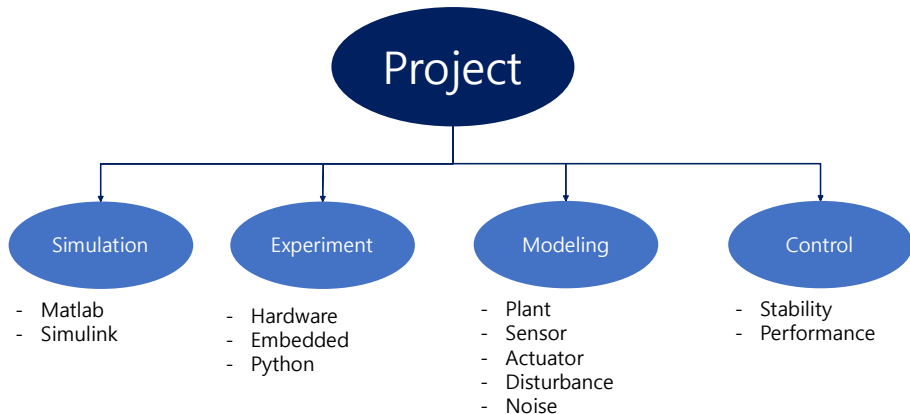


캡스톤 디자인 최종발표

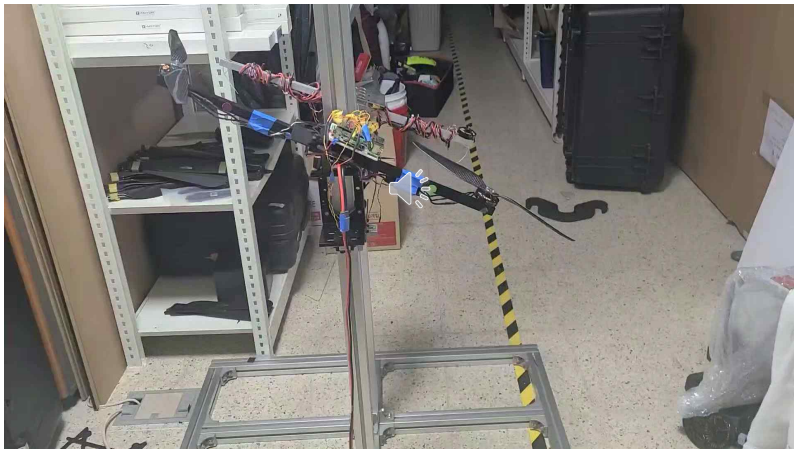
강민구, 박주형, 허홍석

Louis Vuitton

목표

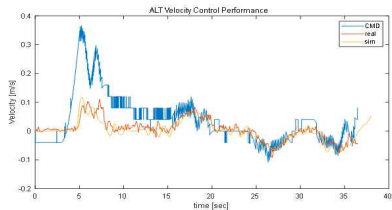
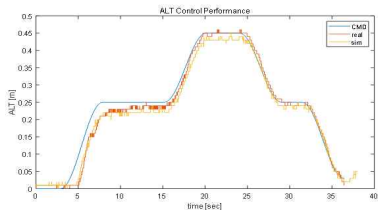
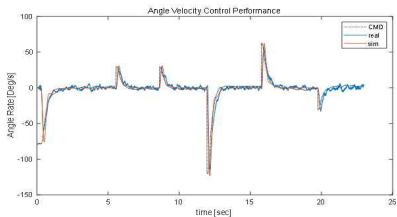
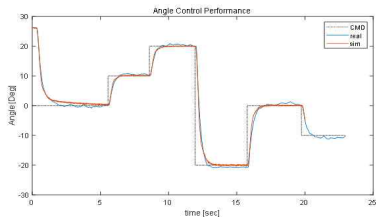


실험 영상



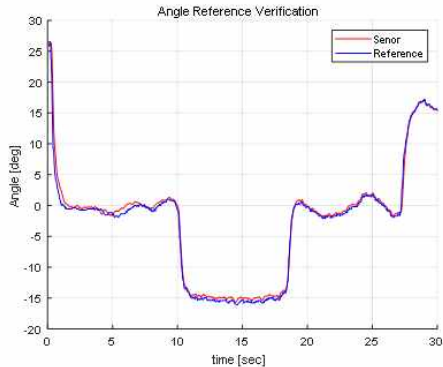
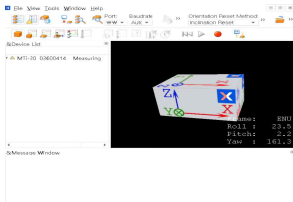
실험 결과

