

# Radiative-convective equilibrium in a grey atmosphere

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## Abstract

Radiative-convective models provide an intermediate complexity approach to the simulation of climate. These models evaluate the atmospheric temperature profile averaged over all latitudes and longitudes, which is function of time and altitude. Physical processes which determine the energy exchange in the model are absorption, transmission, reflection of electromagnetic radiation and convection of fluid. In this work a radiative-convective model is used to derive the temperature of an atmosphere where the optical depth is constant with respect to the frequency of radiation. The resulting temperature profile is compared with the analytical solution provided under the condition of radiative equilibrium.

## 1 Introduction

Climate dynamics of a planet can be studied with models of varying complexity. One of the quantities analysed is the temporal and spatial distribution of temperature in the planetary atmosphere, which is the result of the heat exchange between different processes. Electromagnetic (EM) radiation is emitted, absorbed and scattered by the chemical species distributed in the atmosphere and by the planetary surface. Moreover, the atmosphere receives EM radiation by other celestial bodies, e.g. stars. Radiative processes are described by the Radiative Transfer Equation (RTE). Local temperature differences generate motion of fluid parcels, hence convection. A rough planetary surface can hinder horizontal heat transport. Fluid dynamics equations are needed to represent these processes.

Fluid parcels are treated as open systems and the temperature distribution is obtained by a suitable thermodynamic energy equation, coupled with

the equations of the processes occurring in the atmosphere. Even by limiting the analysis to radiative processes and convection, which are the main drivers of temperature variations, the equations involved are not solvable analytically and are not tractable numerically without simplifications.

A first approximation is to consider the average over all latitudes and longitudes for quantities which depend on spatial position. The resulting atmosphere is represented by plane-parallel layers, identified by their altitude  $z$  ranging from  $z_g$  at ground level to  $z_{\text{TOA}}$  at Top Of the Atmosphere (TOA). With this hypothesis, the differential equation describing the average temperature  $T(t, z)$  as function of time  $t$  and altitude  $z$  is

$$\frac{\partial T}{\partial t} = -\frac{1}{\varrho c_P} \frac{\partial q}{\partial z} \quad , \quad (1)$$

where  $c_P$  is the specific heat at constant pressure of the atmosphere,  $\varrho$  is the average volumetric mass density of the atmosphere and depends on atmospheric pressure  $P$ ,  $q$  is the total energy flux due to heat transfer. In general all these quantities are functions of  $t$  and  $z$ , also through  $T$ . Details on the derivation are in [1, p. 466], where the equation is written initially in terms of volumetric power densities.

A second hypothesis is the radiative-convective equilibrium of the atmosphere. This translates in the existence of a steady state  $\frac{\partial}{\partial t}T(t, z) = 0$  where the planet is in radiative equilibrium, i.e. the total irradiance at TOA is null, and the atmosphere is in convective equilibrium, i.e. fluid parcels are stable with respect to vertical motion.

A model with the previous assumptions is called Radiative-Convective Model (RCM). To simplify further the RTE, in this work the dependence of quantities on the frequency of EM radiation is neglected. An atmosphere with this property is called grey atmosphere.

In the following sections the steady state vertical temperature profile of a grey atmosphere is computed. First the hypothesis of radiative equilibrium is used alone to obtain an analytical solution and use it as validation for the respective numerical solution. Then convection is taken into account and a simple RCM is implemented starting from the numerical scheme for radiative equilibrium.

## 1.1 Hypotheses and conventions

Some additional hypotheses are assumed to simplify the study. Data on constants are listed in table 1 and where possible, values referred to Earth are used for a prompt comparison with reality. Dependencies of quantities are written explicitly when it helps to clarify the discussion.

Some assumptions are made on the planet. It is supposed to have a diurnal cycle, to receive a constant irradiance  $S_0$  and to have a constant Bond albedo  $A$ . These conditions result in a constant irradiance  $S_t$  transmitted to the illuminated hemisphere of the planet at TOA from outer space. The surface of the planet is approximated as blackbody emitting in the upward direction with temperature  $T_g$ . Gravitational acceleration  $g$  is constant. The atmosphere is supposed to be in hydrostatic equilibrium,

$$dP = -\varrho g dz \quad , \quad (2)$$

with  $P$  atmospheric pressure. Specific heat at constant pressure  $c_P$  is assumed constant. Scattering is neglected, hence the attenuation coefficient is equal to the absorption coefficient and the symbol  $\mu(z)$  is used for both. Moreover, the absorption coefficient is supposed to depend on  $z$  through

$$\mu(z) = \mu_m \varrho(z) \quad , \quad (3)$$

where  $\mu_m$  is the mass attenuation coefficient of the atmosphere, assumed constant.

For gases, specific gas constant  $R_m$  is used in thermodynamic relations, which is defined as the gas constant  $R$  divided by the molar mass of the gas. They obey the ideal gas law

$$P = \varrho R_m T \quad . \quad (4)$$

The total heat flux  $q$  is determined by radiative transfer and atmospheric convection. Other means of vertical heat transfer are neglected, e.g. precipitation. The RTE is not solved directly by the RCM,

instead a two-stream approximation is adopted for the radiation inside atmosphere: components of radiometric quantities in the upward and downward directions are treated separately. Neither the contribution to  $q(t, z)$  due to atmospheric convection is obtained by solving the proper fluid dynamics equations, in its place a numerical correction is adopted. With these considerations, equation (1) can be rewritten as

$$\frac{\partial T}{\partial t} = -\frac{1}{\varrho c_P} \frac{\partial}{\partial z} (E_U - E_D) \quad , \quad (5)$$

where  $E_U$  and  $E_D$  are irradiances of upward and downward radiations, respectively.

## 1.2 Vertical coordinates

Altitude is an immediate choice as vertical coordinate used to describe the problem. However, calculations may simplify more if expressed with other coordinates.

An alternative choice is  $P$  and is convenient when used with equation (2) to remove the dependence on  $\varrho$ . A bijective relation relates  $P$  and  $z$  (cfr. section B.1):

$$P(z) = P_g \exp \left( -\frac{z - z_g}{z_0} \right) \quad , \quad (6)$$

where ground level is chosen as reference and constant  $z_0$  acts to remove the dependence on temperature and thus sets the scale of  $z$ . Pressure decreases with altitude from standard value  $P_g$  at ground level to  $P_{\text{TOA}}$  at TOA.

