



The Boundary Element Method

The basis of the (Acoustical) Boundary Element Method is the integral equation

$$\alpha \zeta(\mathbf{x}) p(\mathbf{x}) - \int_{\Gamma} \frac{\partial G(\mathbf{x}, \mathbf{y})}{\partial \mathbf{n}(\mathbf{y})} p(\mathbf{y}) \, dS_{\mathbf{y}} + s(\alpha) k \int_{\Gamma} G(\mathbf{x}, \mathbf{y}) v_{\mathbf{n}}(\mathbf{y}) \, dS_{\mathbf{y}} = 0. \quad (1)$$

In order to discretize the integrals we need to approximate the geometry. This can be done using e.g. elements

$$\mathbf{x}^e(\mathbf{u}) = \mathbf{X}^e \mathbf{N}(\mathbf{u}) \in \Gamma^e, \quad \forall \mathbf{u} \in \mathcal{L}, \quad \bigcup_{e=1}^N \Gamma^e \approx \Gamma \quad (2)$$

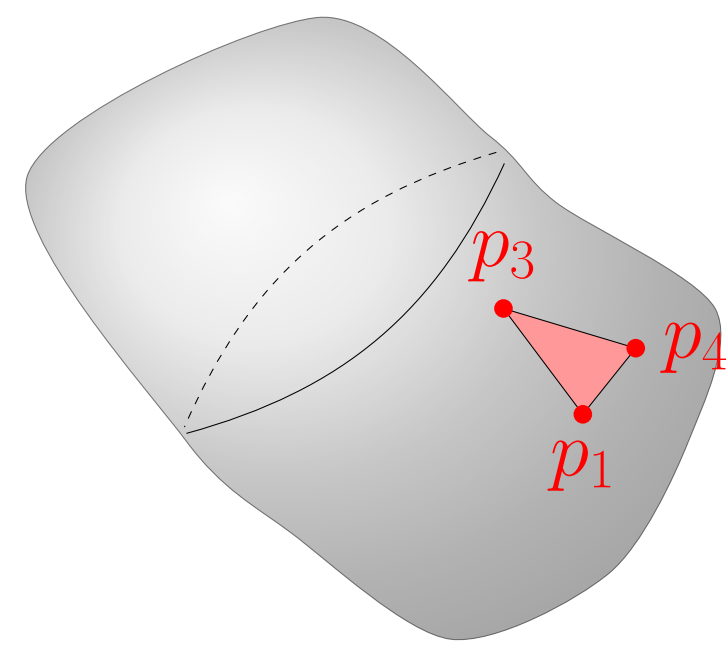


Figure 1. The original domain is shown in gray while a two (linear) elements are shown in red. The red points denote the interpolation nodes of the elements (the columns of \mathbf{X}^e).

The pressure (and its normal derivative) on an element can be approximated as

$$p(\mathbf{x}^e(\mathbf{u})) = \mathbf{T}(\mathbf{x}^e(\mathbf{u})) \mathbf{p} = \underbrace{\mathbf{T}(\mathbf{x}(\mathbf{u}))(\mathbf{L}^e)^{\top}}_{\mathbf{T}^e(\mathbf{u})} \underbrace{\mathbf{L}^e \mathbf{p}}_{\mathbf{p}^e} = \mathbf{T}^e(\mathbf{u}) \mathbf{p}^e, \quad \mathbf{u} \in \mathcal{L}, \quad (3)$$

where \mathbf{L}^e is a matrix that extracts the relevant rows of \mathbf{p} , i.e. for the element in Figure 1 we have that

$$\mathbf{L}^e = \begin{bmatrix} 1 & 0 & 0 & 0 & \dots & 0 \\ 0 & 0 & 0 & 1 & \dots & 0 \\ 0 & 0 & 1 & 0 & \dots & 0 \end{bmatrix}, \quad \text{so that} \quad \begin{bmatrix} p_1 \\ p_4 \\ p_3 \end{bmatrix} = \mathbf{L}^e \mathbf{p}. \quad (4)$$

The final ingredient is to approximate the integral on the e th element by using a quadrature scheme

$$\int_{\Gamma^e} f(\mathbf{y}) \, dS_{\mathbf{y}} = \int_{\mathcal{L}} \text{jacobian}(\mathbf{u}) f(\mathbf{u}) \, d\mathbf{u} \approx \sum_{i=1}^Q \text{jacobian}(\mathbf{u}_i) w_i f(\mathbf{u}_i). \quad (5)$$

