# EPC9149: 36 - 60 V Input, 9 - 15 V Output, 83 A Output Fixed Conversion Ratio 1 kW LLC, $^1/_8$th Brick size Module Quick Start Guide

*EPC2218 and EPC2024*

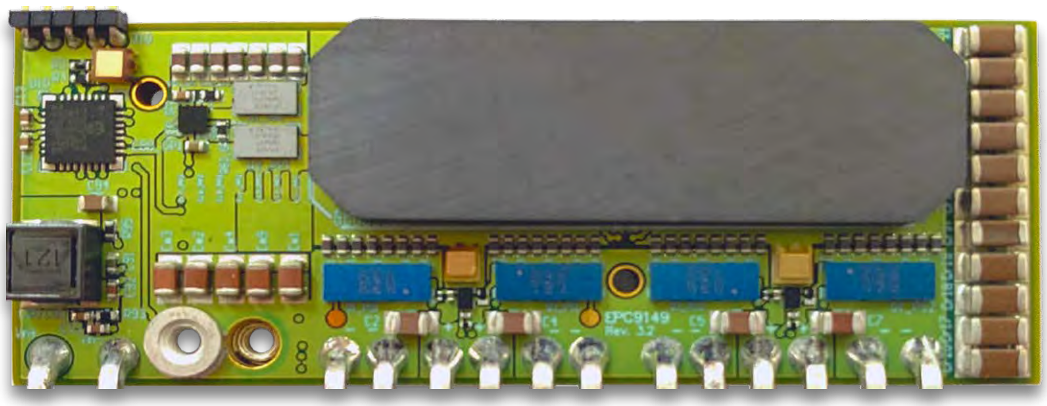
Revision 3.2

EFFICIENT POWER CONVERSION

## DESCRIPTION

The EPC9149 demonstration board is a 1 kW, 48 V input to 12 V output LLC converter that operates as a DC transformer with fixed conversion ratio of 4:1. The simplified schematic diagram is shown in Figure 1. It features the 100 V rated **EPC2218** and 40 V rated **EPC2024** GaN FETs, the uP1966A and LMG1020 gate drivers as well as the Microchip dsPIC33CK32MP102 16-bit digital controller. Other features include:

- Peak efficiency: 97.5 % at 400 W
- Full-load efficiency: 96.7% @ 12 V delivering 83.3 A output
- 22.9 × 58.4 mm (0.90 × 2.30 inches)
- Low profile: 10 mm total converter thickness without heatsink
- Temperature rise: 70 °C @ 12 V with 83.3 A output (with heatsink kit installed
- Fixed switching frequency: 1 MHz
- Soft startup into full resistive load
- High power density: 1227 W/in$^3$ (excluding pins)



*EPC9149 board*

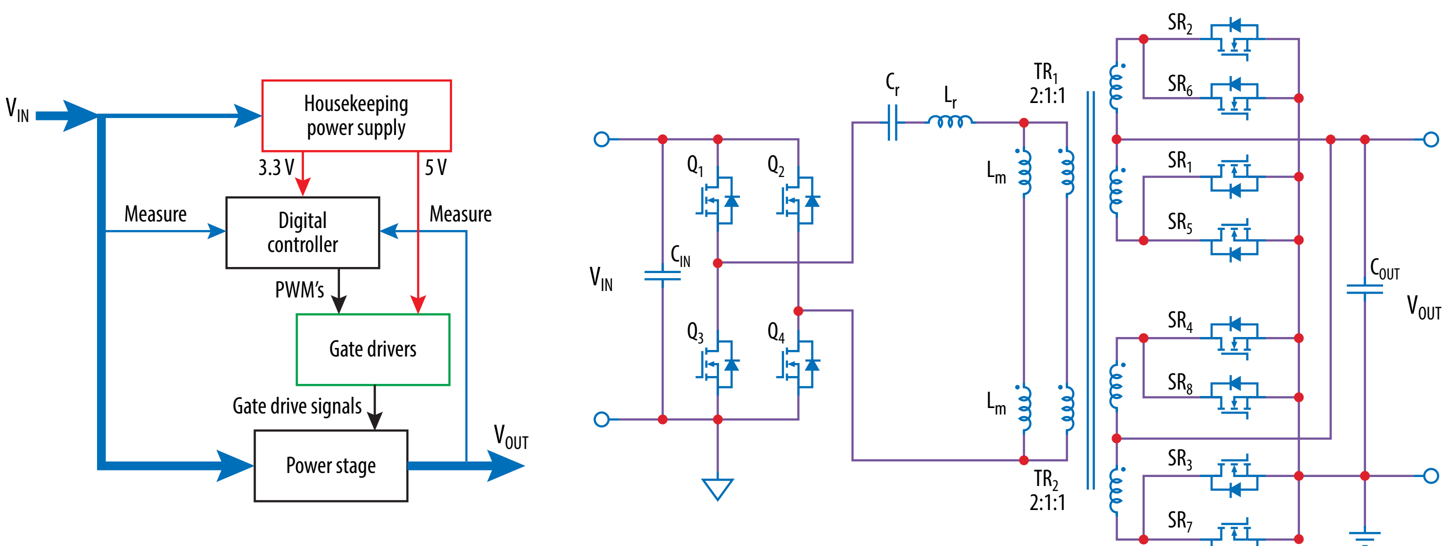



*Figure 1: Simplified schematic diagram of the EPC9149 LLC Module*

## REGULATORY INFORMATION

This converter is intended for evaluation purposes only. It is not a full-featured converter and cannot be used in final products. No EMI test was conducted. It is not FCC approved.

## FIRMWARE UPDATES

Every effort has been made to ensure all control features function as specified. It may be necessary to provide updates to the firmware. Please check the EPC website for the latest firmware updates.

**Table 1: Electrical Characteristics (Ta = 25 °C unless specified otherwise)**

| Symbol | Parameter | Conditions | Min | Typ | Max | Units |
|---|---|---|---|---|---|---|
| $V_{IN}$ | Input Voltage | | 36 | 48 | 60 | V |
| $V_{OUT}$ | Output Voltage | Fixed ratio of 4:1 based on $V_{IN}$ | | 12 | | |
| $I_{OUT}$ | Output Current | Continuous* | 0 | | 83.3 | A |
| $f_S$ | Switching Frequency | | | 1 | | MHz |
| $T_{rise}$ | Temperature Rise | $V_{IN}$ = 48 V, $I_{OUT}$ = 83.3 A, thermal system installed, 400 LFM forced air, measured at heat-spreader | | 70 | | °C |
| $V_{IN,on}$ | Input UVLO turn on voltage | | | 7.5 | | V |
| $V_{IN,off}$ | Input UVLO turn off voltage | | | 5.5 | | |
| $t_{OUT,rise}$ | Output voltage rise time | | | 3 | | ms |

** Without heatsink kit installed requires at least 1700 LFM airflow, with heatsink kit installed required 400 LFM cooling.*

# HIGHLIGHTED PARTS

This converter is intended for evaluation purposes only. It is not a full-featured converter and cannot be used in final products. No EMI test was conducted. It is not FCC approved.

## Power Stage

The EPC9149 features a primary side full bridge and a dual secondary side center tapped half bridge configuration based on EPC2218 and EPC2024 eGaN fets. Available from EPC's website (**epc-co.com**) are **EPC2218's datasheet** and **EPC2024's datasheet**.

## Onboard power supply

The EPC9149 board includes logic and gate driver house-keeping power supplies that are powered from the main input supply voltage to the LLC board.

## Input and output voltage sense

Input and output voltages are measured by resistor dividers and fed back to the microcontroller to be used for control purposes.

## Transformer core

This module uses a customized transformer core with ML91S material from Hitachi metals (part number: U-36-4.57-12.2) which offers low core loss at high frequency operation. The drawing and dimensions of this core is shown in Figure 12. Two half core sections are inserted from top and bottom side of the board as shown in Figure 2 below. Proper spacers are also added in between to achieve the required magnetizing inductance.

# MECHANICAL SPECIFICATIONS

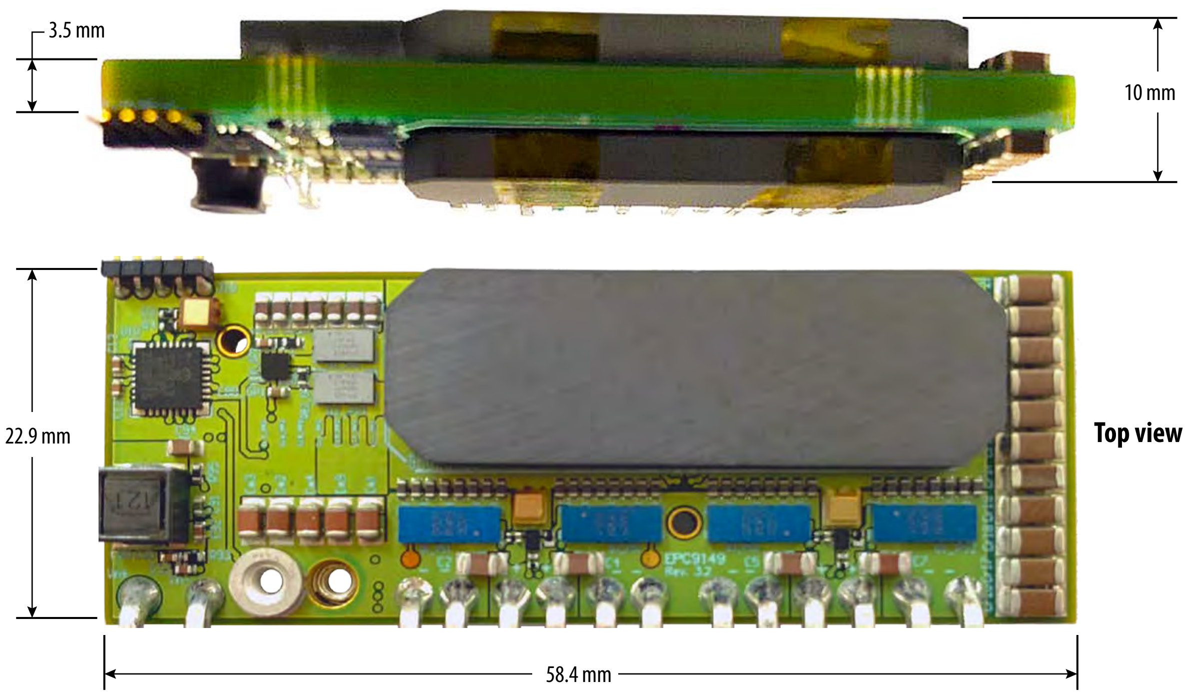


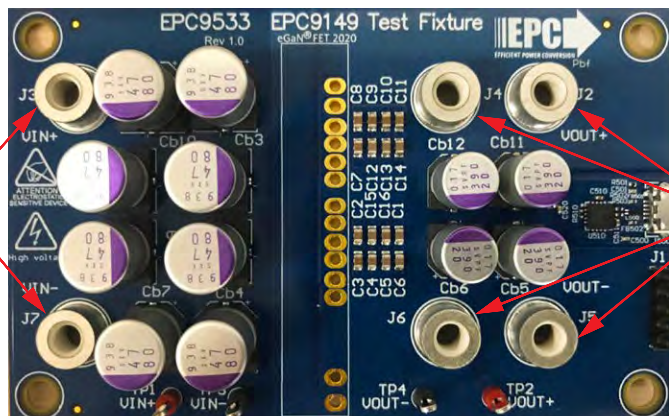

*Figure 2: EPC9149 mechanical dimensions*

## QUICK START PROCEDURE

The EPC9149 LLC converter module is easy to set up for evaluation. Refer to Figures 3-4 and follow the procedure below for proper connection and measurement setup:

