

Radiative-convective equilibrium in a grey atmosphere

Marco Casari

September 11, 2023

Abstract

Radiative-convective models provide an intermediate complexity approach to the simulation of climate. These models evaluate the atmospheric temperature profile averaged over all latitudes and longitudes, which is function of time and altitude. Physical processes which determine the energy exchange in the model are absorption, transmission, reflection of electromagnetic radiation and convection of fluid. In this work a radiative-convective model is used to derive the temperature of an atmosphere where the optical depth is constant with respect to the frequency of radiation. The resulting temperature profile is compared with the analytical solution provided under the condition of radiative equilibrium.

1 Introduction

Climate dynamics of a planet can be studied with models of varying complexity. One of the quantities analysed is the temporal and spatial distribution of temperature in the planetary atmosphere, which is the result of the heat exchange between different processes. Electromagnetic (EM) radiation is emitted, absorbed and scattered by the chemical species distributed in the atmosphere and by the planetary surface. Moreover, the atmosphere receives EM radiation by other celestial bodies, e.g. stars. Radiative processes are described by the Radiative Transfer Equation (RTE). Local temperature differences generate motion of fluid parcels, hence convection. A rough planetary surface can hinder horizontal heat transport. Fluid dynamics equations are needed to represent these processes.

Fluid parcels are treated as open systems and the temperature distribution is obtained by a suitable thermodynamic energy equation, coupled with

the equations of the processes occurring in the atmosphere. Even by limiting the analysis to radiative processes and convection, which are the main drivers of temperature variations, the equations involved are not solvable analytically and are not tractable numerically without simplifications.

A first approximation is to consider the average over all latitudes and longitudes for quantities which depend on spatial position. The resulting atmosphere is represented by plane-parallel layers, identified by their altitude z ranging from z_g at ground level to z_{TOA} at Top Of the Atmosphere (TOA). With this hypothesis, the differential equation describing the average temperature $T(t, z)$ as function of time t and altitude z is

$$\frac{\partial T}{\partial t} = -\frac{1}{\varrho c_P} \frac{\partial q}{\partial z} \quad , \quad (1)$$

where c_P is the specific heat at constant pressure of the atmosphere, ϱ is the average volumetric mass density of the atmosphere and depends on atmospheric pressure P , q is the total energy flux due to heat transfer. In general all these quantities are functions of t and z , also through T . Details on the derivation are in [1, p. 466], where the equation is written initially in terms of volumetric power densities.

A second hypothesis is the radiative-convective equilibrium of the atmosphere. This translates in the existence of a steady state $\frac{\partial}{\partial t}T(t, z) = 0$ where the planet is in radiative equilibrium, i.e. the total irradiance at TOA is null, and the atmosphere is in convective equilibrium, i.e. fluid parcels are stable with respect to vertical motion.

A model with the previous assumptions is called Radiative-Convective Model (RCM). To simplify further the RTE, in this work the dependence of quantities on the frequency of EM radiation is neglected. An atmosphere with this property is called grey atmosphere.

In the following sections the steady state vertical temperature profile of a grey atmosphere is computed. First the hypothesis of radiative equilibrium is used alone to obtain an analytical solution and use it as validation for the respective numerical solution. Then convection is taken into account and a simple RCM is implemented starting from the numerical scheme for radiative equilibrium.

1.1 Hypotheses and conventions

Some additional hypotheses are assumed to simplify the study. Data on constants are listed in table 1 and where possible, values referred to Earth are used for a prompt comparison with reality. Dependencies of quantities are written explicitly when it helps to clarify the discussion.

Some assumptions are made on the planet. It is supposed to have a diurnal cycle, to receive a constant irradiance S_0 and to have a constant Bond albedo A . These conditions result in a constant irradiance

$$S_t = (1 - A) \frac{S_0}{4} \quad (2)$$

transmitted to the illuminated hemisphere of the planet at TOA from outer space. The surface of the planet is approximated as blackbody emitting in the upward direction with temperature T_g . Gravitational acceleration g is constant. The atmosphere is supposed to be in hydrostatic equilibrium,

$$dP = -\varrho g dz \quad , \quad (3)$$

with P atmospheric pressure. Specific heat at constant pressure c_P is assumed constant. Scattering is neglected, hence the attenuation coefficient is equal to the absorption coefficient and the symbol $\mu(z)$ is used for both. Moreover, the absorption coefficient is supposed to depend on z through

$$\mu(z) = \mu_m \varrho(z) \quad , \quad (4)$$

where μ_m is the mass attenuation coefficient of the atmosphere, assumed constant.

For gases, specific gas constant R_m is used in thermodynamic relations, which is defined as the gas constant R divided by the molar mass of the gas. They obey the ideal gas law

$$P = \varrho R_m T \quad . \quad (5)$$

The total heat flux q is determined by radiative transfer and atmospheric convection. The RTE is not solved directly by the RCM, instead a two-stream approximation is adopted for the radiation inside atmosphere: components of radiometric quantities in the upward and downward directions are treated separately. Neither the contribution to $q(t, z)$ due to atmospheric convection is obtained by solving the proper fluid dynamics equations, in its place a numerical correction is adopted. With these considerations, equation (1) can be rewritten as

$$\frac{\partial T}{\partial t} = -\frac{1}{\varrho c_P} \frac{\partial}{\partial z} (E_U - E_D) \quad , \quad (6)$$

where E_U and E_D are irradiances of upward and downward radiations, respectively.

1.2 Vertical coordinates

Altitude is an immediate choice as vertical coordinate used to describe the problem. However, calculations may simplify more if expressed with other coordinates.

