



Sofia University "St. Kliment Ohridski"  
Faculty of Mathematics and Informatics  
**Department of Numerical Methods and  
Algorithms**

## Cloth Simulation

Master's thesis  
in

Mathematical Modeling and Computational Mathematics

*Author:*

Dimitar V. Trendafilov  
FN: 25612

*Supervisor:*

Assist. Prof. Dr.  
Tihomir B. Ivanov

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# Introduction

Cloths are everywhere!

- In featured films.
- In video game.
- The textile and fashion industries.

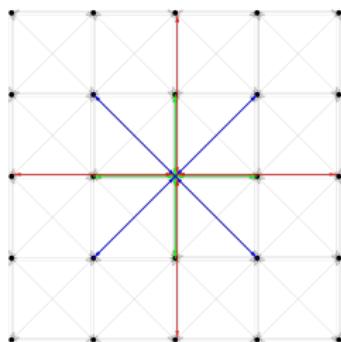


# Particle Mass-Spring Model

- Considers the fabric as a mesh of  $m \times n$  masses (particles).
- Each connected to 12 others through massless springs.
- The evolution of the system is governed by Newton's second law of motion  $\vec{F}_{i,j} = \mu \vec{a}_{i,j}$

# Particle Mass-Spring Model

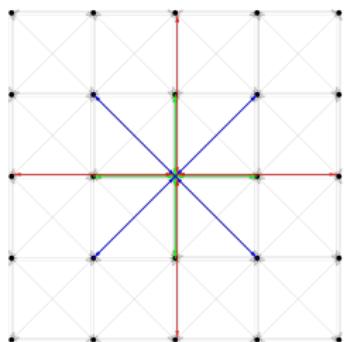
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- Structural springs.
- Shear springs.
- Flexion springs.

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## Internal Forces

$$\vec{F}_{internal}(P_{i,j}) = - \sum_{(k,l) \in R_{i,j}} F_{Hooke}(i,j,k,l)$$

# Particle Mass-Spring Model

## External Forces

$$\vec{F}_{external}(P_{i,j}) = \vec{F}_{gravity}(P_{i,j}) + \vec{F}_{damp}(P_{i,j}) + \vec{F}_{wind}(P_{i,j})$$

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## Initial Value Problem

$$\left\{ \begin{array}{l} \vec{F}_{i,j} = \mu \vec{a}_{i,j} \\ \frac{d\vec{v}_{i,j}}{dt} = \vec{a}_{i,j} \\ \frac{d\vec{P}_{i,j}}{dt} = \vec{v}_{i,j} \end{array} \right. , \text{ where } i = \overline{1, m} \text{ and } j = \overline{1, n}$$

# Simple Explicit Method

## Numerical Scheme

$$\left\{ \begin{array}{l} \vec{a}_{i,j}^n = \frac{1}{\mu} \vec{F}_{i,j}^n \\ \vec{v}_{i,j}^{n+1} = \vec{v}_{i,j}^n + \frac{\Delta t}{\mu} \vec{F}_{i,j}^n \\ \vec{P}_{i,j}^{n+1} = \vec{P}_{i,j}^n + \Delta t \vec{v}_{i,j}^n + \frac{\Delta t^2}{\mu} \vec{F}_{i,j}^n \end{array} \right.$$

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### Pros:

- Extremely easy to implement.
- Low storage complexity.

# Simple Explicit Method

## Numerical Scheme

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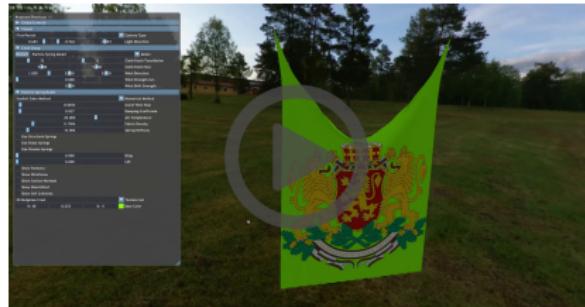
### Pros:

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### Cons:

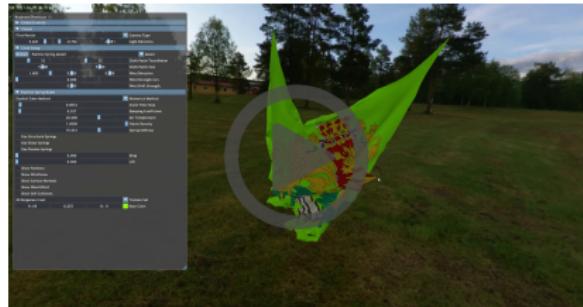
- Has numerical stability issues.
- Due to the previous point it needs small time steps which in turn leads to performance decline.