To simplify radiative calculations optical depth  $\delta$  is used as vertical coordinate, starting from 0 at TOA and increasing downward, up to value  $\delta_g$  at ground level. From the hypotheses on the attenuation coefficient,  $\delta$  is a function of altitude through

$$\delta(z) = \mu_m \int_z^{z_{\text{TOA}}} \varrho(z') dz' \quad , \quad (7)$$

but a simpler relation exists between  $\delta$  and  $P$  using equation (2) to evaluate the integral in equation (7):

$$\delta(P) = \frac{\mu_m}{g} (P - P_{\text{TOA}}) \quad . \quad (8)$$

Relation (8) is used in conjunction with equation (6) to derive a more direct formula for  $\delta(z)$ :

$$\delta(z) = \frac{\mu_m}{g} \left( P_g \exp \left( -\frac{z - z_g}{z_0} \right) - P_{\text{TOA}} \right) \quad . \quad (9)$$

Table 1: Data on constants used in the present work. The middle rule separates standard values on top from arbitrary values chosen for the present work on bottom.

Symbol	Value	Unit	Notes
$A$	0.3		Bond albedo value of Earth compatible with various observations, cfr. [2, p. 1281]
$c_P$	$1.004 \times 10^3$	J/(K kg)	Specific heat at constant pressure of air, from [3, p. 16]
$\delta_{\text{TOA}}$	0		Optical depth at TOA, by definition
$D$	1.66		Diffusion coefficient, commonly used value from [3, p. 55]
$g$	9.80665	m/s <sup>2</sup>	Standard gravitational acceleration of Earth
$\Gamma_0$	$6.5 \times 10^{-3}$	K/m	Environmental lapse rate of Earth's troposphere, from [4, p. 3]
$P_g$	$1.013250 \times 10^5$	Pa	Standard pressure at ground level of Earth, from [4, p. 2]
$R_m$	$2.8705287 \times 10^2$	J/(K kg)	Specific gas constant of dry air
$\sigma$	$5.670374419 \times 10^{-8}$	W/(m <sup>2</sup> K <sup>4</sup> )	Stefan-Boltzmann constant
$S_0$	1361.0	W/m <sup>2</sup>	Nominal total solar irradiance, from [5]
$T_g$	288.15	K	Earth's surface temperature based on [4, p. 2]
$z_g$	0	m	Nominal ground level
$\delta_g$	$\frac{1}{D} \left( \frac{2\sigma T_g^4}{S_t} - 2 \right)$		Optical depth at ground level
$\mu_m$	$\frac{\delta_g g}{P_g - P_{\text{TOA}}}$	m <sup>2</sup> /kg	Mass attenuation coefficient of the atmosphere
$N$	100		Number of atmospheric layers
$P_0$	$1 \times 10^5$	Pa	Arbitrary reference value for pressure
$P_{\text{TOA}}$	3	Pa	Arbitrary TOA pressure
$S_t$	$(1 - A) \frac{S_0}{4}$	W/m <sup>2</sup>	Irradiance transmitted from outer space to TOA
$T_0$	$\left( \frac{S_t}{\sigma} \right)^{\frac{1}{4}}$	K	Arbitrary reference value for temperature
$z_0$	2000	m	Arbitrary constant for normalisation of altitude
$z_{\text{TOA}}$	$z_g - z_0 \ln \left( \frac{P}{P_g} \right)$	m	Arbitrary TOA altitude

Value  $P_{\text{TOA}}$  can be calculated from a fixed  $z_{\text{TOA}}$  comes using equation (6), or vice versa.

Any of the previous relations for  $\delta$  can be used to fix the value of  $\mu_m$  if  $\delta_g$  is known, or conversely  $\mu_m$  can be used as parameter to derive  $\delta_g$ .

## 2 Analytical solution in radiative equilibrium

Steady state temperature profile and irradiances are derived analytically in this section.

The additional hypothesis of Local Thermodynamic Equilibrium (LTE) is considered for the atmosphere. With these hypotheses, the RTE be-

$$\frac{1}{\mu} \frac{\partial L}{\partial z} = B_\nu - L \quad , \quad (10)$$

where  $L(t, z, \theta, \nu)$  is the spectral radiance arriving at altitude  $z$  with angle  $\theta$  with respect to direction  $\hat{z}$  and  $B_\nu(\nu, T(t, z))$  is Planck's function (cfr. section B.2).

To apply equation (10) to irradiances, two integrations are needed: one over the whole EM spectrum and one over the solid angle corresponding to a hemisphere. The latter can be performed adopting the diffusion approximation (cfr. [3, p. 55]), which have the effect to substitute  $\delta$  with  $\delta' = D\delta$ , where  $D$  is the diffusion coefficient. The resulting

equations for irradiances in terms of  $\delta'$  are

$$-\frac{\partial}{\partial \delta'} E_U(t, \delta') = \sigma T(t, \delta')^4 - E_U(t, \delta') \quad , \quad (11)$$

$$\frac{\partial}{\partial \delta'} E_D(t, \delta') = \sigma T(t, \delta')^4 - E_D(t, \delta') \quad (12)$$

and they are coupled with equation (5) written in terms of  $\delta'$ :

$$\frac{\partial}{\partial t} T(t, \delta') = \frac{\mu_m D}{c_P} \frac{\partial}{\partial \delta'} (E_U(t, \delta') - E_D(t, \delta')) \quad . \quad (13)$$

Equations (13), (11) and (12) form a system of Partial Differential Equations (PDEs) of first order in two variables.

