

SIS analytic results

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1 General definitions and properties

Following [Tam+22], we define the amplification factor as

$$F(w) = \frac{w}{2\pi i} \int d^2x e^{iw\phi(\mathbf{x})} \quad (1)$$

where the Fermat potential (or time delay) is

$$\phi(\mathbf{x}) = \frac{1}{2}|\mathbf{x} - \mathbf{y}|^2 - \psi(\mathbf{x}) \quad (2)$$

Fourier-transforming $F(w)/w$ we can define

$$I(\tau) \equiv \frac{1}{2\pi} \int d^2x \int_{-\infty}^{\infty} dw e^{iw(\phi(\mathbf{x}) - \tau - t_{\min})} \quad (3)$$

$$= \int d^2x \delta(\phi(\mathbf{x}) - \tau - t_{\min}) \quad (4)$$

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where we have also defined $t_{\min} \equiv \phi_{\min}$. For the SIS we have

$$\psi(\mathbf{x}) = \psi_0 |\mathbf{x}| \equiv \psi_0 x \quad (5)$$

The minimum of the Fermat potential is¹

$$t_{\min} = -\frac{1}{2}\psi_0(2y + \psi_0) \quad (6)$$

$$\mu_{\min} = 1 + \frac{\psi_0}{y} \quad (7)$$

$$x_{1,\min} = y + \psi_0 \quad (8)$$

$$x_{2,\min} = 0 \quad (9)$$

If $y < \psi_0$, there is a second critical point (a saddle point)

$$t_{\text{saddle}} = \frac{1}{2}\psi_0(2y - \psi_0) \quad (10)$$

$$\mu_{\text{saddle}} = \left| 1 - \frac{\psi_0}{y} \right| \quad (11)$$

$$x_{1,\text{saddle}} = y - \psi_0 \quad (12)$$

$$x_{2,\text{saddle}} = 0 \quad (13)$$

2 Time domain

2.1 Final result for a single SIS

The time-domain integral for the SIS is

$$\begin{aligned} I_{\text{SIS}}(\tau) &= \int d^2x \delta(\phi - t) \\ &= \int dx_1 dx_2 \delta\left(\frac{1}{2}x_1^2 - x_1 y + \frac{1}{2}x_2^2 + \frac{1}{2}y^2 - \psi(x) - \tau - t_{\min}\right) \end{aligned} \quad (14)$$

where²

$$\psi(x) = \psi_0 x, \quad t_{\min} = \frac{1}{2}y^2 - \frac{1}{2}(\psi_0 + y)^2 \quad (15)$$

Its solution can be written as

$$I_{\text{SIS}}(\tau) = \mathcal{I}(u, R) \quad (16)$$

where u is the “time parameter” and r is just a constant³

$$u \equiv \frac{\sqrt{2\tau}}{\psi_0 + y} \quad (17a)$$

$$R \equiv \frac{\psi_0 - y}{\psi_0 + y} \quad (17b)$$

The integral can be compactly defined as

$$\begin{aligned} I_{\text{SIS}}(\tau) &= 4 \mathcal{I}(a, b, c, d), \quad (a > b > c > d) \\ &= \frac{8}{\sqrt{(a-c)(b-d)}} \left\{ (b-c) \Pi\left(\frac{a-b}{a-c}, r\right) + c K(r) \right\}, \quad r \equiv \sqrt{\frac{(a-b)(c-d)}{(a-c)(b-d)}} \end{aligned} \quad (18)$$

¹For axisymmetric lenses the magnification can be written as $\mu^{-1} = |1 - \psi'/x| |1 - \psi''|$.

²We will sometimes write $\tilde{\psi}_0 = \psi_0/y$.

³Notice that $R \sim -1 + 2\tilde{\psi}_0$ corresponds to the weak lensing regime while $R \sim 1 - 2/\tilde{\psi}_0$ is the extremely strong lensing regime. $R = 1$ is the caustic.

where Π and K are the complete elliptic integrals of the third and first kind, respectively⁴. We must distinguish three regions

- *Region 1*: ($u > 1$)

$$\begin{aligned} a &= 1 + u & c &= 1 - u \\ b &= R + \sqrt{u^2 + R^2 - 1} & d &= R - \sqrt{u^2 + R^2 - 1} \end{aligned}$$

- *Region 2*: ($\sqrt{1 - R^2} < u < 1$)

– *Case A*: ($R > 0$)

$$\begin{aligned} a &= 1 & c &= \sqrt{1 - u^2} \\ b &= R & d &= -\sqrt{1 - u^2} \end{aligned}$$

– *Case B*: ($R < 0$)

$$\begin{aligned} a &= 1 & c &= -\sqrt{1 - u^2} \\ b &= \sqrt{1 - u^2} & d &= R \end{aligned}$$

