第 31卷第 2期 2 0 1 1年 4月

# 大地测量与地球动力学 JOURNAL OF GEODESY AND GEODYNAM ICS

Vol 31 No 2 Apr, 2011

文章编号: 1671-5942(2011)02-0129-04

# 地面三维激光扫描的点云配准误差研究

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**摘 要** 针对闭合条件下地面三维激光扫描点云配准产生的闭合差,基于测量平差理论,提出一种闭合差分配方法。首先通过间接平差理论求出各相邻测站间的坐标转换参数及其精度,再对闭合差按与方差成正比分配给各测站。通过多站点云配准实验,验证了该方法能在一定程度上提高点云配准的精度。

关键词 地面三维激光扫描; ICP算法;点云配准;配准误差;误差分配

中图分类号: TP751

文献标识码: A

# RESEARCH ON PO INT CLOUD REG ISTRATION ERROR OF TERRESTRIAL LASER SCANNING

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Abstract The existence of point cloud registration error must cause error propagation of multi-stations registration. A iming at the closed error of point cloud registration of terrestrial <sup>3</sup>D laser scanning a distributing approach of closed error based on the theory of surveying error adjustment is proposed. Firstly, the parameters of coordinate transformation and their accuracy of each adjacent station are worked out according to the indirect adjustment theory. Secondly, the closed error is adjusted to each station by variance proportion. Through the experiment of point cloud registration of multi-stations, the results indicate that the approach improves the point cloud registration accuracy. K eyw ords, terrestrial <sup>3</sup>D laser scanning ICP algorithm; point cloud registration; registration error error adjustment

# 1 引言

近年来,地面三维激光扫描技术在测绘、土木工程、逆向工程、三维城市建模、文物保护等领域的应用越来越广泛<sup>[1,2]</sup>。由于物体的遮挡、扫描仪的限制等原因,要完成对一个物体的完整三维数据获取,

地面三维激光扫描仪需要多测站多角度进行扫描。 但在不同测站进行扫描的坐标系不同,因此需要通 过点云配准将多站扫描数据拼接到同一坐标系下, 以获得物体表面的完整的形状信息。

点云配准<sup>[3]</sup>通常采用 ICP算法<sup>[4,5]</sup>或改进的 ICP算法<sup>[6,7]</sup>,对目标点集的每一个点在参考点集中

<sup>\*</sup> 收稿日期: 2011-01-01

**基金项目**: 教育部博士点基金 (200802900501);教育部博士点基金 (新教师 )(200802901516);国土环境与灾害监测国家测绘局重点实验室开放基金 (LEDM 2009A01)

找一个与之距离最近的点,建立点对的映射关系,然后以点对间距离平方和最小为条件,通过最小二乘法迭代解算出一个最优坐标变换关系式。这类拼接方法的精度高,但只适用于存在明确对应关系的点集之间的拼接,且对海量点云数据进行迭代计算过程速度较慢。简单的方法可以通过相邻测站3个或3个以上的公用标靶采用六参数法进行序列配准,最终将多站扫描数据拼接到同一坐标系下。但由于扫描测量不可避免地存在误差,从而导致点云配准存在误差,多站配准必然会引起误差传递。为了保证点云配准的精度,必须对点云配准的误差传播及误差分配进行研究。

## 2 点云配准的基本模型

点云配准实际上是一种刚体变换,两组点云之间不存在缩放关系,因此可以通过 3个旋转参数  $(\alpha, \beta, \gamma)$ 和 3个平移参数  $(x_0, y_0, z_0)$ 实现坐标转换。 坐标转换模型为:

$$F = \begin{bmatrix} \vec{X} \\ \vec{Y} \\ \vec{Z} \end{bmatrix} = R(\alpha, \beta, \gamma) \begin{bmatrix} \vec{X} \\ \vec{Y} \\ \vec{Z} \end{bmatrix} + \begin{bmatrix} \vec{X} \\ \vec{Y} \\ \vec{Z} \end{bmatrix}$$
(1)

式中,(X,Y,Z)和(x,y,z)分别为同一点在参考坐标系和目标坐标系下的坐标,R为旋转矩阵, $(\alpha,\beta,\gamma)$ 为3个角元素, $(x_0,y_0,z_0)$ 为平移参数。

