

Trajectory Optimization Methods for Energy Efficient Gait Transitions on Multi-Modal Robots

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Abstract—For robots that achieve locomotion through the movement of articulation joints, having a set of gaits can allow them to navigate variable terrain. Effectively transitioning between these gaits on multi-modal robots is important for maintaining locomotive constraints and reducing unnecessary movements during gait switches, which decreases energy usage. While previous works have examined transitions between specific gaits on certain robots, this work aims to propose and experimentally examine general frameworks for transitioning between gaits with a nonlinear, local optimized trajectory over the articulation joints. We compare the maximum joint acceleration, transition time, cost of transport, and heading change between four transition frameworks: an optimized Bezier function, optimized Linear waypoints, an optimized Spline, and resetting to a neutral position before each gait. These transition strategies were then implemented on a four-wheeled multi-modal rover.

When operating in uncertain environments, it's vital that the system can efficiently and safely vary its gait. This means taking into account joint position and velocity constraints. A gait transition should also avoid consuming excess energy caused by taking unnecessary movements and time. To achieve these goals, it's important that a transition should maintain continuity in both joint space and the workspace.



Figure 1. The testing platform, Asterix, executing its squirming gait in the JPL Mini-Mars Yard [1]

1. INTRODUCTION

With increasing demands on robotic mobility, multi-modal robots are useful for their ability to navigate varying terrain. The ability to choose a locomotion mode, or gait, depending on the terrain enables a greater degree of exploration. While there is significant activity in developing multi-modal robotic mechanisms and their accompanying gaits [1] , optimally switching between different gaits remains largely unsolved.

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The difficulty of implementing optimal gait transitions lies in gaits being extremely hardware specific and trying to maintain trajectory continuity in the workspace is computationally intensive. Multi-modal robots are generally custom built for an environment which leads to widely varying hardware mechanisms and gaits. Trying to optimize a workspace trajectory relies heavily on forward dynamics which is difficult to run online. Previous works [2] [3] closely examine specific gaits to generate an optimal transition policy, but this work seeks to present and examine a set of general transition frameworks.

We solve this problem using online non-linear local trajectory optimization in the joint space, where each gait is represented by its motion through joint space. To maintain trajectory continuity in the workspace, the forward dynamics of the robot are calculated in the cost function, which tries to minimize trajectory deviation.

These algorithms were all tested on the Jet Propulsion Laboratory (JPL) Steep Terrain Mobility Asterix platform [1], a four-wheeled rover with two articulation joints, and evaluated based on maximum joint acceleration, trajectory deviation, transition time, and cost of transport.

Our main contributions are:

- Four general gait transition frameworks
- The implementation and evaluation of these transition frameworks on the Asterix platform

2. RELATED WORK

With the development of more complex robots that are capable of different gaits, there has been a desire to efficiently switch between these locomotive modes.

One of the most common applications of gait switching comes from legged robots, such as bipeds and quadrupeds. Gaits on legged robots are related to the footfall patterns of their limbs. Walking, trotting, and running, can be considered different gaits but are very similar in their joint movements but with different timing. Owaki and Ishiguro [4] have shown how to parameterize quadruped gaits with a central pattern generator (CPG), which can smoothly switch between gait types when the speed parameter is increased. Haynes and Rizzi [3] exploit the cyclic joint movement and stability of a hexaped robot to transition between gaits through synchronizing the phase of each leg over time to match the desired gait.

For non-legged robots, Bing [2] demonstrates how a snake robot's gaits can be parameterized using a Central Pattern Generator (CPG) which allows for smooth gait transitions. Work with CPG-driven gait transitions shows they work well in systems with high stability and similar gaits. However, they fail to describe non-cyclic gaits which rules out their usage in a general gait transition algorithm.

Trajectory optimization is a common framework for kinematic trajectory generation. As shown by Sundaralingam [5], it can be implemented as a general framework for hand joint trajectories used for grasping. Similar to that work, we will be proposing general frameworks for gait transition trajectories.

Unlike the work with transitions between highly cyclic gaits, our work in this paper focuses on examining general frameworks for gait transitions on robots that don't necessarily have similarities in their gaits.