- *Region 3*: ($0 < u < \sqrt{1 - R^2}$)

$$\begin{aligned} a &= 1 & c &= R \\ b &= \sqrt{1 - u^2} & d &= -\sqrt{1 - u^2} \end{aligned}$$

2.2 Derivation for region 1

In this region it is more convenient to solve the angular integral first

$$\begin{aligned} I(t) &= \int d^2x \delta(\phi - t) = 2 \int_{-1}^1 \frac{dz}{\sqrt{1 - z^2}} \int_0^\infty r dr \delta\left(\frac{1}{2}r^2 - yrz + \frac{1}{2}y^2 - \psi_0 r - t\right) \\ &= 2 \int_{-1}^1 \frac{dz}{\sqrt{1 - z^2}} \int_0^\infty \tilde{r} d\tilde{r} \delta\left(\frac{1}{2}\tilde{r}^2 - \tilde{r}z + \frac{1}{2} - \tilde{\psi}_0 \tilde{r} - \frac{\tau}{y^2} - \frac{t_{\min}}{y^2}\right) \end{aligned} \quad (19)$$

where we have defined $\psi_0 \equiv \psi_0/y$. Finally we get

$$\begin{aligned} I(\tau) &= 2 \int_{-1}^1 \frac{dz}{\sqrt{1 - z^2}} \int_0^\infty \tilde{r} d\tilde{r} \delta\left\{z - \overbrace{\frac{1}{\tilde{r}} \left(\frac{1}{2}\tilde{r}^2 - \tilde{\psi}_0 \tilde{r} + \frac{1}{2} - \frac{\tau}{y^2} - \frac{t_{\min}}{y^2}\right)}^{z_*}\right\} \\ &= 2 \int_0^\infty \frac{d\tilde{r}}{\sqrt{1 - z_*^2}} \Theta(1 - z_*^2) \end{aligned} \quad (20)$$

We will introduce the following definitions

$$\begin{aligned} a^2 &\equiv \frac{2\tau}{y^2} & \delta &\equiv \tilde{\psi}_0 + 1 \\ z_*^2 - 1 &\equiv \frac{1}{4\tilde{r}^2} \phi_A \phi_B & \delta_{-1} &\equiv \tilde{\psi}_0 - 1 \end{aligned} \quad (21)$$

where (using also $t_{\min}/y^2 = (1 - \delta^2)/2$)

$$\phi_A \equiv 2\tilde{r}(z_* - 1) = \tilde{r}^2 - 2\delta\tilde{r} - (a^2 - \delta^2) \quad (22)$$

$$\phi_B \equiv 2\tilde{r}(z_* + 1) = \tilde{r}^2 - 2\delta_{-1}\tilde{r} - (a^2 - \delta^2) \quad (23)$$

⁴See the appendix for the definitions and the reference for the integral.

The integral can then be rewritten as

$$I(\tau) = 4 \int_0^\infty \frac{\tilde{r} d\tilde{r}}{\sqrt{-\phi_A \phi_B}} \Theta(-\phi_A \phi_B) \quad (24)$$

Equations (20) and (24) are general for any axisymmetric lense. The main simplification for the SIS comes from the fact that ϕ_A and ϕ_B are quadratic and can then be easily factorized, which will allow us to solve the Θ function. In particular, if $a > \delta$ (definition of region 1), we have

$$\phi_A = (r - r_+^A)(r - r_-^A), \quad r_\pm^A = \delta \pm a \quad (25)$$

$$\begin{aligned} \phi_B &= (r - r_+^B)(r - r_-^B), \quad r_\pm^B = \delta_{-1} \pm \sqrt{\delta_{-1}^2 + a^2 - \delta^2} \\ &= \delta - 2 \pm \sqrt{a^2 - 4\tilde{\psi}_0} \end{aligned} \quad (26)$$

In this regime, we can also prove that⁵

$$r_+^A > r_+^B > r_-^A > r_-^B \quad (27)$$

Since $r_-^A < 0$, inside the integral we can only have $r_+^A > r > r_+^B > r_-^A > r_-^B$. Then we get

$$\begin{aligned} I(\tau) &= 4 \int_{r_+^B}^{r_+^A} \frac{r dr}{\sqrt{(r_+^A - r)(r - r_+^B)(r - r_-^A)(r - r_-^B)}} \\ &= 4\mathcal{I}(r_+^A, r_+^B, r_-^A, r_-^B) \end{aligned} \quad (28)$$

2.3 Derivation for regions 2 and 3

For these two regions⁶, it is more convenient to solve the radial integral first. Defining $\delta_z \equiv \tilde{\psi}_0 + z$, we have

$$I(\tau) = 2 \int_{-1}^1 \frac{dz}{\sqrt{1 - z^2}} \int_0^\infty r dr \delta \left(\frac{1}{2} r^2 - \delta_z r + \frac{1}{2} (\delta^2 - a^2) \right) \quad (29)$$