Angle, Height control : experiment & simulation



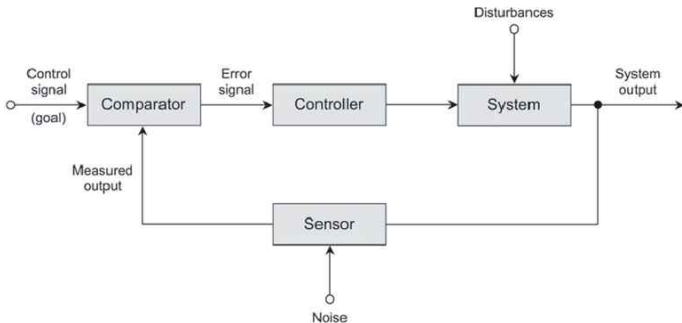
실험 결과

comparison with reference angle



System modeling

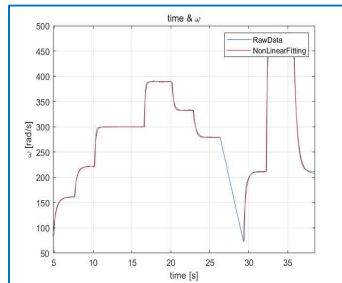
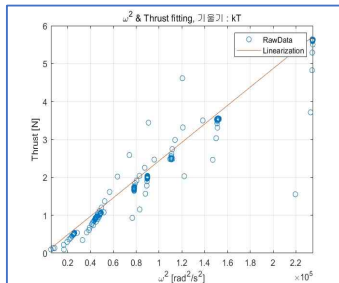
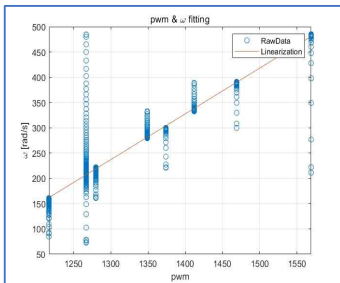
Modeling error



- Sensor modeling
- Plant modeling
- Disturbance
- Noise
- Discrete sampling time

Actuator modeling

Thrust & Propeller test



$$\omega = a \cdot pwm + b$$

$$F = k_T \cdot \omega^2 \quad \longrightarrow \quad Actuator(s) = \frac{K}{\tau s + 1}$$

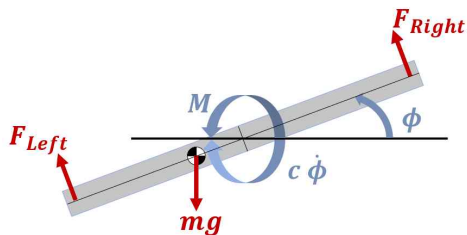
$$\tau = 0.2sec$$

Table 1 Actuator parameter

a	$0.90555s^{-1}$
b	$-940.17s^{-1}$
k_T	$2.4344 \times 10^{-5} kg \cdot m$
τ	$0.2s$

Plant modeling

Dynamic equations



$$m\ddot{z} = F\cos\phi - mg$$

$$I\ddot{\phi} = M - c\dot{\phi} - mgd\cos\phi$$

$$\omega = a \cdot pwm + b$$

$$F = F_{Right} + F_{Left}$$

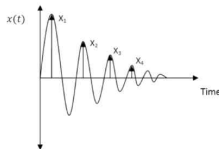
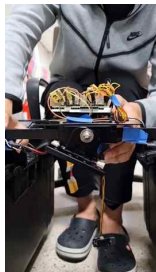
$$= k_T(\omega_{right}^2 + \omega_{left}^2)$$

