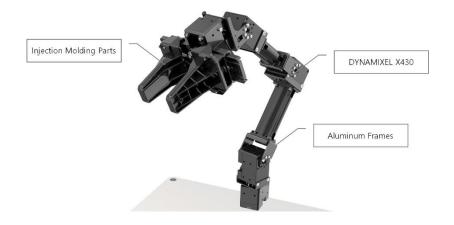
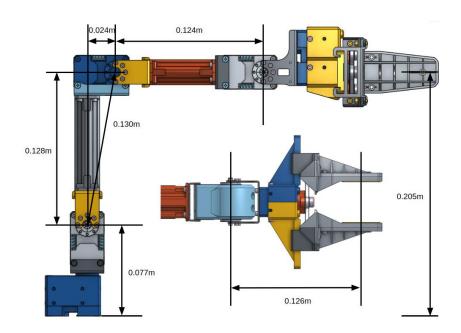
## **Mechatronics Course Project**

### OpenmanipulatorX Robot Control



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#### A) Calculation of Jacobian matrix of the robot:



According to the geometric characteristics of the robot shown in the figure above, the transfer matrix is as follows:

$$P_{EE} = \begin{bmatrix} \cos(\theta_1) \left[ 0.126\cos(\theta_2 + \theta_3 + \theta_4) + 0.124\cos(\theta_2 + \theta_3) + 0.024\cos(\theta_2) \right] \\ \sin(\theta_1) \left[ 0.126\cos(\theta_2 + \theta_3 + \theta_4) + 0.124\cos(\theta_2 + \theta_3) + 0.024\cos(\theta_2) \right] \\ 0.077 + 0.126\sin(\theta_2 + \theta_3 + \theta_4) + 0.124\sin(\theta_2 + \theta_3) + 0.128\sin(\theta_2) \end{bmatrix} = \begin{bmatrix} P_{EE})_1 \\ P_{EE})_2 \\ P_{EE})_3 \end{bmatrix}$$

$$\frac{d}{dt}P_{EE})_{1} = -\dot{\theta}_{1}\sin(\theta_{1})\left[0.126\cos(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\cos(\theta_{2} + \theta_{3}) + 0.024\cos(\theta_{2})\right] \\ -\cos(\theta_{1})\left[0.126(\dot{\theta}_{2} + \dot{\theta}_{3} + \dot{\theta}_{4})\sin(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124(\dot{\theta}_{2} + \dot{\theta}_{3})\sin(\theta_{2} + \theta_{3}) + 0.024\dot{\theta}_{2}\sin(\theta_{2})\right]$$

$$\begin{split} \frac{d}{dt} P_{EE})_2 &= \dot{\theta}_1 \cos(\theta_1) \Big[ 0.126 \cos(\theta_2 + \theta_3 + \theta_4) + 0.124 \cos(\theta_2 + \theta_3) + 0.024 \cos(\theta_2) \Big] \\ &- \sin(\theta_1) \Big[ 0.126 (\dot{\theta}_2 + \dot{\theta}_3 + \dot{\theta}_4) \sin(\theta_2 + \theta_3 + \theta_4) + 0.124 (\dot{\theta}_2 + \dot{\theta}_3) \sin(\theta_2 + \theta_3) + 0.024 \dot{\theta}_2 \sin(\theta_2) \Big] \\ \frac{d}{dt} P_{EE})_3 &= 0.126 (\dot{\theta}_2 + \dot{\theta}_3 + \dot{\theta}_4) \cos(\theta_2 + \theta_3 + \theta_4) + 0.124 (\dot{\theta}_2 + \dot{\theta}_3) \cos(\theta_2 + \theta_3) + 0.128 (\dot{\theta}_2) \cos(\theta_2) \\ \frac{d}{dt} P_{EE} &= \left[ \frac{d}{dt} P_{EE})_1 \quad \frac{d}{dt} P_{EE} \right]_2 \quad \frac{d}{dt} P_{EE} \Big]_3 \end{split}$$

$${}^{0}J_{v1}(\theta) = \begin{bmatrix} -\sin(\theta_{1}) \left[ 0.126\cos(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\cos(\theta_{2} + \theta_{3}) + 0.024\cos(\theta_{2}) \right] \\ \cos(\theta_{1}) \left[ 0.126\cos(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\cos(\theta_{2} + \theta_{3}) + 0.024\cos(\theta_{2}) \right] \\ 0 \end{bmatrix}$$

$${}^{0}J_{v2}(\theta) = \begin{bmatrix} -\cos(\theta_{1}) \left[ 0.126\sin(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\sin(\theta_{2} + \theta_{3}) + 0.024\sin(\theta_{2}) \right] \\ -\sin(\theta_{1}) \left[ 0.126\sin(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\sin(\theta_{2} + \theta_{3}) + 0.024\sin(\theta_{2}) \right] \\ 0.126\cos(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\cos(\theta_{2} + \theta_{3}) + 0.128\cos(\theta_{2}) \end{bmatrix}$$