Solving for r , we get

$$I(\tau) = 2 \sum_* \int_{-1}^1 \frac{dz}{\sqrt{1 - z^2}} \frac{r_* \Theta(r_*)}{|r_* - \delta_z|} \quad (30)$$

where

$$\begin{aligned} r_* &= \delta_z \pm \sqrt{\delta_z^2 - \delta^2 + a^2} \\ &= \delta_z \pm \sqrt{(z - z_*^+)(z - z_*^-)}, \quad z_*^\pm = -\tilde{\psi}_0 \pm \sqrt{\delta^2 - a^2} \end{aligned}$$

To compute the limits of the integral we must analyze when the solution exists and is positive. It is useful to study the behaviour of z_*^\pm beforehand. We can prove that $\frac{dz_*^\pm}{d\tilde{\psi}_0} \neq 0$ for $0 < a < \delta$ so

$$\begin{aligned} z_*^+ &\in \left(-\tilde{\psi}_0 \text{ (for } a = \delta), 1 \text{ (for } a = 0) \right) \\ z_*^- &\in \left(-1 - 2\tilde{\psi}_0 \text{ (for } a = 0), -\tilde{\psi}_0 \text{ (for } a = \delta) \right) \end{aligned}$$

⁵It is easy to see that $r_+^A > r_+^B > (r_-^A, r_-^B)$. For the second inequality, we can write

$$r_-^A - r_-^B = 2 - a + \sqrt{(2 - a)^2 + 4(a - \delta)} > 0 \quad \rightarrow \quad r_-^A > r_-^B$$

⁶ $2\sqrt{\tilde{\psi}_0} < a < \delta$ and $0 < a < 2\sqrt{\tilde{\psi}_0}$

and for

$$\begin{aligned} \text{if } \tilde{\psi}_0 > 1 & \rightarrow z_*^+ < -1 \quad \text{for } a > 2\sqrt{\tilde{\psi}_0} \\ \text{if } \tilde{\psi}_0 < 1 & \rightarrow z_*^- > -1 \quad \text{for } a > 2\sqrt{\tilde{\psi}_0} \end{aligned}$$

We are ready to write the final result.

- *Region 2:* $\delta > a > 2\sqrt{\tilde{\psi}_0}$

– *Case A:* $\tilde{\psi}_0 > 1, \quad (1 > z > -1 > z_*^+ > z_*^-)$

$$\begin{aligned} I(\tau) &= 4 \int_{-1}^1 \frac{(z + \tilde{\psi}_0)}{\sqrt{(1-z)(z+1)(z-z_*^+)(z-z_*^-)}} \\ &= 4\mathcal{I}(1, -1, z_*^+, z_*^-) + 4\tilde{\psi}_0 \mathcal{J}(1, -1, z_*^+, z_*^-) \end{aligned}$$

– *Case B:* $\tilde{\psi}_0 < 1, \quad (1 > z > z_*^+ > z_*^- > -1)$

$$\begin{aligned} I(\tau) &= 4 \int_{z_*^+}^1 \frac{(z + \tilde{\psi}_0)}{\sqrt{(1-z)(z-z_*^+)(z-z_*^-)(z+1)}} \\ &= 4\mathcal{I}(1, z_*^+, z_*^-, -1) + 4\tilde{\psi}_0 \mathcal{J}(1, z_*^+, z_*^-, -1) \end{aligned}$$

- *Region 3:* $0 < a < 2\sqrt{\tilde{\psi}_0}, \quad (1 > z > z_*^+ > -1 > z_*^-)$

$$\begin{aligned} I(\tau) &= 4 \int_{z_*^+}^1 \frac{(z + \tilde{\psi}_0)}{\sqrt{(1-z)(z-z_*^+)(z+1)(z-z_*^-)}} \\ &= 4\mathcal{I}(1, z_*^+, -1, z_*^-) + 4\tilde{\psi}_0 \mathcal{J}(1, z_*^+, -1, z_*^-) \end{aligned}$$

3 Frequency domain

The amplification factor for the SIS can be written as

$$F(w) \equiv \frac{w}{2\pi i} \int d^2x e^{iw\phi(\mathbf{x})} \quad (31)$$

$$= \frac{w}{2\pi i} \int_0^{2\pi} \int_0^\infty r dr \exp \left\{ iw \left(\frac{1}{2} r^2 - ry \cos \theta + \frac{1}{2} y^2 - \psi_0 r \right) \right\} \quad (32)$$

$$\begin{aligned} &= e^{iwy^2/2} \frac{w}{i\pi} \int_0^\pi d\theta \left\{ \int_0^\infty r dr \cos \left(\frac{w}{2} r^2 - wr(\psi_0 + y \cos \theta) \right) \right. \\ &\quad \left. + i \int_0^\infty r dr \sin \left(\frac{w}{2} r^2 - wr(\psi_0 + y \cos \theta) \right) \right\} \quad (33) \end{aligned}$$