An alternative choice is P and is convenient when used with equation (3) to remove the dependence on ϱ . A bijective relation relates P and z (cfr. section B.1):

$$P(z) = P_g \exp \left(-\frac{z - z_g}{z_0} \right) \quad , \quad (7)$$

where ground level is chosen as reference and constant z_0 acts to remove the dependence on temperature and thus sets the scale of z . Pressure decreases with altitude from standard value P_g at ground level to P_{TOA} at TOA.

To simplify radiative calculations optical depth δ is used as vertical coordinate, starting from 0 at TOA and increasing downward, up to value δ_g at ground level. From the hypotheses on the attenuation coefficient, δ is a function of altitude through

$$\delta(z) = \mu_m \int_z^{z_{\text{TOA}}} \varrho(z') dz' \quad , \quad (8)$$

but a simpler relation exists between δ and P using equation (3) to evaluate the integral in equation (8):

$$\delta(P) = \frac{\mu_m}{g} (P - P_{\text{TOA}}) \quad . \quad (9)$$

Table 1: Data on constants used in the present work. The middle rule separates standard values on top from arbitrary values chosen for the present work on bottom.

Symbol	Value	Unit	Notes
A	0.3		Bond albedo value compatible with various observations, cfr. [2, p. 1281]
A_g	0.1		Average surface albedo of Earth, cfr. [3, p. 217]
c_P	1.004×10^3	J/(K kg)	Specific heat at constant pressure of air, from [4, p. 16]
δ_{TOA}	0		Optical depth at TOA, by definition
D	1.66		Diffusion coefficient, commonly used value from [4, p. 55]
g	9.80665	m/s ²	Standard gravitational acceleration of Earth
P_g	1.013250×10^5	Pa	Standard pressure at ground level, from [5, p. 2]
R_m	2.8705287×10^2	J/(K kg)	Specific gas constant of air
σ	$5.670374419 \times 10^{-8}$	W/(m ² K ⁴)	Stefan-Boltzmann constant
S_0	1361.0	W/m ²	Nominal total solar irradiance, from [6]
T_g	288.15	K	Earth's surface temperature based on [5]
z_g	0	m	Nominal ground level
δ_g	$\frac{1}{D} \left(\frac{2\sigma T_g^4}{S_t} - 2 \right)$		Optical depth at ground level
μ_m	$\frac{\delta_g g}{P_g - P_{\text{TOA}}}$		Mass attenuation coefficient of the atmosphere
N	100		Number of atmospheric layers
P_0	1×10^5	Pa	Arbitrary reference value for pressure
P_{TOA}	3	Pa	Arbitrary TOA pressure
z_0	2000	m	Arbitrary constant for normalisation of z
z_{TOA}	$z_g - z_0 \ln \left(\frac{P}{P_g} \right)$	m	Arbitrary TOA altitude

Relation (9) is used in conjunction with equation (7) to derive a more direct formula for $\delta(z)$:

$$\delta(z) = \frac{\mu_m}{g} \left(P_g \exp \left(- \frac{z - z_g}{z_0} \right) - P_{\text{TOA}} \right) . \quad (10)$$

Value P_{TOA} can be calculated from a fixed z_{TOA} using equation (7), or vice versa.

Any of the previous relations for δ can be used to fix the value of μ_m if δ_g is known, or conversely μ_m can be used as parameter to derive δ_g .

2 Analytical solution in radiative equilibrium

Steady state temperature profile and irradiances are derived analytically in this section.

The additional hypothesis of Local Thermodynamic Equilibrium (LTE) is considered for the at-

mosphere. With these hypotheses, the RTE becomes

$$\frac{1}{\mu} \frac{\partial L}{\partial z} = B_\nu - L \quad , \quad (11)$$

where $L(t, z, \theta, \nu)$ is the spectral radiance arriving at altitude z with angle θ with respect to direction \hat{z} and $B_\nu(\nu, T(t, z))$ is Planck's function (cfr. section B.2).

To apply equation (11) to irradiances, two integrations are needed: one over the whole EM spectrum and one over the solid angle corresponding to a hemisphere. The latter can be performed adopting the diffusion approximation (cfr. [4, p. 55]), which have the effect to substitute δ with $\delta' = D\delta$, where D is the diffusion coefficient. The resulting

equations for irradiances in terms of δ' are

$$-\frac{\partial}{\partial \delta'} E_U(t, \delta') = \sigma T(t, \delta')^4 - E_U(t, \delta') \quad , \quad (12)$$

$$\frac{\partial}{\partial \delta'} E_D(t, \delta') = \sigma T(t, \delta')^4 - E_D(t, \delta') \quad (13)$$

and they are coupled with equation (6) written in terms of δ' :

$$\frac{\partial}{\partial t} T(t, \delta') = \frac{\mu_m D}{c_P} \frac{\partial}{\partial \delta'} (E_U - E_D) \quad . \quad (14)$$

Equations (14), (12) and (13) form a system of Partial Differential Equations (PDEs) of first order in two variables.

