

## The Boundary Element Method

The basis of the (Acoustical) Boundary Element Method is the integral equation

$$\alpha \zeta(\mathbf{x}) p(\mathbf{x}) - \int_{\Gamma} \frac{\partial G(\mathbf{x}, \mathbf{y})}{\partial \mathbf{n}(\mathbf{y})} p(\mathbf{y}) \, dS_{\mathbf{y}} + s(\alpha) k \int_{\Gamma} G(\mathbf{x}, \mathbf{y}) v_{\mathbf{n}}(\mathbf{y}) \, dS_{\mathbf{y}} = 0. \quad (1)$$

In order to discretize the integrals we need to approximate the geometry. This can be done using e.g. elements

$$\mathbf{x}^e(\mathbf{u}) = \mathbf{X}^e \mathbf{N}(\mathbf{u}) \in \Gamma^e, \quad \forall \mathbf{u} \in \mathcal{L}, \quad \cup_{e=1}^N \Gamma^e \approx \Gamma \quad (2)$$

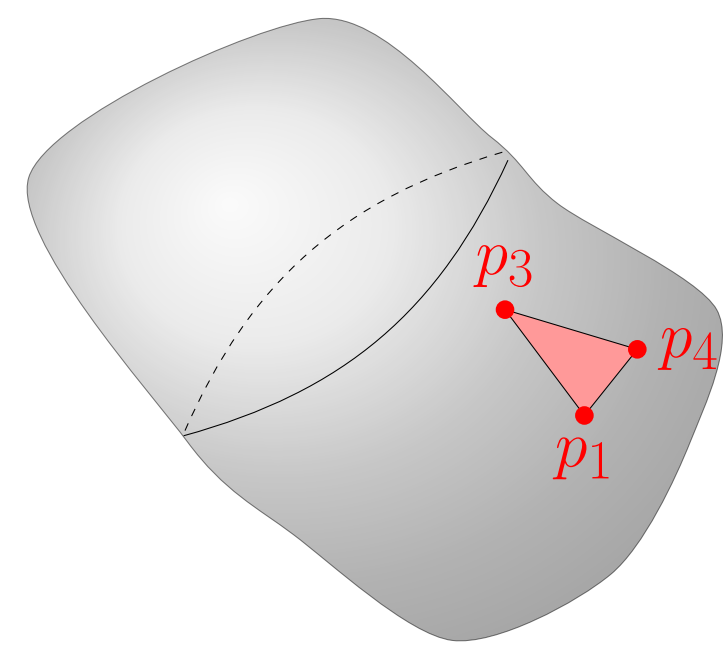


Figure 1. The original domain is shown in gray while a two (linear) elements are shown in red. The red points denote the interpolation nodes of the elements (the columns of  $\mathbf{X}^e$ ).

The pressure (and its normal derivative) on an element can be approximated as

$$p(\mathbf{x}^e(\mathbf{u})) = \mathbf{T}(\mathbf{x}^e(\mathbf{u})) \mathbf{p} = \underbrace{\mathbf{T}(\mathbf{x}(\mathbf{u}))(\mathbf{L}^e)^{\top}}_{\mathbf{T}^e(\mathbf{u})} \underbrace{\mathbf{L}^e \mathbf{p}}_{\mathbf{p}^e} = \mathbf{T}^e(\mathbf{u}) \mathbf{p}^e, \quad \mathbf{u} \in \mathcal{L}, \quad (3)$$

where  $\mathbf{L}^e$  is a matrix that extracts the relevant rows of  $\mathbf{p}$ , i.e. for the element in Figure 1 we have that

$$\mathbf{L}^e = \begin{bmatrix} 1 & 0 & 0 & 0 & \dots & 0 \\ 0 & 0 & 0 & 1 & \dots & 0 \\ 0 & 0 & 1 & 0 & \dots & 0 \end{bmatrix}, \quad \text{so that} \quad \begin{bmatrix} p_1 \\ p_4 \\ p_3 \end{bmatrix} = \mathbf{L}^e \mathbf{p}. \quad (4)$$

The final ingredient is to approximate the integral on the  $e$ th element by using a quadrature scheme

$$\int_{\Gamma^e} f(\mathbf{y}) \, dS_{\mathbf{y}} = \int_{\mathcal{L}} \text{jacobian}(\mathbf{u}) f(\mathbf{u}) \, d\mathbf{u} \approx \sum_{i=1}^Q \text{jacobian}(\mathbf{u}_i) w_i f(\mathbf{u}_i). \quad (5)$$