3. GAITS AND TRANSITIONS

Haynes and Rizzi [3] go into great detail about a mathematical representation of gaits and gait transitions. Similar to that work, in this paper we will define a gait as a periodic motion pattern that produces locomotion. A gait is a function that maps from a phase $\mathbb{P} \in \mathbb{R}$ to a robot configuration in joint

space $\mathbb{Q} \in \mathbb{R}^n$ where n is the number of joints.

$$g : \mathbb{P} \rightarrow \mathbb{Q} \quad (1)$$

Transitions

Transitions between gaits g_1 and g_2 can be seen as a trajectory through joint space that have boundary conditions in g_1 and g_2 . Specifically, we can define a gait transition $q(t) \in \mathbb{R}^n$ over the interval $[t_1, t_1 + T] \in \mathbb{R}$ with the constraints:

$$q(t_1) = g_1(t_1) \quad (2)$$

$$q(t_1 + T) = g_2(t_1 + T - \phi) \quad (3)$$

where ϕ is the phase shift of g_2 . The simplest transition is when g_1 and g_2 overlap at time t_1 , then one would simply set ϕ to satisfy $g_2(t_1 + T - \phi) = g_1(t_1)$. However, this doesn't take into account differences in velocity between those two endpoints, which could result in a jerky transition. Therefore, it's beneficial to enforce continuity in the first derivative too.

$$\dot{q}(t_1) = \dot{g}_1(t_1) \quad (4)$$

$$\dot{q}(t_1 + T) = \dot{g}_2(t_1 + T - \phi) \quad (5)$$

Continuity in the workspace is also desired so the robot doesn't deviate from its intended trajectory during a gait transition. Let $x(t) \in \mathbb{R}^6$ be the robot's resultant trajectory through the workspace by executing $Q(t)$ in the workspace and $G_1(t)$ and $G_2(t)$ be the gait's trajectory through the workspace. Then we desire

$$x(t_1) = G_1(t_1) \quad (6)$$

$$x(t_1 + T) = G_2(t_1 + T - \phi) - G_2(t_1 - \phi) + G_1(t_1) \quad (7)$$

The pose of the robot in the workspace after executing the gait transition should be the same as executing g_2 with ϕ phase shift over $[t_1, t_1 + T]$ with the initial pose of $G_1(t_1)$.

4. GAIT TRANSITIONS THROUGH TRAJECTORY OPTIMIZATION

Three trajectory optimization strategies are implemented and evaluated in this work, as well as a Naive transition strategy. The optimized transition types are a Bezier Curve, Linear Waypoints, and a Spline.

For the three optimization methods, we formulate the optimization problem from a trajectory q in joint space.

$$\min_q w_1 T + w_2 \sum \ddot{q} + w_3 \Delta x \quad (8)$$

The cost function is split into three main components: transition time, joint acceleration, and workspace trajectory deviation which are calculated differently for each transition method. w_1 , w_2 , and w_3 represent the weight associated with each cost.

Naive Transition

The Naive transition strategy has the following policy: at time transition time t_1 , generate a trapezoidal trajectory from $g_1(t_1)$ to $g_2(0)$. Execute this trajectory, then continue executing $g_2(t - \phi)$ from $t = 0$, $\phi = 0$. This method has no optimization components. A one dimensional example is shown in Figure 2.

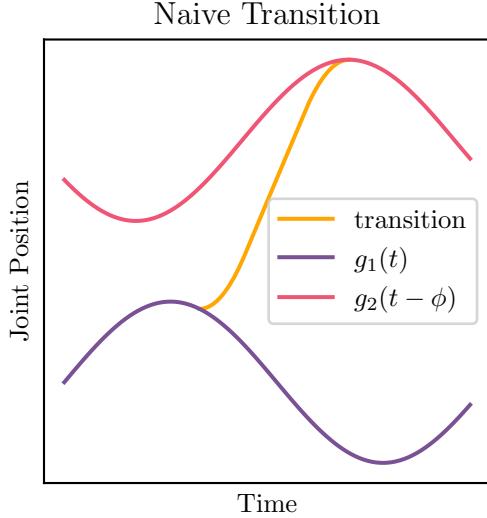


Figure 2. Transition generated by Naive strategy between two sinusoids with $t_1 = 2$