1. EPC9533 is the motherboard for EPC9149 where the main input and output power connections are located.
2. Attach the standoffs for EPC9533.
3. With power off, connect the input power supply to $V_{IN+}$ and $V_{IN-}$ as shown in Figure 3.
4. With power off, connect the load to $V_{OUT+}$ and $V_{OUT-}$ as shown in Figure 3.
5. Connect the input and output kelvin connections shown in Figure 3 to the respective measurement instruments.
6. Apply the input voltage and once operational, adjust the load within the operating range and observe the efficiency, temperature and other characteristics.
7. For shutdown, please follow the above steps in reverse. (**The input supply can be turned off as well**)

In order to measure the input and output currents, proper shunts can be connected in series with the corresponding connections. (input supply and load, respectively)




*Top view*

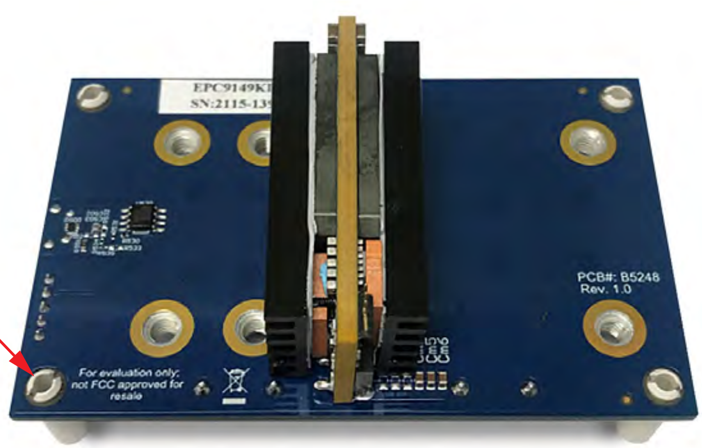



*Figure 3: EPC9149 and motherboard assembly showing the input and output connections*

## ELECTRICAL and THERMAL PERFORMANCE

The module provides maximum efficiency of 97.5% and full load efficiency of 96.7%.

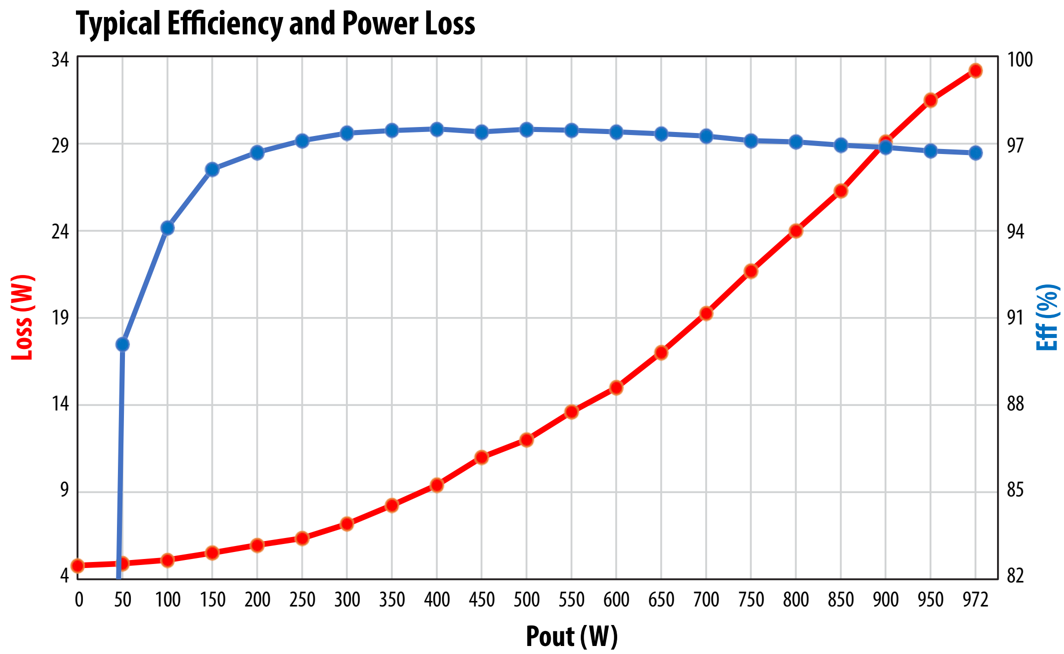



*Figure 4: Total system efficiency and loss @ 12 V output, 48 V input voltage, 400 LFM forced air cooling with heatsink kit installed*

## SOFT START-UP

The EPC9149 controller includes a startup routine that limits the input current drawn when powering up and the output voltage is low or zero. Once the input voltage passes the UVLO of the bias supply IC, the output voltage rises monotonously from 0 to its final value without overshoot in less than 3 ms see figure 5.

The start up waveform is measured while the scope is triggered on the output voltage rise and the module is turned on into the constant resistive load of 144 mΩ that results in 1 kW load at 12 V output voltage. Both primary and secondary FETs are commanded with a minimum pulse width and the duty cycle is slowly ramped up as the output voltage increases to avoid excessive current and voltage stresses during startup.

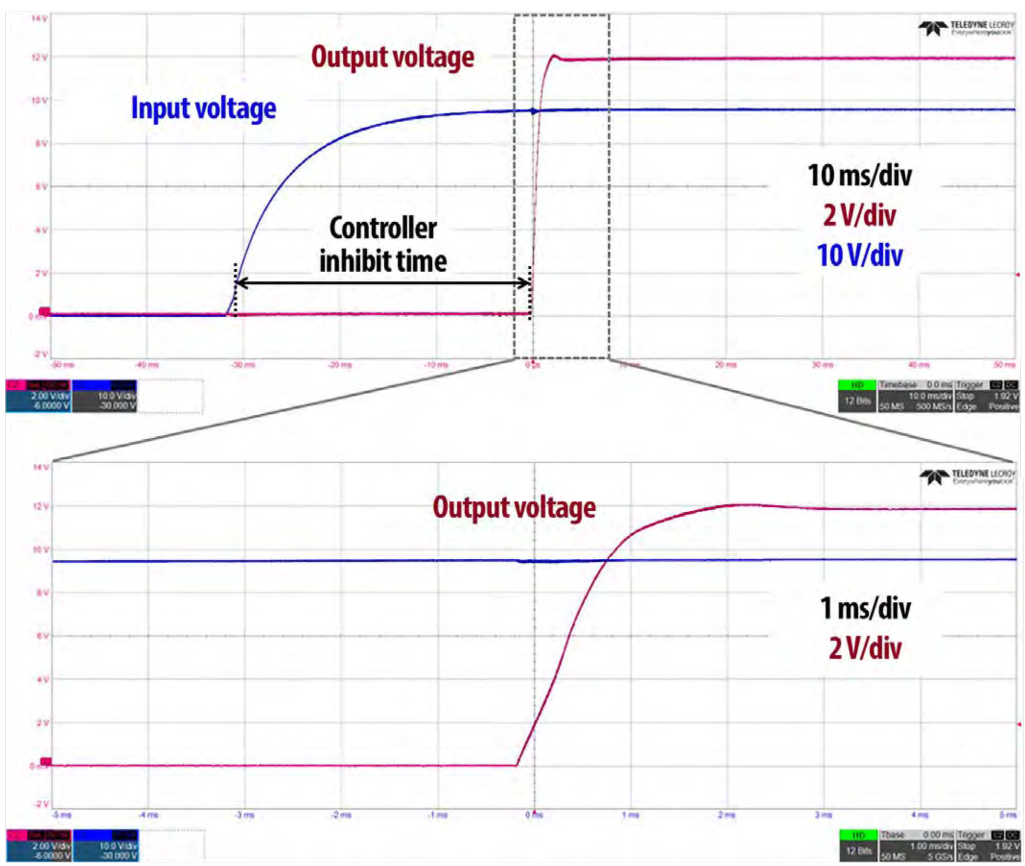



*Figure 5: Startup waveform (larger time scale on top and zoomed in version on the bottom)*

## Output voltage droop

This converter operates in an open loop meaning that output voltage is not regulated at various line and load conditions. Therefore, output voltage droops when higher loads are applied to the module. Figure 6 shows the output voltage droop as function of load current at nominal 48 V input voltage. In DC transformer applications, the lowest possible deviation of the voltage conversion ratio between the input and output across the entire load is desired.

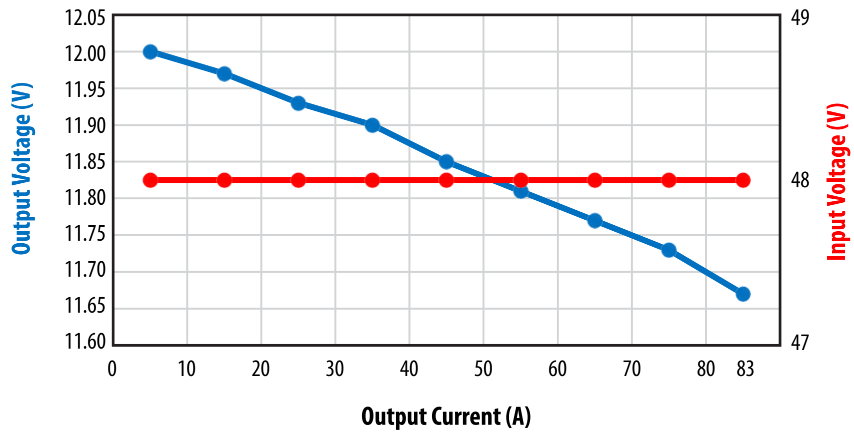
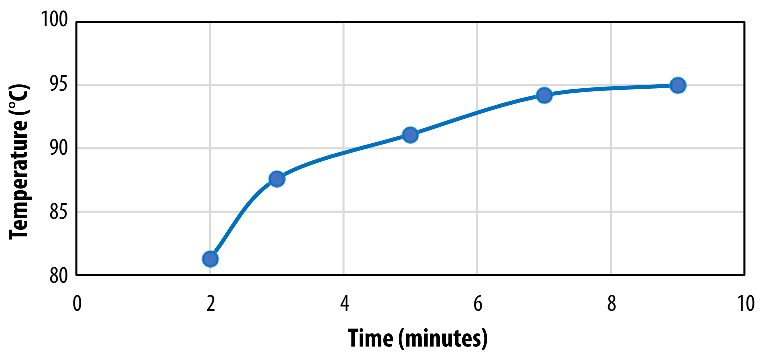



*Figure 6: Output voltage droop vs. output current*

## Thermal performance

The measured thermal performance of the EPC9149 is shown in Figure 7, with the heatsink kit installed. The temperature rise for the hottest portion of the board is 70 °C when operating at full load with 400 LFM forced air cooling.



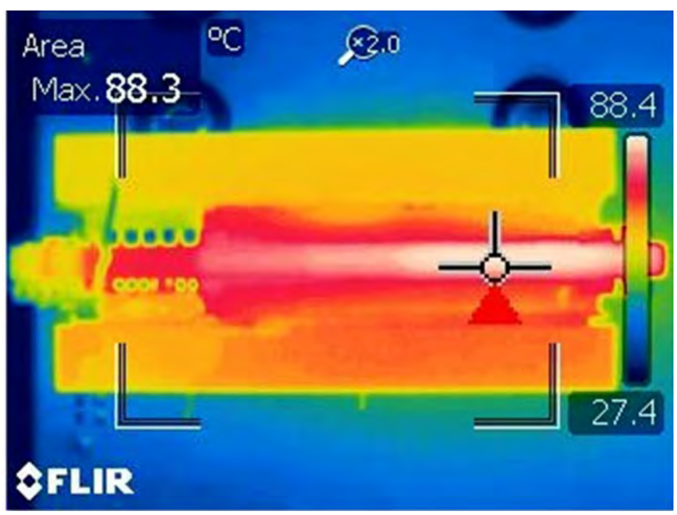




*Figure 7: Thermal image of the EPC9149 operating at 48 $V_{IN}$, 12 V and 83.3 A output, thermal steady state reached after 10 minutes, Top: primary FET junction temperature and Bottom: highest board temperature.*

## THERMAL DERATING

Without sufficient thermal management, the output current capability is reduced. If the user decides to uninstall the heatsink, the module temperature should be monitored to ensure the maximum temperature does not exceed the rating.