Using all of the above it is found that the discrete form of (1) is

$$(\text{diag}(\zeta) - \mathbf{F}) \mathbf{p} + s(\alpha) k \mathbf{G} \mathbf{v}_{\mathbf{n}} = \mathbf{H} \mathbf{p} + s(\alpha) k \mathbf{G} \mathbf{v}_{\mathbf{n}} = \mathbf{0}, \quad (6)$$

## References

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## Reduced Order Series Expansion Boundary Element Method (ROSEBEM)

A drawback of the BEM is that the discrete form of (6) depends on the frequency, meaning that for every frequency of interest it needs to be recomputed. A simple Taylor expansion of the Green's function can alleviate this pain as it transforms the discrete form into<sup>[6]</sup>

$$\left( \text{diag}(\zeta) - \sum_{m=0}^{M-1} \frac{(k - k_0)^m}{m!} \mathbf{F}_m(k_0) \right) \mathbf{p} + s(\alpha) k \left( \sum_{m=0}^{M-1} \frac{(k - k_0)^m}{m!} \mathbf{G}_m(k_0) \right) \mathbf{v}_n \approx \mathbf{0}. \quad (7)$$

This approach, however, increase memory usage due to the storing of  $M$ -times the matrices. So solve this a reduced basis can be used, i.e. introduce  $\mathbf{U}_{\ell}$  such that

$$\mathbf{p} \approx \mathbf{U}_{\ell} \mathbf{p}_{\ell}, \quad \frac{\partial \mathbf{p}}{\partial \mathbf{n}} \approx \mathbf{U}_{\ell} \frac{\partial \mathbf{p}_{\ell}}{\partial \mathbf{n}}. \quad (8)$$

### Including the Boundary Layer Impedance condition

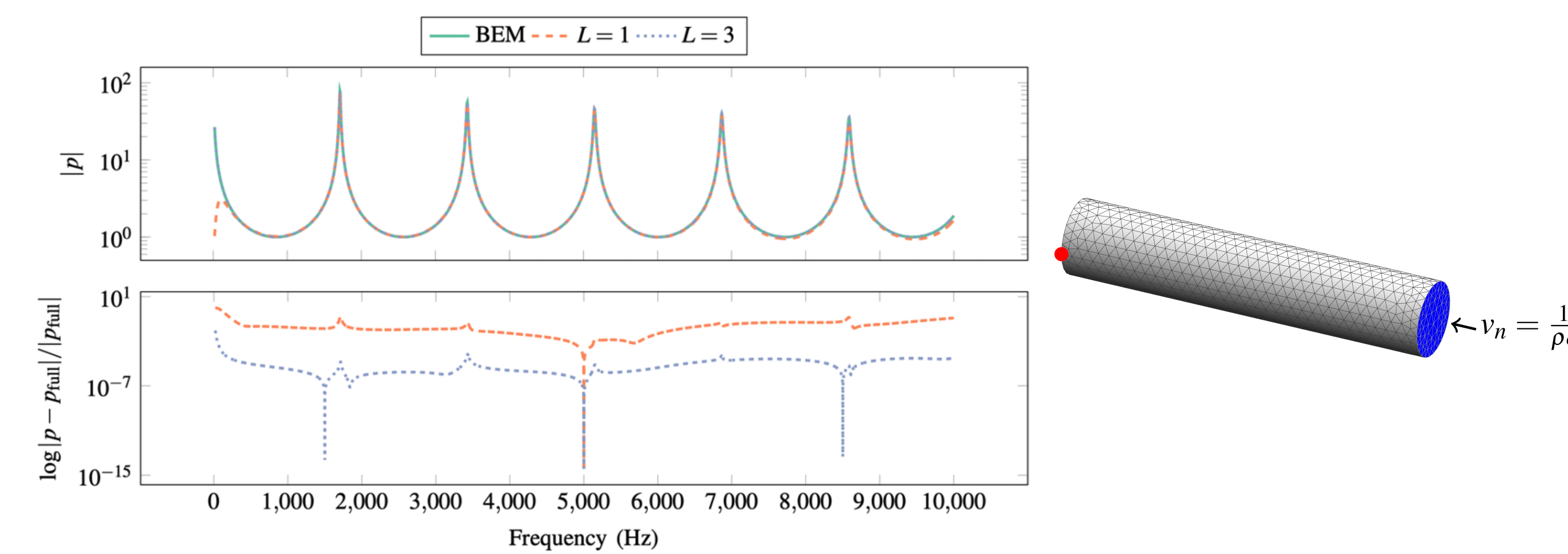
The inclusion of viscothermal losses can sometimes be handed by using the Boundary Layer Impedance condition<sup>[1]</sup>

$$\frac{\partial p}{\partial \mathbf{n}}(\mathbf{x}) = \left[ (\gamma - 1) \frac{ik^2}{k_h} - \frac{i\Delta_{\parallel}}{k_v} \right] p(\mathbf{x}), \quad (9)$$