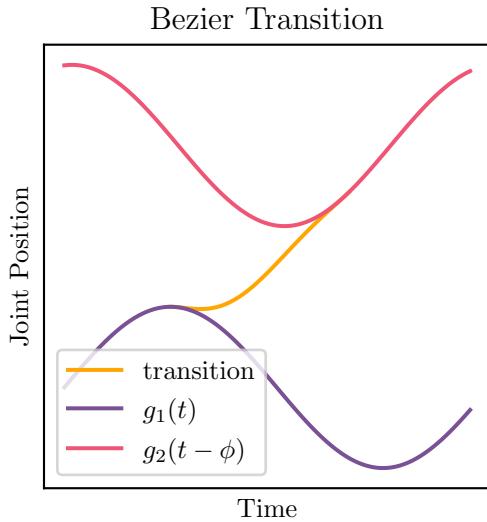


Figure 3. Transition generated by the Bezier trajectory strategy between two sinusoids with $t_1 = \frac{3\pi}{2}$

Bezier Trajectory

To switch between the two gaits, the trajectory optimization algorithm outputs parameters T and ϕ , that define a cubic Bezier Curve trajectory through the joint space over $[t_1, t_1 + T]$ and ϕ is the phase shift of g_2 . The equation of a cubic Bezier curve is:

$$q(t) = \left(1 - \frac{t - t_0}{T}\right)^3 p_0 + 3 \left(1 - \frac{t - t_0}{T}\right)^2 \left(\frac{t - t_0}{T}\right) p_1 + 3 \left(1 - \frac{t - t_0}{T}\right)^3 \left(\frac{t - t_0}{T}\right)^2 p_2 + \left(\frac{t - t_0}{T}\right)^3 p_3 \quad (9)$$

The trajectory is constrained to be continuous with the first derivative, velocity, so the function is fully determined by the

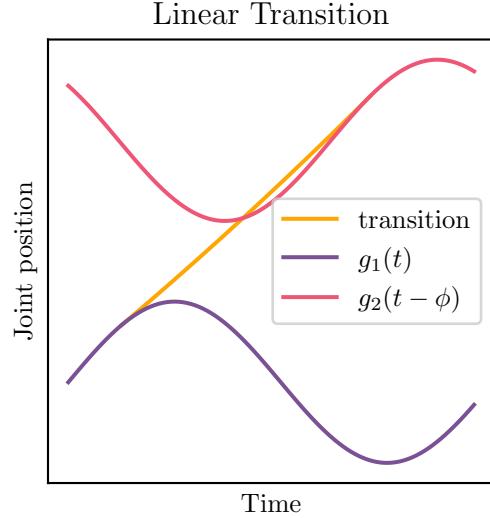


Figure 4. Transition generated by Linear trajectory strategy between two sinusoids with $t_1 = \frac{\pi}{4}$

beginning and end gaits:

$$p_0 = g_1(t_1) \quad (10)$$

$$p_1 = p_0 + \frac{1}{3T} \dot{g}_1(t_1) \quad (11)$$

$$p_2 = p_3 - \frac{1}{3T} \dot{g}_2(t_1 + T - \phi) \quad (12)$$

$$p_3 = g_2(t_1 + T - \phi) \quad (13)$$

where $p_i \in \mathbb{R}^n$ is a vector of the joint positions.

The acceleration cost is calculated by summing up the second derivative of the function uniformly across the time period. The time cost is T . The trajectory deviation cost is calculated by the method described in the Asterix Platform section.

Linear Trajectory

In this strategy, the optimization algorithm outputs a transition duration T and a series of joint angle waypoints $\Theta \in [\theta_1, \theta_T]$ where

$$\theta_1 = g_1(t_1) \quad (14)$$

$$\theta_T = g_2(t_1 + T) \quad (15)$$

Every waypoint is equally spaced in time, so $\Delta t = \frac{T}{||\Theta||}$. We used 100 waypoints in our implementation. Each waypoint is subject to

$$\theta_{min} \leq \theta_t \leq \theta_{max}, \forall t \quad (16)$$

$$-\dot{\theta}_{max} \leq \frac{\theta_t - \theta_{t-1}}{\Delta t} \leq \dot{\theta}_{max}, \forall t \quad (17)$$

The first constraint keeps the trajectory from violating the joint position limits and the second limits the velocity between each set of waypoints.