Defining now

$$\alpha(\theta) \equiv \alpha_0(1 + r \cos \theta) \quad (34)$$

$$\alpha_0 \equiv \psi_0 \sqrt{w/\pi} \quad (35)$$

$$r \equiv y/\psi_0 \quad (36)$$

and using the results in the appendix, we have

$$F(w) = e^{iwy^2/2} \left\{ 1 + \int_0^\pi d\theta \alpha f(-\alpha) - i \int_0^\pi d\theta \alpha g(-\alpha) \right\} \quad (37)$$

Using the symmetry properties of the Fresnel auxiliary functions we can rewrite the two integrals in a more convenient form

$$\int_0^\pi d\theta \alpha g(-\alpha) \stackrel{(r \leq 1)}{=} -I_g(1-r, 1+r, \alpha_0) + \frac{\alpha_0}{2} I_s(1-r, 1+r, \alpha_0^2) + \frac{\alpha_0}{2} I_c(1-r, 1+r, \alpha_0^2) \quad (38)$$

$$\stackrel{(r \geq 1)}{=} -J_g(r-1, r+1, \alpha_0) - J_g(r+1, r-1, \alpha_0) + \frac{\alpha_0}{2} J_s(r-1, r+1, \alpha_0^2) + \frac{\alpha_0}{2} J_c(r-1, r+1, \alpha_0^2) \quad (39)$$

$$\int_0^\pi d\theta \alpha f(-\alpha) \stackrel{(r \leq 1)}{=} -I_f(1-r, 1+r, \alpha_0) - \frac{\alpha_0}{2} I_s(1-r, 1+r, \alpha_0^2) + \frac{\alpha_0}{2} I_c(1-r, 1+r, \alpha_0^2) \quad (40)$$

$$\stackrel{(r \geq 1)}{=} -J_f(r-1, r+1, \alpha_0) - J_f(r+1, r-1, \alpha_0) - \frac{\alpha_0}{2} J_s(r-1, r+1, \alpha_0^2) + \frac{\alpha_0}{2} J_c(r-1, r+1, \alpha_0^2) \quad (41)$$

Each of the integrals is defined as

$$I_s(a, b, \omega) \equiv \int_{a^2}^{b^2} \frac{\sin(\omega u) du}{\sqrt{(b - \sqrt{u})(\sqrt{u} - a)}} = \int_a^b \frac{2\beta \sin(\omega \beta^2) d\beta}{\sqrt{(b - \beta)(\beta - a)}} \quad (42)$$

$$J_s(a, b, \omega) \equiv \int_0^{b^2} \frac{\sin(\omega u) du}{\sqrt{(b - \sqrt{u})(\sqrt{u} + a)}} = \int_0^b \frac{2\beta \sin(\omega \beta^2) d\beta}{\sqrt{(b - \beta)(\beta + a)}} \quad (43)$$

$$I_g(a, b, \alpha) \equiv \int_a^b \frac{d\beta}{\sqrt{(b - \beta)(\beta - a)}} \tilde{g}(\alpha \beta) \quad (44)$$

$$J_g(a, b, \alpha) \equiv \int_0^b \frac{d\beta}{\sqrt{(b - \beta)(\beta + a)}} \tilde{g}(\alpha \beta) \quad (45)$$

with $(a, b, \alpha, \omega > 0)$ and the obvious substitutions $\sin \rightarrow \cos$ and $g \rightarrow f$ for the other half. Using

$$\beta = \frac{b+a}{2} + \frac{b-a}{2} \cos \theta \quad \rightarrow \quad \frac{d\beta}{\sqrt{(b - \beta)(\beta - a)}} = -\text{sign}(\theta) d\theta \quad (46)$$

with $\beta = b \rightarrow \theta = 0$ and $\beta = a \rightarrow \theta = \pi$, we can recover the ‘angular’ integrals. So far, it seems that the best strategy to integrate these expressions at high frequencies is to leave I_f and I_g into their ‘angular’ forms and to rewrite the other two as

$$I_s(a, b, w) = \int_{(a+\Delta)^2}^{(b-\Delta)^2} \frac{\sin(\omega u) du}{\sqrt{(b - \sqrt{u})(\sqrt{u} - a)}} + 2 \int_0^{\theta_b} \beta(\theta) \sin(\omega \beta^2(\theta)) d\theta + 2 \int_{\theta_a}^\pi \beta(\theta) \sin(\omega \beta^2(\theta)) d\theta \quad (47)$$

where $\beta(\theta)$ is defined above and

$$\theta_b = \arccos\left(1 - \frac{2}{b-a}\Delta\right) \quad (48)$$

$$\theta_a = \arccos\left(-1 + \frac{2}{b-a}\Delta\right) \quad (49)$$

$$(50)$$

We can choose Δ as

$$\Delta = \sqrt{\frac{\pi n}{\omega}}, \quad n < \frac{(b-a)^2 \omega}{4\pi} \quad (51)$$

