

Adjoint-Based Optimization of Time-Dependent Fluid-Structure Systems using a High-Order Discontinuous Galerkin Discretization

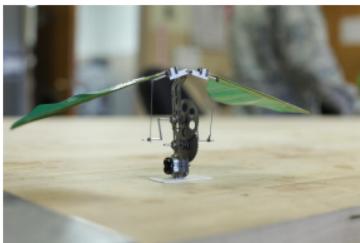
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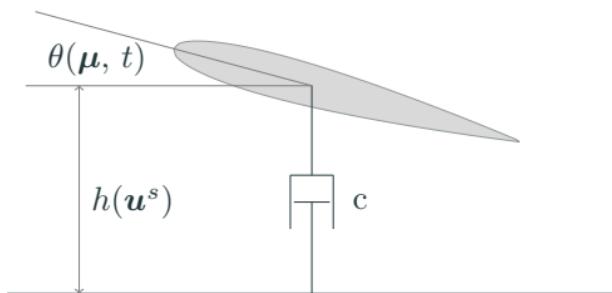
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Optimization of unsteady fluid-structure systems

- Discover energetically optimal **flapping** motions
 - understand biological systems, design Micro Aerial Vehicles (MAVs)



- Design minimal weight structures and vehicles that will not **flutter**
- Design **energy harvesting** mechanisms



Unsteady *single physics* optimization formulation

Goal: Find the solution of the *unsteady PDE-constrained optimization* problem

$$\underset{\boldsymbol{U}, \boldsymbol{\mu}}{\text{minimize}} \quad \mathcal{J}(\boldsymbol{U}, \boldsymbol{\mu})$$

$$\text{subject to} \quad \boldsymbol{C}(\boldsymbol{U}, \boldsymbol{\mu}) \leq 0$$

$$\frac{\partial \boldsymbol{U}}{\partial t} + \nabla \cdot \boldsymbol{F}(\boldsymbol{U}, \nabla \boldsymbol{U}) = 0 \quad \text{in } v(\boldsymbol{\mu}, t)$$

where

- $\boldsymbol{U}(\boldsymbol{x}, t)$ PDE solution
- $\boldsymbol{\mu}$ design/control parameters
- $\mathcal{J}(\boldsymbol{U}, \boldsymbol{\mu}) = \int_{T_0}^{T_f} \int_{\Gamma} j(\boldsymbol{U}, \boldsymbol{\mu}, t) dS dt$ objective function
- $\boldsymbol{C}(\boldsymbol{U}, \boldsymbol{\mu}) = \int_{T_0}^{T_f} \int_{\Gamma} \mathbf{c}(\boldsymbol{U}, \boldsymbol{\mu}, t) dS dt$ constraints



High-order discretization of PDE-constrained optimization

- *Continuous* PDE-constrained optimization problem

$$\underset{\boldsymbol{U}, \boldsymbol{\mu}}{\text{minimize}} \quad \mathcal{J}(\boldsymbol{U}, \boldsymbol{\mu})$$

$$\text{subject to} \quad \boldsymbol{C}(\boldsymbol{U}, \boldsymbol{\mu}) \leq 0$$

$$\frac{\partial \boldsymbol{U}}{\partial t} + \nabla \cdot \boldsymbol{F}(\boldsymbol{U}, \nabla \boldsymbol{U}) = 0 \quad \text{in } v(\boldsymbol{\mu}, t)$$

- *Fully discrete* PDE-constrained optimization problem

$$\begin{array}{ll} \underset{\boldsymbol{u}_0, \dots, \boldsymbol{u}_{N_t} \in \mathbb{R}^{N_u},}{\text{minimize}} & J(\boldsymbol{u}_0, \dots, \boldsymbol{u}_{N_t}, \boldsymbol{k}_{1,1}, \dots, \boldsymbol{k}_{N_t,s}, \boldsymbol{\mu}) \\ & \boldsymbol{k}_{1,1}, \dots, \boldsymbol{k}_{N_t,s} \in \mathbb{R}^{N_u}, \\ & \boldsymbol{\mu} \in \mathbb{R}^{n_\mu} \end{array}$$

$$\text{subject to} \quad \boldsymbol{C}(\boldsymbol{u}_0, \dots, \boldsymbol{u}_{N_t}, \boldsymbol{k}_{1,1}, \dots, \boldsymbol{k}_{N_t,s}, \boldsymbol{\mu}) \leq 0$$

$$\boldsymbol{u}_0 - \boldsymbol{g}(\boldsymbol{\mu}) = 0$$

$$\boldsymbol{u}_n - \boldsymbol{u}_{n-1} - \sum_{i=1}^s b_i \boldsymbol{k}_{n,i} = 0$$