Using this the ROSEBEM system becomes

$$\sum_{m=0}^{M-1} \frac{(k - k_0)^m}{m!} \left( \left[ \mathbf{F}_{\ell m}(k_0) + \frac{(\gamma - 1)ik^2}{k_h} \mathbf{H}_{\ell m}(k_0) + \frac{i}{k_v} \mathbf{T}_{\ell m}(k_0) \right] \mathbf{p}_{\ell} + \mathbf{G}_{\ell m}(k_0) \frac{\partial \mathbf{p}_{\ell}}{\partial \mathbf{n}} \right) \approx \mathbf{0}. \quad (10)$$

## Results



## Improvements in the full formulation

The basis of the full formulation is the Kirchhoff decomposition which splits the problem into three modes<sup>[2,4]</sup>

$$\text{Acoustic Mode: } (\Delta + k_a^2) p_a(\mathbf{x}) = 0, \quad (11)$$

$$\text{Thermal Mode: } (\Delta + k_h^2) p_h(\mathbf{x}) = 0, \quad (12)$$

$$\text{Viscous Mode: } (\Delta + k_v^2) \mathbf{v}_v(\mathbf{x}) = \mathbf{0}, \quad \text{with } \nabla \cdot \mathbf{v}_v(\mathbf{x}) = 0. \quad (13)$$

The modes are coupled on the boundary as

$$\text{Isothermal: } p_a(\mathbf{x}) \tau_a + p_h(\mathbf{x}) \tau_h = 0, \quad \mathbf{x} \in \Gamma, \quad (14)$$

$$\text{No-slip: } \nabla p_a(\mathbf{x}) \phi_a + \nabla p_h(\mathbf{x}) \phi_h + \mathbf{v}_v(\mathbf{x}) = \mathbf{v}_{\text{boundary}}(\mathbf{x}). \quad (15)$$

The new formulation utilizes that the gradient can be split in two as

$$\nabla p = \nabla^{\parallel} p + \nabla^{\perp} p. \quad (16)$$

Using this it turns out that the solution to the KD-BEM can be found by solving

$$\left[ \mathbf{G}_a \left( \mu_a (\mathbf{R}\mathbf{N})^{-1} \mathbf{R} \mathbf{D}_c + \mu_h \mathbf{G}_h^{-1} \mathbf{H}_h \right) - \phi_a \mathbf{H}_a \right] \mathbf{p}_a = \mathbf{G}_a (\mathbf{R}\mathbf{N})^{-1} \mathbf{R} \mathbf{v}_s. \quad (17)$$

Note that in (17) every matrix except  $\mathbf{G}_a$  and  $\mathbf{H}_a$  are *sparse*. However, both matrices can be approximated using an acceleration method such as e.g. the Fast Multipole Method or the H-Matrix approach<sup>[4]</sup>. In the case of the  $\mathbf{G}_a$ -matrix the acceleration is as follows

$$\left( \underbrace{\int_{\Gamma} G_a(\mathbf{t}_k, \mathbf{y}) \mathbf{T}(\mathbf{y}) \, dS_{\mathbf{y}}}_{k\text{th row of } \mathbf{G}} \right) \mathbf{z} = \left( \sum_{j=1}^{NQ} G_a(\mathbf{t}_k, \mathbf{y}_j) \underbrace{\text{jacobian}(\mathbf{u}_j) w_j \mathbf{T}^{e(j)}(\mathbf{u}_j) \mathbf{L}^{e(j)}}_{j\text{th row of } \mathbf{C}} \right) \mathbf{z} \quad (18)$$

$$= [G_a(\mathbf{t}_k, \mathbf{y}_1) \ G_a(\mathbf{t}_k, \mathbf{y}_2) \ \dots \ G_a(\mathbf{t}_k, \mathbf{y}_{NQ})] \mathbf{C} \mathbf{z}$$

## Results

