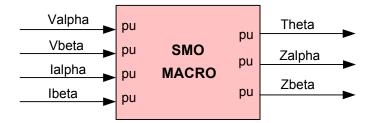
SMO

Sliding-Mode Rotor Position Observer of PMSM

Description

This software module implements a rotor position estimation algorithm for Permanent-Magnet Synchronous Motor (PMSM) based on Sliding-Mode Observer (SMO).

.



Availability

This IQ module is available in one interface format:

1) The C interface version

Module Properties

Type: Target Independent, Application Dependent

Target Devices: 28x Fixed Point or Piccolo

C Version File Names: smopos.h

IQmath library files for C: IQmathLib.h, IQmath.lib

C Interface

Object Definition

The structure of SMOPOS object is defined by following structure definition

```
typedef struct { _iq Valpha;
                                // Input: Stationary alpha-axis stator voltage
                _iq Ealpha;
                                // Variable: Stationary alpha-axis back EMF
                                // Output: Stationary alpha-axis sliding control
                iq Zalpha;
                _iq Gsmopos; // Parameter: Motor dependent control gain
                ig Estlalpha; // Variable: Estimated stationary alpha-axis stator current
                _iq Fsmopos; // Parameter: Motor dependent plant matrix
                                // Input: Stationary beta-axis stator voltage
                iq Vbeta;
                                // Variable: Stationary beta-axis back EMF
                _iq Ebeta;
                _iq Zbeta;
                                // Output: Stationary beta-axis sliding control
                _iq EstIbeta; // Variable: Estimated stationary beta-axis stator current
                _iq lalpha;
                                // Input: Stationary alpha-axis stator current
                _iq lalphaError; // Variable: Stationary alpha-axis current error
               _iq Kslide;
                               // Parameter: Sliding control gain
                _iq Ibeta;
                                // Input: Stationary beta-axis stator current
                _iq IbetaError; // Variable: Stationary beta-axis current error
                                // Parameter: Sliding control filter gain
                iq Kslf;
                                // Output: Compensated rotor angle
                iq Theta;
             } SMOPOS;
```

typedef SMOPOS * SMOPOS_handle;