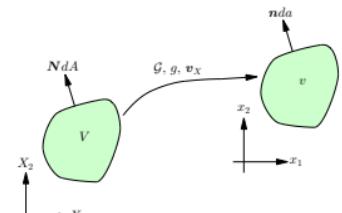
$$\boldsymbol{M} \boldsymbol{k}_{n,i} - \Delta t_n \boldsymbol{r}(\boldsymbol{u}_{n,i}, \boldsymbol{\mu}, t_{n,i}) = 0$$



Highlights of globally high-order discretization

- **Arbitrary Lagrangian-Eulerian formulation:**
Map, $\mathcal{G}(\cdot, \mu, t)$, from physical $v(\mu, t)$ to reference V

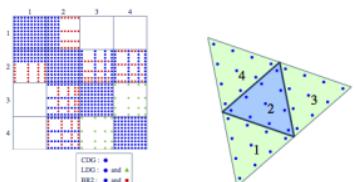
$$\frac{\partial \mathbf{U}_X}{\partial t} \Big|_X + \nabla_X \cdot \mathbf{F}_X(\mathbf{U}_X, \nabla_X \mathbf{U}_X) = 0$$



Mapping-Based ALE

- **Space discretization:** discontinuous Galerkin

$$M \frac{\partial \mathbf{u}}{\partial t} = \mathbf{r}(\mathbf{u}, \mu, t)$$



DG Discretization

$$\mathbf{u}_n = \mathbf{u}_{n-1} + \sum_{i=1}^s b_i \mathbf{k}_{n,i}$$

$$M \mathbf{k}_{n,i} = \Delta t_n \mathbf{r}(\mathbf{u}_{n,i}, \mu, t_{n,i})$$

- **Quantity of interest:** solver-consistency

$$F(\mathbf{u}_0, \dots, \mathbf{u}_{N_t}, \mathbf{k}_{1,1}, \dots, \mathbf{k}_{N_t,s})$$

c_1	a_{11}			
c_2	a_{21}	a_{22}		
\vdots	\vdots	\vdots	\ddots	
c_s	a_{s1}	a_{s2}	\cdots	a_{ss}
	b_1	b_2	\cdots	b_s

Butcher Tableau for DIRK

Adjoint method to efficiently compute gradients of QoI

- Consider the *fully discrete* output functional $F(\mathbf{u}_n, \mathbf{k}_{n,i}, \boldsymbol{\mu})$
 - Represents either the **objective** function or a **constraint**
- The *total derivative* with respect to the parameters $\boldsymbol{\mu}$, required in the context of gradient-based optimization, takes the form

$$\frac{dF}{d\boldsymbol{\mu}} = \frac{\partial F}{\partial \boldsymbol{\mu}} + \sum_{n=0}^{N_t} \frac{\partial F}{\partial \mathbf{u}_n} \frac{\partial \mathbf{u}_n}{\partial \boldsymbol{\mu}} + \sum_{n=1}^{N_t} \sum_{i=1}^s \frac{\partial F}{\partial \mathbf{k}_{n,i}} \frac{\partial \mathbf{k}_{n,i}}{\partial \boldsymbol{\mu}}$$

- The sensitivities, $\frac{\partial \mathbf{u}_n}{\partial \boldsymbol{\mu}}$ and $\frac{\partial \mathbf{k}_{n,i}}{\partial \boldsymbol{\mu}}$, are expensive to compute, requiring the solution of $n_\boldsymbol{\mu}$ linear evolution equations
- **Adjoint method:** alternative method for computing $\frac{dF}{d\boldsymbol{\mu}}$ that require one linear evolution equation for each quantity of interest, F