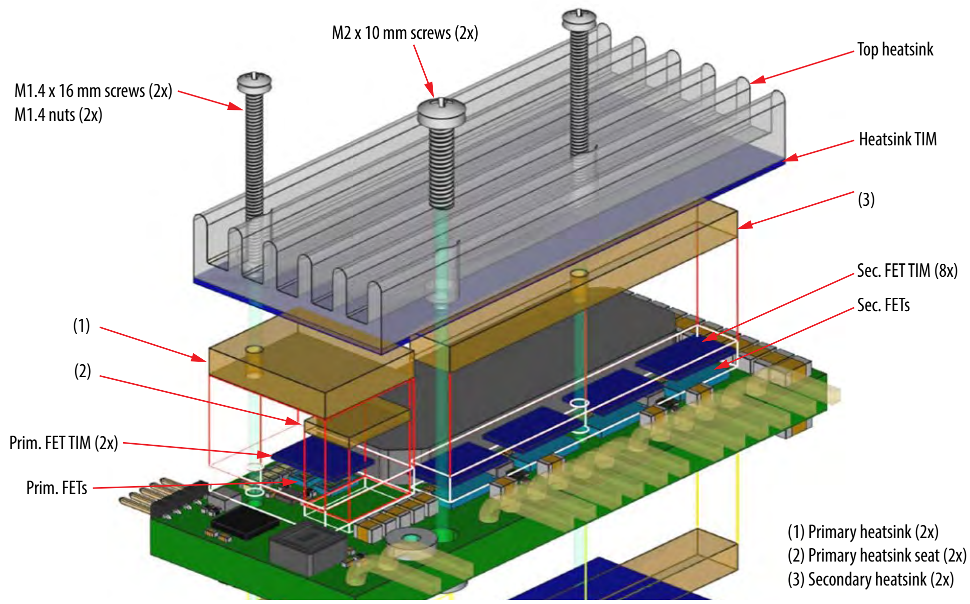
## THERMAL MANAGEMENT

Thermal management is very important to ensure proper and reliable operation. The EPC9149 is intended for bench evaluation at normal ambient temperature. The addition of a heat-spreader or heatsink and forced air cooling can significantly increase the current rating of the power devices, but care must be taken to not exceed the absolute maximum die temperature of 150°C.

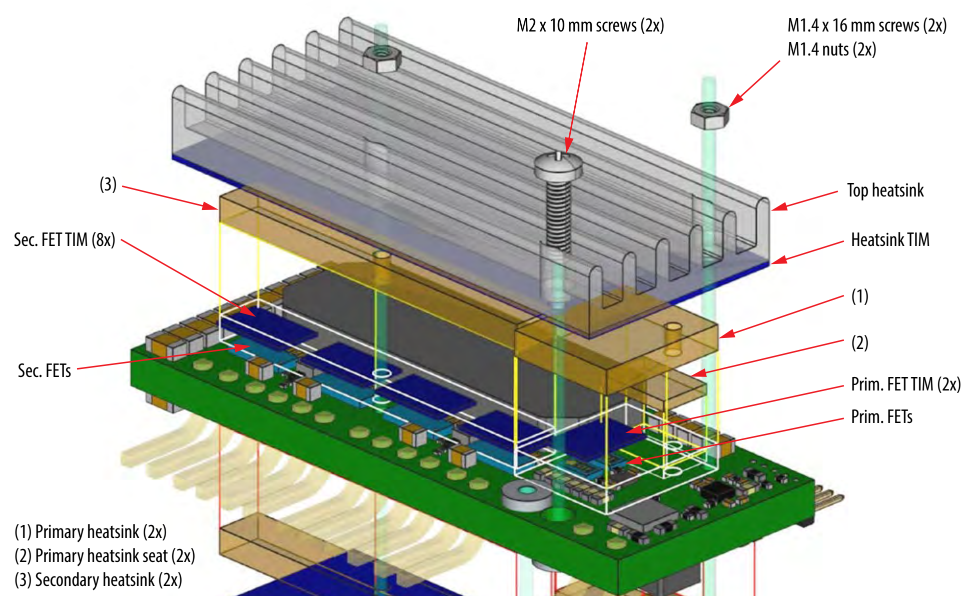
A combination of custom shape heat spreaders and a finned heatsink for the top and bottom side of the EPC9149 board are designed. The thermal solution assembly is shown in Figure 8. Copper heat spreaders (item 1 and 3) are placed on top of both primary and secondary side FETs to spread their heat to the outer structure. Two 1 mm height copper shims (item 2) are used to fill the gaps and help with cooling the board surface. It only requires a gap filler TIM to be added underneath of the heat spreader pieces to provide insulation and high thermal conductivity between the components and the metal surface of heat spreaders. Several mechanical shims help mounting the heat spreader on the PCB surface and maintaining required clearance between the heat spreader and component surfaces. Mechanical screws are inserted on the board to hold the entire mechanical structure together.

A step-by-step assembly guideline are presented.
The needed parts are listed below.

- 2x heatsinks for top and bottom side (not identical)
- 2x Copper (Cu) heat spreaders for primary FETs (item #1)
- 2x Cu spacers/seats for primary FETs (item #2)
- 2x Cu heat spreaders for secondary FETs (item #3)
- 2x M1.4 16mm screws
- 2x M1.4 nuts
- 2x M2 10mm screws
- TIM pads TG-A1780 0.5 mm
- TIM pads TG-A6300 0.5 mm
- TIM gap filler Bergquist GF4000




*Top side*

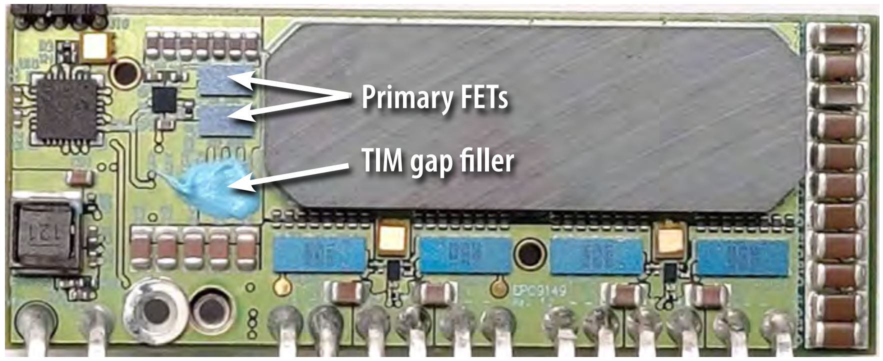



*Bottom side*

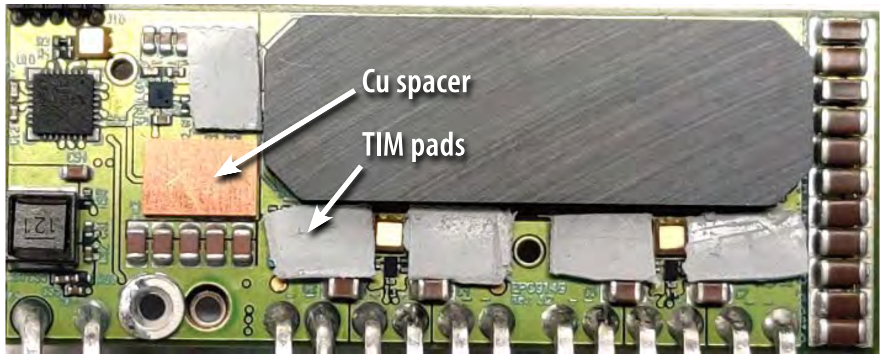
*Figure 8: Thermal solution assembly process for the EPC9149 module*

## THERMAL SOLUTION ASSEMBLY GUIDELINES

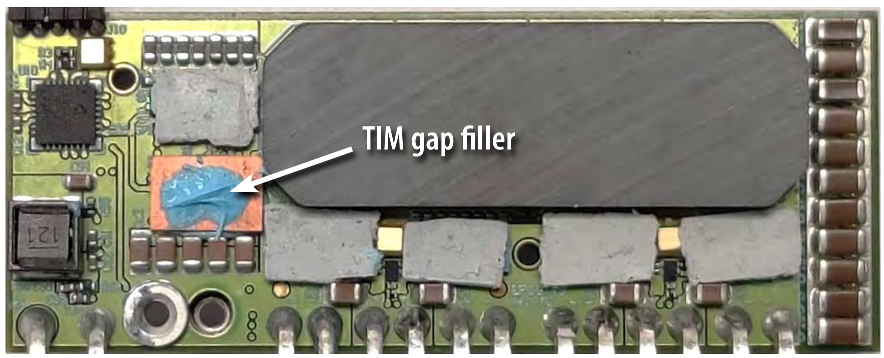
1. Add TIM gap filler (Bergquist GF4000) next to Primary FETs



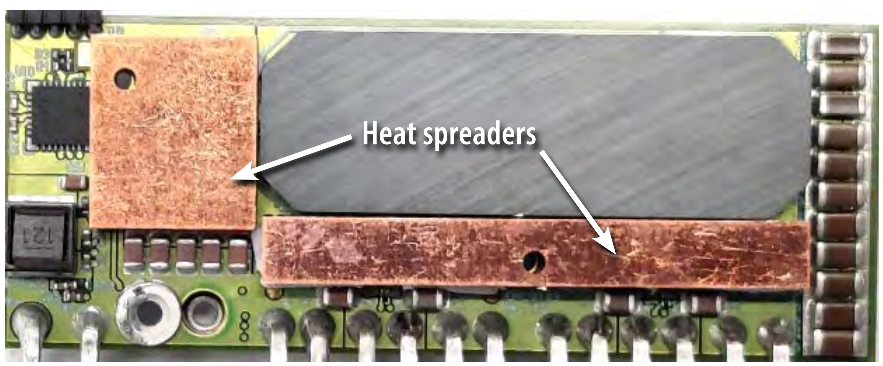

2. Place **Cu spacer** next to primary FETs on TIM gap filler, and place **TIM pads** (TG-A1780) on primary and secondary FETs