$$M = (F_{Right} - F_{Left})l$$

$$= k_T l(\omega_{right}^2 - \omega_{left}^2)$$

Plant parameter

experimental measurement



Logarithmic decrement method

$$\delta = \frac{1}{n} \ln \left| \frac{x_1}{x_{n+1}} \right|$$

$$\text{Damping} = \zeta = \frac{\delta}{\sqrt{4\pi^2 + \delta^2}}$$

$$m\ddot{z} = F\cos\phi - mg$$

$$I\ddot{\phi} + c\dot{\phi} + mgd\cos\phi = M$$

$$\omega = a \cdot pwm + b$$

$$F = k_T (\omega_{right}^2 + \omega_{left}^2)$$

$$M = k_T l (\omega_{right}^2 - \omega_{left}^2)$$

Table 2 Plant parameter

m	$1.45kg$
d	$4mm$
l	$280mm$
c	$0.00019kg \cdot m/s$
I	$0.015kg \cdot m^2$

$$J = \frac{mgD^2}{16\pi^2 f_n^2 h} = \frac{0.895kg \times 9.81m/s^2 \times (0.56m)^2}{16\pi^2 \times (1.37s^{-1})^2 \times (0.62m)} = 0.015kg \cdot m^2$$

$$\delta = 0.289$$

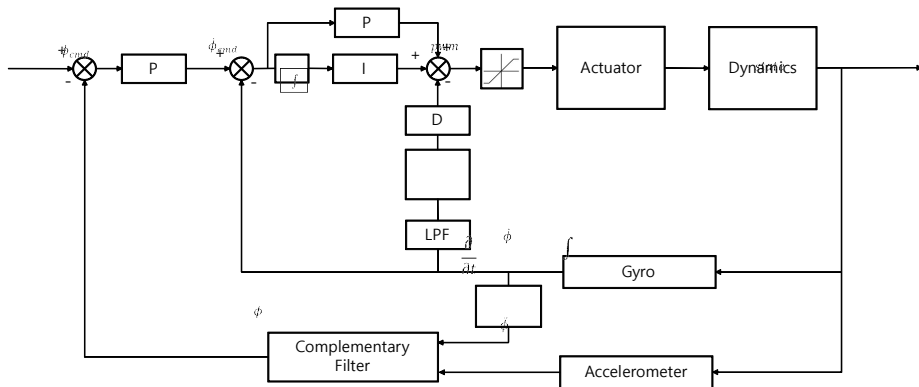
$$\zeta = \frac{0.288}{\sqrt{4\pi^2 + 0.288^2}} = 0.0458$$

$$c = 2 \times J \times \zeta \times \omega_n = 2J\zeta \frac{\omega_d}{\sqrt{1 - \zeta^2}}$$

