

**Homework #7**

Due: Monday, October 20

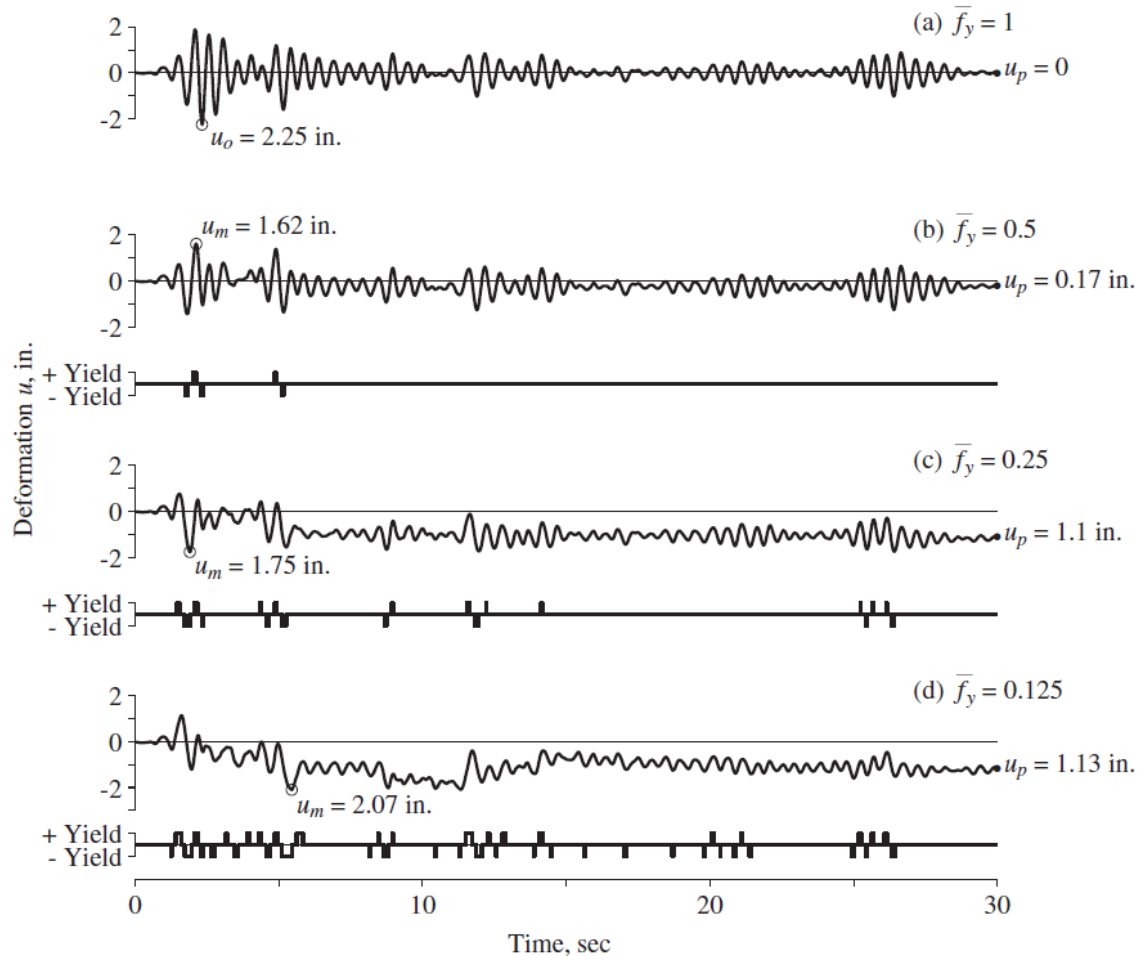
1) The lateral force–deformation relation of the system of a SDOF oscillator is idealized as elastic–perfectly plastic. In the linear elastic range of vibration this SDOF system has the following properties: lateral stiffness  $k = 2.5$  kips/in. and  $\zeta = 5\%$ . The yield strength is  $f_y = 4.0$  kips and the lumped weight  $w = 6000$  lb.

(a) Determine the natural period of this system vibrating at amplitudes smaller than  $u_y$ .