3. Add TIM gap filler (Bergquist GF4000) to **Cu spacer**

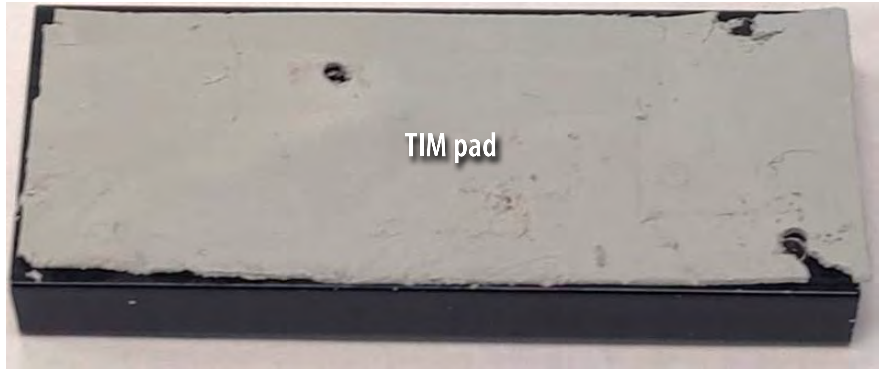



4. Place **heat spreaders** on primary and secondary FETs, holes must align

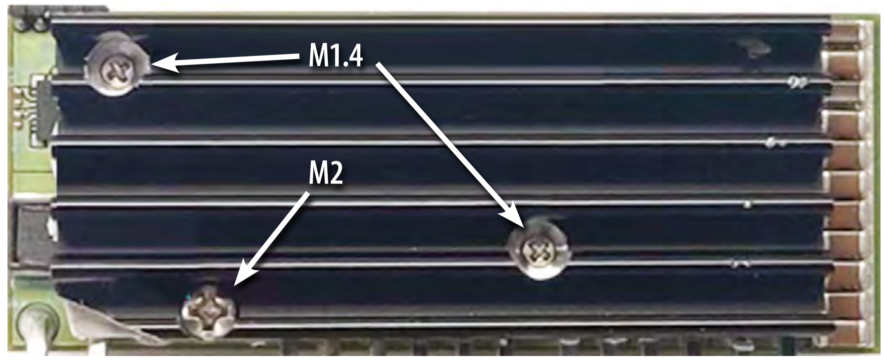



5. Place **TIM pad** (TG-A6200) on inductor core

6. Place **TIM pad** (TG-A6200) on heatsink backside (flat) and align it to screw holes

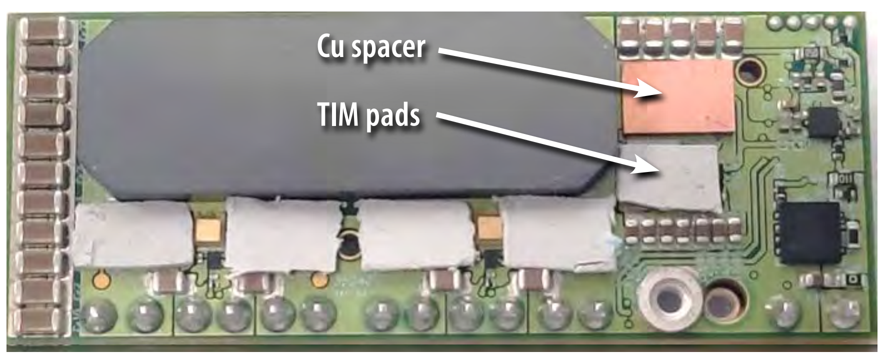



7. Use **M1.4 and M2 screws** for assembly as shown in schematic; M2 can be connected to threaded flange on PCB, do not fully tighten yet



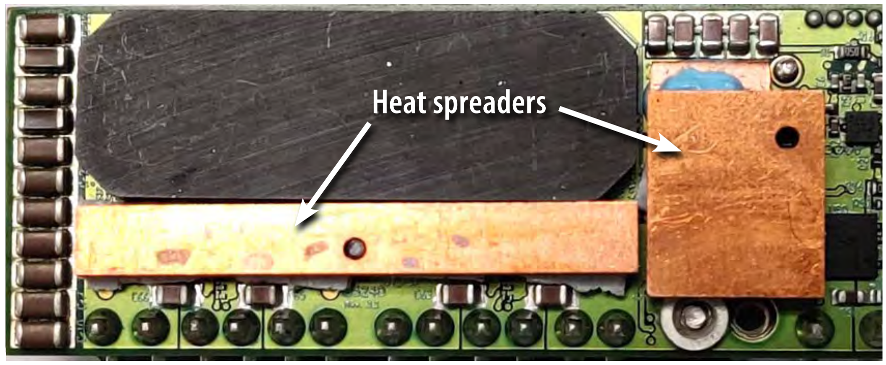

8. Add TIM gap filler (Bergquist GF4000) next to Primary FETs


9. Place Cu spacer next to primary FETs; Place TIM pad (TG-A1780) cutouts to cover primary and secondary FETs



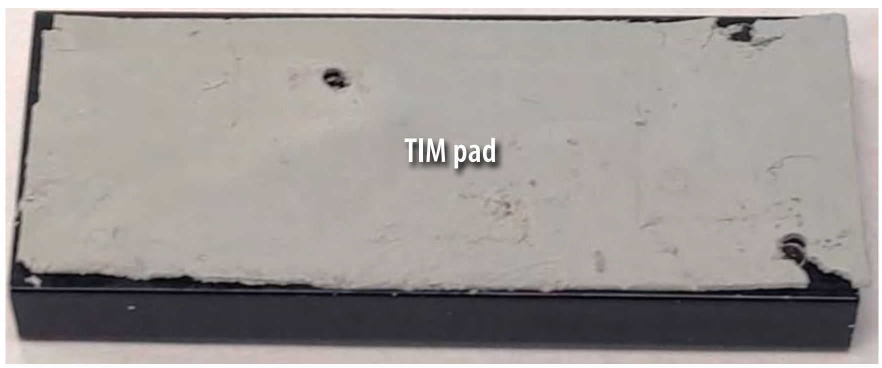

10. Add TIM gap filler (Bergquist GF4000) on Cu spacer

11. Place heat spreaders on primary and secondary FETs, hole near secondary FETs must align

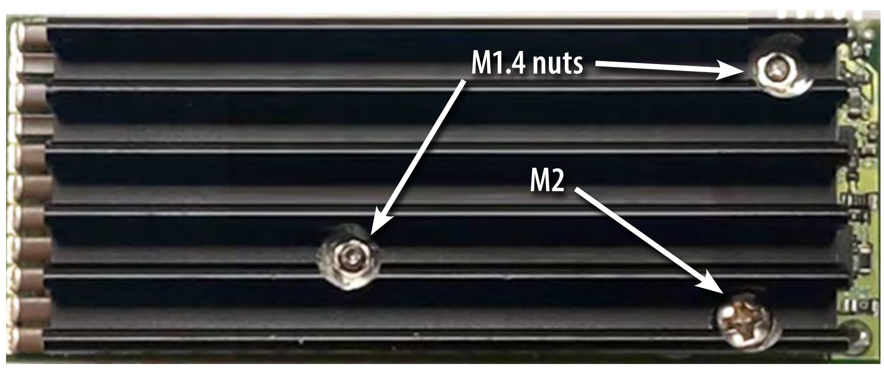



12. Place TIM pad (TG-A6200) on inductor core

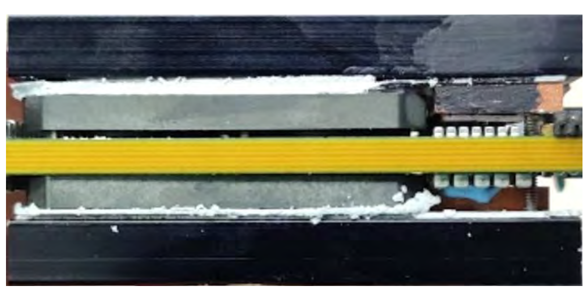

13. Place TIM (TG-A6200) on backside of heatsink and align it to screw holes

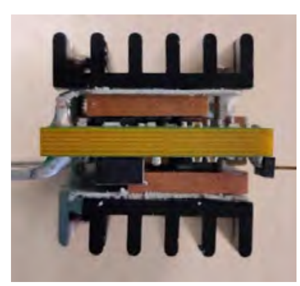



14. Use M1.4 nuts and M2 screws for assembly as shown in schematic; M2 can be connected to threaded flange on PCB




15. Tighten screws in sequence while keeping heatsink parallel to PCB (left: side view and right: end view)





The choice of TIM needs to consider the following characteristics:

- **Mechanical compliance** – The TIM becomes compressed during heatsink attachment and exerts a force on the FETs. A maximum compression of 2:1 is recommended for maximum thermal performance and to constrain the mechanical force that maximizes thermal mechanical reliability.
- **Electrical insulation** – The backside of the eGaN FETs are substrate that are connected to source and the upper FET will thus be connected to the switch-node. The TIM must therefore provide insulation to prevent short-circuiting the upper FET to the ground.
- **Thermal performance** – The choice of thermal material will affect the thermal performance. Higher thermal conductivity materials will result in higher thermal performance.

EPC recommends T-Global: A1780- 500 µm for the thermal interface material between FETs and heat spreaders and T-Global: A6200 for heatsinks. The gap filler TIM recommended is Bergquist GF4000.

## CONTROLLER

The EPC9149 LLC power module features a Microchip dsPIC33CK32MP102 Digital Signal Controller DSC. This 100 MHz single core device is equipped with dedicated peripheral modules for Switched-Mode Power Supply (SMPS) applications, such as a feature-rich 4-channel (8x output), 250 ps resolution pulse width modulation (PWM) logic, three 3.5 Msps Analog-To-Digital Converters (ADC), three 15 ns propagation delay analog comparators with integrated Digital-To-Analog Converters (DAC) supporting ramp signal generation, three operational amplifiers as well as Digital Signal Processing (DSP) core with tightly coupled data paths for high performance real-time control applications. The device used is the smallest derivative of the dsPIC33CK single core and dsPIC33CH dual core DSC families. The device used in this design comes in a 28 pin 4x4 mm UQFN package, specified for ambient temperatures from -40 to +125° C.

The dsPIC33CK device is used to drive the converter in a fully digital fashion. Input voltage and output voltage measurements are fed back to the dsPIC and read using two independent core ADCs.

## PROGRAMMING

The Microchip dsPIC33CK controller can be re-programmed using the MPLAB ICD4 or other Microchip programmer tools and through the 5-pin header on EPC9149 board shown below. RJ11 to ICSP adapter 02-10310-R1 from microchip is used to interface programmer and the main board (Fig. 11(b)). (Please refer to **www.microchip.com** for available options)

EPC9997 board is designed to be specifically used as an ICSP adapter as shown in Fig. 9(a) as well.

