

NE250_HW02_mnegus-prob5

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1 NE 250 – Homework 2

1.1 Problem 5

10/6/2017

A critical reactor has a multiplication factor of $k = 1$. The multiplication factor (for an infinite reactor) can be defined as

$$k_{\infty} \equiv \frac{\# \text{ neutrons produced}}{\# \text{ neutrons absorbed}}$$

Mathematically, the number of neutrons produced is $\int_0^{\infty} \nu \Sigma_f(E) \phi(E) dE$ and the number of neutrons absorbed is $\int_0^{\infty} \Sigma_a(E) \phi(E) dE$. Altogether, we can mathematically describe a critical reactor as

$$1 = \frac{\int_0^{\infty} \nu \Sigma_f(E) \phi(E) dE}{\int_0^{\infty} \Sigma_a(E) \phi(E) dE}$$

or equivalently

$$\int_0^{\infty} \nu \Sigma_f(E) \phi(E) dE = \int_0^{\infty} \Sigma_a(E) \phi(E) dE.$$

Since we are considering only thermal cross sections, we will let $\Sigma_X(E) = \Sigma_X(0.025 \text{ eV}) = \Sigma_{X,T}$ and we find

$$\nu \Sigma_{f,T} \int_0^{\infty} \phi(E) dE = \Sigma_{a,T} \int_0^{\infty} \phi(E) dE.$$

The integrals over flux cancel, and so

$$\nu \Sigma_{f,T} = \Sigma_{a,T}.$$

The macroscopic cross sections can be rewritten as $\Sigma_{f,T} = \Sigma_{f,T,f}$ and $\Sigma_{a,T} = \Sigma_{a,T,f} + \Sigma_{a,T,m}$ where subscripts f and m denote fuel and moderator, respectively. Furthermore, each macroscopic cross section for each material can be expressed in terms of the material's number density and microscopic cross section, $\Sigma = n\sigma$. In total

$$\nu n_f \sigma_{f,T,f} = n_f \sigma_{a,T,f} + n_m \sigma_{a,T,m}.$$

The fuel-to-moderator (number) density ratio at criticality can then be expressed as

$$\frac{n_f}{n_m} = \frac{\sigma_{a,T,m}}{\nu \sigma_{f,T,f} - \sigma_{a,T,f}}.$$

```
In [1]: def FMratio(xsa_mod,xsa_fuel,xf_fuel,nu):
        return xsa_mod/(nu*xf_fuel - xsa_fuel)
```

We can define our thermal cross sections as follows (from ENDF/B-VII.1)

```
In [2]: xsf = {'U235': 585.086}
        xsa = {'C12': 0.00336,
               'Be9': 0.01004,
               'H1': 0.33201,
               'H2': 0.00051,
               'O16': 0.00019,
               'U235': 585.086 + 98.6864
               }
        xsa['graphite'] = xsa['C12']
        xsa['water'] = 2*xsa['H1'] + xsa['O16']
        xsa['heavy water'] = 2*xsa['H2'] + xsa['O16']
```

a) Graphite

```
In [3]: xsa_mod=xsa['graphite']
        print('Critical Fuel-to-Moderator Ratio: ',FMratio(xsa_mod,xsa['U235'],xsf['U235'],nu))
```

Critical Fuel-to-Moderator Ratio: 4.5457204996214396e-06

b) Beryllium

```
In [4]: xsa_mod=xsa['Be9']
        print('Critical Fuel-to-Moderator Ratio: ',FMratio(xsa_mod,xsa['U235'],xsf['U235'],nu))
```

Critical Fuel-to-Moderator Ratio: 1.358304577863073e-05

c) Water

```
In [5]: xsa_mod=xsa['water']
        print('Critical Fuel-to-Moderator Ratio: ',FMratio(xsa_mod,xsa['U235'],xsf['U235'],nu))
```

Critical Fuel-to-Moderator Ratio: 0.0008986050634087967

d) Heavy Water

```
In [6]: xsa_mod=xsa['heavy water']
        print('Critical Fuel-to-Moderator Ratio: ',FMratio(xsa_mod,xsa['U235'],xsf['U235'],nu))
```

Critical Fuel-to-Moderator Ratio: 1.6370005370660543e-06