# Simple Explicit Method



Video experiment showing material properties behavior:

- Changes in sagging with different spring stiffness coefficients.
- Changes in sagging with different material density.



Video experiment showing issues with large damping coefficients:

- Large fabric density can cause instabilities.
- Larger damping coefficient values mitigate the issue.
- Can give the feeling that the atmosphere is too viscose.

# Basic Störmer–Verlet Method

## Numerical Scheme

$$\begin{cases} \vec{a}_{i,j}^n = \frac{1}{\mu} \vec{F}_{i,j}^n \\ \vec{P}_{i,j}^{n+1} = 2\vec{P}_{i,j}^n - \vec{P}_{i,j}^{n-1} + \Delta t^2 \vec{a}_{i,j}^n \end{cases}$$

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### Pros:

- As simple as the simple explicit method.
- Low computation and storage complexity.
- Extremely stable.

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### Pros:

- As simple as the simple explicit method.
- Low computation and storage complexity.
- Extremely stable.

### Cons:

- Global error of  $\mathcal{O}(\Delta t)$ .

# Basic Störmer–Verlet Method

Video experiment demonstrating basic Störmer–Verlet method stability:

0:00 - 0:09 : Time step  $\Delta t$  is fixed at 0.01s.

0:13 - 0:21 : Time step  $\Delta t$  is fixed at 0.02s.

0:25 - 0:33 : Time step  $\Delta t$  is fixed at 0.03s.

0:34 - 0:41 : Time step  $\Delta t$  is fixed at 0.04s.

0:49 - 0:53 : Time step  $\Delta t$  is fixed at 0.005s.



# Variable Time Discretization Step Verlet Methods

## Numerical Scheme

$$\begin{cases} \vec{a}_{i,j}^n = \frac{1}{\mu} \vec{F}_{i,j}^n \\ \vec{P}_{i,j}^{n+1} = \vec{P}_{i,j}^n + (\vec{P}_{i,j}^n - \vec{P}_{i,j}^{n-1}) \frac{\Delta t_n}{\Delta t_{n-1}} + \vec{a}_{i,j}^n \frac{\Delta t_n + \Delta t_{n-1}}{2} \Delta t_n \end{cases}$$

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### Pros:

- In terms of simplicity and precision they are similar to the Basic Störmer–Verlet Method.
- Add small computation overhead, but no storage overhead.

# Variable Time Discretization Step Verlet Methods

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### Pros:

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- Add small computation overhead, but no storage overhead.

### Cons:

- Have precision issues with small time steps.

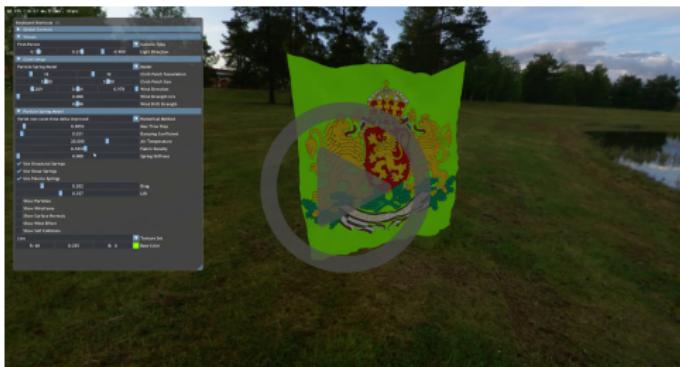
# Variable Time Discretization Step Verlet Methods

Video experiment showing precision issues:

0:03 - 0:15 : At maximum  $\Delta t = 0.0053s$  numerical errors cause vibrations.

0:16 - 0:21 : At maximum  $\Delta t = 0.0113s$  vibrations stop.

0:22 - 0:24 : At maximum  $\Delta t = 0.0165s$  numerical errors lead to catastrophic instabilities.



# Wind Model

## Equation

$$\vec{F}_{wind} = \frac{1}{2}\rho A \left[ (C_D - C_L)(\vec{v}^r \cdot \vec{n})\vec{v}^r + C_L |\vec{v}|^2 \vec{n} \right]$$

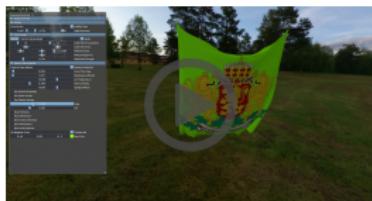
- $\rho$  is air density.
- $A$  is the cloth surface area.
- $\vec{n}$  is the geometry normal.
- $\vec{v}$  and  $\vec{v}^r$  are the velocity and relative velocity.
- $C_D$  and  $C_L$  are drag and lift coefficients

# Wind Model

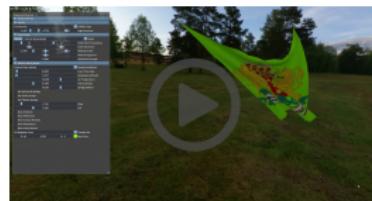
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Drag and lift



Turbulence

# Continuum Mechanics Based Models

- Treating a cloth patch as a planar homogeneous orthotropic material.
- A finite element method for linear elastostatics in 2D is derived.
- Nonlinear effects due to large rotational deformations are handled using corotational formulation.