In our case $b = 1 + r$ and $a = 1 - r$ so we can write

$$\beta = 1 + r \cos(\theta) \quad (52)$$

$$\theta_b = \arccos(1 - \Delta/r) \quad (53)$$

$$\theta_a = \arccos(-1 + \Delta/r) \quad (54)$$

$$n < r^2 \frac{\omega}{\pi} \quad (55)$$

For the weak lensing case we can play the same game

$$J_s(a, b, \omega) = \int_0^{(b-\Delta)^2} \frac{\sin(\omega u) du}{\sqrt{(b - \sqrt{u})(\sqrt{u} + a)}} + 2 \int_0^{\theta_b} \beta(\theta) \sin(\omega \beta^2) d\theta \quad (56)$$

where

$$\beta(\theta) = \frac{b-a}{2} + \frac{b+a}{2} \cos(\theta) \quad (57)$$

$$\theta_b = \arccos\left(1 - \frac{2}{b+a} \Delta\right) \quad (58)$$

$$\theta_0 = \arccos\left(-\frac{b-a}{b+a}\right) \quad (59)$$

$$\Delta = \sqrt{\frac{\pi n}{\omega}}, \quad n < \frac{(b-a)^2 \omega}{4\pi} \quad (60)$$

Now we must distinguish two cases (for J_f and J_g). First, if $b = r - 1$ and $a = r + 1$ we have

$$\beta(\theta) = -1 + r \cos(\theta) \quad (61)$$

$$\theta_b = \arccos(1 - \Delta/r) \quad (62)$$

$$\theta_0 = \arccos(1/r) \quad (63)$$

and n is the same as before. The second case is $b = r + 1$ and $a = r - 1$

$$\beta(\theta) = 1 + r \cos(\theta) \quad (64)$$

$$\theta_b = \arccos(1 - \Delta/r) \quad (65)$$

$$\theta_0 = \arccos(-1/r) \quad (66)$$

A Special functions

A.1 Elliptic integrals

From [GR14] we have

$$\begin{aligned} \mathcal{I}(a, b, c, d) &\equiv \int_b^a \frac{x dx}{\sqrt{(a-x)(b-x)(x-c)(x-d)}}, & [\text{GR}, 3.148.6, \text{ p.276}] \\ &= \frac{2}{\sqrt{(a-c)(b-d)}} \left\{ (b-c) \Pi\left(\frac{a-b}{a-c}, r\right) + c K(r) \right\} \\ \mathcal{J}(a, b, c, d) &\equiv \int_b^a \frac{dx}{\sqrt{(a-x)(b-x)(x-c)(x-d)}}, & [\text{GR}, 3.147.6, \text{ p.275}] \\ &= \frac{2}{\sqrt{(a-c)(b-d)}} K(r) \end{aligned}$$

both for $(a > b > c > d)$ and where

$$r = \sqrt{\frac{(a-b)(c-d)}{(a-c)(b-d)}}$$

The complete elliptic integrals are defined as

$$\begin{aligned} K(k) &\equiv \int_0^{\pi/2} \frac{d\alpha}{\sqrt{1-k^2 \sin^2 \alpha}} \\ E(k) &\equiv \int_0^{\pi/2} \sqrt{1-k^2 \sin^2 \alpha} d\alpha \\ \Pi(n, k) &\equiv \int_0^{\pi/2} \frac{d\alpha}{(1-n \sin^2 \alpha) \sqrt{1-k^2 \sin^2 \alpha}} \end{aligned}$$

All three are equal to $\pi/2$ at the origin $n = k = 0$.