(b) Using plots from the textbook, determine  $\bar{f}_y$  and  $R_y$  for this system subjected to El Centro ground motion scaled up by a factor of 2.

(c) Again using plots from the textbook, estimate the ductility demand  $\mu$ . You may interpolate.

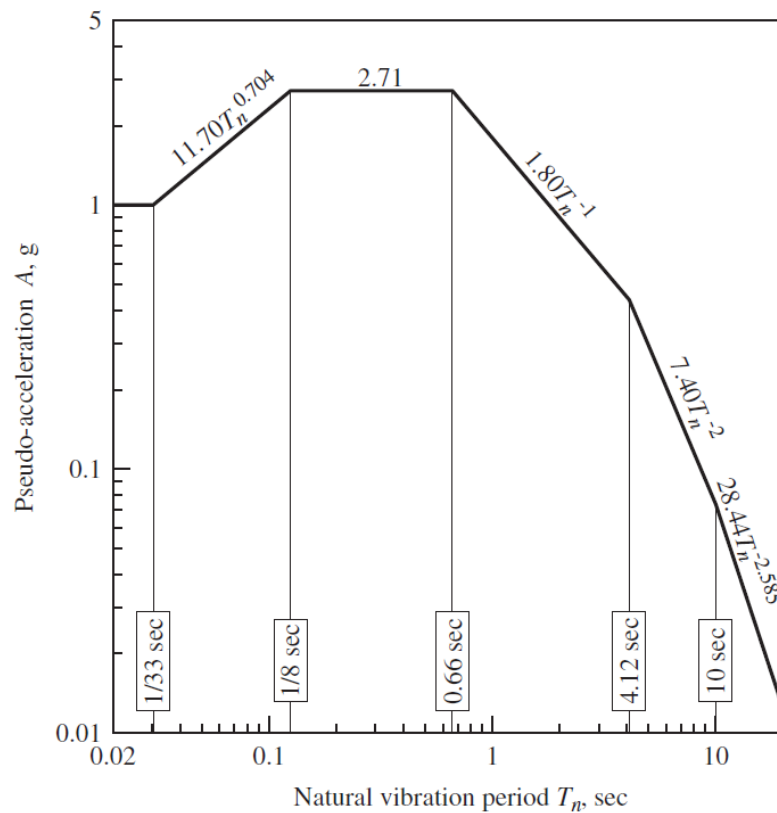
2) From the response results presented below, compute the ductility demands for  $\bar{f}_y = 0.5, 0.25$ , and  $0.125$ .



**Figure 7.4.3** Deformation response and yielding of four systems due to El Centro ground motion;  $T_n = 0.5$  sec,  $\zeta = 5\%$ ; and  $\bar{f}_y = 1, 0.5, 0.25$ , and  $0.125$ .

3) Consider a vertical cantilever tower that supports a lumped weight  $w$  at the top; assume that the tower mass is negligible,  $\zeta = 5\%$ , and that the force–deformation relation is elastoplastic. The design earthquake has a peak ground acceleration of  $0.6g$ , and its elastic design spectrum is given by Fig. 6.9.5 (see below). For three different values of the natural vibration period in the linearly elastic range,  $T_n = 0.1, 0.4$ , and  $2$  sec, determine the lateral deformation and lateral force (in terms of  $w$ ) for which the tower should be designed if (i) the system is required to remain elastic, and (ii) the allowable ductility factor is  $4$ . Comment on how the design deformation and design force are affected by structural yielding.

4) Consider a vertical cantilever tower with lumped weight  $w$ ,  $T_n = 1.5$  sec, and  $f_y = 0.2w$ . Assume that  $\zeta = 5\%$  and assume elastoplastic force–deformation behavior. Determine the maximum lateral deformation using the design spectrum below (Fig. 6.9.5), scaled to a peak ground acceleration of  $0.8g$ .



**Figure 6.9.5** Elastic pseudo-acceleration design spectrum (84.1th percentile) for ground motions with  $\ddot{u}_{go} = 1g$ ,  $\dot{u}_{go} = 48$  in./sec, and  $u_{go} = 36$  in.;  $\zeta = 5\%$ .