Using all of the above it is found that the discrete form of (1) is

$$(\text{diag}(\zeta) - \mathbf{F}) \mathbf{p} + s(\alpha) k \mathbf{G} \mathbf{v}_{\mathbf{n}} = \mathbf{H} \mathbf{p} + s(\alpha) k \mathbf{G} \mathbf{v}_{\mathbf{n}} = \mathbf{0}, \quad (6)$$

References

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Reduced Order Series Expansion Boundary Element Method (ROSEBEM)

The Boundary Layer Impedance (BLI) boundary condition can be used to approximate the viscothermal losses

$$\frac{\partial p}{\partial \mathbf{n}}(\mathbf{x}) = \left[(\gamma - 1) \frac{ik^2}{k_h} - \frac{i\Delta_{\parallel}}{k_v} \right] p(\mathbf{x}). \quad (7)$$

Inserting the above into (1) and doing some manipulation it follows that

$$\zeta(\mathbf{x}) p(\mathbf{x}) = \int_{\Gamma_N} G(\mathbf{x}, \mathbf{y}) \frac{\partial p(\mathbf{y})}{\partial \mathbf{n}(\mathbf{y})} \, dS_{\mathbf{y}} - \int_{\Gamma} \frac{\partial G(\mathbf{x}, \mathbf{y})}{\partial \mathbf{n}(\mathbf{y})} p(\mathbf{y}) \, dS_{\mathbf{y}} + \frac{(\gamma - 1)ik^2}{k_h} \int_{\Gamma_{BLI}} G(\mathbf{x}, \mathbf{y}) p(\mathbf{y}) \, dS_{\mathbf{y}} + \frac{i}{k_v} \int_{\Gamma_{BLI}} \nabla_{\mathbf{y}}^{\parallel} G(\mathbf{x}, \mathbf{y}) \cdot \nabla_{\mathbf{y}}^{\parallel} p(\mathbf{y}) \, dS_{\mathbf{y}}, \quad (8)$$

A drawback of the BEM is that the discrete form of (6) depends on the frequency, meaning that for every frequency of interest it needs to be recomputed. A simple Taylor expansion of the Green's function can alleviate this pain as it transforms the discrete form into^[6]

$$\left(\sum_{m=0}^M \frac{(k - k_0)^m}{m!} \left[\begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} + \frac{(\gamma - 1)ik^2}{k_h} \begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} + \frac{i}{k_v} \begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} \right] \mathbf{p} + \begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} \partial_{\mathbf{n}} \mathbf{p} \right) = \mathbf{0} \quad (9)$$

This approach, however, increase memory usage due to the storing of M -times the matrices. To solve this a reduced basis can be used, i.e. introduce \mathbf{U}_{ℓ} such that

$$\mathbf{p} \approx \mathbf{U}_{\ell} \mathbf{p}_{\ell}, \quad \frac{\partial \mathbf{p}}{\partial \mathbf{n}} \approx \mathbf{U}_{\ell} \frac{\partial \mathbf{p}_{\ell}}{\partial \mathbf{n}}, \quad \left(\begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} = \begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} \begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} \right) \quad (10)$$