To prefer linear trajectories, we introduce another cost term:

Define the linear interpolation between $g_1(t_1)$ and $g_2(t_1 + T)$:

$T - \phi$) as $l(t)$.

$$l(t) = \frac{g_2(t_1 + T - \phi) - g_1(t_1)}{T} * t + g_1(t_1) \quad (18)$$

then the linear cost term is:

$$\text{cost}_{\text{linear}} = \sum_t \|l(t) - \theta_t\|_2 \quad (19)$$

After the waypoints are generated, they are interpolated through by cubic Bezier curves to create a continuous function.

Spline Trajectory

This strategy is identical to the Linear Trajectory one, but without the linear cost term. In result, the generated transition has higher flexibility in its shape.

Asterix Platform

In this work, we examine these algorithms on the Asterix platform, a 7.8 kg four-wheeled platform. The four wheels are accompanied by an actively controlled center steering joint and an active rear roll joint.

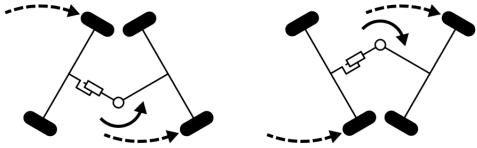


Figure 5. Asterix executing a squirming gait: the center steering joint moves back and forth while the wheels synchronize with its movement. [1]

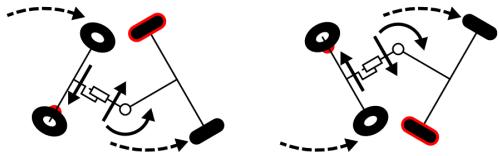


Figure 6. Asterix executing a wheel-walking gait: the center steering joint and the back roll joint moves back and forth while the wheels synchronize with their movement. [1]

Asterix is capable of multiple locomotion modes [1], the two we consider in this work are squirming and wheel-walking. Squirming consists of oscillating the center steering joint between its two limits on either side. The wheels are synchronized with the movement of the steering joint to move forward with theoretically no tangential or lateral skidding on a planar surface. Wheel walking also oscillates the center joint, but moves the rear roll joint as well, resulting in the load being shifted to mainly two wheels while one of the wheels is lifted. Which wheel is lifted depends on the overall static equilibrium.

To calculate the displacement of the rover given a gait transition, we can integrate the velocity of the wheels over time. Define V_r as the forward velocity of the rover, l_x as the longitudinal distance between the wheels when $\theta = 0$, R to be the wheel radius, ω_i for $i \in [1, 4]$ to be the velocity of wheel i , x_i, y_i to be the Cartesian coordinates of wheel i , and β_i to be the yaw of wheel i .

Then for each wheel:

$$\frac{d}{dt}x_i = R\omega_i \cos(\beta_i) \quad (20)$$

$$\frac{d}{dt}y_i = R\omega_i \sin(\beta_i) \quad (21)$$

$$\frac{d}{dt}\beta_i = \frac{V_r}{l_x} \tan(-\frac{\theta}{2}) + (-1)^{\frac{i(i+1)}{2}} \frac{\dot{\theta}}{2} \quad (22)$$

Then the cartesian coordinates x, y at time T of the whole rover can be found by summing the wheel displacements, taking care to note that β changes each timestep.

$$\begin{bmatrix} x \\ y \\ \beta \end{bmatrix} = \sum_i \int_0^T \begin{bmatrix} dx_i \\ dy_i \\ d\beta_i \end{bmatrix} dt \quad (23)$$

Evaluation Metrics

Heading deviation is calculated by taking the difference between the rover's heading before and after a transition. The heading being the yaw of the rover in respect to the world frame.

Cost of transport (COT) is a dimensionless number that quantifies the energy efficiency of a gait transition. We expect cost of transport to be related to maximum joint acceleration as lower joint accelerations leads to less energy usage and higher cost of transport.

$$COT = \frac{E}{mgd} \quad (24)$$

where E is the mechanical energy produced by the motors during the transition, m is the mass of the rover, and d is the distance travelled during the transition.

Transition time is the duration of the transition, which is a direct output of the optimization.

The maximum joint acceleration is calculated for both the steering and bogie joints. The maximum rotational acceleration between consecutive data points is found for each transition.