Adjoint equation derivation: outline

- Define **auxiliary** PDE-constrained optimization problem

$$\underset{\substack{\boldsymbol{u}_0, \dots, \boldsymbol{u}_{N_t} \in \mathbb{R}^{N_u}, \\ \boldsymbol{k}_{1,1}, \dots, \boldsymbol{k}_{N_t,s} \in \mathbb{R}^{N_u}}}{\text{minimize}} \quad F(\boldsymbol{u}_0, \dots, \boldsymbol{u}_{N_t}, \boldsymbol{k}_{1,1}, \dots, \boldsymbol{k}_{N_t,s}, \boldsymbol{\mu})$$

subject to $\boldsymbol{R}_0 = \boldsymbol{u}_0 - \boldsymbol{g}(\boldsymbol{\mu}) = 0$

$$\boldsymbol{R}_n = \boldsymbol{u}_n - \boldsymbol{u}_{n-1} - \sum_{i=1}^s b_i \boldsymbol{k}_{n,i} = 0$$

$$\boldsymbol{R}_{n,i} = \boldsymbol{M} \boldsymbol{k}_{n,i} - \Delta t_n \boldsymbol{r}(\boldsymbol{u}_{n,i}, \boldsymbol{\mu}, t_{n,i}) = 0$$

- Define **Lagrangian**

$$\mathcal{L}(\boldsymbol{u}_n, \boldsymbol{k}_{n,i}, \boldsymbol{\lambda}_n, \boldsymbol{\kappa}_{n,i}) = F - \boldsymbol{\lambda}_n^T \boldsymbol{R}_0 - \sum_{n=1}^{N_t} \boldsymbol{\lambda}_n^T \boldsymbol{R}_n - \sum_{n=1}^{N_t} \sum_{i=1}^s \boldsymbol{\kappa}_{n,i}^T \boldsymbol{R}_{n,i}$$

- The solution of the optimization problem is given by the **Karush-Kuhn-Tucker (KKT) system**

$$\frac{\partial \mathcal{L}}{\partial \boldsymbol{u}_n} = 0, \quad \frac{\partial \mathcal{L}}{\partial \boldsymbol{k}_{n,i}} = 0, \quad \frac{\partial \mathcal{L}}{\partial \boldsymbol{\lambda}_n} = 0, \quad \frac{\partial \mathcal{L}}{\partial \boldsymbol{\kappa}_{n,i}} = 0$$



Dissection of fully discrete adjoint equations

- **Linear** evolution equations solved **backward** in time
- **Primal** state/stage, $\mathbf{u}_{n,i}$ required at each state/stage of dual problem
- Heavily dependent on **chosen output**

$$\boldsymbol{\lambda}_{N_t} = \frac{\partial \mathbf{F}}{\partial \mathbf{u}_{N_t}}^T$$

$$\boldsymbol{\lambda}_{n-1} = \boldsymbol{\lambda}_n + \frac{\partial \mathbf{F}}{\partial \mathbf{u}_{n-1}}^T + \sum_{i=1}^s \Delta t_n \frac{\partial \mathbf{r}}{\partial \mathbf{u}} (\mathbf{u}_{n,i}, \boldsymbol{\mu}, t_{n-1} + c_i \Delta t_n)^T \boldsymbol{\kappa}_{n,i}$$

$$\mathbf{M}^T \boldsymbol{\kappa}_{n,i} = \frac{\partial \mathbf{F}}{\partial \mathbf{u}_{N_t}}^T + b_i \boldsymbol{\lambda}_n + \sum_{j=i}^s a_{ji} \Delta t_n \frac{\partial \mathbf{r}}{\partial \mathbf{u}} (\mathbf{u}_{n,j}, \boldsymbol{\mu}, t_{n-1} + c_j \Delta t_n)^T \boldsymbol{\kappa}_{n,j}$$

- Gradient reconstruction via dual variables

$$\frac{dF}{d\boldsymbol{\mu}} = \frac{\partial F}{\partial \boldsymbol{\mu}} + \boldsymbol{\lambda}_0^T \frac{\partial \mathbf{g}}{\partial \boldsymbol{\mu}}(\boldsymbol{\mu}) + \sum_{n=1}^{N_t} \Delta t_n \sum_{i=1}^s \boldsymbol{\kappa}_{n,i}^T \frac{\partial \mathbf{r}}{\partial \boldsymbol{\mu}}(\mathbf{u}_{n,i}, \boldsymbol{\mu}, t_{n,i})$$

[Zahr and Persson, 2016]