When the steady state of  $T$  is searched, dependence on  $t$  is dropped and the PDEs become Ordinary Differential Equations (ODEs) of first order of an Initial Value Problem (IVP). Initial conditions for irradiances are

$$E_D(0) = 0 \quad (14)$$

because energy released to atmosphere at TOA by the downward flux is negligible and  $E_U(0)$  is a constant called Outgoing Longwave Radiation (OLR). Radiative equilibrium provides the condition for the OLR:

$$E_U(0) = S_t \quad . \quad (15)$$

At the steady state, irradiances are related by

$$\frac{d}{d\delta'} (E_U(\delta') - E_D(\delta')) = 0 \quad , \quad (16)$$

which has solution

$$E_U(\delta') - E_D(\delta') = S_t \quad . \quad (17)$$

Since heat transfer in equation (5) is determined only by radiative processes, this relation is equivalent to the hypotheses of atmosphere in radiative equilibrium at all altitudes and transparent to radiation coming from outside the planet. The ODE for  $T$  is obtained by adding and subtracting equations (11) and (12) and using the conditions provided by equations (16) and (17):

$$2\sigma \frac{d}{d\delta'} T(\delta')^4 = S_t \quad . \quad (18)$$

In a similar way, initial condition for  $T$  is obtained by summing equations (11) and (12) and applying relation (16) and the initial conditions (15)

and (14):

$$T(0) = \left( \frac{S_t}{2\sigma} \right)^{\frac{1}{4}} \quad . \quad (19)$$

The solution of equation (18) in terms of  $\delta$  is

$$T(\delta) = \left( \frac{S_t}{2\sigma} (1 + D\delta) \right)^{\frac{1}{4}} \quad , \quad (20)$$

represented in figure 1.

Once the temperature profile is known,  $E_U(\delta)$  and  $E_D(\delta)$  are evaluated with the same procedure used previously for  $T(\delta')$ , resulting in:

$$E_U(\delta) = \frac{S_t}{2} (2 + D\delta) \quad , \quad (21)$$

$$E_D(\delta) = \frac{S_t}{2} D\delta \quad . \quad (22)$$

Irradiances are shown in figure 2. At every altitude,  $E_U$  and  $E_D$  are greater than their respective values at TOA. This is result of the greenhouse effect of the atmosphere.

Value  $\delta_g$  can be fixed by using the irradiance emitted by the surface of the planet:

$$E_U(\delta_g) = \sigma T_g^4 \quad . \quad (23)$$

With this condition,  $T$  presents a discontinuity at ground level, which is not physical. Other mechanisms of heat transport redistribute energy between the surface and the atmospheric layer directly above, removing the discontinuity. Their effect can be simulated by imposing radiative equilibrium at ground level.

### 3 Numerical solution in radiative equilibrium

To solve numerically the IVP defined in section 2, equations (18), (11) and (12) are rewritten in terms of variable  $\delta$  and normalised,

$$Y_0 = \frac{T^4}{T_0^4} \quad , \quad Y_1 = \frac{E_U}{S_t} \quad , \quad Y_2 = \frac{E_D}{S_t} \quad (24)$$

with  $T_0$  chosen arbitrarily, resulting in the system of ODEs:

$$\begin{cases} \frac{dY_0}{d\delta} = \frac{D}{2} \\ \frac{dY_1}{d\delta} = D(Y_1 - Y_0) \\ \frac{dY_2}{d\delta} = D(Y_0 - Y_2) \end{cases} \quad . \quad (25)$$

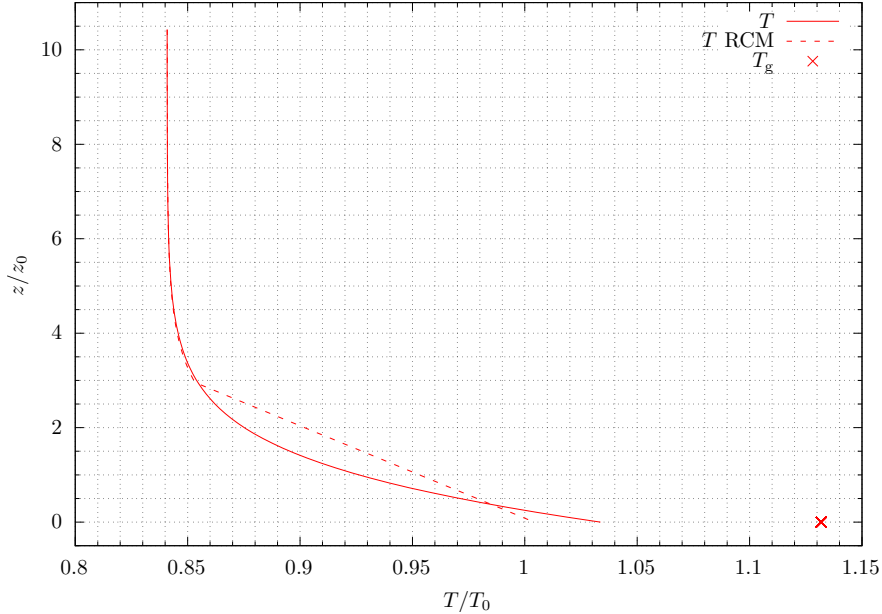


Figure 1: Vertical temperature profile of a grey atmosphere in radiative equilibrium. Lower altitudes are candidate to present instability due to higher values of the slope.

Initial conditions for the normalised functions are

$$Y_0 = \frac{1}{2} \quad , \quad Y_1 = 1 \quad , \quad Y_2 = 0 \quad , \quad (26)$$

from conditions (19), (15) and (14), respectively.

Runge-Kutta method of order 4 is used to integrate system (25), to maintain accuracy when  $T$  is derived from  $Y_0$ . Non-uniform step sizes are adopted, because values  $\delta$  are obtained from uniformly distributed values  $z$  through relation (9).

Errors between numerical and analytical solutions for normalised temperature and irradiances are shown in figure 3. Their values are compatible with 0 based on precision of double-precision floating-point numbers.

### 3.1 Stability analysis

The stability of the numerical method with respect to spatial grid size is studied varying  $N$ . Powers of 2 are chosen as values of  $N$  and step size is constant, obtained by dividing interval  $[\delta_{\text{TOA}}, \delta_{\text{g}}]$  in  $N$  subintervals. Errors are evaluated as absolute differences between numerical and analytical values for each of  $T(\delta_{\text{g}})$ ,  $E_U(\delta_{\text{g}})$  and  $E_U(\delta_{\text{g}})$ .

In figure 4 errors are plotted as function of  $N$ . For  $N \leq 4096$ , they are compatible with 0 within precision, while for greater  $N$ , they increase due to error propagation. In general, this behaviour does not hinder results of simulations because lower values of  $N$  are chosen for the model, otherwise averages approximating dynamics could lose accuracy and the computational demand of the equations involved could increase considerably.