$$= 2 \times 0.00014 \times 0.0458 \times 14.526 = 0.00019kg \cdot m^2/s$$

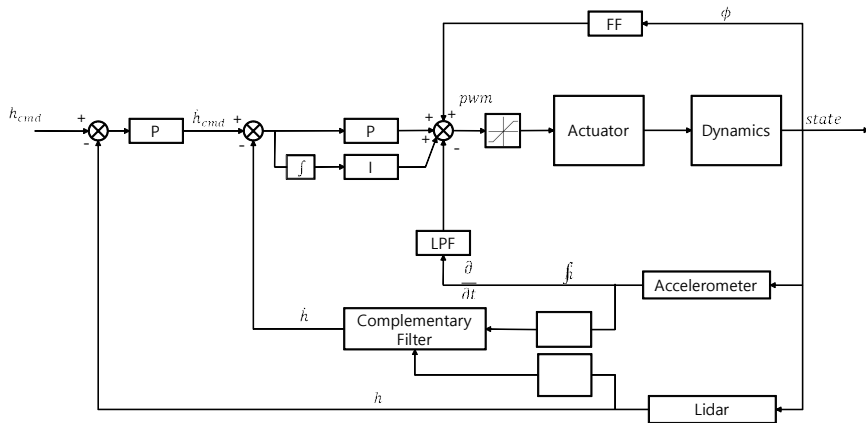
Controller diagram

Attitude controller



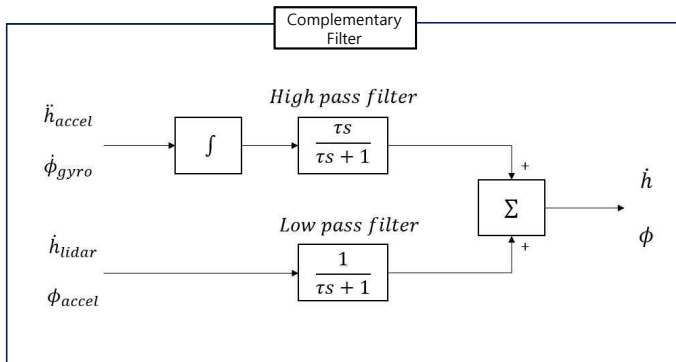
Controller diagram

Position controller



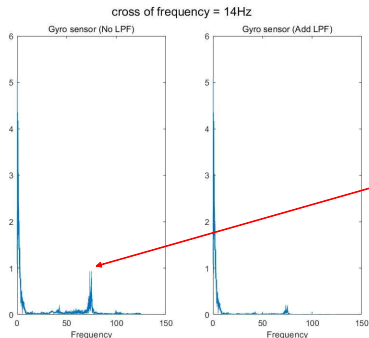
Complementary filter

height rate & angle



Low pass filter

Fourier transform



프로펠러 회전에 의한 노이즈 성분

propeller rotation speed = 453rad/s

$$\frac{1}{\tau s + 1}$$

$$f = \frac{\omega}{2\pi} = 72.3\text{Hz}$$

주파수의 1/5에 해당하는 지점에 교차주파수 설정

$$\omega_{\text{cross}} = 85.7\text{rad/s}$$

Low pass filter



Embedded code

Sampling time (dt) = 5ms

Low pass filter

$$\frac{y(s)}{u(s)} = \frac{1}{\tau s + 1}$$

$$y(s)(\tau s + 1) = u(s)$$

$$\tau \frac{dy}{dt} + y = u$$

$$\tau \frac{y_i - y_{i-1}}{dt} + y_i = u_i$$

$$\tau y_i - \tau y_{i-1} + y_i dt = u_i dt$$

$$y_i(\tau + dt) = \tau y_{i-1} + u_i dt$$

$$y_i = \frac{\tau}{\tau + dt} y_{i-1} + \frac{dt}{\tau + dt} u_i$$

$$y_i = \alpha y_{i-1} + (1 - \alpha) u_i$$

Complementary filter

$$y(s) = \frac{\tau s}{\tau s + 1} \frac{u_1(s)}{s} + \frac{1}{\tau s + 1} u_2(s)$$