A.2 Fresnel integrals

We will follow the DLMF notation [DLM23] for the Fresnel integrals

$$C(z) \equiv \int_0^z \cos\left(\frac{1}{2}\pi t^2\right) dt \quad (67)$$

$$S(z) \equiv \int_0^z \sin\left(\frac{1}{2}\pi t^2\right) dt \quad (68)$$

Other commonly used definitions are

$$C_1(z) \equiv C(\sqrt{2/\pi}z), \quad C_2(z) \equiv C(\sqrt{2z/\pi}) \quad (69)$$

$$S_1(z) \equiv S(\sqrt{2/\pi}z), \quad S_2(z) \equiv S(\sqrt{2z/\pi}) \quad (70)$$

The auxiliary functions are defined as

$$f(z) \equiv \left(\frac{1}{2} - S(z)\right) \cos\left(\frac{\pi}{2}z^2\right) - \left(\frac{1}{2} - C(z)\right) \sin\left(\frac{\pi}{2}z^2\right) \quad (71)$$

$$g(z) \equiv \left(\frac{1}{2} - C(z)\right) \cos\left(\frac{\pi}{2}z^2\right) + \left(\frac{1}{2} - S(z)\right) \sin\left(\frac{\pi}{2}z^2\right) \quad (72)$$

with the symmetries

$$f(-z) = \cos\left(\frac{\pi}{2}z^2\right) - \sin\left(\frac{\pi}{2}z^2\right) - f(z) \quad (73)$$

$$g(-z) = \cos\left(\frac{\pi}{2}z^2\right) + \sin\left(\frac{\pi}{2}z^2\right) - g(z) \quad (74)$$

and derivatives

$$f'(z) = -\pi z g(z) \quad (75)$$

$$g'(z) = \pi z f(z) - 1 \quad (76)$$

From [GR14]

$$\int_0^\infty \sin(ax^2 + 2bx) dx = \sqrt{\frac{\pi}{2a}} f\left(\sqrt{\frac{2}{\pi}} \frac{b}{\sqrt{a}}\right) \quad [\text{GR, 3.693.1, p.417}] \quad (77)$$

$$\int_0^\infty \cos(ax^2 + 2bx) dx = \sqrt{\frac{\pi}{2a}} g\left(\sqrt{\frac{2}{\pi}} \frac{b}{\sqrt{a}}\right) \quad [\text{GR, 3.693.2, p.417}] \quad (78)$$

We can derive both with respect to b to obtain

$$\int_0^\infty x \sin(ax^2 + 2bx) dx = \frac{1}{2a} - \frac{\pi}{2a} \left(\sqrt{\frac{2}{\pi}} \frac{b}{\sqrt{a}} \right) f \left(\sqrt{\frac{2}{\pi}} \frac{b}{\sqrt{a}} \right) \quad (79)$$

$$\int_0^\infty x \cos(ax^2 + 2bx) dx = -\frac{\pi}{2a} \left(\sqrt{\frac{2}{\pi}} \frac{b}{\sqrt{a}} \right) g \left(\sqrt{\frac{2}{\pi}} \frac{b}{\sqrt{a}} \right) \quad (80)$$

We will also use the notation

$$\tilde{g}(z) \equiv zg(z), \quad \tilde{f}(z) \equiv zf(z) \quad (81)$$

We can evaluate the Fresnel integrals using the approximate formulas derived in [Boe60]. In this reference, an approximate expression is found to evaluate

$$f_B(x) = C_2(x) - iS_2(x) \quad (82)$$

that we can also write as

$$e^{ix} f_B(x) = \cos(x)C_2(x) + \sin(x)S_2(x) - i(\cos(x)S_2(x) - \sin(x)C_2(x)) \quad (83)$$

The auxiliary functions can be expressed in terms of this combination as

$$f \left(\sqrt{\frac{2x}{\pi}} \right) = \frac{1}{2} (\cos(x) - \sin(x)) + \Im(f_B e^{ix}) \quad (84)$$

$$g \left(\sqrt{\frac{2x}{\pi}} \right) = \frac{1}{2} (\cos(x) + \sin(x)) - \Re(f_B e^{ix}) \quad (85)$$

So, we can use the results from this reference to approximate f and g as

$$g(x) = \frac{1}{\sqrt{2}} \sin \left(\frac{\pi x^2}{2} + \frac{\pi}{4} \right) - \sqrt{\frac{\pi x^2}{8}} \sum_{n=0}^{11} a_n \left(\frac{\pi x^2}{8} \right)^n \quad (86)$$

$$f(x) = \frac{1}{\sqrt{2}} \cos \left(\frac{\pi x^2}{2} + \frac{\pi}{4} \right) + \sqrt{\frac{\pi x^2}{8}} \sum_{n=0}^{11} b_n \left(\frac{\pi x^2}{8} \right)^n \quad (87)$$

for $0 \leq x \leq 2\sqrt{2/\pi}$, and

$$g(x) = -\sqrt{\frac{8}{\pi x^2}} \sum_{n=0}^{11} c_n \left(\frac{\pi x^2}{8} \right)^n \quad (88)$$

$$f(x) = \sqrt{\frac{8}{\pi x^2}} \sum_{n=0}^{11} d_n \left(\frac{\pi x^2}{8} \right)^n \quad (89)$$

for $x \geq 2\sqrt{2/\pi}$. The coefficients can be found in the original reference. From my experiments, these yield a maximum absolute error of 10^{-8} and a maximum relative error 10^{-6} .