Module Terminal Variables

Name	Description	Format [*]	Range(Hex)
Valpha	stationary d-axis stator voltage	GLOBAL_Q	80000000-7FFFFFF
Vbeta	stationary q-axis stator voltage	GLOBAL_Q	80000000-7FFFFFF
lalpha	stationary d-axis stator current	GLOBAL_Q	80000000-7FFFFFF
Ibeta	stationary q-axis stator current	GLOBAL_Q	80000000-7FFFFFF
Theta	rotor position angle	GLOBAL_Q	00000000-7FFFFFF
			(0 – 360 degree)
Zalfa	stationary d-axis sliding control	GLOBAL_Q	80000000-7FFFFFF
Zbeta	stationary q-axis sliding control	GLOBAL_Q	80000000-7FFFFFF
Fsmopos	Fsmopos = exp(-Rs*T/Ls)	GLOBAL_Q	80000000-7FFFFFF
Gsmopos	Gsmopos = (Vb/lb)*(1- exp(-Rs*T/Ls))/Rs	GLOBAL_Q	80000000-7FFFFFF
Kslide	sliding mode control gain	GLOBAL_Q	80000000-7FFFFFF
Kslf	sliding control filter gain	GLOBAL_Q	80000000-7FFFFFF
Ealpha	stationary d-axis back EMF	GLOBAL_Q	80000000-7FFFFFF
Ebeta	stationary q-axis back EMF	GLOBAL_Q	80000000-7FFFFFF
Estlalpha	stationary d-axis estimated current	GLOBAL_Q	80000000-7FFFFFF
EstIbeta	stationary q-axis estimated current	GLOBAL_Q	80000000-7FFFFFF
lalphaError	stationary d-axis current error	GLOBAL_Q	80000000-7FFFFFF
IbetaError	stationary q-axis current error	GLOBAL_Q	80000000-7FFFFFF
	Valpha Vbeta Ialpha Ibeta Theta Zalfa Zbeta Fsmopos Gsmopos Kslide Kslf Ealpha Ebeta Estlalpha Estlbeta IalphaError	Valpha stationary d-axis stator voltage Vbeta stationary q-axis stator voltage lalpha stationary q-axis stator current lbeta stationary q-axis stator current Theta rotor position angle Zalfa stationary d-axis sliding control Zbeta stationary q-axis sliding control Fsmopos Fsmopos = exp(-Rs*T/Ls) Gsmopos Gsmopos = (Vb/lb)*(1- exp(-Rs*T/Ls))/Rs Kslide sliding mode control gain Kslf sliding control filter gain Ealpha stationary d-axis back EMF Ebeta stationary q-axis back EMF Estlalpha stationary d-axis estimated current Estlbeta stationary q-axis estimated current lalphaError stationary d-axis current error	Valpha stationary d-axis stator voltage GLOBAL_Q Vbeta stationary q-axis stator voltage GLOBAL_Q Ialpha stationary d-axis stator current GLOBAL_Q Ibeta stationary q-axis stator current GLOBAL_Q Theta rotor position angle GLOBAL_Q Zalfa stationary d-axis sliding control GLOBAL_Q Zbeta stationary q-axis sliding control GLOBAL_Q Fsmopos Fsmopos = exp(-Rs*T/Ls) GLOBAL_Q Gsmopos Gsmopos = (Vb/Ib)*(1- exp(-Rs*T/Ls))/Rs Kslide sliding mode control gain GLOBAL_Q Kslf sliding control filter gain GLOBAL_Q Ealpha stationary d-axis back EMF GLOBAL_Q Estlalpha stationary d-axis estimated current GLOBAL_Q Estlalpha stationary d-axis estimated current GLOBAL_Q IalphaError stationary d-axis current error GLOBAL_Q

GLOBAL Q valued between 1 and 30 is defined in the IQmathLib.h header file.

Special Constants and Data types

SMOPOS

The module definition is created as a data type. This makes it convenient to instance an interface to the sliding-mode rotor position observer of Permanent-Magnet Synchronous Motor module. To create multiple instances of the module simply declare variables of type SMOPOS.

SMOPOS handle

User defined Data type of pointer to SMOPOS module

SMOPOS DEFAULTS

Structure symbolic constant to initialize SMOPOS module. This provides the initial values to the terminal variables as well as method pointers.

Methods

SMO_MACRO(SMOPOS_handle);

This definition implements one method viz., the sliding-mode rotor position observer of Permanent-Magnet Synchronous Motor computation macro. The input argument to this macro is the module handle.

Module Usage

Instantiation

The following example instances two SMOPOS objects SMOPOS smo1, smo2;

Initialization

```
To Instance pre-initialized objects
SMOPOS fe1 = SMOPOS_DEFAULTS;
SMOPOS fe2 = SMOPOS_DEFAULTS;
```

Invoking the computation macro

```
SMO_MACRO (smo1);
SMO_MACRO (smo2);
```

Example

The following pseudo code provides the information about the module usage.

```
main()
{

smo1.Fsmopos = parem1_1;  // Pass parameters to smo1
smo1.Gsmopos = parem1_2;  // Pass parameters to smo1
smo1.Kslide = parem1_3;  // Pass parameters to smo1
smo1.Kslf = parem1_4;  // Pass parameters to smo1
```

```
smo2.Fsmopos = parem2 1;
                                             // Pass parameters to smo2
                                             // Pass parameters to smo2
       smo2.Gsmopos = parem2 2;
       smo2.Kslide = parem2_3;
                                             // Pass parameters to smo2
       smo2.Kslf = parem2 4;
                                             // Pass parameters to smo2
}
void interrupt periodic_interrupt_isr()
       smo1.Valpha = voltage dq1.d;
                                             // Pass inputs to smo1
       smo1.Vbeta = voltage_dq1.q;
                                             // Pass inputs to smo1
       smo1.lalpha =current_dq1.d;
                                             // Pass inputs to smo1
                                             // Pass inputs to smo1
       smo1.lbeta =current dq1.q;
       smo2.Valpha = voltage_dq2.d;
                                             // Pass inputs to smo2
       smo2.Vbeta = voltage dq2.q;
                                             // Pass inputs to smo2
       smo2.lalpha =current_dq2.d;
                                             // Pass inputs to smo2
       smo2.lbeta =current_dq2.q;
                                             // Pass inputs to smo2
        SMO MACRO(smopos1)
                                             // Call compute macro for smopos1
       SMO MACRO(smopos2);
                                             // Call compute macro for smopos2
       angle1 = smopos1.Theta;
                                             // Access the outputs of smopos1
       angle2 = smopos2.Theta;
                                             // Access the outputs of smopos2
```