**Please make sure the programming is performed only when the module is not running and no input voltage is applied.**

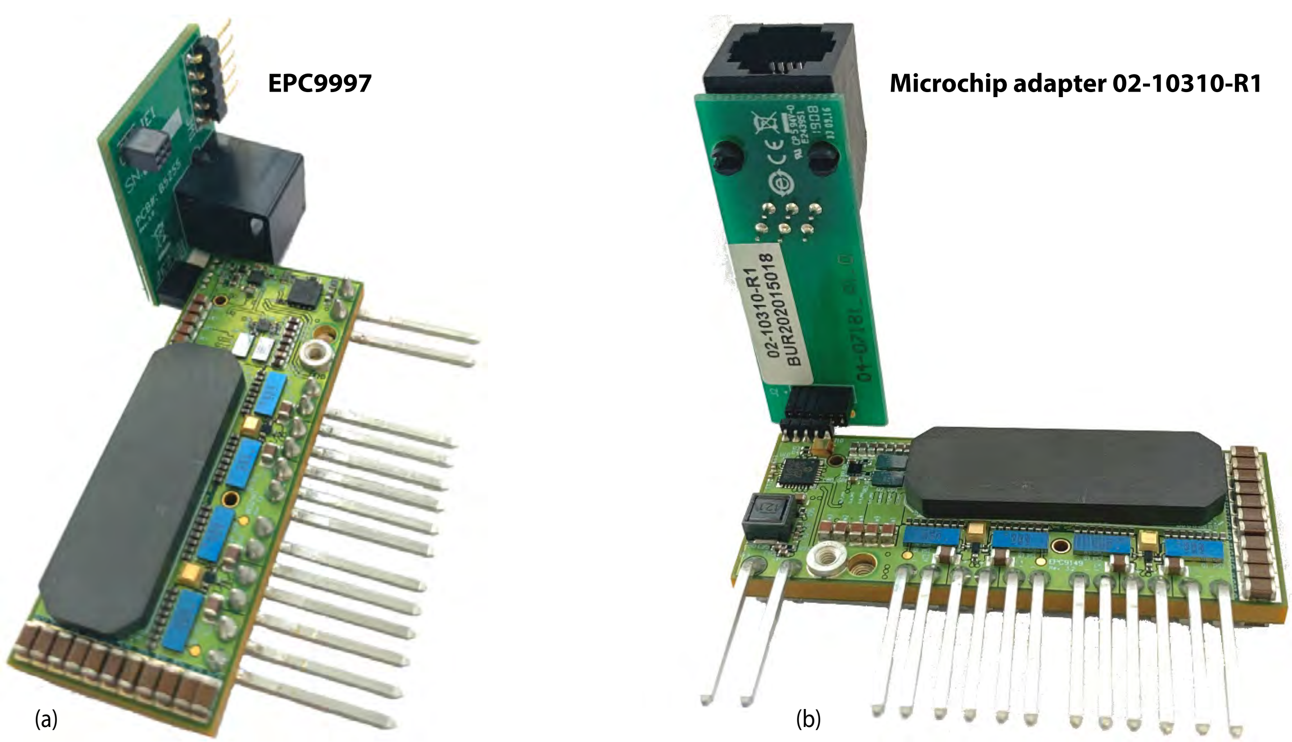


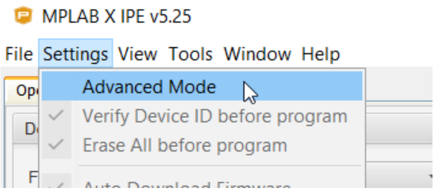

*Figure 9: Programming connection options*

## Programming with HEX file

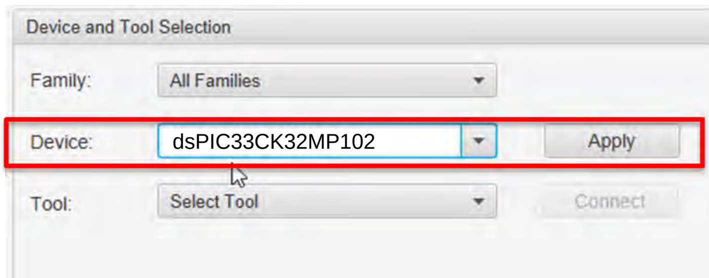
Download the latest MPLAB® X IPE from Microchip website and follow the five steps below:

https://www.microchip.com/mplab/mplab-integrated-programming-environment

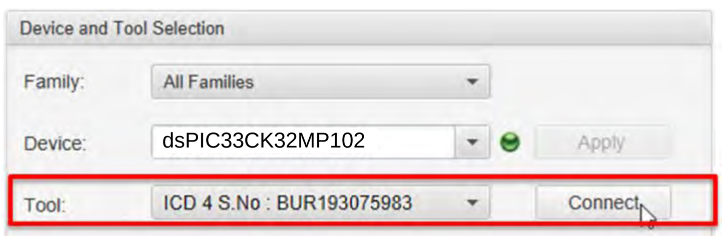
1. **Enable Advanced Mode:**



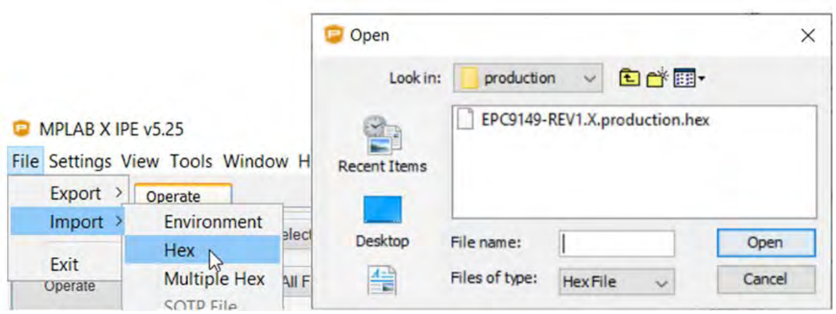

2. **Select Device: dsPIC33CK32MP102 and then apply:**



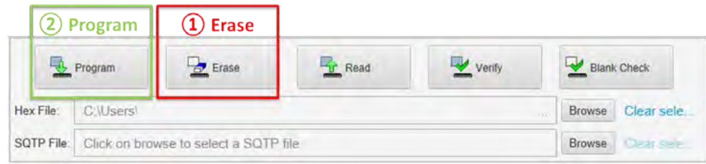

3. **Select programming tool and then connect:**



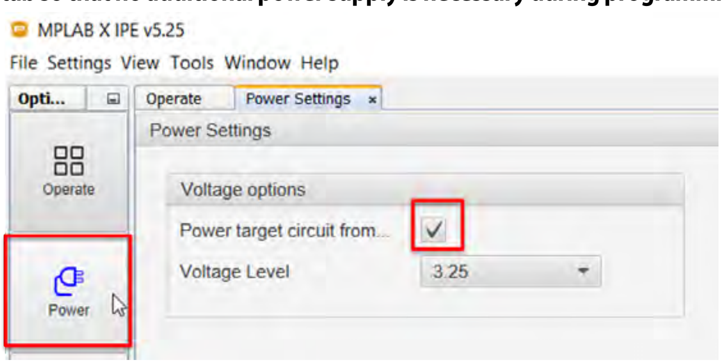

4. **Click 'Browse' to select the provided .hex file:**



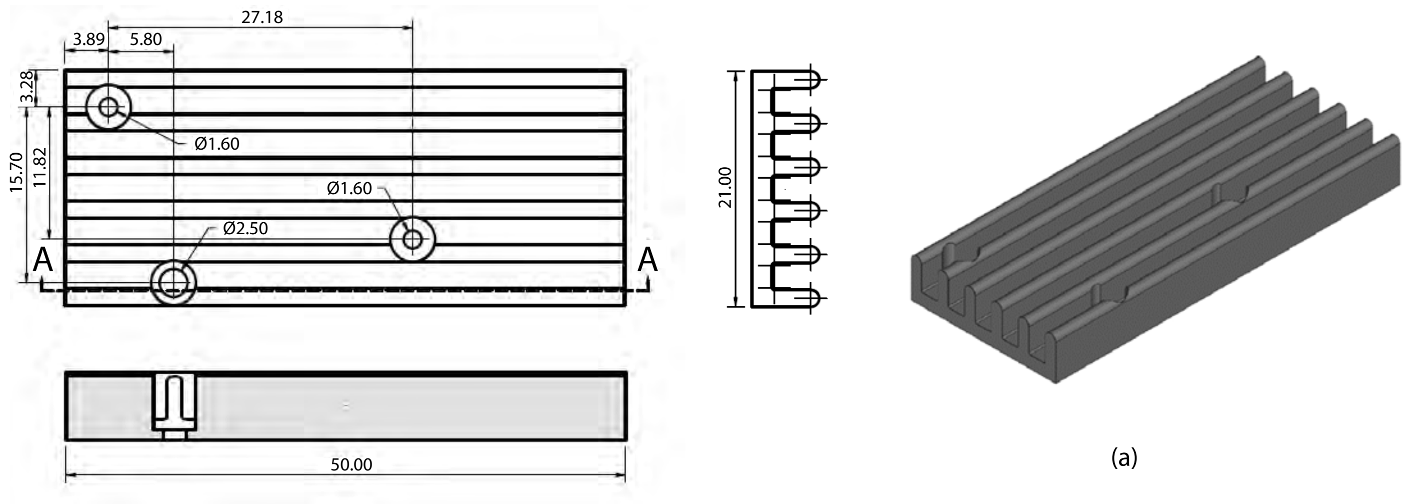

5. **Erase device, and then program device:**



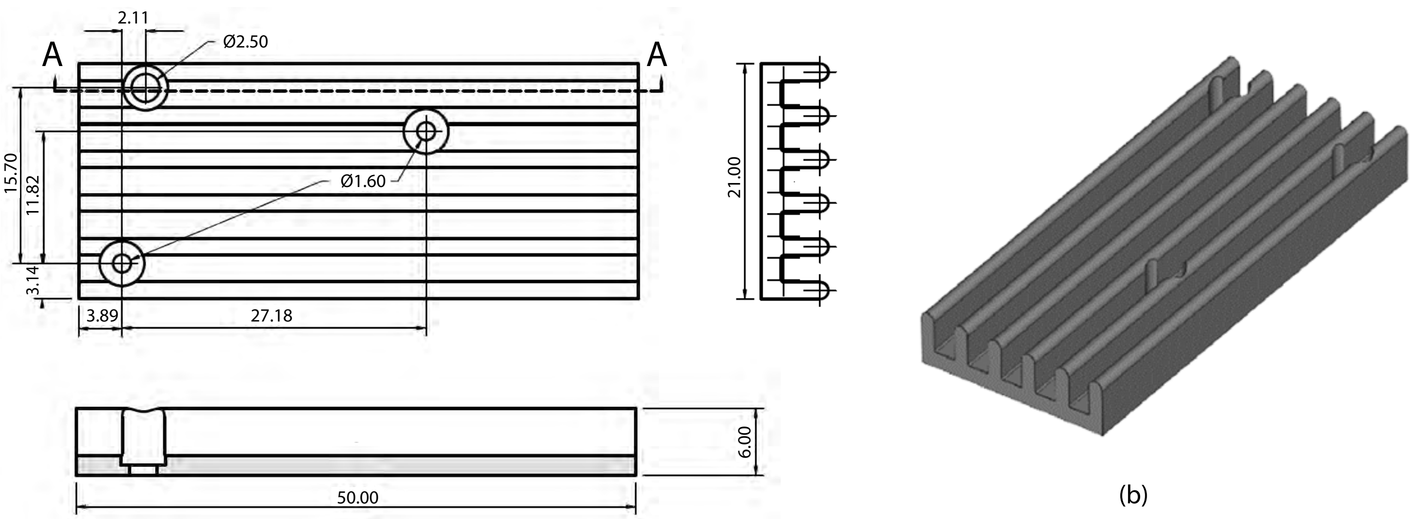

**Optional: Enable 'Power target circuit from programming tool' from left panel 'Power' tab so that no additional power supply is necessary during programming:**



## THERMAL MECHANICAL DRAWINGS




(a)




(b)