将式(1)进行线性化得到:

$$F = F_0 + \left(\frac{\partial F}{\partial x_0}\right) dx_0 + \left(\frac{\partial F}{\partial y_0}\right) dy_0 + \left(\frac{\partial F}{\partial z_0}\right) dz + \left(\frac{\partial F}{\partial \alpha}\right) d\alpha + \left(\frac{\partial F}{\partial \beta}\right) d\beta + \left(\frac{\partial F}{\partial \gamma}\right) d\gamma$$
(2)

由此可得误差方程式为

$$V = B\hat{x} - L \tag{3}$$

其中,  $V = [V_1, V_2, ..., V_n]^T$ ,  $\hat{x} = (dx_0, dy_0, dz_0, d\alpha, d\beta, d\gamma)^T$ ,  $L = F - F_0$ 

$$B = \begin{bmatrix} \frac{\partial F_{x1}}{\partial x_0} & \frac{\partial F_{x1}}{\partial y_0} & \frac{\partial F_{x1}}{\partial z} & \frac{\partial F_{x1}}{\partial \alpha} & \frac{\partial F_{x1}}{\partial \beta} & \frac{\partial F_{x1}}{\partial \gamma} \\ \frac{\partial F_{y1}}{\partial x_0} & \frac{\partial F_{y1}}{\partial y_0} & \frac{\partial F_{y1}}{\partial z} & \frac{\partial F_{y1}}{\partial \alpha} & \frac{\partial F_{y1}}{\partial \beta} & \frac{\partial F_{y1}}{\partial \gamma} \\ \frac{\partial F_{z1}}{\partial x_0} & \frac{\partial F_{z1}}{\partial y_0} & \frac{\partial F_{z1}}{\partial z} & \frac{\partial F_{z1}}{\partial \alpha} & \frac{\partial F_{z1}}{\partial \beta} & \frac{\partial F_{z1}}{\partial \gamma} \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ \frac{\partial F_{xi}}{\partial x_0} & \frac{\partial F_{xi}}{\partial y_0} & \frac{\partial F_{xi}}{\partial z} & \frac{\partial F_{xi}}{\partial \alpha} & \frac{\partial F_{xi}}{\partial \beta} & \frac{\partial F_{xi}}{\partial \gamma} \\ \frac{\partial F_{yi}}{\partial x_0} & \frac{\partial F_{yi}}{\partial y_0} & \frac{\partial F_{yi}}{\partial z} & \frac{\partial F_{yi}}{\partial \alpha} & \frac{\partial F_{yi}}{\partial \beta} & \frac{\partial F_{yi}}{\partial \gamma} \\ \frac{\partial F_{zi}}{\partial x_0} & \frac{\partial F_{zi}}{\partial y_0} & \frac{\partial F_{zi}}{\partial z} & \frac{\partial F_{zi}}{\partial \alpha} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \gamma} \\ \frac{\partial F_{zi}}{\partial x_0} & \frac{\partial F_{zi}}{\partial y_0} & \frac{\partial F_{zi}}{\partial z} & \frac{\partial F_{zi}}{\partial \alpha} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \gamma} \\ \frac{\partial F_{zi}}{\partial \alpha} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \alpha} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \gamma} \\ \frac{\partial F_{zi}}{\partial x_0} & \frac{\partial F_{zi}}{\partial y_0} & \frac{\partial F_{zi}}{\partial z} & \frac{\partial F_{zi}}{\partial \alpha} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \gamma} & \frac{\partial F_{zi}}{\partial \alpha} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \gamma} \\ \frac{\partial F_{zi}}{\partial \alpha} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} \\ \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_{zi}}{\partial \beta} & \frac{\partial F_$$

当两个坐标系具有 n(n ≥ 3)对同名点时,由间接平差原理可得:

$$\hat{\mathbf{x}} = (\mathbf{B}^{\mathsf{T}} \mathbf{P} \mathbf{B})^{-1} \mathbf{B}^{\mathsf{T}} \mathbf{P} \mathbf{L} \tag{4}$$

单位权方差  $\sigma_0^2$ , 参数的协因数阵和协方差阵分别为:

$$\sigma_0^2 = \frac{\mathbf{V}^{\mathrm{T}} \mathbf{P} \mathbf{V}}{3\mathbf{n} - 6} \tag{5}$$

$$Q_{xx} = (B^{\mathsf{T}} P B)^{-1} \tag{6}$$

$$\mathbf{D}_{\mathbf{X}\mathbf{X}} = \sigma_0^2 \mathbf{Q}_{\mathbf{X}\mathbf{X}} \tag{7}$$

