## Deriving the Shell Crossing Time as a Function of the Density

ABSTRACT

The goal of this derivation to estimate the time it will take a reverse shock to cross incoming ejecta material.

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#### 1. INTRODUCTION

In the refreshed shock model, the wind of a GRB 8 can be separated into two regions, (i) early outflow <sub>9</sub> launched with  $\bar{\Gamma} \sim 150$  and (ii) later ejecta launched <sub>10</sub> launched with  $\bar{\Gamma} \sim 15$ . The early material is responsible 11 for producing the prompt emission and the afterglow 12 continuum emission. The later ejecta will eventually 13 catch up to the early ejecta as it sweeps up circum-14 burst medium and decelerates. When the later ejecta 15 catches up and collides with the early material, a "re-16 freshed" shock occurs, injecting energy into the front of 17 the outflow and may be witnessed as bumps in the af-18 terglow light curves (potentially in the optical regime). 19 In this work, we would like to estimate the time it takes 20 the incoming energy injected from the later ejecta to 21 be distributed across the newly shocked material. This 22 timescale should be dominated by the shell crossing time  $_{23}$   $t_{\Delta}$ , where we model the incoming late ejecta as a shell <sup>24</sup> with width  $\Delta$ , density  $n_4$ , and Lorentz factor  $\gamma_4 \sim 15$ . To estimate  $t_{\Delta}$ , we must estimate the density of the  $_{26}$  rapid material  $(n_4)$  and the material which the late 27 ejecta is colliding with  $(n_1)$ .

### 28 2. ESTIMATING DENSITY OF ZONE 1 MATERIAL

The material that the late ejecta is colliding with is composed of early ejecta material that has been crossed by the reverse shock and has time had time to relax. The average particle density of this material  $n_1$  (fluid frame) can be approximated as,

$$n_{\rm ej}(t) = n_1(t) = \frac{E_{\rm iso}\Gamma(t)}{4\pi m_{\rm p}c^2\Gamma_0 R(t)^2 \Delta_1(t)}$$
 (1)

$$\frac{35}{36}$$
 (2)

where R(t) is the distance of the material from the central engine,  $E_{\rm iso}$  is the isotropic equivalent energy,

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 $_{59}$   $\Gamma_0$  is the initial bulk Lorentz factor of the ejecta, and  $_{40}$   $\Gamma(t)$  is the bulk Lorentz factor as a function of time (all  $_{41}$  in the central engine frame).  $\Delta_1(t)$  is the initial width  $_{42}$  of the material.

 $_{43}$   $\Delta_1(t)$  can take two extremes, if we assume that the  $_{44}$  early material relaxes as it propagates along the jet then  $_{45}$   $\Delta_1(t)\approx R(t)/\Gamma_1^2(t),$  and the density approximations be-  $_{46}$  comes

$$n_{1,\min}(t) = \frac{E_{\rm iso}\Gamma(t)}{4\pi m_{\rm p}c^2\Gamma_0 R(t)^3}$$
 (3)

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In the other extreme, if the material does not relax and the width of the material is approximately  $\Delta \sim \beta_0 c t_{\rm inj}$  where  $t_{\rm inj}$  is the duration of the injection time and  $\beta_0 = \sqrt{1-1/\Gamma_0^2}$ . This makes the approximation of the density

$$n_{1,\text{max}}(t) = \frac{E_{\text{iso}}\Gamma(t)}{4\pi m_{\text{p}}c^3\Gamma_0 R(t)^2 t_{\text{inj}}}$$
 (5)

$$\frac{56}{6}$$
 (6)

We can estimate this density using a fiducial val-<sup>59</sup> ues  $E_{\rm iso}=10^{53}$  erg/s,  $\Gamma_0=150,~R(t_{\rm coll})=10^{17}$  cm, <sup>60</sup>  $\Gamma(t_{\rm coll})=5,~{\rm and}~t_{\rm inj}=20$  sec, which leads to a density <sup>61</sup> estimate of  $n_{1,\rm min}=1.8\times10^2~{\rm cm}^{-3}$  and  $n_{1,\rm max}=3\times10^7$ <sup>62</sup> cm<sup>-3</sup>.

