

Grinding screen panel comparrison

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Summary

Ten $250\mu M$ screen aperture panels were installed on Grinding Screen 321-SC-014 to compare efficiency with the standard $230\mu M$ apperture panels. No statistically significant difference in overall efficiency and fines recovery were observed between the two types of panels. The effect on the P80 of the underflow was recognized to be important but due to lack of sampling points this could not be safely assessed.

Introduction

Large amounts of fines ($-38\mu M$) are generated and recirculated in the grinding circuit, resulting in over-grinding of the SCheelite contributing to loss of tungsten in the downstream gravity circuit. The Year to date average of $-38\mu M$ material is 30 by weight of grinding thickener underflow solids. Derrick provided $250\mu M$ aperture (0.25 MTQ) screen trial panels to compare efficiency with the currently installed $230\mu M$ aperture (0.23 MT) panels. The calculated open area of the 0.23 MT screen panels is 36.88 % while that of 0.25 MTQ panels is 37.12 %. Note that Q in the [anel code MTQ indicates the **modifier** added to the urethane to make it more resistant to degradation but essentially 0.23 MT and 0.23 MTQ are geometrically similar. This report presents the results of two screen surveys conducted after the installation of the trial panels.

Method

Design of experiment

Include here. . .

I need to do more research here.. What is DOE, How it was done

Should this be part of Method or separate.

formula used by OEM for efficiency calcultions. Not sure if they modeled the data (what model).

Preparation (maybe include in design of experiment?)

Grinding Screens 321-SC-013 and 321-SC-014 were chosen for the comparison test. Ten 0.25 MTQ panels were installed in 321-SC-014 on the 30th of September.

321-SC-013 was also fitted with relatively new 0.23 MT screen panels. The oldest panels were installed 9th September.

Sampling

Survey 1 was conducted while Mill 2 was offline due to an issue with the mill liners. Survey 2 conducted with two secondary mills online but with higher than usual recirculating load. During the surveys, feed to the mills and recirculating load were steady for at least an hour.

Five (5) personnel were involved in obtaining the survey samples during each survey:

- One person took samples at the Primary Distributor, DI-028, that feeds the seven screen sets.
- Four personnel took overflow cuts from the individual screen decks' lips using deep and wide rimmed plastic containers. care was given to cut streams entirely at constant speeds while ensuring no container overflow or spillage. Samples were simultaneously taken from both sides of individual screen decks by two personnel and then individual deck's samples were combined.

Two sample cuts were taken from the feeds of 321-SC-013 and 321-SC-014, as well as from the individual deck lip overflows.

Screen cluster feed and individual deck overflow samples were weighed, wet screened to get $-38\mu m$ fractions, dried in the oven and sieved to determine the weight of each size fraction.

The following screens sizes were used (μM)

```
## sieves_used
##      0   38   53   75  106  150  180  212  300  425  600 1180
##      1    1    1    1    1    1    1    1    1    1    1    1
```

Each stream sample's cumulative mass distribution function was modelled with two commonly used models in practise represent a vast variety of comminution circuit products very well, namely the:

Rosin-Rammler distribution and
Gauss-Gaudin-Schumann distribution.

The model that best fit each stream was selected with the aid of statistics. The modeled distribution functions enabled more accurate interpolation of cumulative mass percentages.

Interpolation of points following the modelled distributions could then be used to determine screen efficiency and subsequent efficiency comparison between the screens fitted with the 0.23 MT and the 0.24 MTQ panels.

insert table

Model formulas

Rosin Rammler (RR) Model:

The RR model distribution function has been used to describe the particle size distributions of various minerals, powders and liquids of various types and sizes. The function is particularly suited to represent those produced by grinding, milling, and crushing operations. The general expression of the RR model is:

$$F(d) = \exp \left[-\left(\frac{d}{\bar{d}}\right)^m \right]$$

where:

$F(d)$ = distribution function (cum. passing)

d = particle size [mm]

Parameters \bar{d} and m are adjustable parameters characteristic of the distribution.

\bar{d} = scale parameter (mean particle size [mm]) and $= \exp \left(-\frac{\text{intercept}}{\text{slope}} \right)$.

m = slope parameter (measure of the spread of particle sizes).

The RR transformation is achieved by taking the natural log twice and simplified as:

$$\ln \{ -\ln [1 - F(d)] \} = m \times \ln d - m \times \ln \bar{d}$$

Note that the RR distribution transformation is conducted on the cumulative retained distribution (thus the $[1 - F(d)]$.)