5. IMPLEMENTATION AND EXPERIMENTS

Robot Deployment

The trajectory optimization problems were solved using the NLOPT library [6] using Sequential Least Squares Programming (SLSQP) [7] in C++. The solver was set with a maximum time of 0.5 seconds with the previously described cost functions subject to the joint velocity and position constraints. The algorithms were deployed on a Raspberry Pi 4B onboard Asterix which invoked the C++ solver through a Python front end. The forward dynamic calculation was run using the Boost ODE library.

The program outputted joint positions which were followed by the feedback controllers of the articulation. Another controller synchronized the wheel velocities with the steering joint.

Experimental Protocol

Experiments were executed in the JPL Mini Mars Yard, an outdoor sandpit. A Vicon motion capture system was setup to record motion capture data. The Raspberry Pi recorded onboard telemetry to keep track of power draw and transition requests.



Figure 7. Vicon motion capture setup to evaluate gait transitions on the Asterix platform

For each transition type, three different weight distributions for the cost function were empirically selected: minimize transition time, minimize workspace trajectory deviation, or a balance of both. For each weight distribution, three identical experiments were run. In each experiment the rover switched gaits from squirming to wheel-walking at 5 uniform points over the period of the squirming gait. In the same run, the rover repeated the uniformly distributed switching, but from wheel-walking to squirming instead.

Transition Type	Minimize	w_1	w_2	w_3
Bezier	Duration	30	1	1
Bezier	Deviation	1	1	20
Bezier	Balanced	5	1	1
Linear	Duration	20	5	1
Linear	Deviation	4	5	20
Linear	Balanced	4	5	1
Spline	Duration	20	5	1
Spline	Deviation	4	5	20
Spline	Balanced	4	5	1

Table 1. Weight distributions for each trajectory optimization strategy. w_1 corresponds to duration cost, w_2 corresponds to average acceleration, and w_3 corresponds to workspace deviation

A combination of Vicon motion capture data and onboard telemetry was time synced to create the data for each experimental run.

Performance Evaluation

The heading deviation was taken directly from the motion capture data, looking at the robot's pose before and after a transition.

To calculate the Cost of Transport, the mechanical energy expended during the transition was calculated from the ar-

ticulation and wheel motors.

$$E = E_{wheel} + E_{articulation} \quad (25)$$

$$E_{wheel} = k_t I \omega \quad (26)$$

$$E_{articulation} = \tau \omega \quad (27)$$

The articulation motors directly reported torque, while the torque constant on the wheel motors, k_t , was experimentally determined to be 1.45 N m A^{-1} .

The distance traveled is the euclidean distance between the initial position and the final position of the gait transition trajectory

$$d = \|G_2(t_1 + T - \phi) - G_1(t_1)\|_2 \quad (28)$$

which is taken directly from the motion capture data. The mass of the rover is 7.8 kg.

It is important to note that the cost function for Bezier is not the same as the Linear and Spline cost functions as the weights are different. This is due to differences in the calculation for each cost function. The weights were subjectively selected so metrics that were not directly optimized for, such as the Cost of Transport metric, are not directly comparable between the groups of optimizations. Despite this, it is fruitful to look at the cost of transport for each strategy as a way to qualify their individual performance.

6. RESULTS

We now discuss our results with the performance metrics represented in Figures 8-11 as column graphs for each configuration of transition strategy.

Naive Transition

The Naive transition has an extremely low cost of transport at the expense of a long duration and the highest average heading change. This is to be expected since the Naive strategy always resets to the initial position of g_2 : $g_2(0)$, meaning it biases towards that side. Due to the long transition time, the rover travels a large distance so the cost of transport is low, but there is no control over workspace deviation.

Bezier Transition

The Bezier Transition strategy is characterized by low duration, average heading change, and low joint acceleration. This could be due to the constrained nature of the trajectory, there are only two free parameters, so it doesn't have much freedom to correct heading deviation. On the other hand, its simple trajectory leads to short transition times which is less time to cause a trajectory deviation. Since the curve is a continuous function, the joint acceleration is expected to be lower as there's no sudden changes between waypoints that are present in the Linear and Spline strategies.

Linear Waypoints Transition

The Linear transitions have high joint acceleration and duration, while benefiting in the heading change. It's important to note that its improvement in heading change is relatively small, about two degrees compared to the Naive transition, so this metric can be weighted less heavily. The Linear transition trajectory has enough freedom with its waypoints to correct the trajectory deviation but it would come at the heavy expense of duration and acceleration.