*Figure 10: (a) Top side heatsink drawing, (b) Bottom side heatsink*

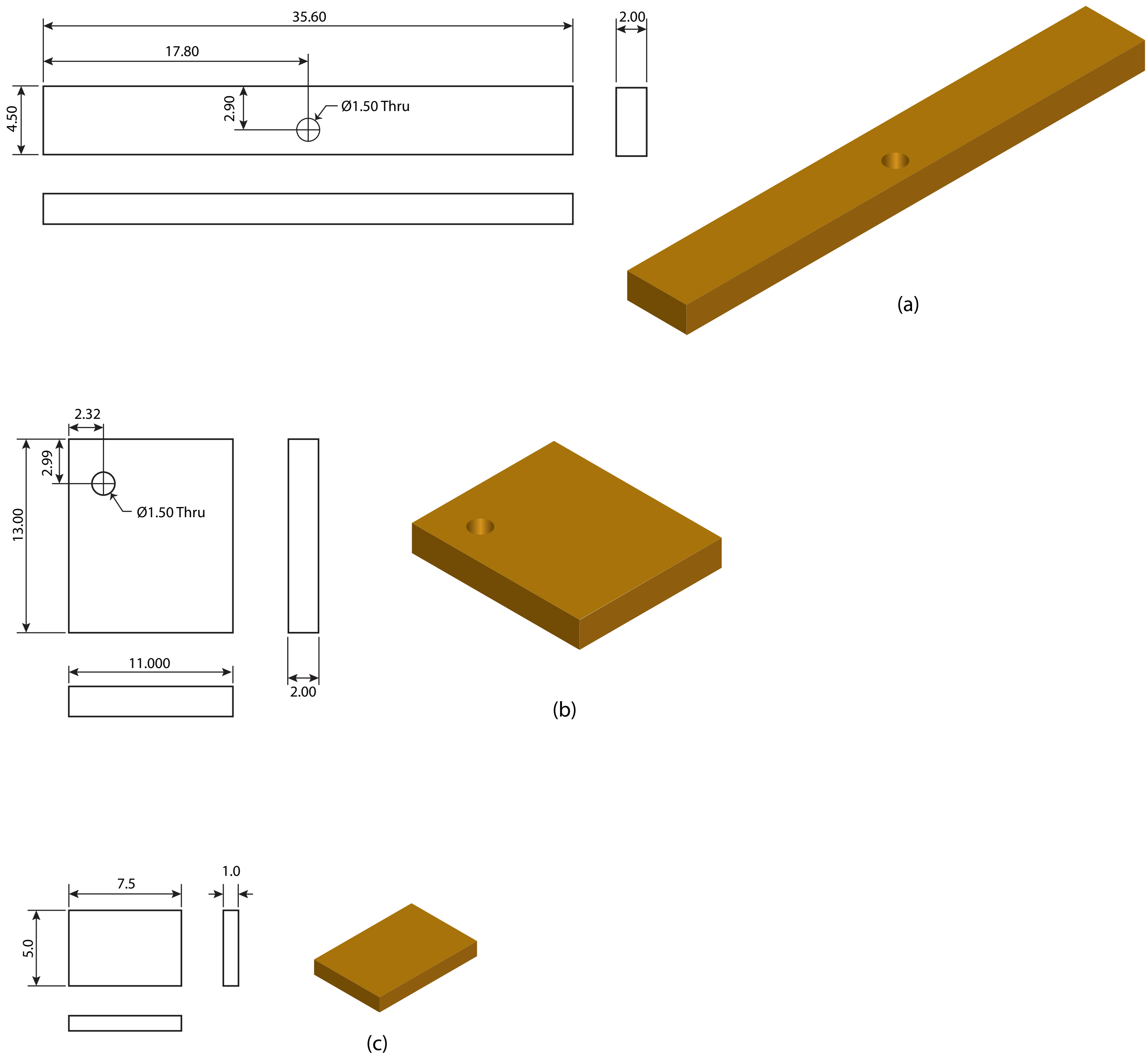
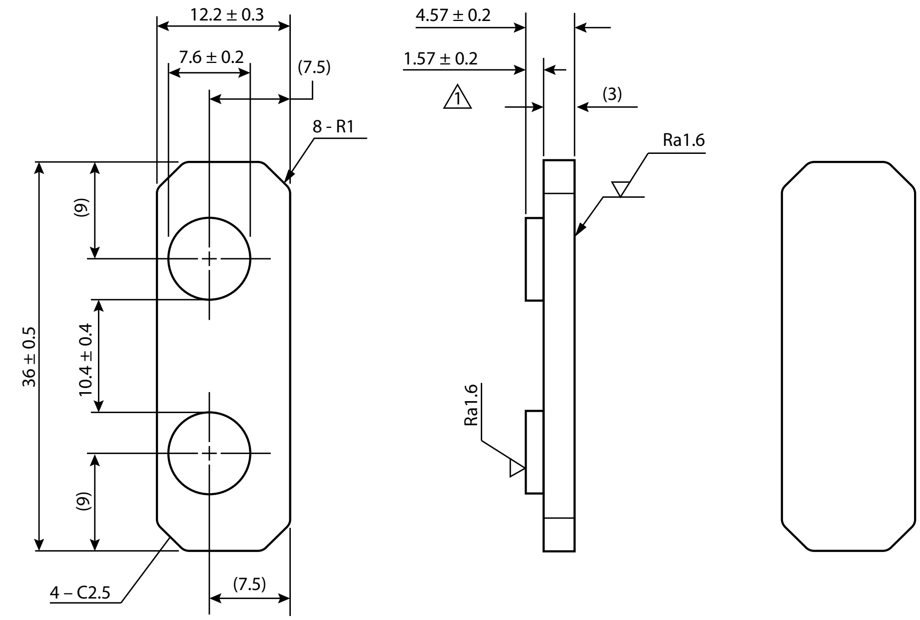



*Figure 11: (a) Secondary FET copper heat-spreader, (b) Primary FET copper heat-spreader, (c) Primary side copper mechanical spacer*

## CORE DRAWING AND DIMENSIONS



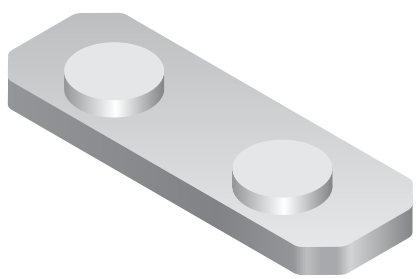



*Figure 12: Drawing with dimensions of the transformer core*

**Table 2: Bill of Materials - Thermal-Mechanical components**

| Item | Qty | Reference | Part Description | Manufacturer | Part # |
|---|---|---|---|---|---|
| 1 | 1 | | Heat Sink Top Side | Fischer Elektrik | SK 476 50 SA |
| 2 | 1 | | Heat Sink Bottom Side | Fischer Elektrik | SK 476 50 SA |
| 3 | 2 | | Secondary FET Heat Spreader | Prototype Shortrun | Machined part |
| 4 | 2 | | Primary FET Heat Spreader | Prototype Shortrun | Machined part |
| 5 | 2 | | Primary FET Heat Spreader Seat | Prototype Shortrun | Machined part |
| 6 | 2 | | Primary TIM pad | T-Global Technology | TG-A1780 X 0.5 mm |
| 7 | 8 | | Secondary TIM pad | T-Global Technology | TG-A1780 X 0.5 mm |
| 8 | 2 | | Heat Sink TIM pad | T-Global Technology | TG-A620 X 0.5 mm |
| 9 | 2 | | M2-0.40x10 mm Screws | Metric Screws US | 10047 |
| 10 | 2 | | M1.4x16 mm Screws | Metric Screws US | 21856 |
| 11 | 2 | | M1.4 Hex Nuts | Metric Screws US | 20680 |

**Table 3: Bill of Materials - EPC9149 module electrical**

| Item | Qty | Reference | Part Description | Manufacturer | Part # |
|---|---|---|---|---|---|
| 1 | 2 | C1, C6 | CAP CER 0402 10 nF 25 V X7R 5% | Kemet | C0402C103J3REC |
| 2 | 8 | C2, C4, C5, C7, C58, C63, C65, C66 | 22 µF ±20% 25 V Ceramic Capacitor X5R 0805 | Murata | GRT21BR61E226ME13L |
| 3 | 1 | C10 | 10000 pF ±10% 16 V Ceramic Capacitor X7R 0402 | Kemet | C0402C103K4RECAUTO |
| 4 | 5 | C11, C12, C13, C81_GP1, C81_GP2 | 0.1 µF, 25 V, 0402, X7R | Yageo | CC0402KRX7R8BB104 |
| 5 | 64 | C14_PS1, C14_PS2, C15_PS1, C15_PS2, C16_PS1, C16_PS2, C17_PS1, C17_PS2, C18_PS1, C18_PS2, C19_PS1, C19_PS2, C20_PS1, C20_PS2, C24_PS1, C24_PS2, C25_PS1, C25_PS2, C26_PS1, C26_PS2, C27_PS1, C27_PS2, C28_PS1, C28_PS2, C29_PS1, C29_PS2, C30_PS1, C30_PS2, C31_PS1, C31_PS2, C32_PS1, C32_PS2, C33_PS1, C33_PS2, C34_PS1, C34_PS2, C35_PS1, C35_PS2, C36_PS1, C36_PS2, C44_PS1, C44_PS2, C45_PS1, C45_PS2, C46_PS1, C46_PS2, C47_PS1, C47_PS2, C48_PS1, C48_PS2, C49_PS1, C49_PS2, C50_PS1, C50_PS2, C51_PS1, C51_PS2, C52_PS1, C52_PS2, C53_PS1, C53_PS2, C54_PS1, C54_PS2, C55_PS1, C55_PS2 | 2.2 µF ±10% 25 V Ceramic Capacitor JB 0402 | TDK | C1005JB1E225K050BC |
| 6 | 2 | C21, C22 | CAP CER 1 µF 25 V X5R 0402 | Murata | GRT155R61E105ME01D |
| 7 | 1 | C23 | CAP CER 22 µF 6.3 V 0402 | Samsung | CL05A226MQ5N6J8 |
| 8 | 4 | C40_GS11, C40_GS12, C40_GS21, C40_GS22 | CAP CER 4.7 µF 6.3 V X5R 0201 | Murata | GRM035R60J475ME15D |
| 9 | 4 | C41_GS11, C41_GS12, C41_GS21, C41_GS22 | CAP CER 33 pF 25 V C0G/NP0 0201 | Murata | GRM0335C1E330JA01D |
| 10 | 2 | C80_GP1, C80_GP2 | CAP CER 1 µF 25 V X5R 0402 | TDK | C1005X5R1A475K050BC |
| 11 | 1 | C90 | CAP CER 22 µF 6.3 V 0402 | Taiyo Yuden | HMK107C7224KAHTE |
| 12 | 1 | C91 | CAP CER 4.7 µF 6.3 V X5R 0201 | TDK | C1005X6S1C105K050BC |
| 13 | 1 | C92 | CAP CER 33PF 25 V C0G/NP0 0201 | TDK | C1005X7S2A103K050BB |
| 14 | 1 | C93 | CAP CER 4.7 µF 10 V X5R 0402 | TDK | CGA2B3X7S2A332M050BB |
| 15 | 1 | C94 | CAP CER 0.22 µF 100 V X7S 0603 | Murata | GRM188R61E106MA73D |
| 16 | 1 | C95 | 1 µF ±10% 16 V Ceramic Capacitor X6S 0402 | Murata | GRM155R71H103KA88D |
| 17 | 14 | Ci1_PP1, Ci1_PP2, Ci2_PP1, Ci2_PP2, Ci3_PP1, Ci3_PP2, Ci4_PP1, Ci4_PP2, Ci5_PP1, Ci5_PP2, Ci6_PP1, Ci6_PP2, Ci7_PP1, Ci7_PP2 | CAP CER 10000 pF 100 V X7S 0402 | Taiyo Yuden | HMK107C7224 |
| 18 | 10 | Cm1, Cm2, Cm3, Cm4, Cm5, Cm6, Cm7, Cm8, Cm9, Cm10 | 750 pF ±5% 50 V Ceramic Capacitor C0G, NP0 0402 | TDK | C2012X7S2A105M125AB |
| 19 | 22 | Cr1, Cr2, Cr3, Cr4, Cr5, Cr6, Cr7, Cr8, Cr9, Cr10, Cr11, Cr12, Cr13, Cr14, Cr15, Cr16, Cr17, Cr18, Cr19, Cr20, Cr21, Cr22 | CAP CER 10 µF 25 V X5R 0603 | Kemet | C1206C224K3JAC7800 |
| 20 | 4 | FB_GS11, FB_GS12, FB_GS21, FB_GS22 | FERRITE BEAD 240 Ω 0201 0.35 A 380 mΩ | Murata | BLM03AX241SN1D |
| 21 | 1 | J10 | 5 pin header | | |
| 22 | 1 | L90 | 120 µH Shielded Wirewound Inductor 950 mA 100 mΩ | Bourns | SRR4828A-121M |
| 23 | 4 | Q1_PP1, Q1_PP2, Q2_PP1, Q2_PP2 | 100 V 60 A 3.2 mΩ | EPC | EPC2218 |
| 24 | 8 | Q1_PS1, Q1_PS2, Q2_PS1, Q2_PS2, Q3_PS1, Q3_PS2, Q4_PS1, Q4_PS2 | 40 V 60 A 1.5mE | EPC | EPC2024 |
| 25 | 1 | R1 | 39 kΩs ±0.1% 0.2 W, 1/5 W Chip Resistor 0603 | Panasonic | RC0603FR-07110KL |
| 26 | 1 | R2 | 4.87 kΩs ±0.1% 0.063 W, 1/16 W Chip Resistor 0402 | Panasonic | ERA-2AEB4871X |
| 27 | 1 | R3 | RES SMD 20 Ω 1% 1/16 W 0402 | Yageo | RC0402FR-0720RL |
| 28 | 1 | R4 | RES SMD 48.7 KΩ 0.1% 1/16 W 0402 | Panasonic | ERA-2AEB183X |
| 29 | 1 | R5 | RES SMD 3.48 KΩ 0.1% 1/16 W 0402 | Panasonic | ERA-2AEB4751X |
| 30 | 1 | R11 | FERRITE BEAD 180 Ω 0603 1LN | Murata | BLM18PG181SN1D |
| 31 | 1 | R16 | 10K 0402 | Yageo | RC0402JR-0710KL |
| 32 | 1 | R21 | 0 Ωs Jumper 1/16 W Chip Resistor 0402 | Yageo | RC0402JR-070RL |
| 33 | 4 | R40_GS11_Off, R40_GS12_Off, R40_GS21_Off, R40_GS22_Off | RES 0.47 Ω 1% 1/10 W 0201 | ROHM | UCR006YVPFLR470 |
| 34 | 4 | R40_GS11_On, R40_GS12_On, R40_GS21_On, R40_GS22_On | RES SMD 2 Ω 5% 1/20 W 0201 | Panasonic | ERJ-1GNJ2R0C |
| 35 | 4 | R41_GS11, R41_GS12, R41_GS21, R41_GS22 | RES 10K Ω 1% 1/20 W 0201 | Panasonic | RMCF0201FT10K0 |
| 36 | 4 | R80_GP1, R80_GP2, R82_GP1, R82_GP2 | RES SMD 1 Ω 5% 1/10 W 0402 | Yageo | RC0402FR-071RL |
| 37 | 1 | R90 | 0 Ωs Jumper 0.1 W, 1/10 W Chip Resistor 0603 | Panasonic | ERJ-3GEY0R00V |
| 38 | 1 | R91 | 86.6 k 0603 | Yageo | RC0603FR-0786K6L |
| 39 | 1 | R92 | 16.5 k 0402 | Yageo | RC0402FR-0716K5L |
| 40 | 1 | R93 | RES SMD 1 Ω 1% 1/16 W 0402 | Yageo | RC0402JR-0768KL |
| 41 | 1 | R94 | 11.3 kΩs ±0.5% 0.063 W, 1/16 W Chip Resistor 0402 | Yageo | RT0402DRD0711K3L |
| 42 | 1 | R95 | 3.65 k 0603 | Yageo | RC0402FR-073K65L |
| 43 | 1 | R96 | 127 k 0603 | Yageo | RC0603FR-07127KL |
| 44 | 2 | SOB, SOT | Round Standoff Threaded M2x0.4 Steel 0.039" (1.00 mm) | Wurth | 9774010243R |
| 45 | 1 | U10 | dsPIC Automotive, AEC-Q100, dsPIC™ 33CK Microcontroller IC 16-Bit 100 MHz 32KB (32K x 8) FLASH 28-UQFN (4x4) | Microchip | DSPIC33CK32MP102T-I/M6 |
| 46 | 1 | U20 | Linear Voltage Regulator IC 1 Output 500 mA 6-WSON (2x2) | TI | TLV75533PDRVR |
| 47 | 4 | U40_GS11, U40_GS12, U40_GS21, U40_GS22 | LMG1020 Low side GaN driver | Texas Instruments | LMG1020YFF |
| 48 | 2 | U80_GP1, U80_GP2 | eGaN 100 V Half Bridge Gate Driver | uPI | uP1966A |
| 49 | 1 | U90 | Buck Regulator 100 V, 300 mA | Texas Instruments | LM5018SD/NOPB |