}

Constant Computation Macro

Since the sliding-mode rotor position observer of Permanent-Magnet Synchronous Motor module requires two constants (Fsmopos and Gsmopos) to be input basing on the machine parameters, base quantities, mechanical parameters, and sampling period. These two constants can be internally computed by the macro (smopos_const.h). The followings show how to use the C constant computation macro.

Object Definition

The structure of SMOPOS_CONST object is defined by following structure definition

typedef SMOPOS CONST *SMOPOS CONST handle;

Module Terminal Variables

Item	Name	Description	Format	Range(Hex)
Inputs	Rs	Stator resistance (ohm)	Floating	N/A
-	Ls	Stator inductance (H)	Floating	N/A
	lb	Base phase current (amp)	Floating	N/A
	Vb	Base phase voltage (volt)	Floating	N/A
	Ts	Sampling period (sec)	Floating	N/A
Outputs	Fsmopos	constant using in observed current calculation	Floating	N/A
	Gsmopos	constant using in observed current calculation	Floating	N/A

Special Constants and Data types

SMOPOS CONST

The module definition is created as a data type. This makes it convenient to instance an interface to the sliding-mode rotor position observer of Permanent-Magnet Synchronous Motor constant computation module. To create multiple instances of the module simply declare variables of type SMOPOS CONST.

SMOPOS CONST handle

User defined Data type of pointer to SMOPOS CONST module

SMOPOS CONST DEFAULTS

Structure symbolic constant to initialize SMOPOS_CONST module. This provides the initial values to the terminal variables as well as method pointers.

Methods

SMO_CONST_MACRO (SMOPOS_CONST_handle);

This definition implements one method viz., the sliding-mode rotor position observer of Permanent-Magnet Synchronous Motor constant computation macro. The input argument to this macro is the module handle.

Module Usage

Instantiation

The following example instances two SMOPOS_CONST objects SMOPOS_CONST smopos1_const, smopos2_const;

Initialization

```
To Instance pre-initialized objects
SMOPOS_CONST smopos1_const = SMOPOS_CONST_DEFAULTS;
SMOPOS_CONST smopos2_const = SMOPOS_CONST_DEFAULTS;
```

Invoking the computation macro

```
SMO_CONST_MACRO (smopos1_const);
SMO_CONST_MACRO (smopos2_const);
```

Example

The following pseudo code provides the information about the module usage.

```
main()
{
```

```
smopos1 const.Rs = Rs1;
                              // Pass floating-point inputs to smopos1 const
smopos1 const.Ls = Ls1;
                              // Pass floating-point inputs to smopos1 const
                              // Pass floating-point inputs to smopos1 const
smopos1 const.lb = lb1;
                              // Pass floating-point inputs to smopos1 const
smopos1 const.Vb = Vb1;
smopos1\_const.Ts = Ts1;
                              // Pass floating-point inputs to smopos1 const
smopos2 const.Rs = Rs2;
                              // Pass floating-point inputs to smopos2 const
smopos2 const.Ls = Ls2;
                              // Pass floating-point inputs to smopos2 const
smopos2 const.lb = lb2;
                              // Pass floating-point inputs to smopos2 const
smopos2 const.Vb = Vb2;
                              // Pass floating-point inputs to smopos2 const
smopos2_const.Ts = Ts2;
                              // Pass floating-point inputs to smopos2 const
SMO CONST MACRO (smopos1 const); // Call compute macro for smopos1 const
SMO_CONST_MACRO (smopos2_const); // Call compute macro for smopos2_const
// Access the outputs of smopos1 const
smopos1.Fsmopos = _IQ(smopos1_const.Fsmopos);
smopos1.Gsmopos = IQ(smopos1 const.Gsmopos);
```

```
// Access the outputs of smopos2_const
smopos2.Fsmopos = _IQ(smopos2_const.Fsmopos);
smopos2.Gsmopos = _IQ(smopos2_const.Gsmopos);
}
```