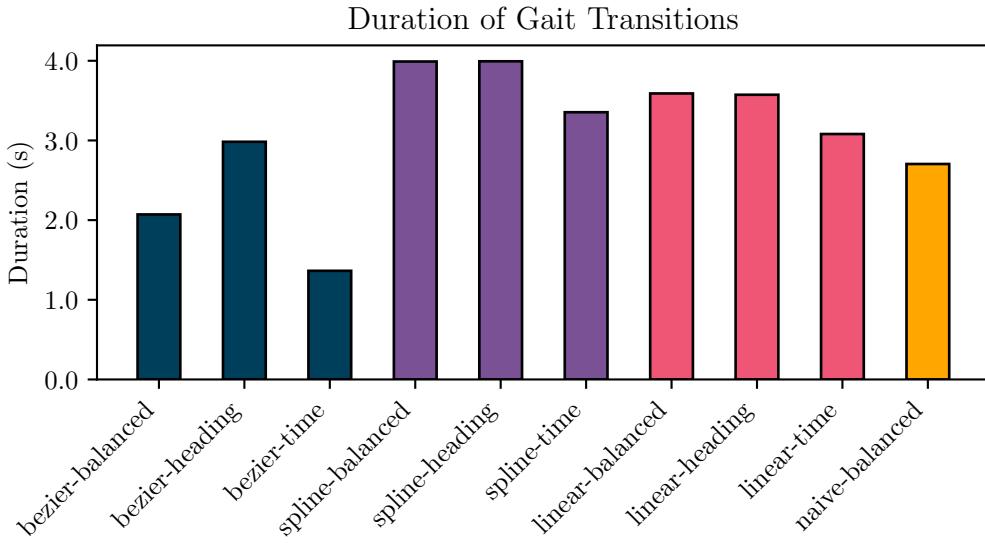


Figure 8. Comparison of average transition duration for each gait-transition type. During each run, the average of the 10 uniformly distributed transitions are taken. Colors indicate the four transition frameworks, "Bezier", "Spline", "Linear", and "Naive", (each of which has three variations of cost functions except the Naive type).

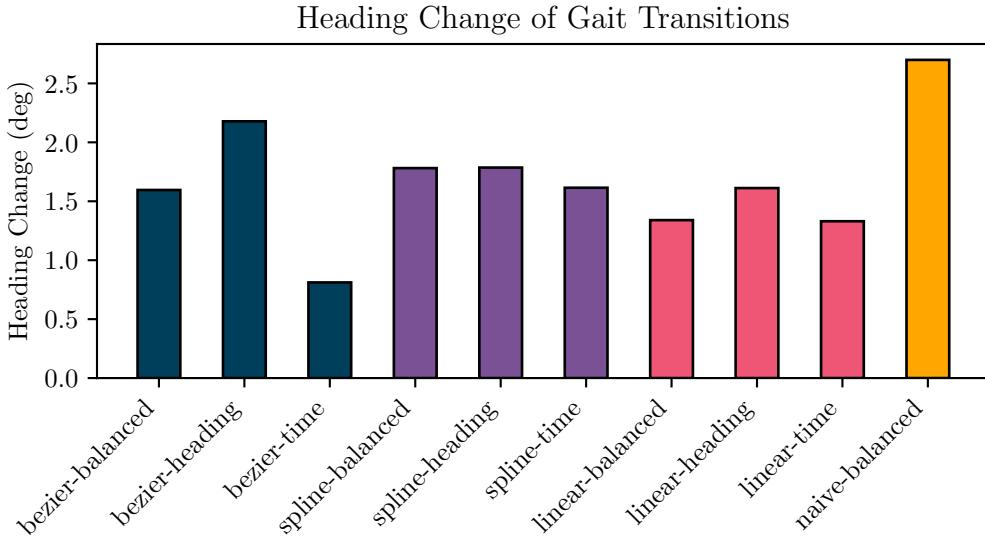


Figure 9. Comparison of average heading deviation caused by transition for each gait-transition type. During each run, the average of the 10 uniformly distributed transitions are taken. Colors indicate the four transition frameworks, "Bezier", "Spline", "Linear", and "Naive", (each of which has three variations of cost functions except the Naive type).

Spline

The Spline strategy performs poorly in the joint acceleration method, possibly due to the lack of constraints between waypoints. Its freedom to place waypoints may have run into computational issues where the optimization could not converge in the allotted time.