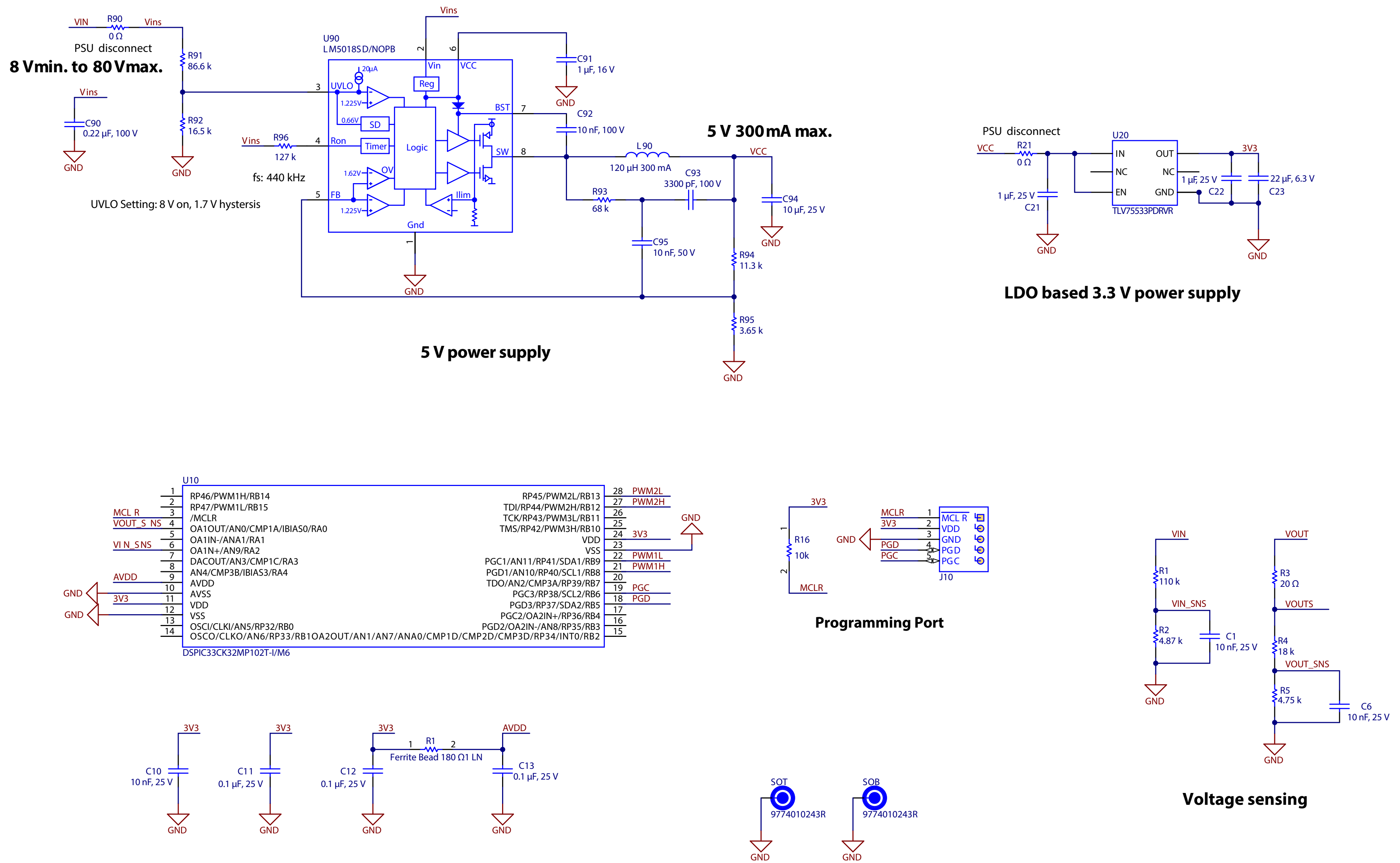
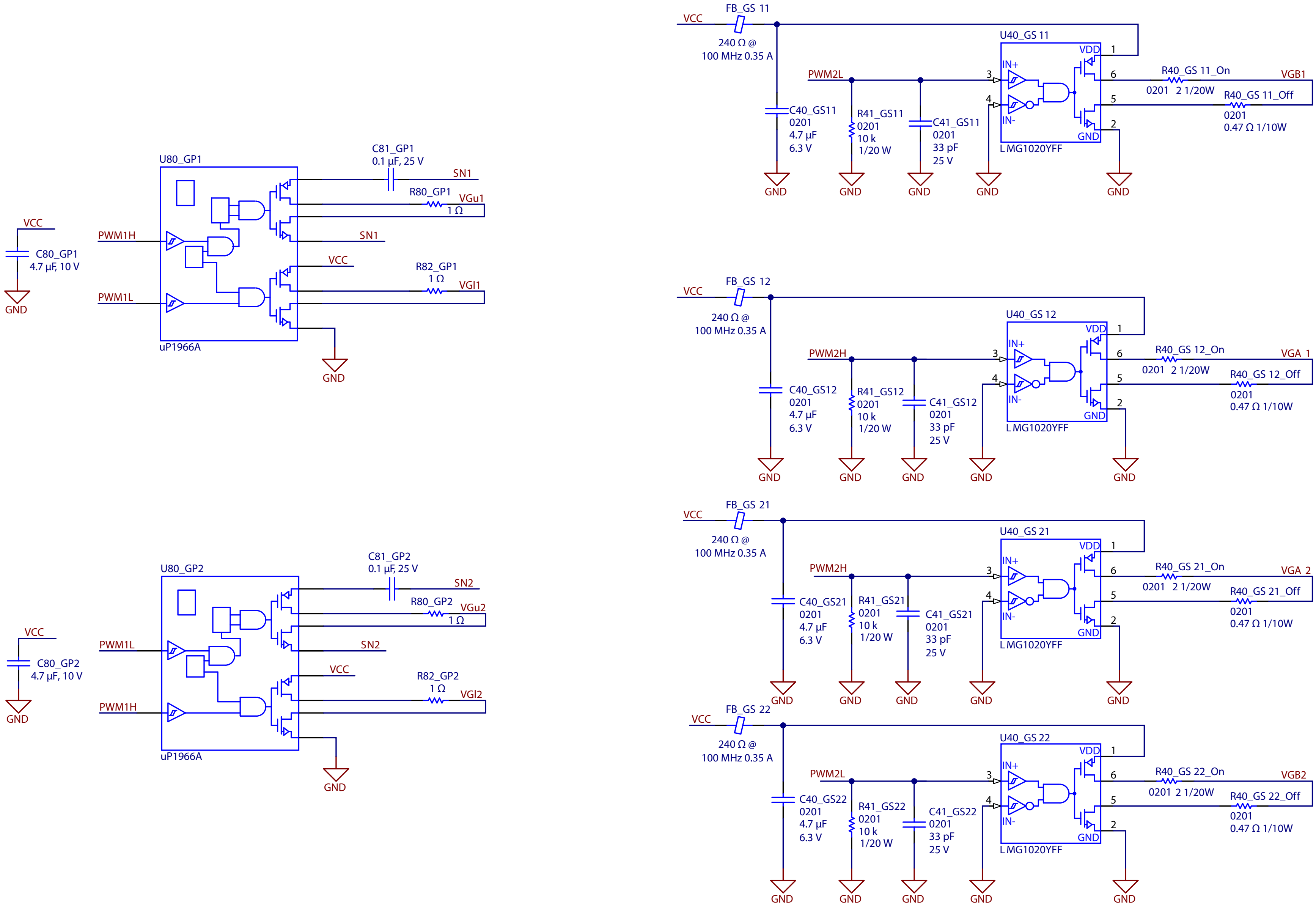



