

ASE387P.2 Mission Analysis and Design

Homework 4: Orbit Design

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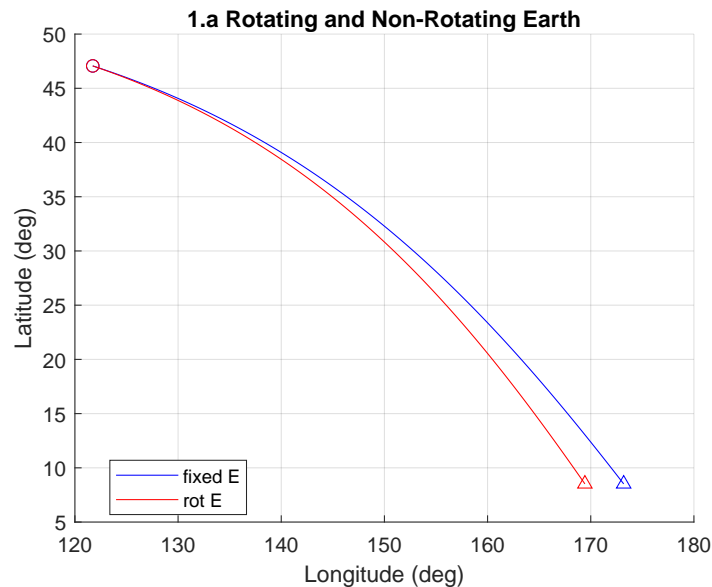
Problem 1: ISS Ground Tracks

A

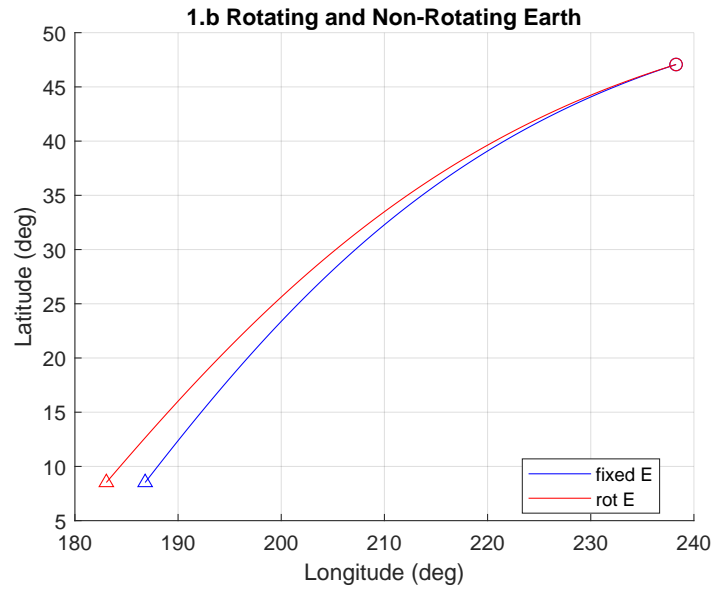
The following parameters were used to initialize the ISS orbit, which were taken from https://in-the-sky.org/spacecraft_elements.php?id=25544 on April 19:

- $a = 6794.588$ km
- $e = 0.00049$
- $i = 51.627$ deg
- $\omega = 40.1116$ deg
- $\Omega = 0$ deg
- $M = 70.88$

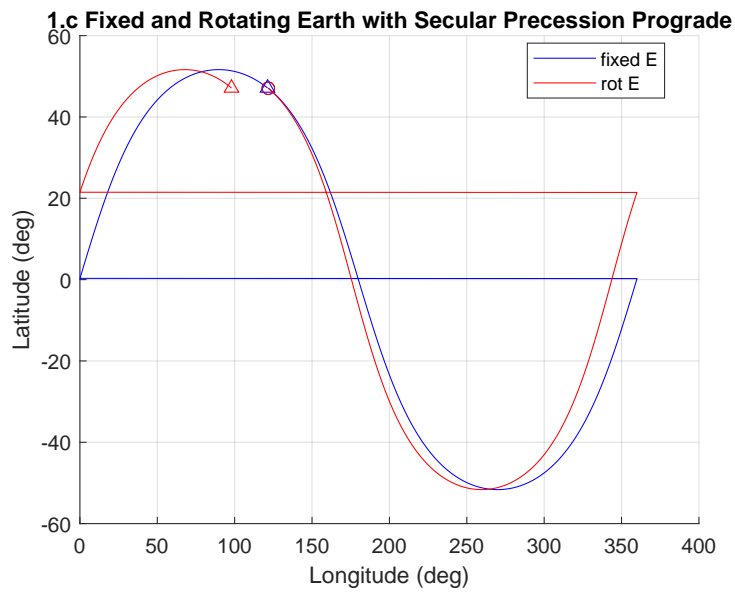
The right ascension of the ascending node, Ω , was set to 0 as stated in the problem statement.