When the steady state of T is searched, dependence on t is dropped and the PDEs become Ordinary Differential Equations (ODEs) of first order of an Initial Value Problem (IVP). Initial conditions for irradiances are

$$E_D(0) = 0 \quad (15)$$

because energy released to atmosphere at TOA by the downward flux is negligible and $E_U(0)$ is a constant called Outgoing Longwave Radiation (OLR). Radiative equilibrium provides the condition for the OLR:

$$E_U(0) = S_t \quad . \quad (16)$$

At the steady state, irradiances are related by

$$\frac{d}{d\delta'} (E_U(\delta') - E_D(\delta')) = 0 \quad , \quad (17)$$

which has solution

$$E_U(\delta') - E_D(\delta') = S_t \quad . \quad (18)$$

Since heat transfer in equation (6) is determined only by radiative processes, this relation is equivalent to the hypotheses of atmosphere in radiative equilibrium at all altitudes and transparent to radiation coming from outside the planet. The ODE for T is obtained by adding and subtracting equations (12) and (13) and using the conditions provided by equations (17) and (18):

$$2\sigma \frac{d}{d\delta'} T(\delta')^4 = S_t \quad . \quad (19)$$

In a similar way, initial condition for T is obtained by summing equations (12) and (13) and applying relation (17) and the initial conditions (16)

and (15):

$$T(0) = \left(\frac{S_t}{2\sigma} \right)^{\frac{1}{4}} \quad . \quad (20)$$

The solution of equation (19) in terms of δ is

$$T(\delta) = \left(\frac{S_t}{2\sigma} (1 + D\delta) \right)^{\frac{1}{4}} \quad , \quad (21)$$

represented in figure 1.

Once the temperature profile is known, $E_U(\delta)$ and $E_D(\delta)$ are evaluated with the same procedure used previously for $T(\delta')$, resulting in:

$$E_U(\delta) = \frac{S_t}{2} (2 + D\delta) \quad , \quad (22)$$

$$E_D(\delta) = \frac{S_t}{2} D\delta \quad . \quad (23)$$

Irradiances are shown in figure 2. At every altitude, E_U and E_D are greater than their respective values at TOA. This is result of the greenhouse effect of the atmosphere.

Value δ_g can be fixed by using the irradiance emitted by the surface of the planet:

$$E_U(\delta_g) = \sigma T_g^4 \quad . \quad (24)$$

With this condition, T presents a discontinuity at ground level, which is not physical. Other mechanisms of heat transport redistribute energy at the lower levels of the atmosphere.

3 Numerical solution in radiative equilibrium

To solve numerically the IVP defined in section 2, equations (19), (12) and (13) are rewritten in terms of variable δ and normalised with respect to S_t ,

$$Y_0 = \frac{\sigma T^4}{S_t} \quad , \quad Y_1 = \frac{E_U}{S_t} \quad , \quad Y_2 = \frac{E_D}{S_t} \quad , \quad (25)$$

resulting in the system of ODEs:

$$\begin{cases} \frac{dY_0}{d\delta} = \frac{D}{2} \\ \frac{dY_1}{d\delta} = D(Y_1 - Y_0) \\ \frac{dY_2}{d\delta} = D(Y_0 - Y_2) \end{cases} \quad . \quad (26)$$

Initial conditions for the normalised functions are

$$Y_0 = \frac{1}{2} \quad , \quad Y_1 = 1 \quad , \quad Y_2 = 0 \quad , \quad (27)$$

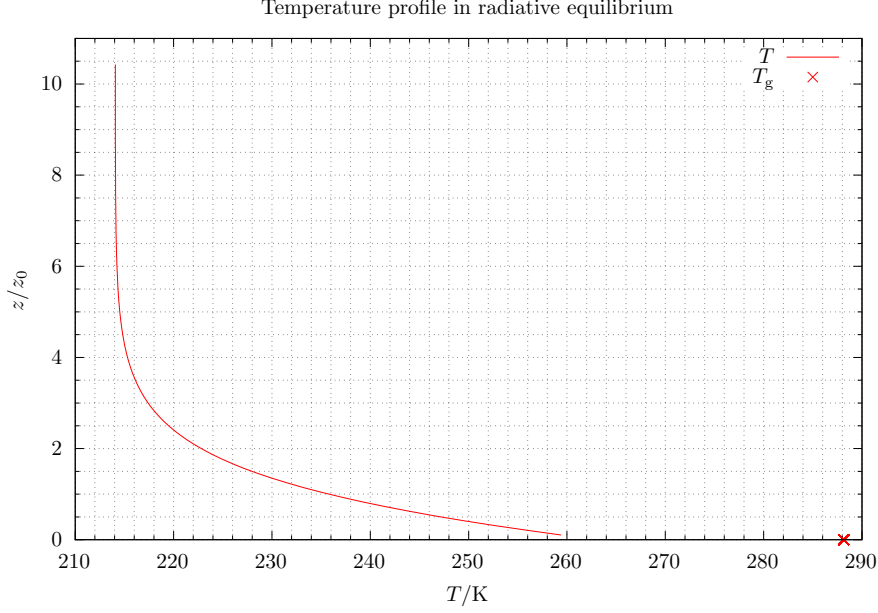


Figure 1: Vertical temperature profile of a grey atmosphere in radiative equilibrium. Lower altitudes are candidate to present instability due to higher values of the slope.

from conditions (20), (16) and (15), respectively.

Runge-Kutta method of order 4 is used to integrate system (26), to maintain accuracy when T is derived from Y_0 . A variable step size is adopted, because values δ are obtained from uniformly distributed values z through relation (10).

Errors between numerical and analytical solutions for normalised temperature and irradiances are shown in figure 3. Their values are compatible with 0 based on precision of double-precision floating-point numbers.

3.1 Stability

Stability analysis of the numerical method is performed on N and this is equivalent to change the spatial grid size. Powers of 2 are chosen as values of N and step size is constant, obtained by dividing interval $[\delta_{\text{TOA}}, \delta_g]$ by N . Errors are evaluated as absolute differences between numerical and analytical values for each of $T(\delta_g)$, $E_U(\delta_g)$ and $E_U(\delta_g)$. For $N \leq 4096$, errors are compatible with 0 within precision, while for greater N , errors increase due to error propagation. Normally this effect does not hinder results of simulations because lower values

of N are chosen for the model, since average dynamics could lose accuracy if thin layers are used.

