Active Filter

TE201414 - Rangkaian Elektronika 2

Program Studi Teknik Elektro

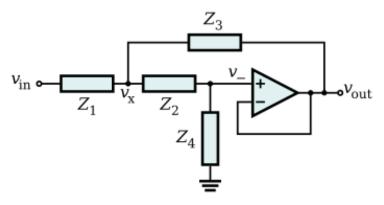


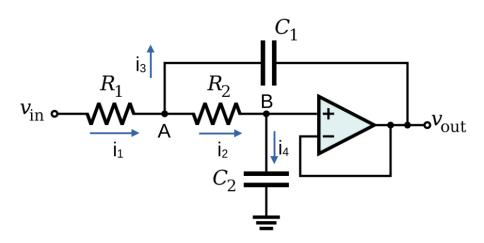
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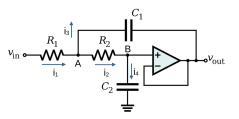
May 18, 2025

Second Order Active Filter: Sallen-Key Topology

the Sallen-Key topology is an electronic filter topology used to implement second-order active filters that is particularly valued for its simplicity.







$$I_2 = \frac{V_A - V_B}{R_2} = \frac{V_A - V_{out}}{R_2}$$

review node B

$$I_2 = I_4 = j\omega C_2 V_{out}$$

 V_{out} is similar with voltage at node B V_B , then:

$$I_4 = \frac{V_{out}}{Xc_2} = j\omega C_2 V_{out}$$

$$\frac{V_A - V_{out}}{R_2} = j\omega C_2 V_{out}$$

$$V_A = V_{out} + j\omega R_2 C_2 V_{out}$$
 $I_3 = \frac{V_A - V_{out}}{X c_1} = (V_A - V_{out}) j\omega C_1$

$$I_3 = (V_{out} + j\omega R_2 C_2 V_{out} - V_{out}) j\omega C_1$$
$$I_3 = -\omega^2 R_2 C_1 C_2 V_{out}$$

review node A:

de A:
$$I_{1} = I_{2} + I_{3}$$

$$I_{1} = \frac{V_{in} - V_{A}}{R_{1}}$$

$$\frac{V_{in} - V_{A}}{R_{1}} = j\omega C_{2}V_{out} + (-\omega^{2}R_{2}C_{1}C_{2}V_{out})$$

$$V_{in} = V_{A} + j\omega R_{1}C_{2}V_{out} - \omega^{2}R_{1}R_{2}C_{1}C_{2}V_{out}$$

$$V_{in} = V_{out} + j\omega R_{2}C_{2}V_{out} + j\omega R_{1}C_{2}V_{out} - \omega^{2}R_{1}R_{2}C_{1}C_{2}$$

$$V_{in} = V_{out}(1 - \omega^{2}R_{1}R_{2}C_{1}C_{2} + j\omega C_{2}(R_{1} + R_{2}))$$

$$\frac{V_{out}}{V_{in}} = \frac{1}{1 - \omega^{2}R_{1}R_{2}C_{1}C_{2} + j\omega C_{2}(R_{1} + R_{2})}$$

Every 1 order increase in the lowpass filter will shift the phase by -45 degrees, so it be -90 degrees phase shift for second order low pass filter at cut off frequency. the real value for -90 degree phase is zero, then

$$0 = 1 - \omega_c^2 R_1 R_2 C_1 C_2$$
$$\omega_c^2 = \frac{1}{R_1 R_2 C_1 C_2}$$
$$f_c = \frac{1}{2\pi \sqrt{R_1 R_2 C_1 C_2}}$$

to find signal amplification of bode plot: assume that $R_1=R_2=R$ and $C_1=C_2=C$

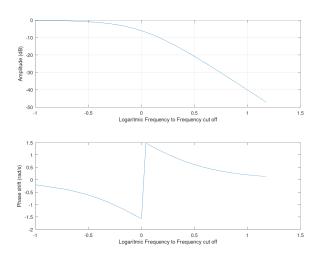
$$C = \frac{1}{\omega_c R}$$

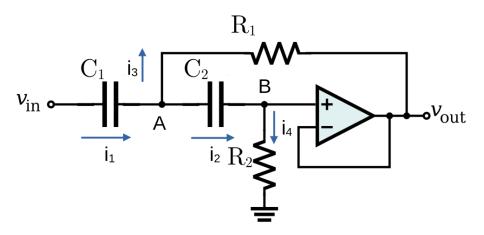
$$\begin{split} \frac{V_{out}}{V_{in}} &= \frac{1}{1 - \omega^2 R R \frac{1}{\omega_c R} \frac{1}{\omega_c R} + j \omega \frac{1}{\omega_c R} (2R)} \\ &\frac{V_{out}}{V_{in}} = \frac{1}{1 - (\frac{\omega}{\omega_c})^2 + j 2 \frac{\omega}{\omega_c}} \\ |A_{v}|_{\omega} &= \frac{1}{\sqrt{(2 \frac{\omega}{\omega_c})^2 + (1 - (\frac{\omega}{\omega_c})^2)^2}} \end{split}$$

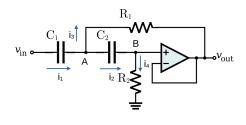
to find phase shift of bode plot:

$$\phi = 0 - \arctan rac{2rac{\omega}{\omega_c}}{1 - (rac{\omega}{\omega_c})^2}$$