B



C



To derive a formula for predicting the westward drift, first calculate the Draconitic period:

$$T_d = \frac{2\pi}{\dot{\omega} + \dot{M}} \quad (1)$$

Then calculate the rate of secular variation for the ascending node due to J2:

$$\dot{\Omega} = -\frac{3}{2}\bar{n}J_2\left(\frac{a_e}{\bar{a}}\right)^2\frac{1}{(1-\bar{e}^2)^2}\cos\bar{I} \quad (2)$$

\bar{a} , \bar{e} , and \bar{I} can be taken from the initial ISS orbit parameters, and \bar{n} is the mean motion of the orbit:

$$\bar{n} = \sqrt{\frac{\mu}{\bar{a}^3}} \quad (3)$$

Finally, the change in lambda was calculated as:

$$\Delta\lambda = -(w_E - \dot{\Omega})T_d \quad (4)$$

where w_E is the rotation rate of the Earth. $\Delta\lambda$ came out to **-22.870°**.

The calculated change in drift of the ascending node was taken from the difference between the initial longitude and the final longitude after one revolution, which came out to be **-22.790°**. The calculated drift was within 0.1° of the analytical prediction.

Problem 2: Orbit Design

Continuing from Equation 4, after m revolutions,

$$m\Delta\lambda = -(w_E - \dot{\Omega})T_d m \quad (5)$$

A condition for ground track repeat is that $m\Delta\lambda$ needs to be a multiple (let's say k) of 2π , or

$$k = \frac{m\Delta\lambda}{2\pi} = \frac{m(w_E - \dot{\Omega})T_d}{2\pi} = m \frac{T_d}{D_n} \quad (6)$$

For a ground track repeat orbit, the conditions for which the sub-satellite point repeatedly passes a geographical location (ϕ, λ) at regular intervals are given by:

$$(\omega_e - \dot{\Omega})D_n = k2\pi \quad (7)$$

$$(\dot{\omega} + \dot{M})T_d = m2\pi \quad (8)$$

As for frozen orbits, the largest perturbation on gravitational acceleration is due to J2, which is on the order of 10^{-3} . The next-largest perturbation is J3, which is on the order of 10^{-6} . Equation 2 gives the scalar secular variation on $\dot{\Omega}$ due to J2 which grows indefinitely. Equations 9 and 10 give the secular variations due to J2 for $\dot{\omega}$ and \dot{M} :

$$\dot{\omega} = -\frac{3}{4}\bar{n}J_2\left(\frac{a_e}{\bar{a}}\right)^2\frac{1}{(1-\bar{e}^2)^2}(1-5\cos^2\bar{I}) \quad (9)$$

$$\dot{M} = \bar{n}\left[1 - \frac{3}{4}\left(\frac{a_e}{\bar{a}}\right)^2J_2\frac{1}{(1-\bar{e}^2)^{\frac{3}{2}}}(1-3\cos^2\bar{I})\right] \quad (10)$$

J2 also leads to a short-period perturbation on all elements, but only semi-major axis is of interest:

$$\Delta a_{SP}(t) = \bar{a}J_2\left(\frac{a_e}{\bar{a}}\right)^2\left[\left(1 - \frac{3}{2}\sin^2\bar{I}\right)\left(\left(\frac{\bar{a}}{r}\right)^3 - \frac{1}{(1-\bar{e}^2)^{\frac{3}{2}}}\right) + \frac{3}{2}\left(\frac{\bar{a}}{r}\right)^3\sin^2\bar{I}\cos 2(\bar{w} + \bar{f})\right] \quad (11)$$

