

Line Equation

$$\vec{r} = t \cdot \vec{v} + \vec{r}_0$$

$$\text{Arc length} = \int_b^a \sqrt{f'(t)^2 + g'(t)^2 + h'(t)^2} dt = \int_a^b |\vec{v}(t)| dt$$

$$\text{Arc length Parameter} = s(t) = \int_a^t |\vec{v}(\tau)| d\tau$$

$$\text{Curvature} := \left| \frac{d\vec{T}}{ds} \right| = \kappa = \left| \frac{d\vec{T}}{dt} \frac{dt}{ds} \right|$$

$$\xrightarrow{\vec{v} = \frac{ds}{dt}} \kappa = \frac{1}{|\vec{v}|} \left| \frac{d\vec{T}}{dt} \right|$$

Plane Equation

$$\vec{n} \cdot \overrightarrow{P_0P} = 0$$

cartesian - polar coordinate

$$dx dy = r dr d\theta$$

cartesian - Spherical coordinate:

$$dx dy dz = \rho^2 \sin \phi d\rho d\phi d\theta$$

$$\text{Torsion} := -\frac{d\vec{B}}{ds} \cdot \vec{N} = \tau$$

- Torsion τ shows how that plane twists.
- Curvature κ shows how points curve in the plane defined by \vec{T} and \vec{N}

$$\vec{v} = \frac{d\vec{r}}{dt} \quad \vec{a} = \frac{d\vec{v}}{dt}$$

$$a_{\vec{T}} = \frac{d|\vec{v}|}{dt} \quad a_{\vec{N}} = \kappa |\vec{v}|^2$$

$$\text{Acceleration} := |\vec{a}| = \sqrt{|a_{\vec{T}}|^2 + |a_{\vec{N}}|^2}$$

Theorem: if $\frac{\partial f}{\partial x}$ and $\frac{\partial f}{\partial y}$ are continuous on an open region R , then f is differentiable on R

$$\text{Chain Rule} := \frac{dw}{dt} = \sum \frac{\partial w}{\partial x_i} \frac{dx_i}{dt}$$

$$\text{Directional Derivatives} := D_{\vec{u}} f(x_0, y_0) = \nabla f|_{(x_0, y_0)} \cdot \vec{u}$$

$$\text{Tangent Plane} := \left. \frac{\partial f}{\partial x} \right|_{(x_0, y_0)} (x - x_0) + \left. \frac{\partial f}{\partial y} \right|_{(x_0, y_0)} (y - y_0) + z_0 = z$$

Lagrange Multipliers:

$$\nabla f = \lambda \nabla g$$

$$g = 0$$

$$\nabla f = \lambda \nabla g_1 + \mu \nabla g_2$$

$$g_1 = 0 \quad g_2 = 0$$

tips to find the local Max/Min of a function:

1. Find critical points where $f_x(a, b) = f_y(a, b) = 0$
2. classify each critical point with 2nd derivative test:
 - f has a local **max** if $f_{xx} < 0$ and $f_{xx}f_{yy} - f_{xy}^2 > 0$
 - f has a local **min** if $f_{xx} > 0$ and $f_{xx}f_{yy} - f_{xy}^2 > 0$
 - f has a **saddle** if $f_{xx}f_{yy} - f_{xy}^2 < 0$
 - f is **inconclusive** if $f_{xx}f_{yy} - f_{xy}^2 = 0$

$$V = \int_{x=a}^{x=b} \int_{y=g_1(x)}^{y=g_2(x)} \int_{z=f_1(x,y)}^{z=f_2(x,y)} dz dy dx$$

The Jacobian is useful when changing variables in multivariable integrals:

$$\iint_R f(x, y) dx dy = \iint_G f(g(u, v), h(u, v)) J(u, v) du dv$$

$$J(u, v) = \begin{vmatrix} \frac{\partial x}{\partial u} & \frac{\partial x}{\partial v} \\ \frac{\partial y}{\partial u} & \frac{\partial y}{\partial v} \end{vmatrix}$$

$$\text{Line Integral} := \int_C f(x, y, z) ds = \int_a^b f(g(t), h(t), k(t)) \sqrt{g'(t)^2 + h'(t)^2 + k'(t)^2} dt$$

Arc Length

$$\text{Line Integral of Vector Field} \int_C \vec{F} \cdot \vec{T} ds = \int_a^b \vec{F}(\vec{r}(t)) \frac{d\vec{r}}{dt} dt = \int_C \vec{F} d\vec{r}$$

conservative fields

$$\frac{\partial N}{\partial x} = \frac{\partial M}{\partial y} \quad \frac{\partial N}{\partial z} = \frac{\partial P}{\partial y} \quad \frac{\partial P}{\partial x} = \frac{\partial M}{\partial z}$$

1. equivalent to $\vec{F} = \nabla f$
2. fundamental theorem of line integrals:

$$\int_C \vec{F} \cdot d\vec{r} = f(B) - f(A)$$
3. $\text{curl} = 0$, the vector field is conservative.

Flow (flow density = curl)

$$\text{Curl } \vec{F} = \nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ M & N & P \end{vmatrix}$$

- with parametrization:

$$\text{Flow} = \int_a^b M dx + \int_a^b N dy$$

- without parametrization: (Green's Theorem)

$$\oint_C \vec{F} \cdot d\vec{r} = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx dy$$

Flux (flux density = divergence)

$$\text{Div } \vec{F} = \nabla \cdot \vec{F} = \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} + \frac{\partial P}{\partial z}$$

- with parametrization:

$$\text{Flux} = \int_a^b M dy - \int_a^b N dx$$

- without parametrization: (Green's Theorem)

$$\oint_C \vec{F} \cdot \vec{n} ds = \iint_R \left(\frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} \right) dx dy$$

Surface Area

Parametric : $\vec{r}(u, v) = f(u, v) \hat{i} + g(u, v) \hat{j} + h(u, v) \hat{k}$

$$SA_p = \int_c^d \int_a^b |\vec{r}_u \times \vec{r}_v| du dv$$

$(\vec{p} \in \hat{i}, \hat{j}, \hat{k})$

Implicit : $F(x, y, z) = c$

$$SA_i = \iint_R \frac{|\nabla F|}{|\nabla F \cdot \vec{p}|} dA$$

Explicit : $z = f(x, y)$

$$SA_e = \iint_R \sqrt{f_x^2 + f_y^2 + 1} dA$$

Surface Integrals

$$SI = \iint_R G(f(u, v), g(u, v), h(u, v)) \mathbf{SA}_p du dv$$

$$SI = \iint_R G(x, y, z) \mathbf{SA}_i dA$$

$$SI = \iint_R G(x, y, f(x, y)) \mathbf{SA}_e dA$$

Flux of a vector field across a surface

$$\text{Flux} = \iint_S \vec{F} \cdot \vec{n} d\sigma$$

Parametric

$$\text{Flux} = \iint_S \vec{F} \cdot (\vec{r}_u \times \vec{r}_v) du dv$$

Implicit

$$\text{Flux} = \iint_S \vec{F} \cdot \frac{\nabla g}{|\nabla g \cdot \vec{p}|} du dv$$

as only boundary is important to us, we can choose a simpler surface instead of given one and apply the stokes or divergence theorem.

Stoke's Theorem

$$\oint_C \vec{F} \cdot d\vec{r} = \iint_S (\nabla \times \vec{F}) \cdot \vec{n} d\sigma$$

flow density over boundary

Divergence Theorem

$$\iint_S \vec{F} \cdot \vec{n} ds = \iiint_D \nabla \cdot \vec{F} dV$$

flux density over boundary

Amin