$$(\tau s + 1)y(s) = \tau u_1(s) + u_2(s)$$

$$\tau \frac{dy}{dt} + y = \tau u_1 + u_2$$

$$\tau \frac{y_i - y_{i-1}}{dt} + y_i = \tau u_1 + u_2$$

$$\tau(y_i - y_{i-1}) + y_i dt = \tau u_1 dt + u_2 dt$$

$$y_i(\tau + dt) = \tau y_{i-1} + \tau u_1 dt + u_2 dt$$

$$y_i = \frac{\tau}{\tau + dt} (y_{i-1} + u_1 dt) + \frac{dt}{\tau + dt} u_2$$

$$y_i = \alpha (y_{i-1} + u_1 dt) + (1 - \alpha) u_2$$

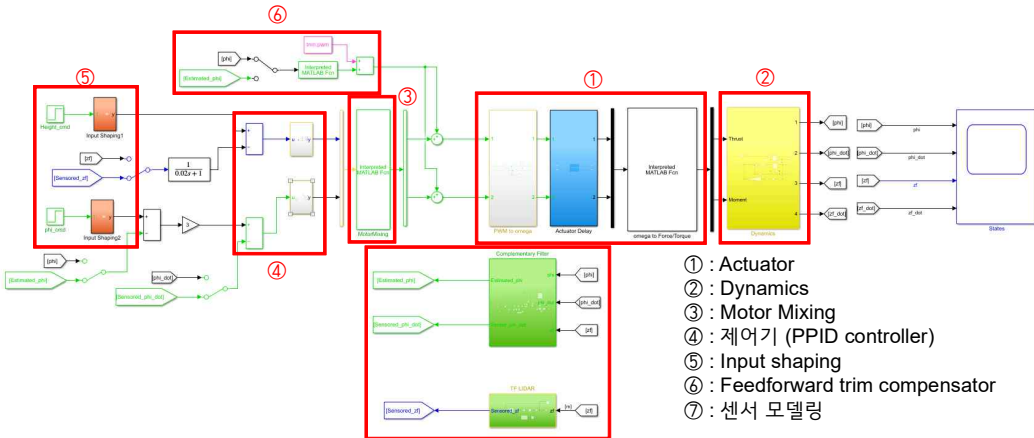
backward difference method

```
def dispPID(CMD, distance, z2dot, dt, kp1, kp2, ki1, kd1, tau, d_tau):
    global comp_vel, predistance, H_item, H_dterm_prev, distance_vel_prev
    height_Error = CMD - distance
    VelCMD = height_Error * kp1
    vel = (distance - predistance)/dt
    distance_vel = (distance - predistance)/dt
    distance_vel = tau*distance_vel_prev + (1-tau)*(distance_vel)
    distance_vel_prev = distance_vel
    predistance = distance
    comp_vel = tau * (comp_vel + z2dot*dt) + (1-tau)*(distance_vel)
    VelError = VelCMD - comp_vel
    pterm = VelError * kp2
    H_item += ki1 * VelError * dt
    dterm = -kd1 * z2dot
    H_dterm_LPF = d_tau*(H_dterm_prev) + (1-d_tau)*(dterm)
    H_dterm_prev = H_dterm_LPF
    output = pterm + H_item + H_dterm_LPF
    output = min(output, 100)
    output = max(output, -100)
    return output, VelCMD, pterm, H_item, dterm, comp_vel, H_dterm_LPF
```

```
def PPID(CMD, roll, gyro, dt, kp1, kp1_1, ki1, kd1, tau2):
    global item1, prevgyro, dterm_prev, RateCMD
    PPID_Error = CMD - roll
    RateCMD = kp1 * PPID_Error
    RateError = RateCMD - gyro
    RateDelta = gyro - prevgyro
    prevgyro = gyro
    pterm1 = kp1_1 * RateError
    item1 += ki1 * RateError * dt
    dterm_now = -kd1 * (RateDelta)/dt
    dterm_LPF = tau2 * dterm_prev + (1-tau2) * dterm_now
    dterm_prev = dterm_LPF
    item1 = max(item1, -30)
    item1 = min(item1, 30)
    dterm_LPF = max(dterm_LPF, -50)
    dterm_LPF = min(dterm_LPF, 50)
    output = pterm1 + item1 + dterm_LPF
    output = min(output, 100)
    output = max(output, -100)
    return output, RateCMD, pterm1, item1, dterm_now, dterm_LPF
```

Simulation structure

Simulink



- ① : Actuator
- ② : Dynamics
- ③ : Motor Mixing
- ④ : 제어기 (PID controller)
- ⑤ : Input shaping
- ⑥ : Feedforward trim compensator
- ⑦ : 센서 모델링

제어기 설계

Transfer function

$$\begin{aligned} \dot{x} &= f(x, u) \\ y &= h(x, u) \end{aligned} \longrightarrow \begin{aligned} \dot{x} &= A x + B u \\ y &= C x \end{aligned}$$

$$f(x, u) = f(x_0, u_0) + \frac{\partial f}{\partial x} x + \dots$$

$$x_0 = \begin{bmatrix} \phi_0 \\ \dot{\phi}_0 \\ z_0 \\ \dot{z}_0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

시스템 선형화

$$G(s) = C(sI - A)^{-1}B$$

↓
ss2tf

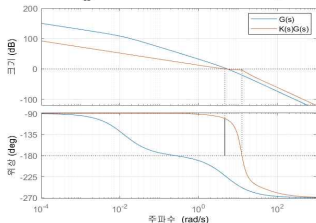
$$G_1(s) = \frac{\phi(s)}{\phi_{cmd}(s)} = \frac{203.6}{s^3 + 5.013s^2 + 0.0633s}$$