Energetically optimal flapping vs. required thrust

Energy = 0.21935

Thrust = 0.0000

Energy = 3.00404

Thrust = 1.5000

Energy = 6.2869

Thrust = 2.5000

Optimal $T_x = 0$

Optimal
 $T_x = 1.5$

Optimal
 $T_x = 2.5$



Structure: semi-discretization, first-order form

$$M^s \frac{\partial \mathbf{u}^s}{\partial t} = \mathbf{r}^s(\mathbf{u}^s; t) = \mathbf{r}^{ss}(\mathbf{u}^s) + \mathbf{r}^{sf} \cdot \mathbf{t}$$

- Semidiscretization (CG-FEM) of **continuum** (hyperelasticity)

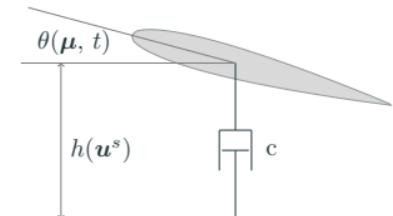
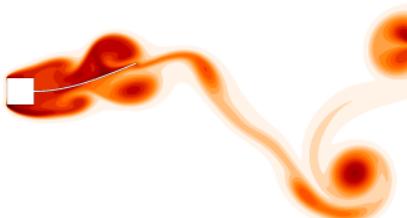
$$\frac{\partial \mathbf{p}}{\partial t} - \nabla \cdot \mathbf{P}(\mathbf{G}) = \mathbf{b} \quad \text{in } \Omega_0$$

$$\mathbf{P}(\mathbf{G}) \cdot \mathbf{N} = \mathbf{t} \quad \text{on } \Gamma_N$$

$$\mathbf{x} = \mathbf{x}_D \quad \text{on } \Gamma_D$$

- Force balance on **rigid body**

$$M \frac{\partial^2 \mathbf{q}}{\partial t^2} + \mathbf{C} \frac{\partial \mathbf{q}}{\partial t} + \mathbf{K} \mathbf{q} = \mathbf{t}$$



Coupled fluid-structure formulation

- Write discretized fluid and structure equations as ODEs

$$\begin{aligned}\boldsymbol{M}^f \dot{\boldsymbol{u}}^f &= \boldsymbol{r}^f(\boldsymbol{u}^f; \boldsymbol{x}) \\ \boldsymbol{M}^s \dot{\boldsymbol{u}}^s &= \boldsymbol{r}^s(\boldsymbol{u}^s; \boldsymbol{t}) \\ &= \boldsymbol{r}^{ss}(\boldsymbol{u}^s) + \boldsymbol{r}^{sf} \cdot \boldsymbol{t}\end{aligned}$$

in the fluid \boldsymbol{u}^f and structure \boldsymbol{u}^s variables

- Apply couplings
 - Structure-to-fluid: deform fluid domain $\boldsymbol{x} = \boldsymbol{x}(\boldsymbol{u}^s)$
 - Fluid-to-structure: apply boundary traction $\boldsymbol{t} = \boldsymbol{t}(\boldsymbol{u}^f)$
- Write coupled system as $\boldsymbol{M}\dot{\boldsymbol{u}} = \boldsymbol{r}(\boldsymbol{u})$

$$\boldsymbol{u} = \begin{bmatrix} \boldsymbol{u}^f \\ \boldsymbol{u}^s \end{bmatrix} \quad \boldsymbol{r}(\boldsymbol{u}) = \begin{bmatrix} \boldsymbol{r}^f(\boldsymbol{u}^f; \boldsymbol{x}(\boldsymbol{u}^s)) \\ \boldsymbol{r}^s(\boldsymbol{u}^s; \boldsymbol{t}(\boldsymbol{u}^f)) \end{bmatrix} \quad \boldsymbol{M} = \begin{bmatrix} \boldsymbol{M}^f & \\ & \boldsymbol{M}^s \end{bmatrix}$$



High-order partitioned FSI solver: IMEX Runge-Kutta¹

- Exploit **linear dependence** of structure residual (\mathbf{r}^s) on traction (\mathbf{t})

$$\mathbf{r}(\mathbf{u}) = \begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \mathbf{t}(\mathbf{u}^f)) \end{bmatrix} = \underbrace{\begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \tilde{\mathbf{t}}) \end{bmatrix}}_{\mathbf{f}(\mathbf{u})} + \underbrace{\begin{bmatrix} \mathbf{0} \\ \mathbf{r}^s(\mathbf{u}^s; \tilde{\mathbf{t}}) \end{bmatrix}}_{\mathbf{g}(\mathbf{u})}$$