Overall, the Bezier method performed the best, possibly due to its short transition durations which led to less movement of the platform and, in turn, better cost of transport and heading deviation. The Bezier method also had the lowest cost of transport out of all strategies which speaks to its energy efficiency. The waypoint methods, Spline and Linear, had more freedom in their trajectories but it may be that in wheeled platforms, maintaining continuity in the workspace trajectory is too expensive in terms of duration and cost of

transport.

Another explanation comes from the optimization time which was limited to 0.5 seconds. This favors optimization problems with less degrees of freedom as they can reach their optima faster. It could be that the Bezier method with its two degrees of freedom outperformed the Spline and Linear methods because the Bezier method was less computationally intensive to optimize.

7. CONCLUSION

We presented four general transition frameworks for gait transitions. Each was evaluated based on cost of transport, duration, maximum joint accelerations, and workspace tra-

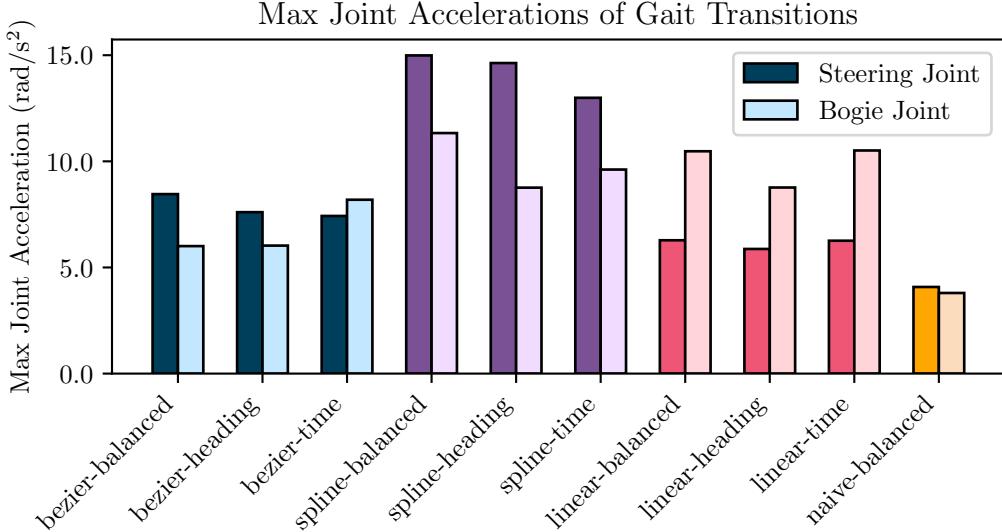


Figure 10. Comparison of maximum rotational acceleration experienced at the steering and bogie joints over the transition for each gait-transition type. Colors indicate the four transition frameworks, “Bezier”, “Spline”, “Linear”, and “Naive”, (each of which has three variations of cost functions except the Naive type). For each pair of columns, the left column (darker color) represents the steering joint and the right column (lighter color) represents the bogie joint.