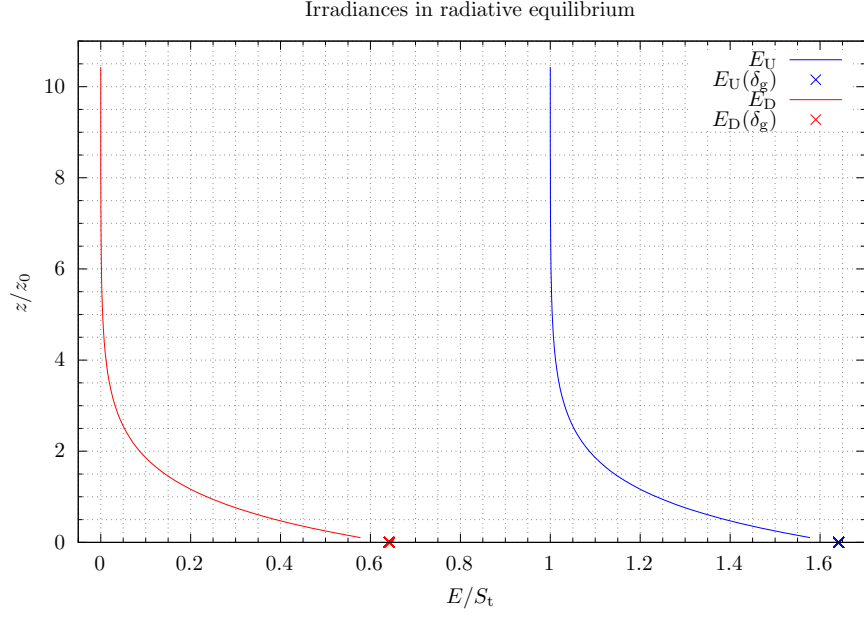


Figure 2: Upward and downward irradiances in a grey atmosphere in radiative equilibrium.

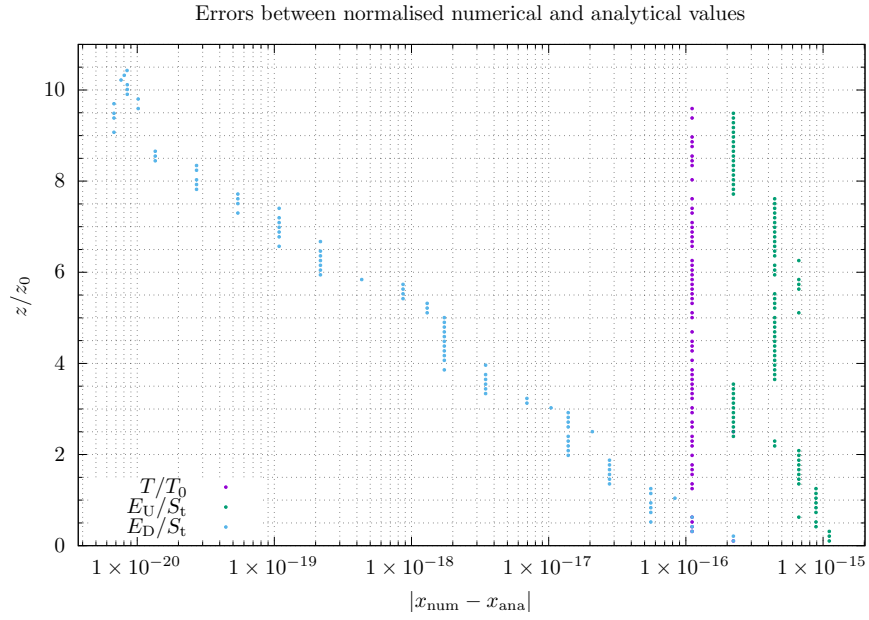


Figure 3: Errors

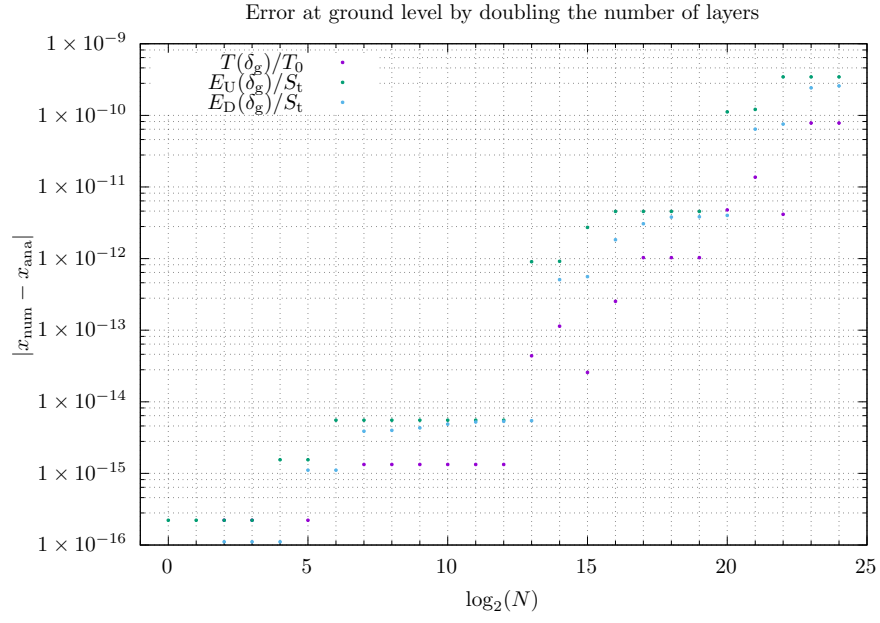


Figure 4: Stability analysis.