#### 3. ESTIMATING THE SHELL CROSSING TIME

The width of the late time ejecta can be described as

$$\Delta(t) = \Delta_0 + R(t)/\gamma^2(t) \tag{7}$$

where  $\Delta_0 = \beta c t_{\rm inj}$  is the approximate width of the material launched from the central engine over an interval  $t_{\rm inj}$  and  $R(t)/\gamma^{\rm t}(t)$  accounts for the spread of the material as it propagates away from the central engine. The minimum width assumes there is no spreading, i.e.,

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 $_{72}$   $\Delta_{\min} \approx \Delta_0$ . The maximum width will be dominated by  $_{73}$  the spread  $\Delta_{\max} \approx R(t)/\gamma^2(t)$ . For the relevant param-74 eter values of our scenario

$$\Delta_{\min} \approx 6 \times 10^{11} \text{ cm}$$
 (8)

$$\Delta_{\text{max}} \approx 4.5 \times 10^{14} \text{ cm} \tag{9}$$

Following Sari and Piran 1995 (hereafter SP95), the observed timescale of emission is

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$$\Delta t_{\rm obs} = R_{\rm e}/\gamma_4^2 c \tag{10}$$

$$= \begin{cases} \Delta/c, & \text{if } \xi < 1 \text{ (Relativistic)} \\ l\gamma^{8/3}c, & \text{if } \xi > 1 \text{ (Newtownian)} \end{cases}$$
 (11)

where  $l=(E/n_1m_{\rm p}c^2)$  is the Sedov length and we have replaced their  $\gamma_2$  with  $\gamma_4$  as the relevant Lorentz factor for our incoming thin-shell situation. According to the density ratio we are within the relativistic regime, i.e.,  $f=n_4/n_1<<\gamma^2$ , but when estimating the dimensionless quantity  $\xi=(l/\Delta)^{1/2}\gamma^{-4/3}$  we are in the commonly in the Newtownian regime, i.e.,  $\xi>1$ . Luckily, we do no have to worry about this, because estimating  $\Delta t_{\rm obs}$  in the relativistic regime using  $\Delta_{\rm min}$  and  $\Delta_{\rm max}$  encompasses the Newtownian estimate.

For our situation, we would like  $\Delta t_{\rm obs} = \Delta/c \lesssim 3 \times 10^4$  sec, which gives the upper limit to the shell width  $\Delta \lesssim$  9× 10<sup>14</sup> cm, which is greater than  $\Delta_{\rm max}$ . So, I think we are good.

# 4. ESTIMATING SPREAD OF THE LORENTZ FACTOR

We can use the spread of the late time material as an upper limit to what the possible spread of the Lorentz factor can be in the late material. Consider two photon launched at the same time and position with Lorentz factor  $\gamma$  and  $\gamma + \delta \gamma$ . At a later time t, the distance between the two photons can be expressed as

$$\Delta = \beta_{\rm f} c t - \beta_{\rm s} c t \tag{12}$$

$$= ct \left[ \left( 1 - \frac{1}{2(\gamma + \delta \gamma)^2} \right) - \left( 1 - \frac{1}{2\gamma^2} \right) \right]$$
 (13)

$$\approx R \frac{\delta \gamma}{\gamma^3} \tag{14}$$

where  $\beta_{\rm f}$  and  $\beta_{\rm s}$  are the defined for the faster and slower photons, respectively. The dynamical timescale of the system is determined by the Lorentz factor of the early material. In principle, the early material is constantly decelerating as it sweeps up circumburst material, but to an order unity we can write

$$t_{\rm dyn} \approx \frac{R}{2c\gamma_1^2}$$
 (15)

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$$\Rightarrow \frac{R}{c} \approx 2\gamma_1^2 t \tag{16}$$

Substituting Equation 14 and 16 into Equation 10 (assuming we are in the relativistic regime), we obtain

$$\Delta t_{\rm obs} = \frac{\Delta}{c} \tag{17}$$

$$=\frac{R}{c}\frac{\Delta\gamma}{\gamma^3}\tag{18}$$

$$=2t\frac{\Delta\gamma}{\gamma}\left(\frac{\gamma_1}{\gamma}\right)^2\tag{19}$$

$$\frac{\Delta t}{t} = 2 \frac{\Delta \gamma}{\gamma} \left(\frac{\gamma_1}{\gamma}\right)^2 \tag{20}$$

Using the observed timescale from the rise times of the jumps in the light of GRB 030329, i.e.,  $\Delta t_{\rm obs}/t_{\rm obs} \sim$  127 0.3, and assuming that the early and late ejecta have a Lorentz factor ratio of  $\gamma_1/\gamma_4 \sim 1/3$  (or  $\sim 1/2$ ), we can constrain the spread of the Lorentz factors as a function of the average Lorentz factor, i.e.,  $\delta \gamma/\gamma \sim 1.14$  (or  $\sim$  131 0.6).