#### 3 点云配准误差分配

坐标转换模型 (1)通过变换可以得到:

$$\begin{bmatrix} \mathbf{X} \\ \mathbf{Y} \\ \mathbf{Z} \\ 1 \end{bmatrix} = \begin{bmatrix} \mathbf{a}_{11} & \mathbf{a}_{12} & \mathbf{a}_{13} & \mathbf{x}_{0} \\ \mathbf{a}_{21} & \mathbf{a}_{22} & \mathbf{a}_{23} & \mathbf{y}_{0} \\ \mathbf{a}_{31} & \mathbf{a}_{32} & \mathbf{a}_{33} & \mathbf{z}_{0} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \mathbf{x} \\ \mathbf{y} \\ \mathbf{z} \\ 1 \end{bmatrix}$$
(8)

今

$$\mathbf{T} = \begin{bmatrix} \mathbf{a}_{11} & \mathbf{a}_{12} & \mathbf{a}_{13} & \mathbf{x}_{0} \\ \mathbf{a}_{21} & \mathbf{a}_{22} & \mathbf{a}_{23} & \mathbf{y}_{0} \\ \mathbf{a}_{31} & \mathbf{a}_{32} & \mathbf{a}_{33} & \mathbf{z}_{0} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
(9)

由式 (8)知, T为坐标转换矩阵,通过左乘 T即可完成坐标转换。假设将第 i+1站点云数据转换到第 i站的坐标转换矩阵为  $T_{i+1}$ ,则从最后一站——第 n站转换到第 1站的变换矩阵为  $T_n T_{n-2}$   $\cdots$   $T_3 T_2$ , 当满足闭合条件,即从第 1站转换到第 1站时,应满足 [8]:

$$T_{n+1}T_{n}T_{n-1}\cdots T_{3}T_{2} = E$$
 (10)

但由于点云序列配准累积误差的存在,导致模型端点处的配准误差比较大,使得上式不成立,从而产生旋转角和平移参数闭合差。若干个旋转矩阵的乘积仍为旋转矩阵,因此  $T = T_{n+1} T_n T_{n-1} \cdots T_3 T_2$  仍为一个旋转矩阵,可由 T求出旋转角和平移量的闭合差。

$$\begin{cases}
\mathbf{f}_{a} = \alpha' - 0 = \alpha' \\
\mathbf{f}_{b} = \beta' - 0 = \beta' \\
\mathbf{f}_{y} = \gamma' - 0 = \gamma' \\
\mathbf{f}_{x_{0}} = \mathbf{x}_{0}' - 0 = \mathbf{x}_{0}' \\
\mathbf{f}_{y_{0}} = \mathbf{y}_{0}' - 0 = \mathbf{y}_{0}'
\end{cases} (11)$$

式中, $\alpha'$ 、 $\beta'$ 、 $\gamma'$ 、 $\chi_0$ 、 $\chi_0$ 、 $\chi_0$  分别为由第 1站计算到第 1站的旋转矩阵计算出来的 3个旋转角和 3个平移量。

相邻测站间的配准误差累积产生的,且各相邻测站之间的配准精度不相同。由闭合导线闭合差分配可知,角度闭合差平均分配,坐标闭合差与距离成正比分配,是按与其相应方差成正比进行分配的。因此将点云配准闭合差按照与方差成正比,依次递增的分配给各测站,即各测站的旋转角参数和平移量参数改正数为:

$$\frac{\sum_{k=2}^{i} \sigma_{\alpha_{k}}^{2}}{\sum_{k=2}^{i+1} \sigma_{\alpha_{k}}^{2}}, \quad v_{\beta_{i}} = \frac{\sum_{k=2}^{i} \sigma_{\beta_{k}}^{2}}{\sum_{k=2}^{i+1} \sigma_{\beta_{k}}^{2}}, \quad v_{\gamma_{i}} = \frac{\sum_{k=2}^{i} \sigma_{\gamma_{k}}^{2}}{\sum_{k=2}^{i+1} \sigma_{\gamma_{k}}^{2}} \qquad (13)$$

$$v_{x_{0}}^{i} = \frac{\sum_{k=2}^{i} (\sigma_{x_{0}}^{k})^{2}}{\sum_{k=2}^{i+1} (\sigma_{x_{0}}^{k})^{2}}, \quad v_{y_{0}}^{i} = \frac{\sum_{k=2}^{i} (\sigma_{y_{0}}^{k})^{2}}{\sum_{k=2}^{i+1} (\sigma_{y_{0}}^{k})^{2}}, \quad v_{x_{0}}^{i} = \frac{\sum_{k=2}^{i} (\sigma_{x_{0}}^{k})^{2}}{\sum_{k=2}^{i+1} (\sigma_{x_{0}}^{k})^{2}}$$