A Source code

In this section the C++ code used to obtain the results presented in this work is shown and commented.

First, the parametrization of the vertical coordinate is chosen among three alternatives: altitude z in m, atmospheric pressure P in Pa, coordinate $\sigma = \frac{P-P_{\text{TOA}}}{P_S-P_{\text{TOA}}}$ adimensional, with P_{TOA} pressure at the top of the modelised atmosphere and P_S pressure at the surface. One parametrisation can be written in term of another through a monotonic function (e.g. pressure decreases with altitude, cfr. section B.1). For the initial development the altitude z is chosen as vertical coordinate because it is more intuitive, moreover plots in [7] are expressed in terms of both z and P .

Second, the atmospheric layers are configured. In [7] 20 layers are used and they are numbered from the top of the atmosphere down as it is common in RCMs. The vertical coordinate refers to the center of each layer, with the exception of the last layer which is in direct contact with the surface and needs to be treated separately. Therefore two arrays are needed: one for the point and one with the corresponding layer thicknesses. Values are then assigned as double precision numbers. The value corresponding to the top of the atmosphere is set in a proper variable and a uniform distribution of layer thicknesses is assumed for ease.

```
1 #include <cmath>
2 #include <fstream>
3 #include <iomanip>
4 #include <iostream>
5
6 #include "constants.h"
7 #include "../mclib/mclib.h"
8 #include "radiation.h"
9 #include "utilities.h"
10 #include "configuration.h" // Include last to allow redefinitions.
11
12 void rhs(double t, double const * Y_0, double * R);
```



```

13
14 int main(int argc, char * argv[]) {
15     using namespace std;
16     cout << fixed << setprecision(N_PRECISION);
17
18     // Configure vertical coordinates.
19     double * z, * dz; // / m
20     z = new double[global_N];
21     dz = new double[global_N];
22     set_layers_uniform(global_z_g, get_altitude(global_P_TOA), global_N, z, dz);
23
24     // Precompute other vertical coordinates.
25     double * P; // / Pa
26     double * delta, * sigma;
27     delta = new double[global_N];
28     P = new double[global_N];
29     sigma = new double[global_N];
30     for (int i = 0; i < global_N; i++) {
31         delta[i] = get_optical_depth_z(z[i], global_P_TOA);
32         P[i] = get_pressure(z[i]);
33         sigma[i] = get_sigma(P[i], global_P_TOA);
34     }
35
36
37
38     /* Analytical solution in radiative equilibrium */
39
40     // Prepare variables.
41     double * T, * theta, * E_U, * E_D;
42     double T_0; // / K
43     T = new double[global_N];
44     theta = new double[global_N];
45     E_U = new double[global_N];
46     E_D = new double[global_N];
47     T_0 = pow(global_S_t / global_sigma, 0.25);
48
49     // Prepare output files.
50     ofstream file_temperature, file_irradiance;
51     char fn_temperature_analytical[] = DIR_DATA "/temperature_analytical.dat";
52     char fn_irradiance_analytical[] = DIR_DATA "/irradiance_analytical.dat";
53     file_temperature << fixed << setprecision(N_PRECISION);
54     file_temperature.open(fn_temperature_analytical);
55     file_temperature << "#z/z_0 T delta P sigma theta" << endl;
56     file_temperature << "'1' 'K' '1' 'Pa' '1' 'K'" << endl;
57     file_irradiance << fixed << setprecision(N_PRECISION);
58     file_irradiance.open(fn_irradiance_analytical);
59     file_irradiance << "#z/z_0 E_U/S_t E_D/S_t delta P sigma" << endl;
60     file_irradiance << "'1' '1' '1' '1' 'Pa' '1'" << endl;
61
62     // Plot analytical solutions.
63     for (int i = 0; i < global_N; i++) {
64         T[i] = temperature_norm(delta[i]);
65         theta[i] = get_theta(T[i], P[i]);
66         file_temperature << z[i] / global_z_0 << ' ' << T_0 * T[i] << ' ' << delta[i] << ' ' << P[i] << ' ' << sigma[i] << ' ' << T_0 * theta[i] << '\n';
67         E_U[i] = irradiance_upward_norm(delta[i]);
68         E_D[i] = irradiance_downward_norm(delta[i]);
69         file_irradiance << z[i] / global_z_0 << ' ' << E_U[i] << ' ' << E_D[i] << ' ' << delta[i] << ' ' << P[i] << ' ' << sigma[i] << '\n';
70     }
71     file_temperature.close();
72     cout << "Analytical solution temperature profile in radiative equilibrium calculated,