- Apply **high-order** implicit-explicit Runge-Kutta scheme to discretize

$$M \frac{\partial \mathbf{u}}{\partial t} = \mathbf{r}(\mathbf{u}) = \underbrace{\mathbf{f}(\mathbf{u})}_{\text{explicit}} + \underbrace{\mathbf{g}(\mathbf{u})}_{\text{implicit}}$$

- Explicit Runge-Kutta scheme $\hat{c}, \hat{A}, \hat{b}$ for $\mathbf{f}(\mathbf{u})$
- Diagonally implicit scheme c, A, b for $\mathbf{g}(\mathbf{u})$

$$\mathbf{u}_n = \mathbf{u}_{n-1} + \sum_{i=1}^s \hat{b}_i \hat{\mathbf{k}}_{n,i} + \sum_{i=1}^s b_i \mathbf{k}_{n,i}$$

$$M \mathbf{k}_{n,i} = \Delta t_n \mathbf{g} \left(\mathbf{u}_{n-1} + \sum_{j=1}^{i-1} \hat{a}_{ij} \hat{\mathbf{k}}_{n,j} + \sum_{j=1}^i a_{ij} \mathbf{k}_{n,j} \right)$$

$$M \hat{\mathbf{k}}_{n,i} = \Delta t_n \mathbf{f} \left(\mathbf{u}_{n-1} + \sum_{j=1}^{i-1} \hat{a}_{ij} \hat{\mathbf{k}}_{n,j} + \sum_{j=1}^i a_{ij} \mathbf{k}_{n,j} \right)$$

¹[van Zuijlen and Bijl, 2005, Froehle and Persson, 2014]

High-order partitioned FSI solver: IMEX Runge-Kutta¹

- Exploit **linear dependence** of structure residual (\mathbf{r}^s) on traction (\mathbf{t})

$$\mathbf{r}(\mathbf{u}) = \begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \mathbf{t}(\mathbf{u}^f)) \end{bmatrix} = \underbrace{\begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \tilde{\mathbf{t}}) \end{bmatrix}}_{\mathbf{f}(\mathbf{u})} + \underbrace{\begin{bmatrix} \mathbf{0} \\ \mathbf{r}^s(\mathbf{u}^s; \mathbf{t} - \tilde{\mathbf{t}}) \end{bmatrix}}_{\mathbf{g}(\mathbf{u})}$$

- Solve: (1) implicit **structure**, (2) implicit **fluid**, (3) explicit **structure**
- Due to choice of IMEX partition: **no explicit fluid stages**

¹[van Zuijlen and Bijl, 2005, Froehle and Persson, 2014]

High-order partitioned FSI solver: IMEX Runge-Kutta

- Define **stage solutions**

$$\begin{aligned}\mathbf{u}_{n,i}^s &= \mathbf{u}_{n-1}^s + \sum_{j=1}^i a_{ij} \mathbf{k}_{n,j}^s + \sum_{j=1}^{i-1} \hat{a}_{ij} \hat{\mathbf{k}}_{n,j}^s \\ \mathbf{u}_{n,i}^f &= \mathbf{u}_{n-1}^f + \sum_{j=1}^i a_{ij} \mathbf{k}_{n,j}^f\end{aligned}$$

- Define **traction predictor** as true traction at previous stage

$$\tilde{\mathbf{t}}_{n,i} = \mathbf{t}(\mathbf{u}_{n,i-1})$$

- Solve for **stage velocities** ($i = 1, \dots, s$)

$$\begin{aligned}\mathbf{M}^s \mathbf{k}_{n,i}^s &= \Delta t_n \mathbf{r}^s(\mathbf{u}_{n,i}^s; \tilde{\mathbf{t}}_{n,i}) \\ \mathbf{M}^f \mathbf{k}_{n,i}^f &= \Delta t_n \mathbf{r}^f(\mathbf{u}_{n,i}^f; \mathbf{x}(\mathbf{u}_{n,i}^s)) \\ \mathbf{M}^s \hat{\mathbf{k}}_{n,i}^s &= \Delta t_n \mathbf{r}^{sf}(\mathbf{t}(\mathbf{u}_{n,i}^f) - \tilde{\mathbf{t}}_{n,i})\end{aligned}$$