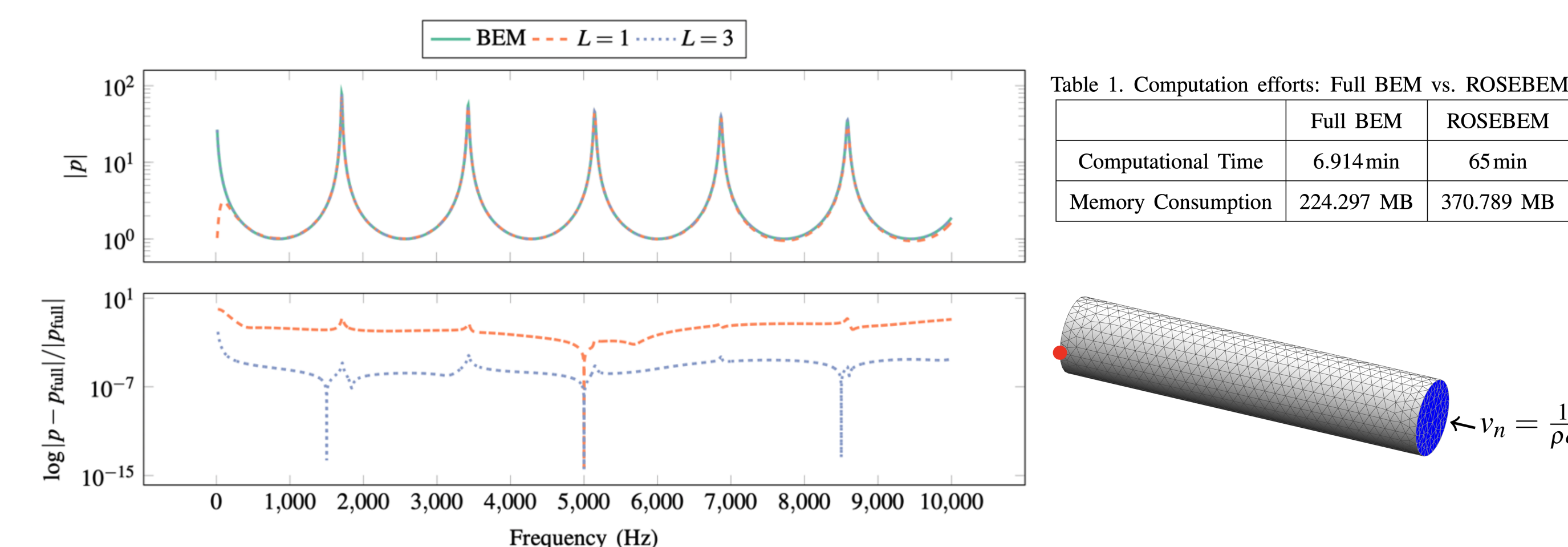
As such (9) becomes

$$\left(\sum_{m=0}^M \frac{(k - k_0)^m}{m!} \left[\begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} + \frac{(\gamma - 1)ik^2}{k_h} \begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} + \frac{i}{k_v} \begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} \right] \mathbf{p}_{\ell} + \begin{bmatrix} \square & \square & \square & \square & \square & \square \end{bmatrix} \partial_{\mathbf{n}} \mathbf{p}_{\ell} \right) = \mathbf{0}. \quad (11)$$

In many practical cases storing all the matrices from the above requires about the same memory as the original BEM system from (8).

Results

The results shows that the model accurately describes the pressure while decreasing the computational efforts by 100x using only 1.65x the memory.



Improvements in the full formulation

Visually the new formulation looks as

$$\begin{bmatrix} \square & \square & 0 & 0 & 0 & 0 \\ 0 & 0 & \square & \square & 0 & 0 \\ 0 & 0 & 0 & 0 & \square & \square \\ 0 & 0 & 0 & 0 & \square & \square \\ \square & \square & 0 & 0 & 0 & 0 \\ \square & \square & \square & \square & \square & 0 \end{bmatrix} \begin{bmatrix} \mathbf{p}_a \\ \partial_n \mathbf{p}_a \\ \mathbf{p}_h \\ \partial_n \mathbf{p}_h \\ \begin{bmatrix} \mathbf{v}_x \\ \mathbf{v}_y \\ \mathbf{v}_z \end{bmatrix} \\ \begin{bmatrix} \partial_n \mathbf{v}_x \\ \partial_n \mathbf{v}_y \\ \partial_n \mathbf{v}_z \end{bmatrix} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ \begin{bmatrix} \mathbf{v}_{b,x} \\ \mathbf{v}_{b,y} \\ \mathbf{v}_{b,z} \end{bmatrix} \end{bmatrix}$$

The acoustical pressure can be found by solving the following

$$\left[\mathbf{G}_a \left(\mu_a (\mathbf{R}\mathbf{N})^{-1} \mathbf{R} \mathbf{D}_c + \mu_h \mathbf{G}_h^{-1} \mathbf{H}_h \right) - \phi_a \mathbf{H}_a \right] \mathbf{p}_a = \mathbf{G}_a (\mathbf{R}\mathbf{N})^{-1} \mathbf{R} \mathbf{v}_s. \quad (12)$$

Note that in (12) every matrix except \mathbf{G}_a and \mathbf{H}_a are *sparse*. However, both matrices can be approximated using an acceleration method such as e.g. the Fast Multipole Method or the H-Matrix approach by approximating the multiplication^[4]

$$\left(\underbrace{\int_{\Gamma} G_a(\mathbf{t}_k, \mathbf{y}) \mathbf{T}(\mathbf{y}) \, dS_{\mathbf{y}}}_{k\text{th row of } \mathbf{G}} \right) \mathbf{z} \approx \underbrace{\left[G_a(\mathbf{t}_k, \mathbf{y}_1) \, G_a(\mathbf{t}_k, \mathbf{y}_2) \, \dots \, G_a(\mathbf{t}_k, \mathbf{y}_{NQ}) \right]}_{\text{multiplication with this can be accelerated}} \mathbf{C} \mathbf{z}, \quad (13)$$

where \mathbf{C} is a sparse matrix.

Results