B Sketch of derivation for two SIS with additional symmetries

The main trick for solving the SIS was to convert the integral into a factorization problem for quadratic equations. The same trick can be applied to other systems, in particular to a lense composed of two SIS

$$\phi(\mathbf{x}, \mathbf{y}) = \frac{1}{2} |\mathbf{x} - \mathbf{y}|^2 - \psi_1(|\mathbf{x} - \mathbf{L}/2|) - \psi_2(|\mathbf{x} + \mathbf{L}/2|) \quad (90)$$

in two particular configurations:

- *Configuration x_1* : Both lenses aligned with \mathbf{y} , i.e. in the \hat{x}_1 axis.
- *Configuration x_2* : When \mathbf{y} and the vector \mathbf{L} joining the center of the two lenses are perpendicular, i.e. both lenses at the same x_1 and situated at symmetric positions $x_2^{\text{obs}} + L/2$ and $x_2^{\text{obs}} - L/2$ with respect to the observer (only for equal lenses).

B.1 Alternative coordinate systems

Two-center bipolar coordinates. r_1 is the distance with respect to a point situated in $(L/2, 0)$ and r_2 with respect to a point in $(-L/2, 0)$

$$x_1 = \frac{r_2^2 - r_1^2}{2L} \quad (91)$$

$$x_2 = \pm \frac{1}{2L} \sqrt{4L^2 r_2^2 - (r_2^2 - r_1^2 + L^2)^2} \quad (92)$$

The variable x_2 can be rewritten in a number of ways

$$x_2 = \pm \frac{1}{2L} \sqrt{(r_2^2 - r_1^2 + L^2 + 2Lr_2)(r_1^2 - r_2^2 + 2Lr_2 - L^2)} \quad (93)$$

$$= \pm \frac{1}{2L} \sqrt{(r_2 + r_1 + L)(r_2 - r_1 + L)(r_1 + r_2 - L)(r_1 - r_2 + L)} \quad (94)$$

$$= \pm \sqrt{\frac{1}{2}(r_1^2 + r_2^2) - \frac{1}{4}L^2 - \frac{1}{4L^2}(r_2^2 - r_1^2)^2} \quad (95)$$

The limits are transformed as (check)

$$r_1^{\min} = |r_2 - L| \quad (96)$$

$$r_1^{\max} = r_2 + L \quad (97)$$

Jacobian

$$\frac{\partial x_1}{\partial r_1} = -\frac{r_1}{L} \quad \frac{\partial x_2}{\partial r_1} = \frac{2r_1}{x_2}(r_2^2 - r_1^2 + L^2) \quad (98)$$

$$\frac{\partial x_1}{\partial r_2} = \frac{r_2}{L} \quad \frac{\partial x_2}{\partial r_2} = \frac{4L^2 r_2}{x_2} - \frac{2r_2}{x_2}(r_2^2 - r_1^2 + L^2) \quad (99)$$

so that

$$J = \frac{4Lr_1r_2}{|x_2|} \quad (100)$$

We also have

$$\frac{1}{2}(x_1^2 + x_2^2) = \frac{1}{4}(r_1^2 + r_2^2) - \frac{1}{8}L^2 \quad (101)$$

Rotated version

$$u \equiv \frac{1}{\sqrt{2}}(r_1 + r_2) \ , \quad r_2 = \frac{1}{\sqrt{2}}(v + u) \quad (102)$$

$$v \equiv \frac{1}{\sqrt{2}}(r_2 - r_1) \ , \quad r_1 = \frac{1}{\sqrt{2}}(u - v) \quad (103)$$

The Cartesian coordinates in this system are

$$x_1 = \frac{uv}{L} \quad (104)$$

$$x_2 = \pm \sqrt{\frac{1}{2}(u^2 + v^2) - \frac{1}{4}L^2 - \frac{1}{L^2}u^2v^2} \quad (105)$$

$$= \pm \sqrt{(u + L)(v + L)(u - L)(L - v)} \quad (106)$$

and some other useful combinations are

$$r_2^2 - r_1^2 = 2uv \quad (107)$$

$$r_1 r_2 = -\frac{1}{2}(v^2 - u^2) \quad (108)$$

$$= -\frac{1}{2}\left((v+L)(v-L) - (u+L)(u-L)\right) \quad (109)$$

B.2 Configuration x_1

In this case, it is more convenient to use the two-center bipolar coordinates.