J3 exerts a long-period perturbation on all elements other than the semi-major axis, but only the eccentricity and perigee are of interest:

$$\Delta e_{LP}(t) = -\frac{1}{2}\frac{J_3}{J_2}\frac{a_e}{\bar{a}}\sin\bar{I}\sin\bar{w}(t) \quad (12)$$

$$\bar{e}\Delta\omega_{LP}(t) = -\frac{1}{2}\frac{J_3}{J_2}\frac{a_e}{\bar{a}}\frac{1}{(1-\bar{e}^2)}\sin\bar{I}\cos\bar{w}(t) \quad (13)$$

For frozen orbits, the average variation rates of e and w are set to 0. Thus, the mean argument of perigee should be around 90° .

$$w = 90^\circ \quad (14)$$

An orbit is sun-synchronous when the precession rate equals the mean motion of the Earth around the Sun. the Ω nodal rate needs to match the average rate of the Sun's motion projected onto the Earth's equator:

$$\frac{d\Omega}{dt} = \dot{\Omega} = \frac{360^\circ}{365.242 \text{ days/year}} = 0.9856^\circ/\text{day} \quad (15)$$

The angular precession for an Earth orbiting satellite is given by Equation 2. One can reform Equation 2 as a formula for inclination:

$$\bar{I} = \cos^{-1} \left[-\frac{2}{3} \frac{d\Omega}{dt} \frac{1}{J_2 \bar{n}} \left(\frac{\bar{a}(1 - \bar{e}^2)}{R_E} \right)^2 \right] \quad (16)$$

The process for determining the mean elements \bar{a} , \bar{e} , and \bar{I} involves making initial guesses and then minimizing the misclosure rate through an optimization routine:

$$\epsilon = m(w_E - \dot{\Omega}) - k(\dot{\omega} - \dot{M}) \quad (17)$$

Initial computed states for position and velocity will be integrated and iterated until a sun-synchronous, frozen, and repeated ground track orbit is found.

B

Problem 3

The calculations for this section were taken from the paper **Five Special Types of Orbits Around Mars** (2010 Liu, Baoyin, and Ma). A frozen orbit is possible on Mars. Mars' $J_2 = 1.95545\text{e-}3$ and $J_3 = 3.14498\text{e-}5$. In comparison, the Earth $J_2 = 1.08263\text{e-}3$ and $J_3 = -2.53266\text{e-}6$. The same positive sign between J_2 and J_3 must be accounted for to prevent the desired eccentricity from becoming negative. For Earth, ω is set to 90° . For Mars, ω must be set to around 270° .

The average variation rate of e from Equation 12 is given by:

$$\dot{e} = \frac{3nJ_3R_p^3 \sin \bar{I}}{4a^3(1 - e^2)^2} \left(\frac{5}{2} \sin^2 \bar{I} - 2 \right) \cos \omega \quad (18)$$

And from Equation 13, the average variation rate of ω is given by:

$$\dot{\omega} = \frac{3\bar{n}J_2R_p^2}{2a^2(1 - e^2)^2} \left[\left(2 - \frac{5}{2} \sin^2 \bar{I} \right) \left(1 + \frac{J_3R_p}{2J_2a(1 - e^2)} \left(\frac{\sin^2 \bar{I} - \bar{e}^2 \cos^2 \bar{I}}{\sin \bar{I}} \right) \frac{\sin \omega}{\bar{e}} \right) + \frac{3J_2R_p^2}{2\bar{a}^2(1 - e^2)^2} D \right] \quad (19)$$

where

$$D = (4 + \frac{7}{12} \bar{e}^2 + 2\sqrt{1 - \bar{e}^2}) - \sin^2 \bar{I} \left(\frac{103}{102} + \frac{3}{8} \bar{e}^2 + \frac{11}{2} \sqrt{1 - \bar{e}^2} \right) + \sin^4 \bar{I} \left(\frac{215}{418} - \frac{15}{32} \bar{e}^2 + \frac{15}{4} \sqrt{1 - \bar{e}^2} \right) + \dots H.O.T. \quad (20)$$

H.O.T. stands for higher order terms than J_3 . As stated in Problem 2, for frozen orbits, the average variation rates of e and ω are set to 0.

Solving the above equations yields the following for e and ω :

$$e = \frac{\frac{J_3R_p}{2J_2\bar{a}} \sin \bar{I} \sin \omega}{1 - \frac{3J_2R_p^2E}{\bar{a}^2(5\sin^2 \bar{I} - 4)}} \quad (21)$$

$$\omega = 270^\circ \quad (22)$$

Appendix

MATLAB code

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1  
2      %% HW 4  
3      % Junette Hsin
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