$$G_2(s) = \frac{h(s)}{h_{cmd}(s)} = \frac{0.1313}{s^3 + 5s^2}$$

제어기 설계

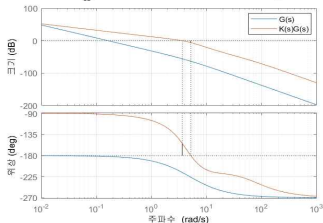
controller design

$\omega_{\infty} = 4.63\text{rad/s}$ GM = 4.88dB PM = 79.3deg



Alt controller design

$\omega_{\infty} = 3.62\text{rad/s}$ GM = 5.94dB PM = 26.5deg

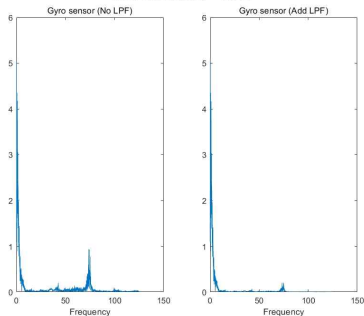


K_{P1}	4
K_{P2}	0.7
K_D	0.01
K_I	0.25

K_{P1}	4
K_{P2}	150
K_D	7
K_I	7

bode plot

cross of frequency = 14Hz



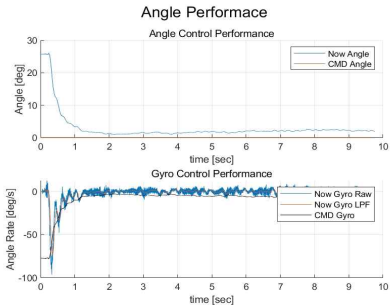
$$S_G^C = \frac{G}{C} \frac{\partial C}{\partial G} = \frac{1}{1+GH} \quad \longrightarrow \quad \lim_{GH \rightarrow \infty} S_G^C = 0$$

$$S_H^C = \frac{H}{C} \frac{\partial C}{\partial H} = -\frac{GH}{1+GH} \quad \longrightarrow \quad \lim_{GH \rightarrow \infty} S_H^C = -1$$

제어기 설계

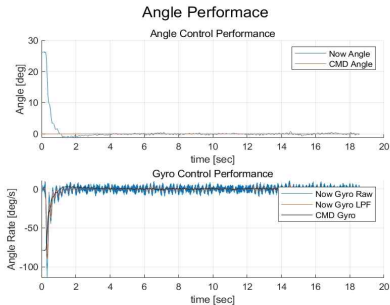
편심 질량과 적분제어기 영향

K_{P1}	4
K_{P2}	0.7
K_D	0.01
K_I	0.25



I Gain = 0.01

편심질량에 의한 정상상태 오차 발생

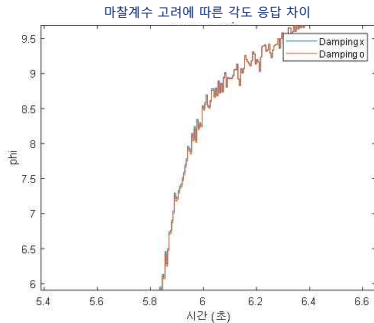
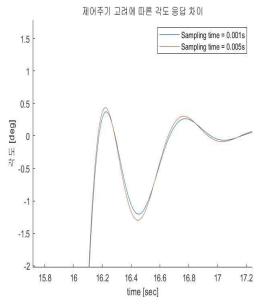
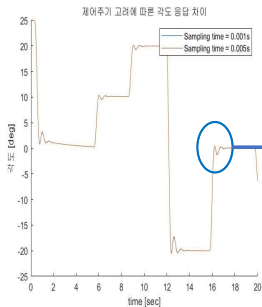


I Gain 0.25

편심질량에 의한 정상상태 오차 제거

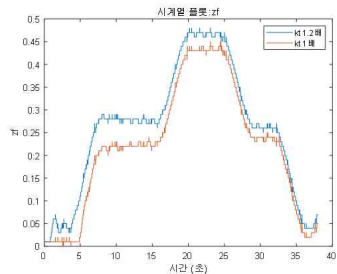
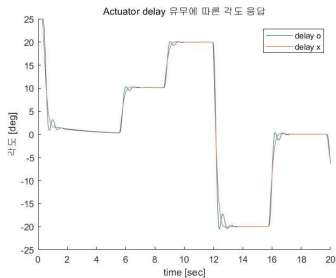
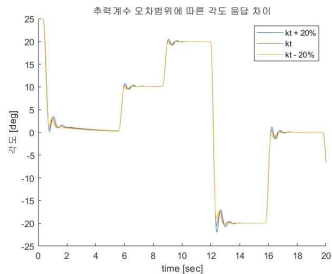
모델링 정확성

Sampling time, Damping coefficient



모델링 정확성

Actuator Parameter



감사합니다

강민구, 박주형, 허홍석

Louis Vuitton