(14)

式中, n为测站总数, i为第 i测站 ( i=2, 3, ..., n+1, i=n+1时即为第 1站 )。

通过坐标转换矩阵求出的旋转角和平移量参数加上其相应的改正数,则可得出各扫描站相对于项目坐标系旋转参数的平差结果,然后代入式(1)计算各站扫描点云在项目坐标系中的坐标。

#### 4 实验验证

采取闭合环的多站配准实验方案,即从起点站 开始,沿闭合环进行多站配准,最后再回到起点站。 扫描仪设站 4次,按序列拼接依次计算各相邻测站 间的配准参数,中误差及参数方差,并通过计算最终 得到闭合差,按式(13)(14)进行误差分配,结果如 表 1。

表 1 各扫描站的坐标转换参数及其改正数

Tab 1 Coordinate transformation parameters and their adjustments at each scanning station

扫描站		1	2		3			4			1			
旋转角 (°)	α	0	<b>—</b> 0.	160	4	<b>-0.</b>	241	3	<b>—0.</b>	447	5	<b>-0.</b>	032	5
	$\mathbf{V}_{\!$	0	0.	001	3	0.	019	8	0.	027	5	0.	032	5
	β	0	-0.	200	5	0.	293	0	0.	286	8	0.	109	5
	<b>V</b> β	0	-0.	004	4	-0.	066	9	-0.	092	8	-0.	109	5
	γ	0	85.	296	3	179.	873	7	146.	209	6	<b>-</b> 0.	034	7
	$\mathbf{v}_{\!\scriptscriptstyle\gamma}$	0	0.	001	4	0.	021	2	0.	029	4	0.	034	7
	$\mathbf{X}_{()}$	0	3.	976	9	6.	941	2	5.	078	8	0.	000	3
平移量 (m)	$\mathbf{V}_{\mathbf{x}()}$	0	<b>—</b> 0.	000	0	<b>—</b> 0.	000	2	<b>-0.</b>	000	3	<b>-</b> 0.	000	3
	$\mathbf{y}_0$	0	8.	351	6	2.	283	4	-7.	406	1	0.	010	1
	$\mathbf{v}_{\mathbf{y}0}$	0	<b>—</b> 0.	000	4	<b>—</b> 0.	006	2	-0.	008	5	-0.	010	1
	<b>Z</b> )	0	<b>—</b> 0.	001	5	<b>—</b> 0.	032	3	-0.	021	6			0
	$\mathbf{v}_{\mathbf{z}_0}$	0			0			0			0			0

为了近似地评价误差分配的好坏,选择经过点 云精度影响最大的第一4站,选择若干点,分别计算出 在闭合差分配前后经点云配准后的坐标,并与其在第 1站中的同名点进行比较,计算坐标差值  $\Delta_{\mathbf{X}}$   $\Delta_{\mathbf{y}}$  和  $\Delta_{\mathbf{z}}$  点位中误差为:

$$_{\mathbf{m}_{p}} = \sqrt{\frac{\sum_{i=1}^{n} \left(\Delta_{\mathbf{X}}^{2} + \Delta_{\mathbf{y}}^{2} + \Delta_{\mathbf{z}}^{2}\right)}{n}}$$
(15)

通过计算可以得到,闭合差分配前的点位中误差为 11 mm,闭合差分配后的点位中误差为 6.4 mm,通过闭合差分配后的配准精度要好于分配前的配准精度。因此通过闭合差分配后的点云配准可以更好的反映物体完整的三维信息,从而提高其测量结果的可靠性。

# 5 结语

针对点云序列配准中产生的误差积累,给出了误差闭合差的分配方法。该方法是基于在各站配准后的参数方差,根据有限的同名点对计算各站的坐标平移和旋转参数及闭合条件将闭合差按照与方差成正比进行分配,计算量小。从实验可以看出,本文提出的闭合差分配方法对点云配准结果有一定的改善。但由于闭合差实际上是由各相邻测站的配准误差的非线性函数,简单的将其线性处理不能在真正意义上将闭合差完全正确分配,为了更好地分配点云配准闭合差,应对点云配准误差传播规律<sup>[9]</sup>及非线性条件下的闭合差分配等理论进行研究。

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