```

```

73     values are stored in file " << fn_temperature_analytical << endl;
74     file_irradiance.close();
75     cout << "Analytical solution irradiances in radiative equilibrium calculated, values
76         are stored in file " << fn_irradiance_analytical << endl;
77
78     /* Numerical solution in radiative equilibrium */
79
80     // Prepare variables and set initial conditions.
81     double Y[3];
82     double T_tmp, theta_tmp;
83     Y[0] = 0.5;
84     Y[1] = 1.0;
85     Y[2] = 0.0;
86     T_tmp = pow(Y[0], 0.25);
87     theta_tmp = get_theta(T_tmp, P[0]);
88
89     // Prepare output files.
90     char fn_irradiance_numerical[] = DIR_DATA "/irradiance_numerical.dat";
91     char fn_temperature_numerical[] = DIR_DATA "/temperature_numerical.dat";
92     ofstream file_errors;
93     char fn_errors[] = DIR_DATA "/errors.dat";
94     file_temperature << fixed << setprecision(N_PRECISION);
95     file_temperature.open(fn_temperature_numerical);
96     file_irradiance << "#z/z_0 T delta P sigma theta" << endl;
97     file_temperature << "#'1' 'K' '1' 'Pa' '1' 'K'" << endl;
98     file_irradiance << fixed << setprecision(N_PRECISION);
99     file_irradiance.open(fn_irradiance_numerical);
100    file_irradiance << "#z/z_0 E_U/S_t E_D/S_t delta P sigma" << endl;
101    file_irradiance << "#'1' '1' '1' '1' 'Pa' '1'" << endl;
102    file_errors << scientific << setprecision(N_PRECISION);
103    file_errors.open(fn_errors);
104    file_errors << "#z/z_0 T/T_0 theta/T_0 E_U/S_t E_D/S_t delta P sigma" << endl;
105    file_errors << "#'1' '1' '1' '1' '1' '1' 'Pa' '1'" << endl;
106
107    // Integrate equations.
108    file_temperature << z[0] / global_z_0 << ' ' << T_0 * T_tmp << ' ' << delta[0] << ' '
109        << P[0] << ' ' << sigma[0] << ' ' << T_0 * theta[0] << '\n';
110    file_irradiance << z[0] / global_z_0 << ' ' << Y[1] << ' ' << Y[2] << ' ' << delta[0]
111        << ' ' << P[0] << ' ' << sigma[0] << '\n';
112    file_errors << z[0] / global_z_0 << ' ' << fabs(T_tmp - T[0]) << ' ' << fabs(theta_tmp
113        - theta[0]) << ' ' << fabs(Y[1] - E_U[0]) << ' ' << fabs(Y[2] - E_D[0]) << ' ' <<
114        delta[0] << ' ' << P[0] << ' ' << sigma[0] << '\n';
115    for (int i = 1; i < global_N; i++) {
116        rungekutta4(delta[i], delta[i] - delta[i-1], Y, rhs, 3);
117        T_tmp = pow(Y[0], 0.25);
118        theta_tmp = get_theta(T_tmp, P[i]);
119        file_temperature << z[i] / global_z_0 << ' ' << T_0 * T_tmp << ' ' << delta[i] << ' '
120            << P[i] << ' ' << sigma[i] << ' ' << T_0 * theta[i] << '\n';
121        file_irradiance << z[i] / global_z_0 << ' ' << Y[1] << ' ' << Y[2] << ' ' << delta[i]
122            << ' ' << P[i] << ' ' << sigma[i] << '\n';
123        file_errors << z[i] / global_z_0 << ' ' << fabs(T_tmp - T[i]) << ' ' << fabs(
124            theta_tmp - theta[i]) << ' ' << fabs(Y[1] - E_U[i]) << ' ' << fabs(Y[2] - E_D[i]) <<
125            ' ' << delta[i] << ' ' << P[i] << ' ' << sigma[i] << '\n';
126    }
127    file_temperature.close();
128    cout << "Numerical solution temperature profile in radiative equilibrium stored in
129        file " << fn_temperature_numerical << endl;
130    file_irradiance.close();
131    cout << "Numerical solution irradiances in radiative equilibrium stored in file " <<
132        fn_irradiance_numerical << endl;

```

```

123 file_errors.close();
124 cout << "Absolute errors between normalised numerical and analytical solutions stored
      in file " << fn_errors << endl;
125
126
127
128 /* Stability analysis of numerical solution in radiative equilibrium */
129
130 // Prepare variables.
131 int n;
132 double ddelta;
133
134 // Prepare output file.
135 char fn_stability[] = DIR_DATA "/stability.dat";
136 file_errors << scientific << setprecision(N_PRECISION);
137 file_errors.open(fn_stability);
138 file_errors << "#N T/T_0 E_U/S_t E_D/S_t" << endl;
139 file_errors << "#'1' '1' '1' '1'" << endl;
140
141 // Integrate up to ground level.
142 for (int i = 0; i < N_STABILITY; i++) {
143     n = 1 << i;
144     ddelta = (global_delta_g - global_delta_T0A) / n;
145     Y[0] = 0.5;
146     Y[1] = 1.0;
147     Y[2] = 0.0;
148     integrate_IVP(n, ddelta, Y, rhs, 3, rungekutta4);
149     T_tmp = pow(Y[0], 0.25);
150     file_errors << n << ' ' << fabs(T_tmp - temperature_norm(global_delta_g)) << ' ' <<
      fabs(Y[1] - irradiance_upward_norm((global_delta_g))) << ' ' << fabs(Y[2] -
      irradiance_downward_norm((global_delta_g))) << '\n';
151 }
152 file_errors.close();
153 cout << "Errors for stability analysis of numerical solution stored in file " <<
      fn_stability << endl;
154
155 // Tear down.
156 delete[] z;
157 delete[] dz;
158 delete[] P;
159 delete[] delta;
160 delete[] sigma;
161 delete[] T;
162 delete[] theta;
163 delete[] E_U;
164 delete[] E_D;
165
166 return 0;
167 }
168
169 void rhs(double t, double const * Y_0, double * R) {
170     R[0] = 0.5 * global_D;
171     R[1] = global_D * (Y_0[1] - Y_0[0]);
172     R[2] = global_D * (Y_0[0] - Y_0[2]);
173 }

```

B Mathematical derivations

In this appendix mathematical derivations of some ancillary results and formulae used in the main text are explicitly shown.

B.1 Relation between pressure and altitude

A general result regarding planetary atmospheres is that atmospheric pressure decreases with increasing altitude. Theoretical relations which approximate this behaviour can be obtained. Hypotheses considered in section 1 are valid.