- Update state solution at new time

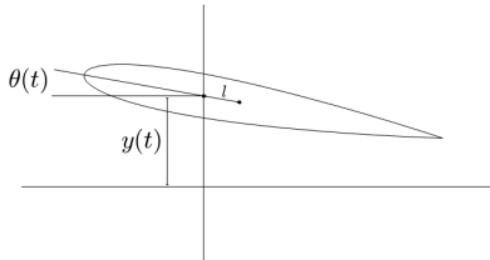
$$\mathbf{u}_n^f = \mathbf{u}_{n-1}^f + \sum_{j=1}^s b_j \mathbf{k}_{n,j}^f, \quad \mathbf{u}_n^s = \mathbf{u}_{n-1}^s + \sum_{j=1}^s b_j \mathbf{k}_{n,j}^s + \sum_{j=1}^s \hat{b}_j \hat{\mathbf{k}}_{n,j}^s$$


BERKELEY LAB 13/24



Validation: benchmark pitching airfoil system

- Simple FSI benchmark problem for studying the high-order accuracy of the IMEX scheme
- Rigid pitching/heaving NACA 0012 airfoil, torsional spring
- Smooth heaving step $y(t)$ prescribed, angle $\theta(t)$ measured



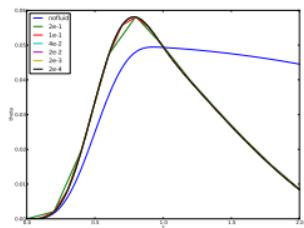
Setup

Mach number

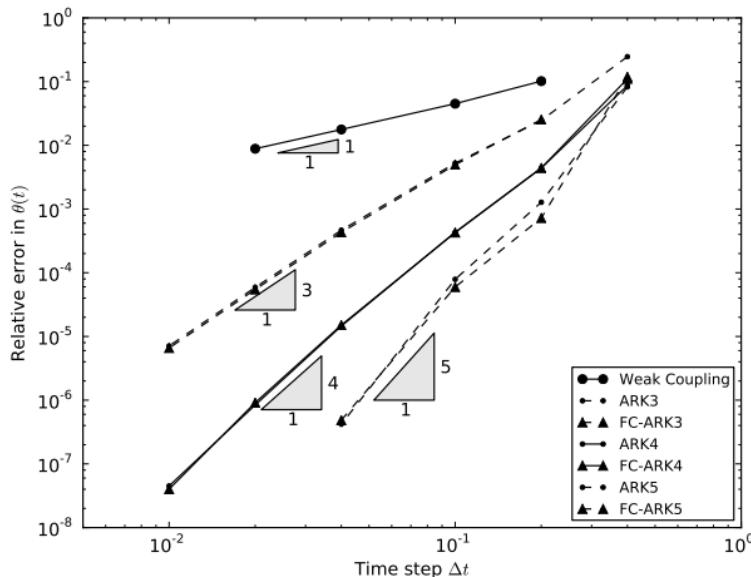


Validation: benchmark pitching airfoil system

- Up to 5th order of convergence in time.
- Similar accuracy as solving fully coupled system



Angle $\theta(t)$ vs time t

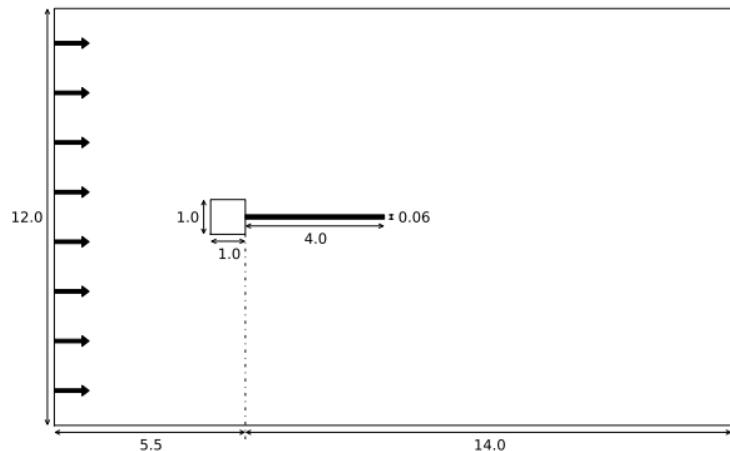


Entropy



Validation: cantilever system

- Standard FSI benchmark problem.
- Elastic cantilever behind a square bluff body in incompressible flow.