Technical Background

Figure 1 is an illustration of a permanent-magnet synchronous motor control system based on field orientation principle. The basic concept of field orientation is based on knowing the position of rotor flux and positioning the stator current vector at orthogonal angle to the rotor flux for optimal torque output. The implementation shown in Figure 1 derives the position of rotor flux from encoder feedback. However, the encoder increases system cost and complexity.

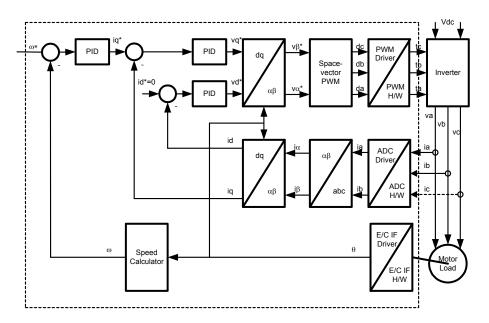


Figure 1 Field Oriented Control of PMSM

Therefore for cost sensitive applications, it is ideal if the rotor flux position information can be derived from measurement of voltages and currents. Figure 2 shows the block diagram of a sensorless PMSM control system where rotor flux position is derived from measurement of motor currents and knowledge of motor voltage commands.

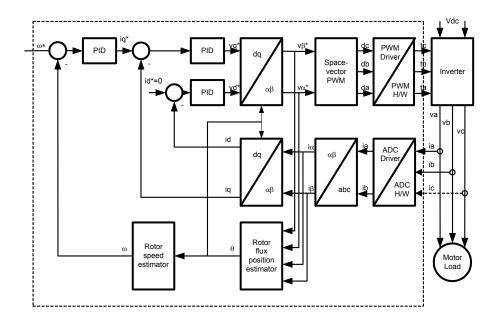


Figure 2 Sensorless Field Oriented Control of PMSM

This software module implements a rotor flux position estimator based on a sliding mode current observer. As shown in Figure 3, the inputs to the estimator are motor phase currents and voltages expressed in α - β coordinate frame.

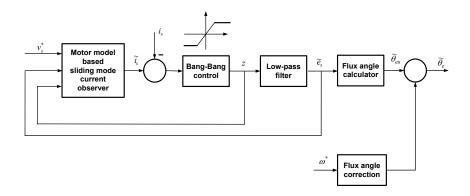


Figure 3 Sliding Mode Observer Based Rotor Flux Position Estimator

Figure 4 is an illustration of the coordinate frames and voltage and current vectors of PMSM, with a, b and c being the phase axes, α and β being a fixed Cartesian coordinate frame aligned with phase a, and d and q being a rotating Cartesian coordinate frame aligned with rotor flux. v_s , i_s and e_s are the motor phase voltage, current and back emf vectors (each with two coordinate entries). All vectors are expressed in α - β coordinate frame for the purpose of this discussion. The α - β frame expressions are obtained by applying Clarke transformation to their corresponding three phase representations.