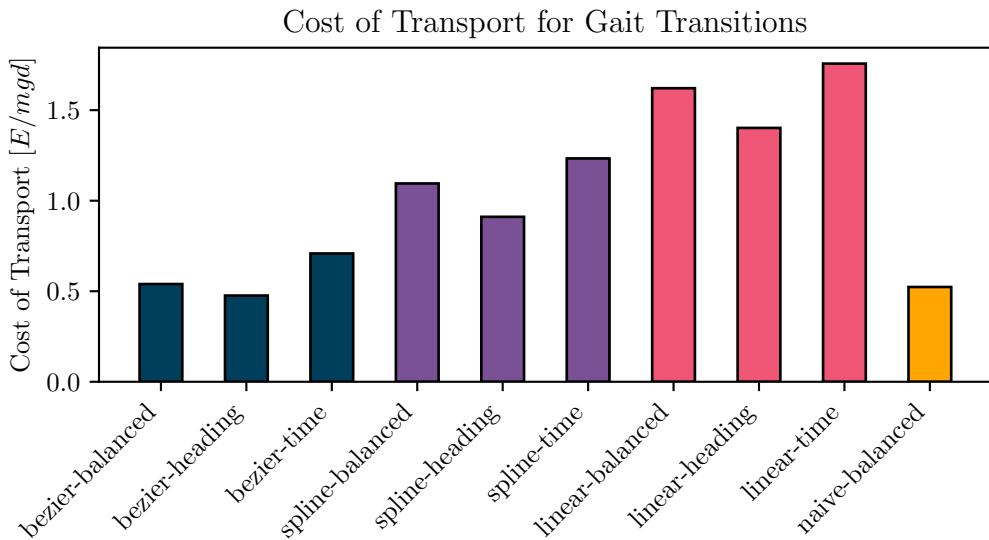


Figure 11. Comparison of average cost of transport over the 3 runs for each gait-transition type. During each run, the average of the 10 uniformly distributed transitions are taken. Colors indicate the four transition frameworks, “Bezier”, “Spline”, “Linear”, and “Naive”, (each of which has three variations of cost functions except the Naive type).

jectory deviation. While the strategies were framed to be for general frameworks, they were evaluated on the wheeled Asterix platform. We outline how to implement the described strategies on real hardware and how it performed. The results showed that the best performing transition strategy was the Bezier strategy which may be primarily explained through its short transition times and simpler problem formulation. In other platforms, the optimization weight distributions should be tuned to the task at hand. For example, the frequency of transitions affects which strategy is optimal as one could trade off the higher per-transition duration cost for better trajectory deviation.

8. FUTURE WORK

To draw more conclusions about the effectiveness of the different frameworks, it would be beneficial to subject them to a unified cost function. In this way we can more accurately compare their effectiveness in minimizing the cost and metrics that are not directly optimized, such as cost of transport.

For robots with a higher number of kinematic constraints, adding those into the frameworks as well as collision avoidance would be beneficial.

Implementing these frameworks on other four-wheeled robots with articulation joints would be a good comparison

to our testing platform. The implementation of other gaits to transition between would also shed more insight into the performance of each strategy.

Rather than using optimization, a reinforcement-learning based trajectory generator could be useful as the optimization has to be time constrained when run online.

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BIOGRAPHY



Minh Nguyen is an intern at JPL and a student at the University of California, Berkeley. His research interests are in control and hardware acceleration. He is currently working towards a B.A. in Computer Science.



Matthew Suntup is a Visiting Student Researcher at JPL and a student at the University of Sydney, Australia. His research focuses on steep terrain mobility for planetary rovers. He received both his B.Eng. Honours (Mechatronic Engineering) majoring in Space Engineering and B.Sci. (Advanced) majoring in Physics and Computer Science from the University of Sydney in 2023.



Arthur Bouton is a Robotics Technologist at JPL. His primary areas of research include wheel-on-limb hybrid locomotion, mechanical design, machine learning and control. He received his M.Sc.Eng. degree in Advanced Systems and Robotics from E’cole Nationale Sup’erieure d’Arts et M’etiers ParisTech in France and his Ph.D degree from Sorbonne Universit’és, Université Pierre et Marie Curie, Paris, in 2017. After a postdoc at Surrey Space Centre, Guildford, UK, he joined JPL in 2021.



William Reid is a JPL Robotics Technologist investigating novel mobility systems for planetary surface exploration. William received a PhD in Robotics from the Australian Centre for Field Robotics at the University of Sydney in 2018. He has Bachelor’s degrees in Mechatronics Engineering and Computer Science from the University of Melbourne.



Travis Brown is a robotic systems engineer in the Robotic Mobility Group at JPL. He holds a Ph.D. in robotics from the University of Notre Dame, where he studied planning and control of underactuated bipedal robots. He has been with JPL since 2016, working on a variety of projects such as the Axel Rappelling Rover, Mars Helicopter (*Ingenuity*), Moon Diver Mission Concept, Perseverance Rover, ColdArm, and many others. He is interested in the design and control of advanced robotic mobility systems. He is currently serving as the deputy chief engineer for *Ingenuity*.



Hari Nayar Hari Nayar is a principal technologist in the Mobility and Robotics Systems Section at JPL. He is the Principal Investigator of the Steep Terrain Mobility task at JPL where this work was done. He was a Visiting Lecturer in the Mechanical and Aerospace Engineering Department at UCLA. His research interests include analysis & modeling, manipulation, mobility, tele-operation and autonomy for space and medical robotics applications. He received his ScD in Mechanical Engineering at MIT.