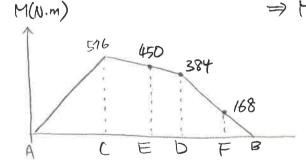


$$\Sigma F_8 = 0$$
; $R_A - F_C - F_B + R_B = 0$

$$IMA=0$$
; $-F_c.l-F_d(2R)+R_B.(3R)=0$
 $\Rightarrow R_A=2.5kN, R_B=2.0kN$

$$(l=192mm)$$

$$ZM=0$$
; $M=RAX+FC(X-R)+FO(X-2R)=0$
 $\Rightarrow M=(RA-FC-FO)+FC(R+FO(2R))$



$$6c = \frac{M_{\text{C} \cdot \text{C}}}{I} = \frac{(516 \text{ N·m})(40/2 \text{ mm})}{7c (40 \text{mm})^4} = 91.7 \text{ MPa}$$

$$60 = \frac{M_{D.C}}{I} = \frac{(3840.m)(45/2mm)}{7(45mm)^4} = 42.9 MPa$$





$$6E = K_{\pm} \frac{MeC}{I} = (2.3) \frac{(450N.m)(40/2mm)}{\pi (40mm)^{*}} = 164.7 MPa$$

(K+ = 2.3 determined from the 1st mid-term exam)

$$G_F = K_E \frac{M_{FC}}{I} = (1.96) \frac{(168 \text{ N·m})(45/2\text{mm})}{\pi (45\text{mm})^t} = 45.3\text{MPa}$$

(K+=1.96 at F from the 1st mid-term exam)

GE is the largest and thus E is the critical location.

$$Gal = (K_f)_{bending} (G_n)_{bending} + (K_f)_{axial} \frac{(G_n)_{axial}}{0.85}$$

$$G_{mr} = (K_f)_{bending} (G_m)_{bending} + (K_f)_{axial} (G_m)_{axial}$$

Using Egns. (7-3) and $(6a)_{arial} = \frac{P_a}{A}$ and $(6m)_{arial} = \frac{F_m}{A}$

where Pa = atternating oxial load, Pm = mean oxial load and

A = cross sectional area of the shaft,

$$Ga' = (K_f)_{bending} \left(\frac{32M_o}{\pi d^3}\right) + \frac{(K_f)_{axial}}{0.85} \frac{4P_a}{\pi d^2}$$

$$Gm' = (K_f)_{bending} \left(\frac{32M_m}{\pi d^3}\right) + (K_f)_{axial} \frac{4P_m}{\pi d^2}$$

$$6m' = (K_f)_{bending} \left(\frac{32Mm}{\pi d^3}\right) + (K_f)_{arial} \frac{4Pm}{\pi d^2}$$

: Eq. (1-1) is rewritten as

$$\frac{1}{n} = \frac{1}{Se} \left[(K_f)_{bending} \left(\frac{32M_a}{\pi d^3} \right) + \frac{(K_f)_{axial}}{0.85} \frac{4P_a}{\pi d^3} \right] + \frac{1}{Sut} \left[(K_f)_{bending} \left(\frac{32M_m}{\pi d^3} \right) + \frac{1}{Sut} \left[\frac{32M_m}{\pi d^3} \right] + \frac{$$

+ (Kf)axal 4Pm

Eq. (7-8) can be modified as

$$\frac{1}{n} d^3 - (K_f)_{axiral} \left[\frac{1}{Se} \frac{4P_a}{0.85\pi L} + \frac{1}{Sut} \frac{4P_m}{\pi L} \right] d = (K_f)_{bonding} \left[\frac{1}{Se} \left(\frac{32M_a}{\pi d^3} \right) \right]$$

+ (32 Mm)



(C) From Part (b)

$$\frac{1}{n} = \frac{6a'}{5a} + \frac{6m'}{5ut}$$
 (6a' and 6m' from part (b))

$$S_{t} = (274 \times (10^{4})^{-0.132})$$
 (Eq. 6-13 in text book)
= 377.7 MPa a, b from the 1st mid-term exam.

$$6a = \frac{Pa}{A}$$
, $6m = \frac{Pm}{A}$ $Pa = \frac{Pmax - Pmin}{2}$, $P_m = \frac{Pmax + Pmin}{2}$

$$P_{max} = 50 \text{ kN}$$
 and $P_{min} = 10 \text{ kN} = 3$ $G_{m} = 15.9 \text{ MPa}$ $G_{m} = 23.9 \text{ MPa}$

Ma=ME=450N.m Mm=0 (completely reversed bending)

$$6a' = 176.8 \text{ MPa}$$
 } from the solution in part (b) $6m' = 43.8 \text{ MPa}$ (Kf) bending from 1^{56} mid-term exam

$$\frac{6a'}{5e} + \frac{6m'}{5p} = \frac{1}{n} = n = 1.844$$

(Se = 205.4 MPa from the 1st mid-term exam)

(d)
$$6a' = (K_f)_{bending} \left(\frac{32M_a}{\pi d^3}\right) + \frac{(K_f)_{axial}}{0.85} \frac{4P_a}{\pi d^2}$$
Solve for P_a from $\frac{1}{n} = \frac{6a'}{5e} + \frac{6m'}{5ue}$ when $n = 1$

$$=) P_a = 27.8 \text{ kN}.$$

 $(K_f)_{axial}$? 1/d = 0.0375, $D/d = 45/40 = 1.125 \Rightarrow K_t = 2.1$ from Fig. A-15-7. Then, $(K_f)_{axial} = 1 + g(K_t - 1) = 1 + (0.76)(2.1 - 1) = 1.836$ $(g from K_t)_{axial} = 1 + g(K_t)_{axial} = 1 + g(K_t)_{axial}$