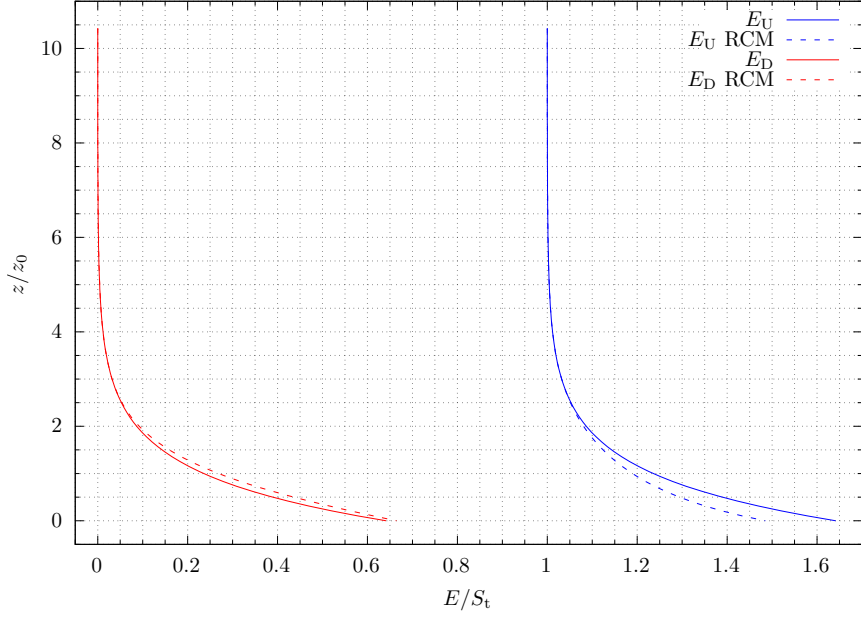


Figure 2: Upward and downward irradiances in a grey atmosphere in radiative equilibrium.

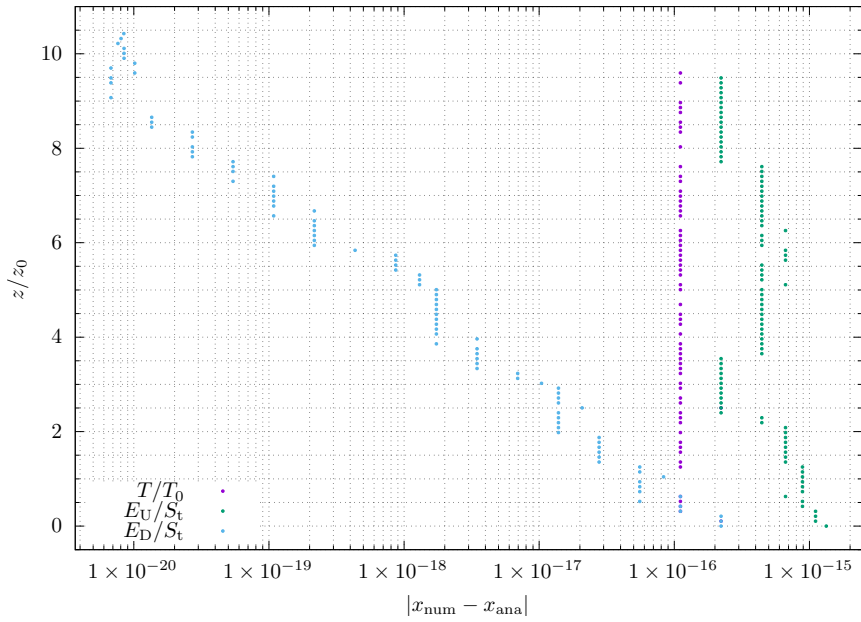


Figure 3: Errors

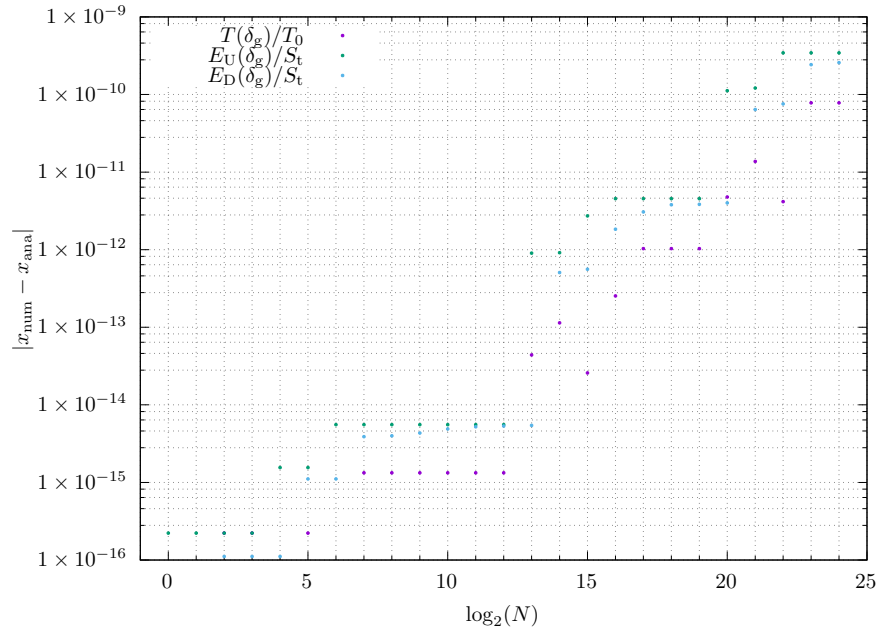


Figure 4: Stability analysis.

## A Source code

In this section the C++ code used to obtain the results presented in this work is shown and commented.

First, the parametrization of the vertical coordinate is chosen among three alternatives: altitude  $z$  in m, atmospheric pressure  $P$  in Pa, coordinate  $\sigma = \frac{P-P_{\text{TOA}}}{P_S-P_{\text{TOA}}}$  adimensional, with  $P_{\text{TOA}}$  pressure at the top of the modelised atmosphere and  $P_S$  pressure at the surface. One parametrisation can be written in term of another through a monotonic function (e.g. pressure decreases with altitude, cfr. section B.1). For the initial development the altitude  $z$  is chosen as vertical coordinate because it is more intuitive, moreover plots in [6] are expressed in terms of both  $z$  and  $P$ .