## ODE System of the Model

$$M\ddot{x} + D\dot{x} + K(x - x_0) = f_{ext}$$

## Mass Matrix

- The mass distribution is defined by a diagonal matrix  $M$ .
- Masses of the model are concentrated at the vertices of the mesh.
- Mass is the area “corresponding” to the respective vertex in the triangle mesh, times the material density.
- The area corresponding to a vertex is defined by the Voronoi area.

# Continuum Mechanics Based Models

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## Damping Matrix

Rayleigh damping is used to simulate viscosity.

$$D = \alpha M + \beta K$$

where  $\alpha$  and  $\beta$  are the damping coefficients for mass and stiffness damping, respectively.

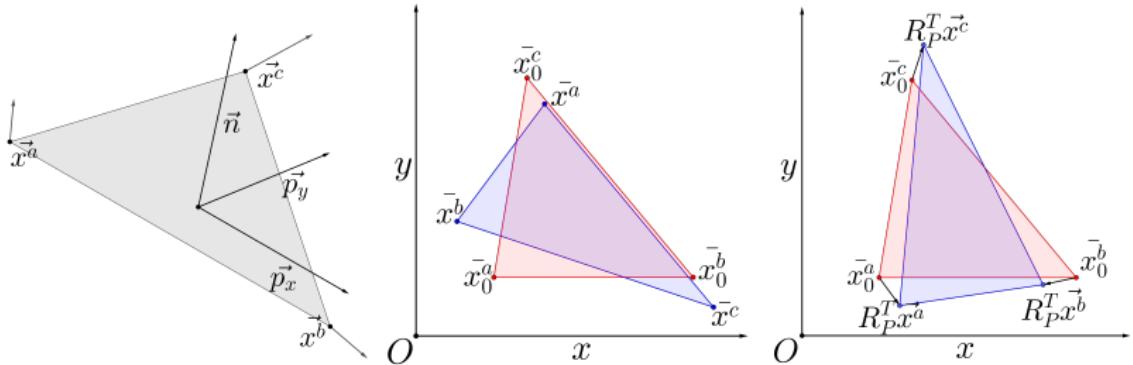
# Continuum Mechanics Based Models

## Stiffness Matrix

$K = (\iiint_{\Omega} B^T C B d\Omega)$  is the stiffness matrix for the 2D problem.

Using corotational formulation it is transformed to

$K^{CR} = R_P K R_P^T$  and  $\hat{K}^{CR} = R_P K$ . Using those the linear elastostatics problem becomes  $F^{CR} = K^{CR}x - \hat{K}^{CR}\bar{x}_0$ .



# Continuum Mechanics Based Models

The ODE system of the model is numerically solved using an implicit method:

$$\begin{aligned} & \left( M + \Delta t D + \Delta t^2 K^{CR} \right) \Delta v = \\ & = -\Delta t \left( K^{CR} x_n - F_0^{CR} - f_{ext,n} + \Delta t K^{CR} v_n + Dv_n \right) \\ & \Delta x = \Delta t(v_n + \Delta v) \end{aligned}$$

# Results



Simulating wool with:

- $\Delta t = 0.003s$
- $\alpha = 0.2, \beta = 0.01$



Simulating viscose with:

- $\Delta t = 0.003s$
- $\alpha = 0.2, \beta = 0.01$

# Results



Simulating wool with:

- $\Delta t = 0.099s$
- $\alpha = 0.2, \beta = 0.01$



Simulating wool with:

- $\Delta t = 0.003s$
- $\alpha = 0.2, \beta = 0.05$

# Future Work

- Collision detection
  - Arbitrary geometry sweep tests
  - Bounding volume hierarchy
  - Friction forces
- Wind simulation
  - Use vector field generated by user-defined “wind sources”
  - Cloth affecting air currents
- Other models
  - Nonlinear hinge models
  - Geometry based models
  - Artificial intelligence based
  - Position based dynamics
- Computational performance optimizations
  - Parallelization
  - Conjugate gradient methods
  - Mesh subdivision

# Questions



Thank you  
for your attention!