Frequency response of second order active low filter.







$$I_2 = rac{V_A - V_B}{Xc_2} = j\omega C_2 (V_A - V_{out})$$
 review node B:

$$I_2 = I_4 = \frac{V_{out}}{R_2}$$

 V_{out} is similar with voltage at node B V_B , then:

$$I_4 = \frac{V_{out}}{R_2}$$

$$j\omega C_2(V_A - V_{out}) = \frac{V_{out}}{R_2}$$

$$j\omega R_2 C_2 (V_A - V_{out}) = V_{out}$$

$$V_A = V_{out} + \frac{V_{out}}{j\omega R_2 C_2}$$

$$I_3 = \frac{V_A - V_{out}}{R_1}$$

review node A:

$$I_1 = I_2 + I_3$$

$$I_1 = \frac{V_{in} - V_A}{Xc_1}$$

$$\frac{V_{in} - V_A}{Xc_1} = \frac{V_A - V_{out}}{Xc_2} + \frac{V_A - V_{out}}{R_1}$$

$$\frac{V_{in} - \left(\frac{V_{out}}{j\omega R_2 C_2} + V_{out}\right)}{\frac{1}{j\omega C_1}} = frac\left(\frac{V_{out}}{j\omega R_2 C_2} + V_{out}\right) - V_{out}\frac{1}{j\omega C_2} + \frac{\left(\frac{V_{out}}{j\omega R_2 C_2} + V_{out}\right)}{R_1}$$

$$\frac{V_{in} - \left(\frac{V_{out}}{j\omega R_2 C_2} + V_{out}\right)}{\frac{1}{j\omega C_2}} = \frac{\frac{V_{out}}{j\omega R_2 C_2}}{\frac{1}{j\omega C_2}} + \frac{\frac{V_{out}}{j\omega R_2 C_2}}{R_1}$$

$$\frac{V_{in} - (\frac{V_{out}}{j\omega R_2 C_2} + V_{out})}{\frac{1}{j\omega C_1}} = \frac{V_{out}}{R_2} + \frac{V_{out}}{j\omega R_1 R_2 C_2}$$

$$V_{in} - \frac{V_{out}}{j\omega R_2 C_2} - V_{out} = \frac{V_{out}}{j\omega R_2 C_1} + \frac{V_{out}}{j\omega^2 R_1 R_2 C_1 C_2}$$

$$V_{in} = V_{out} - \frac{V_{out}}{\omega^2 R_1 R_2 C_1 C_2} + \frac{V_{out}}{j\omega R_2 C_1} + \frac{V_{out}}{j\omega R_2 C_2}$$

$$\frac{V_{out}}{V_{in}} = 1 - \omega^2 R_1 R_2 C_1 C_2 + j\omega R_2 C_2 + j\omega R_2 C_1$$

Every 1 order increase in the lowpass filter will shift the phase by +45 degrees, so it be +90 degrees phase shift for second order low pass filter at cut off frequency. the real value for +90 degree phase is zero, then

$$0 = 1 - \omega_c^2 R_1 R_2 C_1 C_2$$
$$\omega_c^2 = \frac{1}{R_1 R_2 C_1 C_2}$$
$$f_c = \frac{1}{2\pi \sqrt{R_1 R_2 C_1 C_2}}$$

to find signal amplification of bode plot: assume that $R_1 = R_2 = R$ and $C_1 = C_2 = C$

$$C = \frac{1}{\omega_c R}$$

$$\frac{V_{out}}{V_{in}} = 1 - \omega^2 R^2 (\frac{1}{\omega_c R})^2 + 2j\omega R \frac{1}{\omega_c R}$$

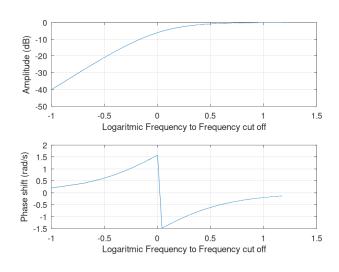
$$\frac{V_{out}}{V_{in}} = 1 - (\frac{\omega}{\omega_c})^2 + 2j\frac{\omega}{\omega_c}$$

$$|A_V|_{\omega} = \sqrt{(2\frac{\omega}{\omega_c})^2 + (1 - (\frac{\omega}{\omega_c})^2)^2}$$

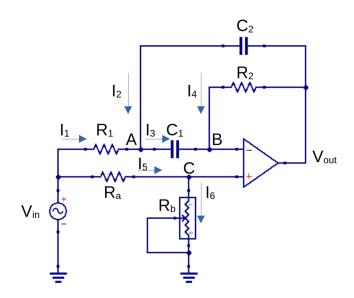
to find phase shift of bode plot:

$$\phi = 0 + \arctan rac{2rac{\omega}{\omega_c}}{1 - (rac{\omega}{\omega_c})^2}$$

Frequency response of second order active low filter.



Notch Filter/Bandstop Filter



References

Floyd, T.L., Fundamentals of Analog Circuits, Prentince Hall, .
Malvino, A., Electronic Principle, McGrawHill, 2016.
Boylestad, R.L., Nashelsky, L., Electronics Devices and Circuit Theory, Pearson, 2014.

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