Second, the atmospheric layers are configured. In [6] 20 layers are used and they are numbered from the top of the atmosphere down as it is common in RCMs. The vertical coordinate refers to the center of each layer, with the exception of the last layer which is in direct contact with the surface and needs to be treated separately. Therefore two arrays are needed: one for the point and one with the corresponding layer thicknesses. Values are then assigned as double precision numbers. The value corresponding to the top of the atmosphere is set in a proper variable and a uniform distribution of layer thicknesses is assumed for ease.

```
1 #include <cmath>
2 #include <fstream>
3 #include <iomanip>
4 #include <iostream>
5
6 #include "constants.h"
7 #include "convection.h"
8 #include "../mclib/mclib.h"
9 #include "radiation.h"
10 #include "utilities.h"
11 #include "configuration.h" // Include last to allow redefinitions.
12
```



```

13 double * global_z; // / m
14 double * global_P; // / Pa
15 double * global_delta, * global_sigma;
16 double global_T_0; // / K
17
18 void rhs_delta(double t, double const * Y_0, double * R);
19
20 void rhs_t(double t, double const * Y_0, double * R);
21
22 int main(int argc, char * argv[]) {
23     using namespace std;
24     cout << fixed << setprecision(N_PRECISION);
25
26     // Configure vertical coordinates.
27     double z_TOA, dz; // / m
28     z_TOA = get_altitude(global_P_TOA);
29     dz = (z_TOA - const_z_g) / global_N;
30     global_z = new double[global_N + 1];
31     global_delta = new double[global_N + 1];
32     global_P = new double[global_N + 1];
33     global_sigma = new double[global_N + 1];
34     for (int i = 0; i <= global_N; i++) {
35         global_z[i] = z_TOA - i * dz;
36         global_delta[i] = get_optical_depth_z(global_z[i], global_P_TOA);
37         global_P[i] = get_pressure(global_z[i]);
38         global_sigma[i] = get_sigma(global_P[i], global_P_TOA);
39     }
40
41
42
43     /* Analytical solution in radiative equilibrium */
44
45     // Prepare variables.
46     double * Y_3_ana, * theta_norm, * Y_1_ana, * Y_2_ana;
47     Y_3_ana = new double[global_N + 1];
48     theta_norm = new double[global_N + 1];
49     Y_1_ana = new double[global_N + 1];
50     Y_2_ana = new double[global_N + 1];
51     global_T_0 = pow(global_S_t / const_sigma, 0.25);
52
53     // Prepare output files.
54     ofstream file_temperature, file_irradiance;
55     char fn_temperature_analytical[] = DIR_DATA "/temperature_analytical.dat";
56     char fn_irradiance_analytical[] = DIR_DATA "/irradiance_analytical.dat";
57     file_temperature << fixed << setprecision(N_PRECISION);
58     file_temperature.open(fn_temperature_analytical);
59     file_temperature << "#z/z_0 T/T_0 delta P sigma theta/T_0" << endl;
60     file_temperature << "#'1' '1' '1' 'Pa' '1' '1'" << endl;
61     file_irradiance << fixed << setprecision(N_PRECISION);
62     file_irradiance.open(fn_irradiance_analytical);
63     file_irradiance << "#z/z_0 E_U/S_t E_D/S_t delta P sigma" << endl;
64     file_irradiance << "#'1' '1' '1' '1' 'Pa' '1'" << endl;
65
66     // Plot analytical solutions.
67     for (int i = 0; i <= global_N; i++) {
68         Y_3_ana[i] = temperature_norm(global_delta[i]);
69         theta_norm[i] = get_theta(Y_3_ana[i], global_P[i]);
70         file_temperature << global_z[i] / global_z_0 << ' '
71             << Y_3_ana[i] << ' '
72             << global_delta[i] << ' '
73             << global_P[i] << ' '
74             << global_sigma[i] << ' '

```

```

75     << theta_norm[i] << '\n';
76     Y_1_ana[i] = irradiance_upward_norm(global_delta[i]);
77     Y_2_ana[i] = irradiance_downward_norm(global_delta[i]);
78     file_irradiance << global_z[i] / global_z_0 << ' ',
79     << Y_1_ana[i] << ' ',
80     << Y_2_ana[i] << ' ',
81     << global_delta[i] << ' ',
82     << global_P[i] << ' ',
83     << global_sigma[i] << '\n';
84 }
85 file_temperature.close();
86 cout << "Analytical solution temperature profile in radiative equilibrium calculated,
      values are stored in file " << fn_temperature_analytical << endl;
87 file_irradiance.close();
88 cout << "Analytical solution irradiances in radiative equilibrium calculated, values
      are stored in file " << fn_irradiance_analytical << endl;
89
90
91
92 /* Numerical solution in radiative equilibrium */
93
94 // Prepare variables and set initial values.
95 double Y[3];
96 double Y_3_tmp, theta_tmp;
97 Y[0] = 0.5;
98 Y[1] = 1.0;
99 Y[2] = 0.0;
100 Y_3_tmp = pow(Y[0], 0.25);
101 theta_tmp = get_theta(Y_3_tmp, global_P[0]);
102
103 // Prepare output files.
104 char fn_temperature_numerical[] = DIR_DATA "/temperature_numerical.dat";
105 char fn_irradiance_numerical[] = DIR_DATA "/irradiance_numerical.dat";
106 file_temperature << fixed << setprecision(N_PRECISION);
107 file_temperature.open(fn_temperature_numerical);
108 file_temperature << "#z/z_0 T/T_0 T_err/T_0 delta P sigma theta/T_0 theta_err/T_0" <<
      endl;
109 file_temperature << "#'1' '1' '1' '1' 'Pa' '1' '1' '1'" << endl;
110 file_irradiance << fixed << setprecision(N_PRECISION);
111 file_irradiance.open(fn_irradiance_numerical);
112 file_irradiance << "#z/z_0 E_U/S_t E_D/S_t E_U_err/S_t E_D_err/S_t delta P sigma" <<
      endl;
113 file_irradiance << "#'1' '1' '1' '1' '1' '1' 'Pa' '1'" << endl;
114
115 // Integrate equations.
116 file_temperature << global_z[0] / global_z_0 << ' ',
117 << Y_3_tmp << ' ',
118 << scientific << fabs(Y_3_tmp - Y_3_ana[0]) << fixed << ' ',
119 << global_delta[0] << ' ',
120 << global_P[0] << ' ',
121 << global_sigma[0] << ' ',
122 << theta_tmp << ' ',
123 << scientific << fabs(theta_tmp - theta_norm[0]) << fixed << '\n';
124 file_irradiance << global_z[0] / global_z_0 << ' ',
125 << Y[1] << ' ',
126 << Y[2] << ' ',
127 << scientific << fabs(Y[1] - Y_1_ana[0]) << ' ',
128 << fabs(Y[2] - Y_2_ana[0]) << fixed << ' ',
129 << global_delta[0] << ' ',
130 << global_P[0] << ' ',
131 << global_sigma[0] << '\n';
132 for (int i = 1; i <= global_N; i++) {