If density is assumed constant, equation (3) can be solved easily resulting in a linear dependence of pressure P on altitude z ,

$$P(z) = P_0 - \rho g(z - z_0) \quad , \quad (28)$$

where (z_0, P_0) is a reference point inside the atmosphere.

If density is not constant its expression is given by the ideal gas law (cfr. equation (5)) and, assuming constant temperature T , equation (3) becomes

$$\begin{aligned} dP &= -\frac{Pg}{R_m T} dz \iff \\ \iff \frac{dP}{P} &= -\frac{g}{R_m T} dz \end{aligned} \quad (29)$$

with solution

$$\begin{aligned} \ln(P') \Big|_{P_0}^{P(z)} &= -\frac{g}{R_m T} z' \Big|_{z_0}^z \iff \\ \iff P(z) &= P_0 \exp \left(-\frac{g}{R_m T} (z - z_0) \right) \quad . \end{aligned} \quad (30)$$

This relation is not meaningful, since the aim of the work is to derive the non-constant temperature profile of the atmosphere. However, it can be used inside atmospheric layers where the temperature is considered constant (e.g. stratosphere).

A better approximation assumes non-constant density and constant lapse rate Γ , hence temperature depends linearly on altitude,

$$\Gamma = -\frac{dT}{dz} \iff T(z) = T_0 - \Gamma(z - z_0) \quad , \quad (31)$$

with T_0 temperature corresponding to reference altitude z_0 . Using these assumptions and the den-

sity rewritten through the ideal gas law (5), equation (3) becomes

$$\begin{aligned} dP &= -\frac{Pg}{R_m T} \left(-\frac{dT}{\Gamma} \right) \iff \\ \iff \frac{dP}{P} &= \frac{g}{R_m \Gamma} \frac{dT}{T} \quad , \end{aligned} \quad (32)$$

which has solution

$$\begin{aligned} \ln(P') \Big|_{P_0}^{P(z)} &= \frac{g}{R_m \Gamma} \ln(T') \Big|_{T_0}^{T(z)} \iff \\ \iff P(z) &= P_0 \left(\frac{T_0 - \Gamma(z - z_0)}{T_0} \right)^{\frac{g}{R_m \Gamma}} \quad . \end{aligned} \quad (33)$$

Equation (33) can be used also with a piecewise constant lapse rate in altitude intervals where it is not null. Otherwise, in altitude intervals where lapse rate is null, equation (30) is valid with appropriate boundary conditions to ensure continuity between layers.

B.2 Radiometric quantities

Refer to [8] for more details on quantities reviewed in this section.

Consider electromagnetic radiation emitted by a point source. The total emitted power is called *radiant flux*, with unit W. The density of radiant flux with respect to a solid angle in the direction of emission is called *radiant intensity*, expressed in W/sr. When radiation interacts with a surface, i.e. it gets absorbed, transmitted or reflected, its radiant intensity distributed over the surface is measured through *radiance* in W/(m² sr). If the area on which the radiation is incident is expressed through the solid angle it subtends, the integral of radiance over this solid angle is called *irradiance*, expressed in W/m². Note that the coordinate system where the solid angles of radiant intensity and irradiance are defined may not be the same. Radiant flux emitted by a body normalised over the surface of emission is measured by *radiant exitance* in W/m².

All previous quantities can be expressed as densities with respect to the wavelength or the wavenumber and the adjective *spectral* is prefixed to their names. Their units are divided by the respective spectral quantity (e.g. spectral radiance with wavenumber in 1/cm has units W cm/(m² sr)).

Spectral radiance of a blackbody is given by Planck's law

$$B_\nu(\nu, T) = 2hc^2\nu^3 \frac{1}{e^{\frac{hc\nu}{k_B T}} - 1} \quad , \quad (34)$$

where ν is the wavenumber in unit 1/cm, T in unit K is the temperature of the emitting body and the other quantities are constants (cfr. table 1). Note that Planck's law has different form when it is expressed in terms of wavelength, due to its definition as density and the resulting change of variables:

$$B_\lambda(\lambda, T) = \frac{2hc^2}{\lambda^5} \frac{1}{e^{\frac{hc}{\lambda k_B T}} - 1} \quad . \quad (35)$$

If radiance is isotropic, i.e. it is not dependent on the direction of the radiation, the corresponding irradiance is proportional. For instance, if the radiation is absorbed by a hemispheric surface approximated by a blackbody, the spectral irradiance of the surface is

$$\begin{aligned} & \int B_\nu(\nu, T) d\phi \sin(\theta) d\theta \cos(\theta) = \\ & = B_\nu(\nu, T) \int_0^{2\pi} d\phi \int_0^{\frac{\pi}{2}} \sin(\theta) \cos(\theta) d\theta = \\ & = 2\pi B_\nu(\nu, T) \int_0^1 \sin(\theta) d(\sin(\theta)) = \\ & = 2\pi B_\nu(\nu, T) \frac{1}{2} = \\ & = \pi B_\nu(\nu, T) \quad , \end{aligned} \quad (36)$$

where spherical coordinates are used to describe the surface and the term $\cos(\theta)$ considers the component of radiation along the normal of the infinitesimal solid angle.

B.3 Radiation attenuation

Details on quantities appearing in this section can be found in [9, p. 285]. Radiation crossing a medium loses energy due to absorption and scattering. The effect of chemical species on these processes is quantified through the *attenuation coefficient* (commonly called *extinction coefficient* in atmospheric sciences), which has different definitions based on the way it is derived (cfr. [4, p. 44]). The attenuation coefficient is the sum of *absorption coefficient* and *scattering coefficient* which contain

information on the attenuation due to the respective physical processes. The *optical depth* (also called *optical thickness*) takes in consideration the amount of substance involved in the absorption.