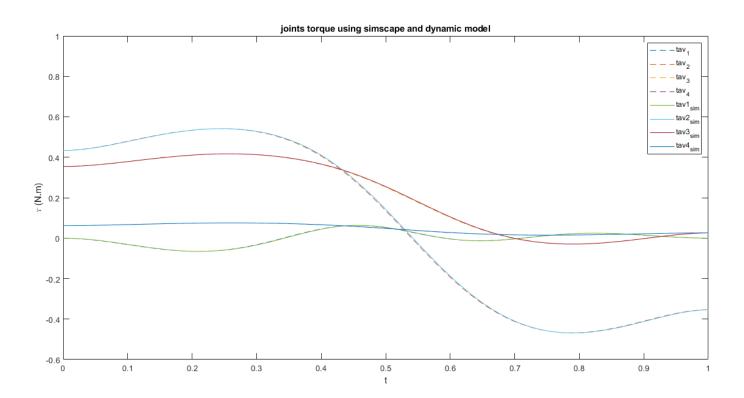
$${}^{0}J_{v2}(\theta) = \begin{bmatrix} -\cos(\theta_{1}) \left[ 0.126\sin(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\sin(\theta_{2} + \theta_{3}) + 0.024\sin(\theta_{2}) \right] \\ -\sin(\theta_{1}) \left[ 0.126\sin(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\sin(\theta_{2} + \theta_{3}) + 0.024\sin(\theta_{2}) \right] \\ 0.126\cos(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\cos(\theta_{2} + \theta_{3}) + 0.128\cos(\theta_{2}) \end{bmatrix}$$

$${}^{0}J_{\nu 3}(\theta) = \begin{bmatrix} -\cos(\theta_{1}) \left[ 0.126\sin(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\sin(\theta_{2} + \theta_{3}) \right] \\ -\sin(\theta_{1}) \left[ 0.126\sin(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\sin(\theta_{2} + \theta_{3}) \right] \\ 0.126\cos(\theta_{2} + \theta_{3} + \theta_{4}) + 0.124\cos(\theta_{2} + \theta_{3}) \end{bmatrix}$$

$${}^{0}J_{v4}(\theta) = \begin{bmatrix} -0.126\cos(\theta_{1})\sin(\theta_{2} + \theta_{3} + \theta_{4}) \\ -0.126\sin(\theta_{1})\sin(\theta_{2} + \theta_{3} + \theta_{4}) \\ 0.126\cos(\theta_{2} + \theta_{3} + \theta_{4}) \end{bmatrix}$$

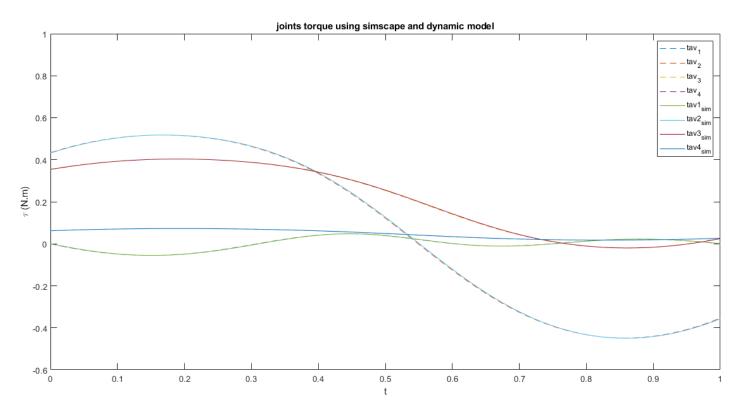
$${}^{0}J(\theta) = \begin{bmatrix} 0 & 1 & 1 & 1 \\ {}^{0}J_{v1} & {}^{0}J_{v2} & {}^{0}J_{v3} & {}^{0}J_{v4} \end{bmatrix}$$

**B**) Torque diagram of joints moving towards  $\theta_f = \left[ -\frac{\pi}{2}, \frac{\pi}{3}, \frac{\pi}{6}, -\frac{\pi}{5} \right]$  in 4567 routing:



C) Torque diagram of joints moving towards  $\theta_f = \left[ -\frac{\pi}{2}, \frac{\pi}{3}, \frac{\pi}{6}, -\frac{\pi}{5} \right]$  in 345 routing:

$$s(\tau) = 6\tau^5 - 15\tau^4 + 10\tau^3$$



# **D**) The calculation of the Robot end point position using *ode23s* ode function

```
function dp = odefun(t, p, th, dth)
i = floor(t*10^4 + 1);
th1 = th(1,i);
th2 = th(2,i);
th3 = th(3,i);
th4 = th(4,i);
dth1 = dth(1,i);
dth2 = dth(2,i);
dth3 = dth(3,i);
dth4 = dth(4,i);
dp = zeros(3,1);
J1 = [-\sin(th1)*(0.126*\cos(th2+th3+th4) + 0.124*\cos(th2+th3) +
0.024*\cos(th2));
       cos(th1)*(0.126*cos(th2+th3+th4) + 0.124*cos(th2+th3) +
0.024*cos(th2));
       01;
J2 = [-\cos(th1)*(0.126*\sin(th2+th3+th4) + 0.124*\sin(th2+th3) +
0.024*sin(th2));
      -\sin(th1)*(0.126*\sin(th2+th3+th4) + 0.124*\sin(th2+th3) +
0.024*sin(th2));
       0.126 \times \cos(th2 + th3 + th4) + 0.124 \times \cos(th2 + th3) + 0.128 \times \cos(th2);
J3 = [-\cos(th1)*(0.126*\sin(th2+th3+th4) + 0.124*\sin(th2+th3));
      -\sin(th1)*(0.126*\sin(th2+th3+th4) + 0.124*\sin(th2+th3));
       0.126*\cos(th2+th3+th4) + 0.124*\cos(th2+th3)];
J4 = [-\cos(th1) * 0.126* \sin(th2 + th3 + th4);
      -\sin(th1)*0.126*\sin(th2+th3+th4);
       0.126*cos(th2+th3+th4)];
J = [J1, J2, J3, J4];
v = J * [dth1;dth2;dth3;dth4];
dp(1) = v(1);
dp(2) = v(2);
dp(3) = v(3);
```

#### main function

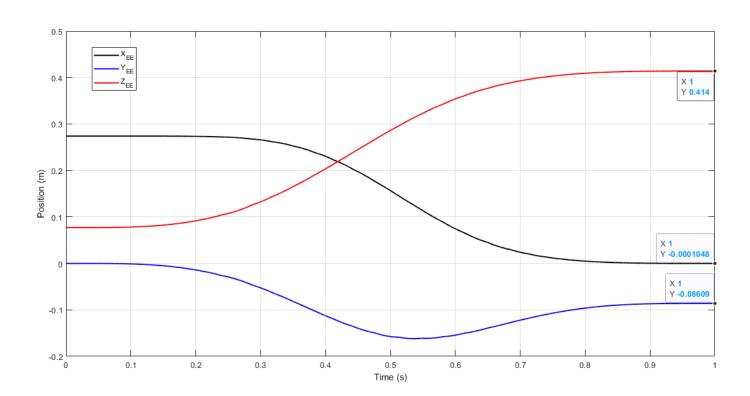
```
main_4567;

th = [theta1_num; theta2_num; theta3_num; theta4_num];

dth = [theta1_dot_num; theta2_dot_num; theta3_dot_num; theta4_dot_num];

[t, p] = ode23s(@(t,p) odefun(t,p,th,dth), T, [0.274;0;0.077]);

plot(T,p(:,1),'k','LineWidth',1.5);
hold on
plot(T,p(:,2),'b','LineWidth',1.5);
plot(T,p(:,3),'r','LineWidth',1.5);
xlabel('Time (s)')
ylabel('Position (m)')
grid on
legend('X_{EE}','Y_{EE}','Z_{EE}')
```



**E**) The calculation of the Robot end point position using cinematics directly:

$$\theta_f = \left[ -\frac{\pi}{2}, \frac{\pi}{3}, \frac{\pi}{6}, -\frac{pi}{5} \right]$$

$$P_{EE} = \begin{bmatrix} \cos(\theta_1) \left[ 0.126\cos(\theta_2 + \theta_3 + \theta_4) + 0.124\cos(\theta_2 + \theta_3) + 0.024\cos(\theta_2) \right] \\ \sin(\theta_1) \left[ 0.126\cos(\theta_2 + \theta_3 + \theta_4) + 0.124\cos(\theta_2 + \theta_3) + 0.024\cos(\theta_2) \right] \\ 0.077 + 0.126\sin(\theta_2 + \theta_3 + \theta_4) + 0.124\sin(\theta_2 + \theta_3) + 0.128\sin(\theta_2) \end{bmatrix} = \begin{bmatrix} P_{EE})_1 \\ P_{EE})_2 \\ P_{EE})_3 \end{bmatrix}$$

$$x_{EE}=0$$

$$y_{EE} = -1 \left[ 0.126 \cos \left( \frac{\pi}{3} + \frac{\pi}{6} - \frac{\pi}{5} \right) + 0.124 \cos \left( \frac{\pi}{3} + \frac{\pi}{6} \right) + 0.024 \cos \left( \frac{\pi}{3} \right) \right]$$
$$= -0.0861$$

$$z_{EE} = 0.077 + 0.126 \sin\left(\frac{\pi}{3} + \frac{\pi}{6} - \frac{\pi}{5}\right) + 0.124 \sin\left(\frac{\pi}{3} + \frac{\pi}{6}\right) + 0.128 \sin\left(\frac{\pi}{3}\right)$$
$$= 0.4138$$

As shown, the results from cinematics calculation matches the ones from ode23s.