```

```

133     rungekutta4(global_delta[i], global_delta[i] - global_delta[i-1], Y, rhs_delta, 3);
134     Y_3_tmp = pow(Y[0], 0.25);
135     theta_tmp = get_theta(Y_3_tmp, global_P[i]);
136     file_temperature << global_z[i] / global_z_0 << ' ',
137         << Y_3_tmp << ' ',
138         << scientific << fabs(Y_3_tmp - Y_3_ana[i]) << fixed << ' ',
139         << global_delta[i] << ' ',
140         << global_P[i] << ' ',
141         << global_sigma[i] << ' ',
142         << theta_tmp << ' ',
143         << scientific << fabs(theta_tmp - theta_norm[i]) << fixed << '\n';
144     file_irradiance << global_z[i] / global_z_0 << ' ',
145         << Y[1] << ' ',
146         << Y[2] << ' ',
147         << scientific << fabs(Y[1] - Y_1_ana[i]) << ' ',
148         << fabs(Y[2] - Y_2_ana[i]) << fixed << ' ',
149         << global_delta[i] << ' ',
150         << global_P[i] << ' ',
151         << global_sigma[i] << '\n';
152 }
153 file_temperature.close();
154 cout << "Numerical solution temperature profile in radiative equilibrium stored in
155     file " << fn_temperature_numerical << endl;
156 file_irradiance.close();
157 cout << "Numerical solution irradiances in radiative equilibrium stored in file " <<
158     fn_irradiance_numerical << endl;
159
160 /* Stability analysis of numerical solution in radiative equilibrium */
161
162 // Prepare support variables.
163 int n;
164 double ddelta;
165
166 // Prepare output file.
167 ofstream file_stability;
168 char fn_stability[] = DIR_DATA "/stability.dat";
169 file_stability << scientific << setprecision(N_PRECISION);
170 file_stability.open(fn_stability);
171 file_stability << "#N T/T_0 E_U/S_t E_D/S_t" << endl;
172 file_stability << "#'1' '1' '1' '1'" << endl;
173
174 // Integrate up to ground level.
175 for (int i = 0; i < N_STABILITY; i++) {
176     n = 1 << i;
177     ddelta = (global_delta_g - const_delta_TOA) / n;
178     Y[0] = 0.5;
179     Y[1] = 1.0;
180     Y[2] = 0.0;
181     integrate_IVP(n, ddelta, Y, rhs_delta, 3, rungekutta4);
182     Y_3_tmp = pow(Y[0], 0.25);
183     file_stability << n << ' ',
184         << fabs(Y_3_tmp - Y_3_ana[global_N]) << ' ',
185         << fabs(Y[1] - Y_1_ana[global_N]) << ' ',
186         << fabs(Y[2] - Y_2_ana[global_N]) << '\n';
187 }
188 file_stability.close();
189 cout << "Errors for stability analysis of numerical solution stored in file " <<
190     fn_stability << endl;
191

```

```

192  /* Radiative-convective equilibrium */
193
194
195  // Set integration parameters.
196  int i_t, i_0_Y_1, i_0_Y_2, is_steady;
197  double * Y_3, * Y_3_prev;
198  double t, dt; // / s
199  i_t = 0;
200  i_0_Y_1 = global_N + 1;
201  i_0_Y_2 = i_0_Y_1 + global_N + 1;
202  Y_3 = new double[3 * (global_N + 1)]; // Used also to store irradiances.
203  Y_3_prev = new double[global_N + 1];
204  dt = 12 * 3600.0;
205
206  // Set initial values.
207  Y_3[0] = temperature_norm(const_delta_TOA);
208  for (int i = 1; i <= global_N; i++) {
209      Y_3[i] = const_T_g / global_T_0;
210  }
211  Y_3[i_0_Y_1] = 1.0;
212  Y_3[i_0_Y_2] = 0.0;
213
214  // Run model.
215  do {
216      Y_3_prev[0] = Y_3[0];
217      i_t++;
218      t = i_t * dt;
219      Y[1] = 1.0;
220      Y[2] = 0.0;
221      for (int i = 1; i <= global_N; i++) {
222          Y_3_prev[i] = Y_3[i];
223          Y[0] = Y_3[i]*Y_3[i]*Y_3[i]*Y_3[i];
224          rungekutta4(global_delta[i], global_delta[i] - global_delta[i-1], Y, rhs_delta, 3)
225          ;
226          Y_3[i_0_Y_1 + i] = Y[1];
227          Y_3[i_0_Y_2 + i] = Y[2];
228      }
229      eulerstep(t, dt, Y_3, rhs_t, global_N + 1);
230      convective_adjustment(const_Gamma_0 / global_T_0, global_N, Y_3, global_z);
231      // Temperature profile steady state condition.
232      is_steady = 1;
233      for (int i = 0; i <= global_N; i++) {
234          if (fabs(Y_3[i] - Y_3_prev[i]) > TOLERANCE) {
235              is_steady = 0;
236              break;
237          }
238      }
239      while (! is_steady);
240      cout << "Steady state reached in " << i_t << " iterations" << endl;
241
242  // Prepare output files.
243  char fn_temperature_RCM[] = DIR_DATA "/temperature_RCM.dat";
244  char fn_irradiance_RCM[] = DIR_DATA "/irradiance_RCM.dat";
245  file_temperature << fixed << setprecision(N_PRECISION);
246  file_temperature.open(fn_temperature_RCM);
247  file_temperature << "#z/z_0 T/T_0 T_err/T_0 delta P sigma theta/T_0 theta_err/T_0" <<
248  endl;
249  file_temperature << "#'1' '1' '1' '1' 'Pa' '1' '1' '1'" << endl;
250  file_irradiance << fixed << setprecision(N_PRECISION);
251  file_irradiance.open(fn_irradiance_RCM);
252  file_irradiance << "#z/z_0 E_U/S_t E_D/S_t E_U_err/S_t E_D_err/S_t delta P sigma" <<
253  endl;