Ratios between radiant fluxes are related by the conservation of energy: the sum of *internal transmittance* and *internal absorptance* is 1, as well as the sum of *reflectance*, *absorptance* and *transmittance*.

In general these coefficients are functions of wavelength or wavenumber, in which case the prefix *spectral* is adopted. If the medium is a fluid, they depends on temperature and pressure of the medium. Another related quantity is the spectral internal transmittance

$$\tau_1(\nu, s, s_0) = e^{-\delta(\nu, s, s_0)} \quad , \quad (37)$$

where $\delta(\nu, s, s_0)$ is the spectral optical depth, which depends only on the spectral attenuation coefficient $\mu(\nu, s')$ of the medium traversed by the radiation from s_0 to s on the optical path. In the RCM optical paths are straight and form an angle θ with the direction normal to the layers, hence the definition of the spectral optical depth becomes:

$$\delta(\nu, s, s_0) = \frac{1}{\cos \theta} \int_{s_0}^s \mu(\nu, s') ds' \quad . \quad (38)$$

If the absorbing species do not interact, $\mu(\nu, s')$ is simply the sum of the spectral attenuation coefficients of the individual components of the medium.

Moreover, if the medium is homogenous, in the sense that quantities affecting radiative calculations are not dependent on spatial position (e.g. attenuation coefficients μ are constant inside the medium), the spectral attenuation coefficient depends only on the concentration of the absorbing species contained, hence the spectral attenuation coefficient can be rewritten as

$$\mu(\nu, s') = \mu_m(\nu) \rho(s') \quad (39)$$

where $\mu_m(\nu)$ is the spectral mass attenuation coefficient and $\rho(s')$ is the volumetric mass density of the absorber.

Names of radiative properties ending with suffix *-ance* are generally used for rough surfaces, while suffix *-ivity* indicates smooth surfaces. In this work the former is adopted. Refer to [9, p. 59] for more information and to the definition of spectral absorptivity in [8] for an example of the difference.

B.4 Quantities commonly used in atmospheric sciences

Earth’s surface horizontal profile is not uniform, hence altitude and pressure near ground level could present sudden variations. In models where this is taken into consideration, the sigma coordinate system is commonly used instead, defined by

$$\sigma = \frac{P - P_{\text{TOA}}}{P_g - P_{\text{TOA}}} . \quad (40)$$

To avoid confusion, in this work symbol σ is used for the Stefan-Boltzmann constant (cfr. table 1), except for equation (40).

An alternative quantity evaluated in place of $T(t, z)$ for a given parcel of fluid is the potential temperature

$$\theta(t, z) = T(t, z) \left(\frac{P_0}{P(z)} \right)^{\frac{R_m}{c_P}} , \quad (41)$$

where P_0 is a reference pressure and quantities $P(z)$, R_m and c_P refer to the fluid.

C Supplementary information

C.1 Plotting

Software gnuplot is used to generate plots shown in this work. Output values from the simulation are stored in a DAT file.

References

- [1] V. Ramanathan and J. A. Coakley Jr., “Climate modeling through radiative-convective models,” *Reviews of Geophysics*, vol. 16, no. 4, pp. 465–489, 1978. DOI: <https://doi.org/10.1029/RG016i004p00465>. eprint: <https://agupubs.onlinelibrary.wiley.com/doi/pdf/10.1029/RG016i004p00465>. [Online]. Available: <https://agupubs.onlinelibrary.wiley.com/doi/abs/10.1029/RG016i004p00465>.
- [2] J. E. Harries and C. Belotti, “On the variability of the global net radiative energy balance of the nonequilibrium earth,” *Journal of Climate*, vol. 23, no. 6, pp. 1277–1290, 2010. DOI: <https://doi.org/10.1175/2009JCLI2797.1>. [Online]. Available: <https://journals.ametsoc.org/view/journals/clim/23/6/2009jcli2797.1.xml>.
- [3] K. McGuffie and A. Henderson-Sellers, *The Climate Modelling Primer*, 4th ed. Wiley-Blackwell, 2014.
- [4] D. C. Catling and J. F. Kasting, *Atmospheric evolution on inhabited and lifeless worlds*. Cambridge University Press, 2017, ISBN: 9781316825488.
- [5] N. Oceanic and A. Administration, “Us standard atmosphere, 1976,” *Technical Report*, 1976.
- [6] A. Prša, P. Harmanec, G. Torres, *et al.*, “Nominal values for selected solar and planetary quantities: Iau 2015 resolution b3,” *The Astronomical Journal*, vol. 152, no. 2, p. 41, Aug. 2016. DOI: 10.3847/0004-6256/152/2/41. [Online]. Available: <https://dx.doi.org/10.3847/0004-6256/152/2/41>.
- [7] R. P. Turco, O. B. Toon, T. P. Ackerman, J. B. Pollack, and C. Sagan, “Nuclear winter: Global consequences of multiple nuclear explosions,” *Science*, vol. 222, no. 4630, pp. 1283–1292, 1983. DOI: 10.1126/science.222.4630.1283. eprint: <https://www.science.org/doi/pdf/10.1126/science.222.4630.1283>. [Online]. Available: <https://www.science.org/doi/abs/10.1126/science.222.4630.1283>.

- [8] International Commission on Illumination, “CIE S 017:2020 ILV: International Lighting Vocabulary, 2nd edition,” International Commission on Illumination, Standard, 2020.
- [9] M. F. Modest and S. Mazumder, *Radiative Heat Transfer*, 4th ed. Academic Press, 2021.