$$\begin{aligned} \phi(x_1, x_2, y) &= \frac{1}{2}(x_1^2 + x_2^2) + \frac{1}{2}y^2 - x_1 y - \psi_1 - \psi_2 \\ &= \frac{1}{4}(r_1^2 + r_2^2) - \frac{1}{8}L^2 + \frac{1}{2}y^2 - \frac{y}{2L}(r_2^2 - r_1^2) - \psi_1(r_1) - \psi_2(r_2) \\ &= \frac{1}{4}(A_+ r_1^2 + A_- r_2^2) - \psi_1(r_1) - \psi_2(r_2) - \frac{L^2}{8}A_+ A_- \end{aligned} \quad (110)$$

where $A_{\pm} \equiv 1 \pm 2y/L$. The complete integral is

$$I(t) = \int d^2x \delta(\phi - t) \quad (111)$$

$$= 8L \int_0^\infty dr_2 \int_{|r_2-L|}^{r_2+L} dr_1 \frac{r_1 r_2}{|x_2|} \delta(\phi - t) \quad (112)$$

If the first lense is a SIS ($\psi_1 = \psi_0^1 r_1$), we can solve the δ function and reduce the problem to a single integral for any axisymmetric lense ψ_2 . Furthermore, if both are SIS, we only have to deal with quadratic equations to obtain the limits, so the problem can be completely solved.

B.3 Configuration x_2

This problem can be reduced to a (bi-)quadratic form using the rotated version of the two-center bipolar coordinates.

$$\begin{aligned} \phi(x_1, x_2, y) &= \frac{1}{2}(x_1^2 + x_2^2) + \frac{1}{2}y^2 - x_2 y - \psi_1 - \psi_2 \\ &= \frac{1}{4}(r_1^2 + r_2^2) - \frac{1}{8}L^2 + \frac{1}{2}y^2 - yx_2 - \psi_1(r_1) - \psi_2(r_2) \\ &= \frac{1}{4}(u^2 + v^2) - \frac{1}{8}L^2 + \frac{1}{2}y^2 \mp \frac{y}{4} \sqrt{\left(\frac{2u^2}{L^2} - 1\right) \left(1 - \frac{2v^2}{L^2}\right)} - \psi_1(r_1) - \psi_2(r_2) \end{aligned} \quad (113)$$

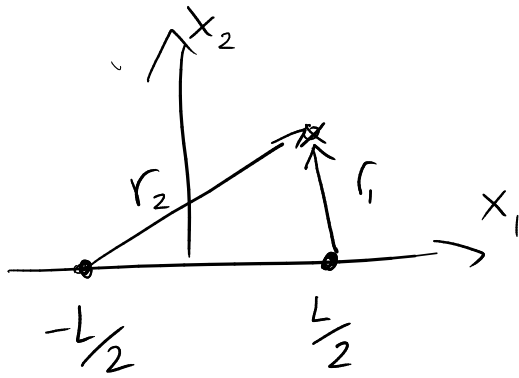
The key simplification for two equal-mass SIS is

$$\psi_1(r_1) + \psi_2(r_2) = \psi_0 r_1 + \psi_0 r_2 = \sqrt{2}\psi_0 u \quad (114)$$

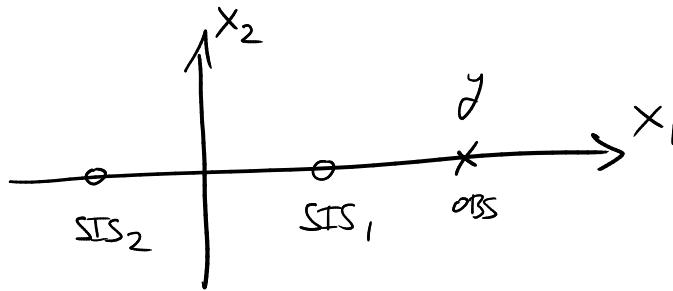
so

$$\phi = \frac{1}{4}(u^2 + v^2) - \frac{1}{8}L^2 + \frac{1}{2}y^2 \mp \frac{y}{4} \sqrt{\left(\frac{2u^2}{L^2} - 1\right) \left(1 - \frac{2v^2}{L^2}\right)} - \sqrt{2}\psi_0 u \quad (115)$$

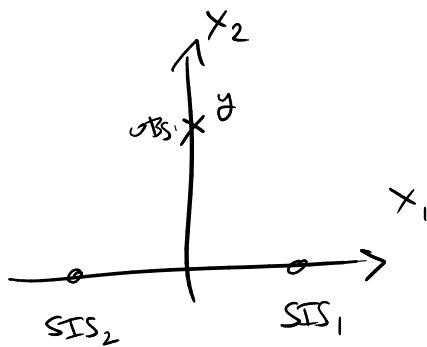
Written in this way, when solving for $\phi = t$ we will get a biquadratic equation for v .



Two-center dipole
coordinates



Configuration x_1



Configuration x_2
($SIS_1 = SIS_2$)

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