```

```

251 file_irradiance << "#'1' '1' '1' '1' '1' '1' 'Pa' '1'" << endl;
252
253 // Print output values.
254 for (int i = 0; i <= global_N; i++) {
255     theta_tmp = get_theta(Y_3[i], global_P[i]);
256     file_temperature << global_z[i] / global_z_0 << ' ',
257     << Y_3[i] << ' ',
258     << scientific << fabs(Y_3[i] - Y_3_ana[i]) << fixed << ' ',
259     << global_delta[i] << ' ',
260     << global_P[i] << ' ',
261     << global_sigma[i] << ' ',
262     << theta_tmp << ' ',
263     << scientific << fabs(theta_tmp - theta_norm[i]) << fixed << '\n';
264     file_irradiance << global_z[i] / global_z_0 << ' ',
265     << Y_3[i_0_Y_1 + i] << ' ',
266     << Y_3[i_0_Y_2 + i] << ' ',
267     << scientific << fabs(Y_3[i_0_Y_1 + i] - Y_1_ana[i]) << ' ',
268     << fabs(Y_3[i_0_Y_2 + i] - Y_2_ana[i]) << fixed << ' ',
269     << global_delta[i] << ' ',
270     << global_P[i] << ' ',
271     << global_sigma[i] << '\n';
272 }
273 file_temperature.close();
274 cout << "Numerical solution temperature profile in radiative-convective equilibrium
275 stored in file " << fn_temperature_RCM << endl;
276 file_irradiance.close();
277 cout << "Numerical solution irradiances in radiative-convective equilibrium stored in
278 file " << fn_irradiance_RCM << endl;
279
280 // Tear down.
281 delete[] global_z;
282 delete[] global_P;
283 delete[] global_delta;
284 delete[] global_sigma;
285 delete[] Y_3_ana;
286 delete[] theta_norm;
287 delete[] Y_1_ana;
288 delete[] Y_2_ana;
289 delete[] Y_3;
290 delete[] Y_3_prev;
291
292 return 0;
293 }
294
295 void rhs_delta(double t, double const * Y_0, double * R) {
296     R[0] = 0.5 * const_D;
297     R[1] = const_D * (Y_0[1] - Y_0[0]);
298     R[2] = const_D * (Y_0[0] - Y_0[2]);
299 }
300
301 void rhs_t(double t, double const * Y_0, double * R) {
302     double const * Y_1, * Y_2;
303     Y_1 = Y_0 + global_N + 1;
304     Y_2 = Y_1 + global_N + 1;
305     R[0] = 0.0;
306     for (int i = 1; i <= global_N; i++) {
307         R[i] = global_S_t * global_mu_m / (const_c_P * global_T_0) * (Y_1[i] - Y_1[i-1] -

```

## B Mathematical derivations

In this appendix mathematical derivations of some ancillary results and formulae used in the main text are explicitly shown.

### B.1 Relation between pressure and altitude

A general result regarding planetary atmospheres is that atmospheric pressure decreases with increasing altitude. Theoretical relations which approximate this behaviour can be obtained. Hypotheses considered in section 1 are valid.

If density is assumed constant, equation (2) can be solved easily resulting in a linear dependence of pressure  $P$  on altitude  $z$ ,

$$P(z) = P_0 - \rho g(z - z_0) \quad , \quad (27)$$

where  $(z_0, P_0)$  is a reference point inside the atmosphere.

If density is not constant its expression is given by the ideal gas law (cfr. equation (4)) and, assuming constant temperature  $T$ , equation (2) becomes

$$\begin{aligned} dP &= -\frac{Pg}{R_m T} dz \iff \\ \iff \frac{dP}{P} &= -\frac{g}{R_m T} dz \end{aligned} \quad (28)$$

with solution

$$\begin{aligned} \ln(P') \Big|_{P_0}^{P(z)} &= -\frac{g}{R_m T} z' \Big|_{z_0}^z \iff \\ \iff P(z) &= P_0 \exp \left( -\frac{g}{R_m T} (z - z_0) \right) \quad . \end{aligned} \quad (29)$$

This relation is not meaningful, since the aim of the work is to derive the non-constant temperature profile of the atmosphere. However, it can be used inside atmospheric layers where the temperature is considered constant (e.g. stratosphere).

A better approximation assumes non-constant density and constant lapse rate  $\Gamma$ , hence temperature depends linearly on altitude,

$$\Gamma = -\frac{dT}{dz} \iff T(z) = T_0 - \Gamma(z - z_0) \quad , \quad (30)$$

with  $T_0$  temperature corresponding to reference altitude  $z_0$ . Using these assumptions and the den-

sity rewritten through the ideal gas law (4), equation (2) becomes

$$\begin{aligned} dP &= -\frac{Pg}{R_m T} \left( -\frac{dT}{\Gamma} \right) \iff \\ \iff \frac{dP}{P} &= \frac{g}{R_m \Gamma} \frac{dT}{T} \quad , \end{aligned} \quad (31)$$

which has solution

$$\begin{aligned} \ln(P') \Big|_{P_0}^{P(z)} &= \frac{g}{R_m \Gamma} \ln(T') \Big|_{T_0}^{T(z)} \iff \\ \iff P(z) &= P_0 \left( \frac{T_0 - \Gamma(z - z_0)}{T_0} \right)^{\frac{g}{R_m \Gamma}} \quad . \end{aligned} \quad (32)$$

Equation (32) can be used also with a piecewise constant lapse rate in altitude intervals where it is not null. Otherwise, in altitude intervals where lapse rate is null, equation (29) is valid with appropriate boundary conditions to ensure continuity between layers.

### B.2 Radiometric quantities

Refer to [7] for more details on quantities reviewed in this section.