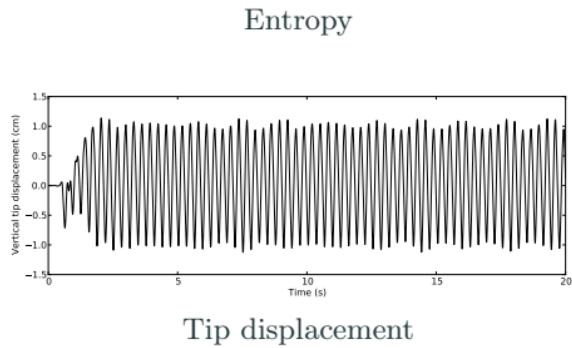
- Cantilever:
 $\rho_s = 100 \text{ kg/m}^3$, $\nu_s = 0.35$,
 $E = 2.5 \times 10^5 \text{ Pa}$.
- Fluid & Flow:
 $\rho_f = 1.18 \text{ kg/m}^3$,
 $\nu_f = 1.54 \times 10^{-5} \text{ m}^2/\text{s}$,
 $v_f = 0.513 \text{ m/s}$, $\text{Re} = 333$,
 $\text{Ma} = 0.2$.

- Vortex shedding frequency: $\sim 6.3 \text{ Hz}$

Cantilever first mode: 3.03 Hz



Validation: cantilever system



- Tip frequency:
 $f = 3.14 \text{ Hz}$
(Literature:
2.98 – 3.25 Hz)
- Tip displacement:
 $d_{max} = 1.09 \text{ cm}$
(Literature:
0.95 – 1.25 cm)



Flow around Membrane, 3-D

- Angle of attack 22.6° , Reynolds number 2000.
- Flexible structure prevents leading edge separation.



Adjoint equations for high-order partitioned IMEX FSI solver

- Define

$$\mathbf{r}_{n,i}^f = \mathbf{r}^f(\mathbf{u}_{n,i}^f; \mathbf{x}(\mathbf{u}_{n,i}^s)) \quad \mathbf{r}_{n,i}^s = \mathbf{r}^s(\mathbf{u}_{n,i}^s; \tilde{\mathbf{t}}_{n,i})$$

- Final condition for state Lagrange multipliers (F is quantity of interest)

$$\boldsymbol{\lambda}_{N_t}^f = \frac{\partial F}{\partial \mathbf{u}_{N_t}^f}^T, \quad \boldsymbol{\lambda}_{N_t}^s = \frac{\partial F}{\partial \mathbf{u}_{N_t}^s}^T$$

- Solve for stage Lagrange multipliers ($j = s, \dots, 1$)

- Explicit structure stage

$$\mathbf{M}^{sT} \hat{\boldsymbol{\kappa}}_{n,j}^s = \frac{\partial F}{\partial \hat{\mathbf{k}}_{n,j}^s}^T + \hat{b}_j \boldsymbol{\lambda}_n^s + \Delta t_n \sum_{i=j+1}^s \hat{a}_{ij} \frac{\partial \mathbf{r}_{n,i}^f}{\partial \mathbf{u}^s}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=j+1}^s \hat{a}_{ij} \frac{\partial \mathbf{r}_{n,i}^s}{\partial \mathbf{u}^s}^T \boldsymbol{\kappa}_{n,i}^s$$

- Implicit fluid stage

$$\begin{aligned} \mathbf{M}^{fT} \boldsymbol{\kappa}_{n,j}^f &= \frac{\partial F}{\partial \mathbf{k}_{n,j}^f}^T + b_j \boldsymbol{\lambda}_n^f + \Delta t_n \sum_{i=j}^s a_{ij} \frac{\partial \mathbf{r}_{n,i}^f}{\partial \mathbf{u}^f}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=j+1}^s a_{ij} \frac{\partial \tilde{\mathbf{t}}_{n,i}}{\partial \mathbf{u}^f}^T \mathbf{r}^{sfT} \boldsymbol{\kappa}_{n,i}^s \\ &\quad - \Delta t_n \sum_{i=j}^s a_{ij} \frac{\partial \mathbf{t}_{n,i}}{\partial \mathbf{u}^f}^T \mathbf{r}^{sfT} \hat{\boldsymbol{\kappa}}_{n,i}^s + \Delta t_n \sum_{i=j+1}^s a_{ij} \frac{\partial \tilde{\mathbf{t}}_{n,i}}{\partial \mathbf{u}^f}^T \mathbf{r}^{sfT} \hat{\boldsymbol{\kappa}}_{n,i}^s \end{aligned}$$