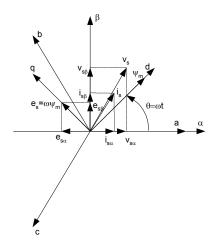


Figure 4 PMSM Coordinate Frames and Vectors

Equation 1 is the mathematical model of PMSM in α - β coordinate frame.

$$\frac{d}{dt}i_s = Ai_s + B(v_s - e_s) \tag{1}$$

The matrices A and B are defined as $A=-\frac{R}{L}I_2$ and $B=\frac{1}{L}I_2$ with $L=\frac{3}{2}L_m$, where L_m and R are the magnetizing inductance and resistance of stator phase winding and I_2 is a 2 by 2 identity matrix. Next the mathematical equations for the blocks in Figure 3 are discussed.

1. Sliding Mode Current Observer

The sliding mode current observer consists of a model based current observer and a bang-bang control generator driven by error between estimated motor currents and actual motor currents. The mathematical equations for the observer and control generator are given by Equations 2 and 3.

$$\frac{d}{dt}\widetilde{i}_{S} = A\widetilde{i}_{S} + B(v_{S}^{*} - \widetilde{e}_{S} + z)$$
(2)

$$z = k \operatorname{sign}(\widetilde{i}_{s} - i_{s})$$
(3)

The goal of the bang-bang control z is to drive current estimation error to zero. It is achieved by proper selection of k and correct formation of estimated back emf, e_s . Note that the symbol \sim indicates that a variable is estimated. The symbol * indicates that a variable is a command.

The discrete form of Equations 2 and 3 are given by Equations 4 and 5.

$$\widetilde{i}_{S}(n+1) = F \widetilde{i}_{S}(n) + G(v_{S}^{*}(n) - \widetilde{e}_{S}(n) + z(n))$$
(4)

$$z(n) = k \operatorname{sign}(\widetilde{i}_{s}(n) - i_{s}(n))$$
(5)

The matrices F and G are given by $F = e^{-\frac{R}{L}T_s}I_2$ and $G = \frac{1}{R}(1-e^{-\frac{R}{L}T_s})I_2$ where T_s is the sampling period.

2. Estimated Back EMF

Estimated back emf is obtained by filtering the bang-bang control, z, with a first order low-pass filter described by Equation 6.

$$\frac{d}{dt}\widetilde{e}_s = -\omega_0\widetilde{e}_s + \omega_0 z \tag{6}$$

The parameter ω_0 is defined as $\omega_0=2\pi f_0$, where f_0 represents the cutoff frequency of the filter. The discrete form of Equation 6 is given by Equation 7.

$$\widetilde{e}_{s}(n+1) = \widetilde{e}_{s}(n) + 2\pi f_{0}(z(n) - \widetilde{e}_{s}(n)) \tag{7}$$

3. Rotor Flux Position Calculation

Estimated rotor flux angle is obtained based on Equation 8 for back emf.

$$e_s = \frac{3}{2} k_e \omega \begin{pmatrix} -\sin\theta \\ \cos\theta \end{pmatrix} \tag{8}$$

Therefore given the estimated back emf, estimated rotor position can be calculated based on Equation 9.

$$\widetilde{\theta}_{eu} = \arctan(-\widetilde{e}_{s\alpha}, \widetilde{e}_{s\beta})$$
 (9)

Next, Table 1 shows the correspondence of notations between variables used here and variables used in the program (i.e., smopos.c, smopos.h). The software module requires that both input and output variables are in per unit values.

	Equation Variables	Program Variables
	V _{Sα} *	Valpha
Inputs	ν _{sβ} *	Vbeta
	i_{slpha}	lalpha
	i_{seta}	Ibeta
0	$\widetilde{ heta}_e$	Theta
Outputs	z_{α}	Zalpha
	Z _B	Zbeta
	\widetilde{i}_{slpha}	Estlalpha
	\widetilde{i}_{seta}	Estibeta
Othoro	\widetilde{e}_{slpha}	Ealpha
Others	\widetilde{e}_{seta}	Ebeta
	$e^{-\frac{R}{L}T_s}$	Fsmopos
	$\frac{1}{R}(1-e^{-\frac{R}{L}T_s})$	Gsmopos
	k	Kslide
	$2\pi\!f_0$	Kslf

Table 1: Correspondence of notations