Basic Definitions and Equations

$$\omega_n = \sqrt{\frac{k}{m}}$$
 $T_n = \frac{2\pi}{\omega_n}$ $f_n = \frac{1}{T_n}$ $(u_{st})_o = \frac{p_o}{k}$

$$\zeta = \frac{c}{2m\omega_n} = \frac{c}{c_{cr}} \hspace{1cm} \zeta > 1 \text{ overdamped} \\ \zeta = 1 \text{ critically damped} \\ \zeta < 1 \text{ underdamped}$$

$$\zeta = \frac{c}{2m\omega_n} = \frac{c}{c_{cr}}$$

$$\zeta = 1$$
 critically damped $\zeta < 1$ underdamped

$$\omega_D = \omega_n \sqrt{1 - \zeta^2}$$

Free Vibration

$$m\ddot{u} + c\dot{u} + ku = 0$$

For $\zeta = 0$:

$$u(t) = u(0)\cos\omega_n t + \frac{\dot{u}(0)}{\omega_n}\sin\omega_n t$$

For $0 < \zeta < 1$:

$$u(t) = e^{-\zeta \omega_n t} \left(u(0) \cos \omega_D t + \frac{\dot{u}(0) + \zeta \omega_n u(0)}{\omega_D} \sin \omega_D t \right)$$

$$\frac{u_i}{u_{i+j}} = \exp\left(\frac{2\pi j\zeta}{\sqrt{1-\zeta^2}}\right) \qquad \qquad \zeta = \frac{1}{2\pi j} \ln \frac{u_i}{u_{i+j}}$$

Harmonic Excitation $m\ddot{u} + c\dot{u} + ku = p_0 \sin \omega t$ Steady State Response

$$u(t) = u_0 \sin(\omega t - \phi)$$

$$R_d = \frac{u_0}{\omega t} = \frac{u_0}{\omega t}$$

$$R_d = \frac{u_0}{(u_{st})_o} = \frac{1}{\sqrt{[1 - (\omega/\omega_n)^2]^2 + [2\zeta(\omega/\omega_n)]^2}}$$

$$\omega = \tan^{-1} \frac{2\zeta(\omega/\omega_n)}{(u_{st})_o} = \frac{1}{(\omega/\omega_n)^2}$$

$$\varphi = \tan^{-1} \frac{2\zeta(\omega/\omega_n)}{1 - (\omega/\omega_n)^2}$$

Resonance at
$$\omega_n \sqrt{1 - 2\zeta^2}$$
 with $R_d = \frac{1}{2\zeta\sqrt{1 - \zeta^2}}$

Half-Power Bandwidth

$$\frac{\omega_b - \omega_a}{\omega_n} = 2\zeta$$

Vibration Generator

$$p(t) = (m_e e \omega^2) \sin \omega t$$

Transmissibility:
$$TR = (f_T)_o/p_o = \ddot{u}_o^t/\ddot{u}_{go} = u_o^t/u_{go}$$

$$TR = R_d \sqrt{1 + [2\zeta(\omega/\omega_n)]^2}$$

Equivalent Viscous Damping

$$\zeta_{\text{eq}} = \frac{1}{4\pi} \frac{E_D}{E_{so}}$$

Arbitrary Excitation $m\ddot{u} + c\dot{u} + ku = p(t)$

Response to unit impulse: $p(t) = \delta(t - \tau)$

$$h(t-\tau) \equiv u(t) = \frac{1}{m\omega_n} \sin(\omega_n(t-\tau)) \qquad (\zeta = 0)$$

Duhamel's integral

$$u(t) = \int_0^t p(\tau)h(t-\tau)d\tau$$

Response to step force ($\zeta = 0$)

$$u(t) = (u_{st})_o(1 - \cos \omega_n t)$$

Response to ramp force ($\zeta = 0$)

$$p(t)=p_0\frac{t}{t_r} \qquad \qquad u(t)=(u_{st})_0\left(\frac{t}{t_r}-\frac{\sin\omega_n t}{\omega_n t_r}\right)$$
 Response to rectangular pulse ($\zeta=0$)

$$R_d = \begin{cases} 2\sin \pi t_d / Tn & t_d < T_n / 2 \\ 2 & t_d \geq T_n / 2 \end{cases}$$

Short pulse

$$I = \int p(t)dt \qquad u(t) = I\left(\frac{1}{m\omega_n}\sin\omega_n t\right)$$

Earthquake Response $p(t) = p_{eff}(t) = -m\ddot{u}_g(t)$

$$u_o \equiv u_o(T_n, \zeta) \equiv \max(u(t))$$

$$\equiv u_0$$
 $V = \omega_n D$

$$=\omega_n D$$
 $A=$

$$D \equiv u_0$$
 $V = \omega_n D$ $\frac{A}{\omega_n} = V = \omega_n D$ $f_{so} = kD = mA$

For One Story Structure

$$V_{bo} = f_{so} = \frac{A}{\sigma} w \qquad M_{bo} = h V_{bo}$$

EQ Response of Inelastic Systems

Equation of Motion

$$m\ddot{u} + c\dot{u} + f_s(u, \dot{u}) = p_{\text{eff}}(t) = -m\ddot{u}_g(t)$$

Normalized Yield Strength

$$\bar{f}_y = \frac{f_y}{f_o} = \frac{u_y}{u_o}$$

 f_y and u_y are yield strength and yield displacement. f_0 and u_0 are peak force and deformation in corresponding linear system.

Yield Strength Reduction Factor

$$R_y = \frac{f_o}{f_y} = \frac{u_o}{u_y}$$

$$f_0 = ku_0$$

 f_0 is min strength required for structure to remain elastic.

Ductility Factor

$$\mu = \frac{u_m}{u_v}$$
 (u_m is peak deformation of elastoplastic system)

Response Spectrum for Inelastic Systems

$$D_y = u_y$$
 $V_y = \omega_n D_y$ $A_y = \omega_n^2 D_y$
 $f_y = \frac{A_y}{g} w$ $u_m = \mu \left(\frac{T_n}{2\pi}\right)^2 A_y$

Elastic pseudo-acceleration design spectrum for ground motions with $\ddot{u}_{go}=1$ g, $\dot{u}_{go}=48$ in/s, and $u_{go}=36$ in; $\zeta=5\%$