Consider electromagnetic radiation emitted by a point source. The total emitted power is called *radiant flux*, with unit W. The density of radiant flux with respect to a solid angle in the direction of emission is called *radiant intensity*, expressed in W/sr. When radiation interacts with a surface, i.e. it gets absorbed, transmitted or reflected, its radiant intensity distributed over the surface is measured through *radiance* in W/(m<sup>2</sup> sr). If the area on which the radiation is incident is expressed through the solid angle it subtends, the integral of radiance over this solid angle is called *irradiance*, expressed in W/m<sup>2</sup>. Note that the coordinate system where the solid angles of radiant intensity and irradiance are defined may not be the same. Radiant flux emitted by a body normalised over the surface of emission is measured by *radiant exitance* in W/m<sup>2</sup>.

All previous quantities can be expressed as densities with respect to the wavelength or the wavenumber and the adjective *spectral* is prefixed to their names. Their units are divided by the respective spectral quantity (e.g. spectral radiance with wavenumber in 1/cm has units W cm/(m<sup>2</sup> sr)).

Spectral radiance of a blackbody is given by Planck's law

$$B_\nu(\nu, T) = 2hc^2\nu^3 \frac{1}{e^{\frac{hc\nu}{k_B T}} - 1} \quad , \quad (33)$$

where  $\nu$  is the wavenumber in unit 1/cm,  $T$  in unit K is the temperature of the emitting body and the other quantities are constants (cfr. table 1). Note that Planck's law has different form when it is expressed in terms of wavelength, due to its definition as density and the resulting change of variables:

$$B_\lambda(\lambda, T) = \frac{2hc^2}{\lambda^5} \frac{1}{e^{\frac{hc}{\lambda k_B T}} - 1} \quad . \quad (34)$$

If radiance is isotropic, i.e. it is not dependent on the direction of the radiation, the corresponding irradiance is proportional. For instance, if the radiation is absorbed by a hemispheric surface approximated by a blackbody, the spectral irradiance of the surface is

$$\begin{aligned} & \int B_\nu(\nu, T) d\phi \sin(\theta) d\theta \cos(\theta) = \\ & = B_\nu(\nu, T) \int_0^{2\pi} d\phi \int_0^{\frac{\pi}{2}} \sin(\theta) \cos(\theta) d\theta = \\ & = 2\pi B_\nu(\nu, T) \int_0^1 \sin(\theta) d(\sin(\theta)) = \\ & = 2\pi B_\nu(\nu, T) \frac{1}{2} = \\ & = \pi B_\nu(\nu, T) \quad , \end{aligned} \quad (35)$$

where spherical coordinates are used to describe the surface and the term  $\cos(\theta)$  considers the component of radiation along the normal of the infinitesimal solid angle.

### B.3 Radiation attenuation

Details on quantities appearing in this section can be found in [8, p. 285]. Radiation crossing a medium loses energy due to absorption and scattering. The effect of chemical species on these processes is quantified through the *attenuation coefficient* (commonly called *extinction coefficient* in atmospheric sciences), which has different definitions based on the way it is derived (cfr. [3, p. 44]). The attenuation coefficient is the sum of *absorption coefficient* and *scattering coefficient* which contain

information on the attenuation due to the respective physical processes. The *optical depth* (also called *optical thickness*) takes in consideration the amount of substance involved in the absorption.

Ratios between radiant fluxes are related by the conservation of energy: the sum of *internal transmittance* and *internal absorptance* is 1, as well as the sum of *reflectance*, *absorptance* and *transmittance*.

In general these coefficients are functions of wavelength or wavenumber, in which case the prefix *spectral* is adopted. If the medium is a fluid, they depends on temperature and pressure of the medium. Another related quantity is the spectral internal transmittance

$$\tau_1(\nu, s, s_0) = e^{-\delta(\nu, s, s_0)} \quad , \quad (36)$$

where  $\delta(\nu, s, s_0)$  is the spectral optical depth, which depends only on the spectral attenuation coefficient  $\mu(\nu, s')$  of the medium traversed by the radiation from  $s_0$  to  $s$  on the optical path. In the RCM optical paths are straight and form an angle  $\theta$  with the direction normal to the layers, hence the definition of the spectral optical depth becomes:

$$\delta(\nu, s, s_0) = \frac{1}{\cos \theta} \int_{s_0}^s \mu(\nu, s') ds' \quad . \quad (37)$$

If the absorbing species do not interact,  $\mu(\nu, s')$  is simply the sum of the spectral attenuation coefficients of the individual components of the medium.

Moreover, if the medium is homogenous, in the sense that quantities affecting radiative calculations are not dependent on spatial position (e.g. attenuation coefficients  $\mu$  are constant inside the medium), the spectral attenuation coefficient depends only on the concentration of the absorbing species contained, hence the spectral attenuation coefficient can be rewritten as

$$\mu(\nu, s') = \mu_m(\nu) \rho(s') \quad (38)$$

where  $\mu_m(\nu)$  is the spectral mass attenuation coefficient and  $\rho(s')$  is the volumetric mass density of the absorber.

Names of radiative properties ending with suffix *-ance* are generally used for rough surfaces, while suffix *-ivity* indicates smooth surfaces. In this work the former is adopted. Refer to [8, p. 59] for more information and to the definition of spectral absorptivity in [7] for an example of the difference.

## B.4 Quantities commonly used in atmospheric sciences

Earth’s surface horizontal profile is not uniform, hence altitude and pressure near ground level could present sudden variations. In models where this is taken into consideration, the sigma coordinate system is commonly used instead, defined by

$$\sigma = \frac{P - P_{\text{TOA}}}{P_g - P_{\text{TOA}}} . \quad (39)$$

To avoid confusion, in this work symbol  $\sigma$  is used for the Stefan-Boltzmann constant (cfr. table 1), except for equation (39).

An alternative quantity evaluated in place of  $T(t, z)$  for a given parcel of fluid is the potential temperature

$$\theta(t, z) = T(t, z) \left( \frac{P_0}{P(z)} \right)^{\frac{R_m}{c_P}} , \quad (40)$$

where  $P_0$  is a reference pressure and quantities  $P(z)$ ,  $R_m$  and  $c_P$  refer to the fluid.

## C Supplementary information

### C.1 Plotting

Software gnuplot is used to generate plots shown in this work. Output values from the simulation are stored in a DAT file.

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