Figure 14: **Control stage**: Microcontroller, input and output voltage sensing, 5V bias supply for the drivers and 3.3V regulator for the dSPIC supply




**Primary-side Gate Drivers**

**Secondary-side Gate Drivers**

Figure 15: **Driver stage**: For the primary and secondary side FETs

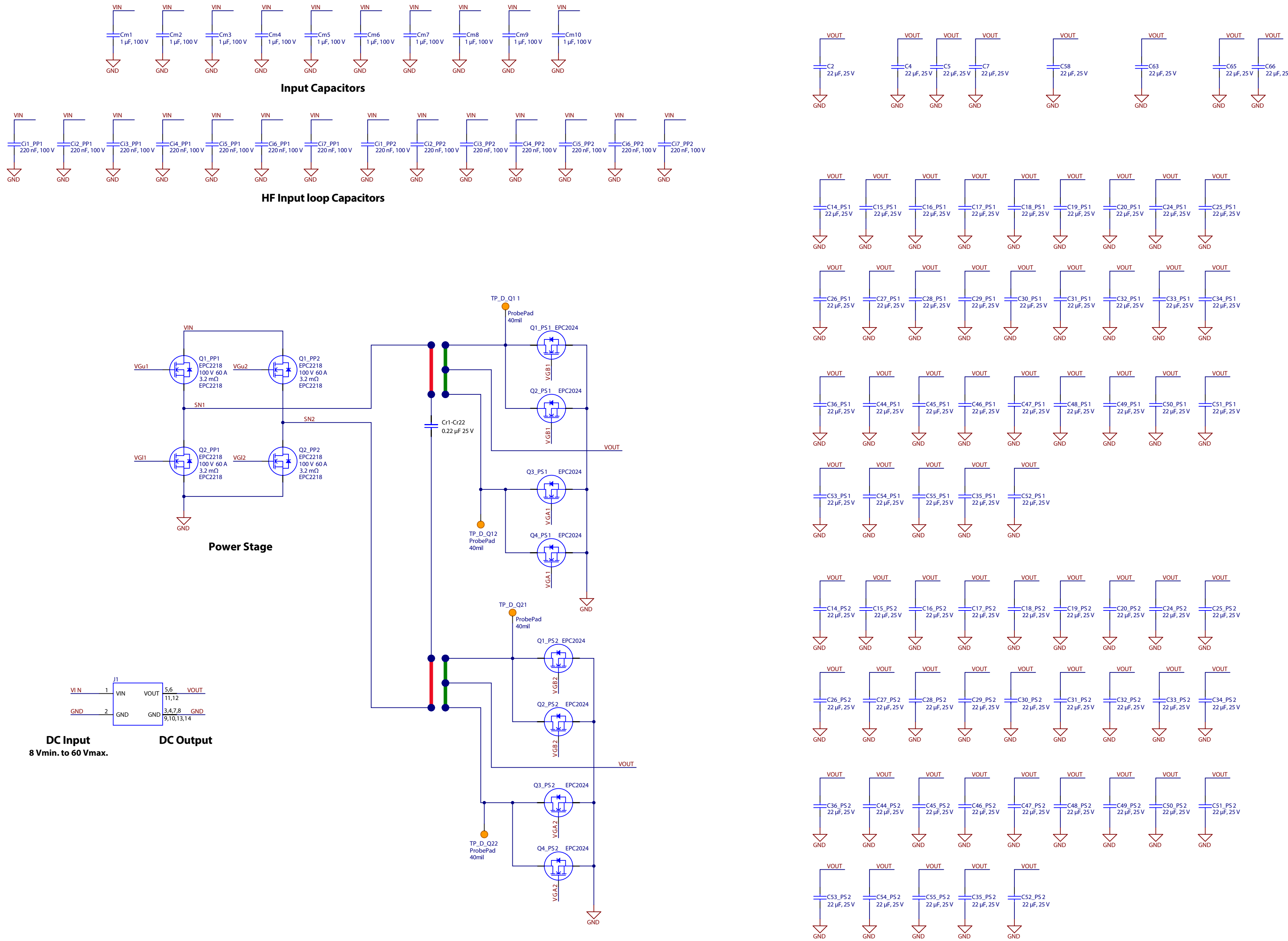



Figure 16: **Power stage:** Topology including FETs, transformer and input, output and resonant capacitors

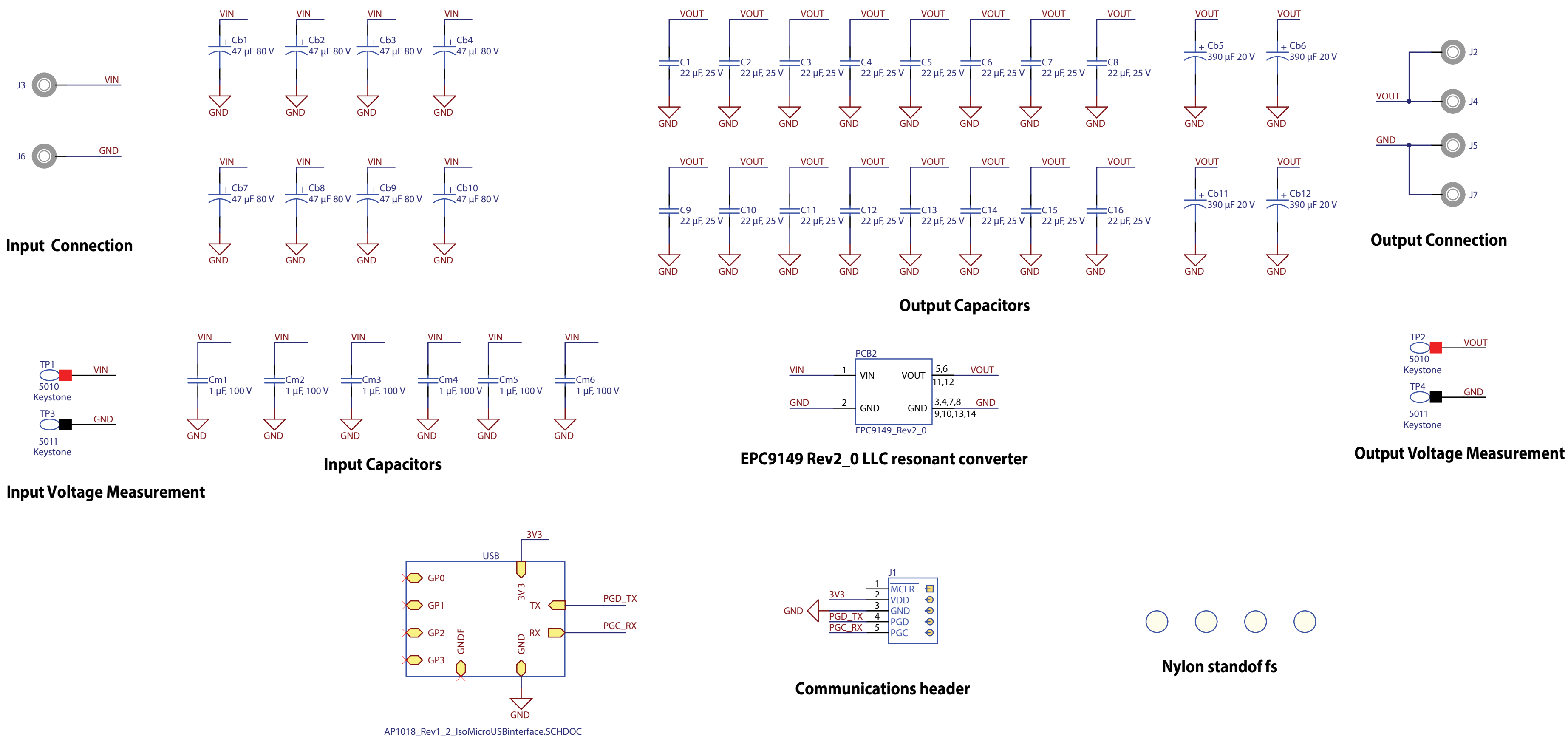



Figure 17: EPC9533 power circuit schematic

## Data type selector

Default set to UART using 5 V

| UART 5 V | | I²C 3.3 V | |
|---|---|---|---|
| Install | DNP | Install | DNP |
| R530 | R532 | R532 | R530 |
| R531 | R533 | R533 | R531 |
| R551 | R534 | R534 | R551 |
| | R535 | R535 | |
| | R520 | R520 | |
| | R521 | R521 | |
| | R552 | R552 | |

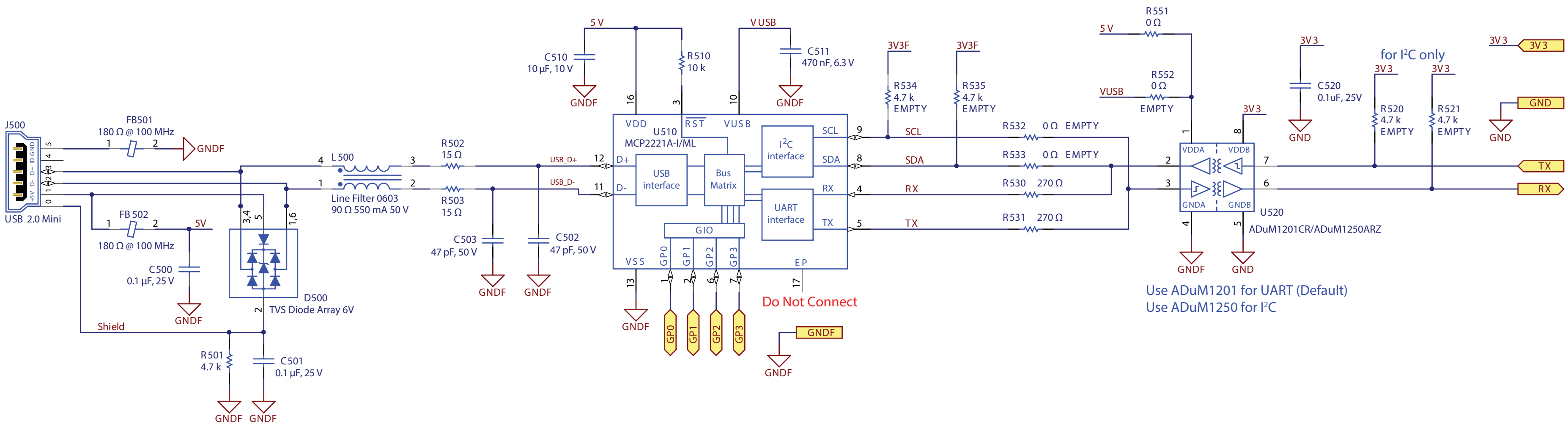



Figure 18: Isolated USB circuit on the EPC9533 motherboard

EPC would like to acknowledge Microchip Technology Inc. (www.microchip.com) for their support of this project.

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The EPC9149 system features the **dsPIC33CK32MP102** 16-Bit Digital Signal Controller with High-Speed ADC, Op Amps, Comparators and High-Resolution PWM. Learn more at www.microchip.com.

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