If a distribution plots a straight line after the above RR transformation, then the distribution can be represented by the RR distribution function. This will allow percentile interpolation according to the distribution and not a straight line between two points obtained from screening.

$$Y = mX + C$$

$$\underbrace{\ln \{ -\ln [1 - F(d)] \}}_Y = \underbrace{m}_{\text{slope}} \times \underbrace{\ln d}_X + \underbrace{(-m \times \ln \bar{d})}_C$$

Back-transformation (This is really the reason why we're doing the model fitting; so that we can better estimate the size at which a certain specified mass fraction will pass). The back-transform is then conducted to determine the required percentile values:

$$x = \bar{d} (-\ln(1 - Y))^{\frac{1}{m}}$$

$$\text{size} = \text{scaleparameter} \times (-\ln(1 - \text{percentile}))^{1/\text{slopeparameter}}$$

, where the scale_parameter; is a function of the slope and intercept of the transformed RR model fit, as follows:

$$\text{scaleparameter} = \exp \left(-\frac{\text{intercept}}{\text{slope}} \right)$$

Gates-Gaudin-Schumann (GGS) Model:

The Gates-Gaudin-Schumann plot is a graph of **cumulative % passing versus nominal sieve size**, with both the X and Y axes being logarithmic plots. In this type of plot, most of the data points (except for the two or three coarsest sizes measured) should lie nearly in a straight line.

$$y = F(x) = \left(\frac{x}{k} \right)^n$$

or similarly: The above formula can be rewritten as: $x = k \times y^{\frac{1}{n}}$

where:

$y = F(x)$ = cumulative undersize distribution function.

x = particle size,

k = maximum particle size of the transformed straight line corresponding to 100 cum. passing.

Log transformation of the distribution yields:

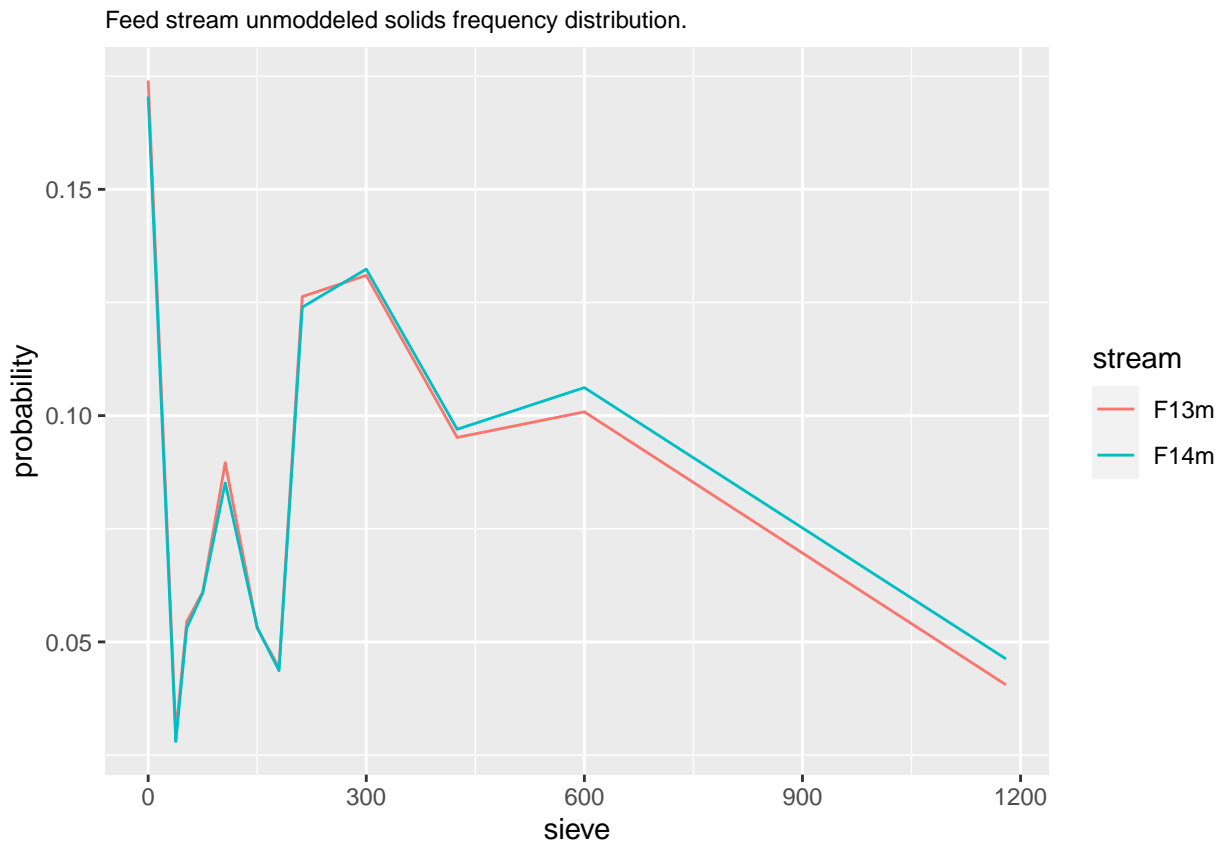
$$\ln y = n \ln x - n \ln k$$

Applying this transformation to the measured observed distribution data points will yield near straight lines if the data fits the model, and interpolation on along a straight line is much easier than along the curved arithmetic distribution function.

RR model fits the feed streams means (F13m and F14m) better (near straight line QQ fits) than the Oversize streams.

Results and Discussion

Each test's feed stream PSD results were first compared to confirm that their distributions were similar to allow for comparative statistics.



The two most commonly used distributions in Geology and Mineral Processing and specifically comminution circuits are the Rosin-Rammler and the Gates-Gaudin-Schumann distributions.

Both models were used to model all PSD screening data to, and the subsequent best fit model was selected in each case. Model selection was determined by comparing each PSD's transformed linear model's determinant (R^2).

If the transformed size distributions from a crushing or grinding operation do not approximate a straight line, it suggests that there may have been a problem with the data collection, or there is something unusual happening in the comminution process (hang-ups or unusual recirculation). The size modulus is a measure of how coarse the size distribution is, and the distribution modulus is a measure of how broad the size distribution is. Size modulus for a size distribution can be determined from a graph by extrapolating the straight-line portion up to 100% passing and finding the corresponding size value. The distribution modulus can be calculated by choosing two points in the linear portion of the graph, calculating the logs of the sizes and % passing values, and calculating the slope.

Interpolation between measured sizing points is conducted by the back-transformation of the model-fitted points along the respective model's distribution function.

Table 1: RR Model(formula)

stream	r.squared	adj.r.squared	provalue	AIC
F13m	0.996	0.995	0	-26.0
F14m	0.996	0.995	0	-25.7
OS13m	0.935	0.928	0	11.2
OS14m	0.919	0.910	0	14.2
US13m	0.972	0.968	0	0.8
US14m	0.971	0.967	0	0.5

Table 2: GGS Model(formula)

stream	r.squared	adj.r.squared	provalue	AIC
F13m	0.838	0.820	0.0001	14.4
F14m	0.839	0.821	0.0001	13.4
OS13m	0.682	0.646	0.0017	17.0
OS14m	0.655	0.617	0.0025	16.9
US13m	0.778	0.750	0.0007	38.8
US14m	0.764	0.735	0.0009	40.0

To Do

lots of advice to follow here

<https://holtzy.github.io/Pimp-my-rmd/>

https://cran.r-project.org/web/packages/kableExtra/vignettes/awesome_table_in_html.html

Data

Write up

Im not too happy with the layout structure and flow. compare with professional technical report in the industry.

Tables, Plot, Figs, Formulas

Plot

move plot (unmodelled psd) out of “sampling” section; should be in results. this same plot can be plot next to the OS and US streams. Then do the same for the modelled streams.

Formulas

- double check RR Latex formula in (d/l?)

$$F(d) = \exp \left[-\left(\frac{d}{l}\right)^m \right]$$

- add regression formulas that include the coefficients
- result, discussion section?

Tables

- add row in distribution figures
- wrap text in col names of R2 tables <https://community.rstudio.com/t/wrap-column-name-in-pdf-table-from-knitr-kable/3278/4> +also add latex formulas
- repair layout of model coef tables in "Results and Discussion" section:
- fix rounding
- fix layout

The RR transformation is achieved by taking the natural log twice and simplified as: #

$$\ln \{-\ln [1 - F(d)]\} = m \times \ln d - m \times \ln \bar{d}$$