1 = 1125 \Omega$$

$$R_i = 1 \text{ K}\Omega$$

$$R_2 = 2244 \Omega$$

$$R_f = 10 \text{ Kg}$$

$$C = 0.1 \ \mu F$$