- Implicit structure stage

$$\mathbf{M}^{sT} \boldsymbol{\kappa}_{n,j}^s = \frac{\partial F}{\partial \mathbf{k}_{n,j}^s}^T + b_j \boldsymbol{\lambda}_n^s + \Delta t_n \sum_{i=j}^s a_{ij} \frac{\partial \mathbf{r}_{n,i}^f}{\partial \mathbf{u}^s}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=j}^s a_{ij} \frac{\partial \mathbf{r}_{n,i}^s}{\partial \mathbf{u}^s}^T \boldsymbol{\kappa}_{n,i}^s$$

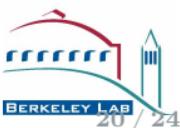
Adjoint equations for high-order partitioned IMEX FSI solver

- Update state Lagrange multipliers at new time

$$\begin{aligned}\boldsymbol{\lambda}_{n-1}^f &= \boldsymbol{\lambda}_n^f + \frac{\partial F}{\partial \boldsymbol{u}_{n-1}^f}^T + \Delta t_n \sum_{i=1}^s \frac{\partial \boldsymbol{r}_{n,i}^f}{\partial \boldsymbol{u}^f}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=1}^s \frac{\partial \tilde{\boldsymbol{t}}_{n,i}}{\partial \boldsymbol{u}^f}^T \boldsymbol{r}_{n,i}^{sf T} \boldsymbol{\kappa}_{n,i}^s \\ &\quad + \Delta t_n \sum_{i=1}^s \left[\frac{\partial \tilde{\boldsymbol{t}}_{n,i}}{\partial \boldsymbol{u}^f} - \frac{\partial \boldsymbol{t}_{n,i}}{\partial \boldsymbol{u}^f} \right]^T \boldsymbol{r}_{n,i}^{sf T} \hat{\boldsymbol{\kappa}}_{n,i}^s \\ \boldsymbol{\lambda}_{n-1}^s &= \boldsymbol{\lambda}_n^s + \frac{\partial F}{\partial \boldsymbol{u}_{n-1}^s}^T + \Delta t_n \sum_{i=1}^s \frac{\partial \boldsymbol{r}_{n,i}^f}{\partial \boldsymbol{u}^s}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=1}^s \frac{\partial \boldsymbol{r}_{n,i}^s}{\partial \boldsymbol{u}^s}^T \boldsymbol{\kappa}_{n,i}^s\end{aligned}$$

- Reconstruct **total derivative** of quantity of interest F as

$$\begin{aligned}\frac{dF}{d\boldsymbol{\mu}} &= \frac{\partial F}{\partial \boldsymbol{\mu}} + \boldsymbol{\lambda}_0^f{}^T \frac{\partial \bar{\boldsymbol{u}}^f}{\partial \boldsymbol{\mu}} + \boldsymbol{\lambda}_0^s{}^T \frac{\partial \bar{\boldsymbol{u}}^s}{\partial \boldsymbol{\mu}} - \sum_{n=0}^{N_t} \Delta t_n \sum_{i=1}^s \boldsymbol{\kappa}_{n,i}^f{}^T \frac{\partial \boldsymbol{r}_{n,i}^f}{\partial \boldsymbol{\mu}} \\ &\quad - \sum_{n=0}^{N_t} \Delta t_n \sum_{i=1}^s \boldsymbol{\kappa}_{n,i}^s{}^T \frac{\partial \boldsymbol{r}_{n,i}^s}{\partial \boldsymbol{\mu}} - \sum_{n=0}^{N_t} \Delta t_n \sum_{i=1}^s \hat{\boldsymbol{\kappa}}_{n,i}^{s,T} \frac{\partial \boldsymbol{r}_{n,i}^{sf}}{\partial \boldsymbol{\mu}}\end{aligned}$$

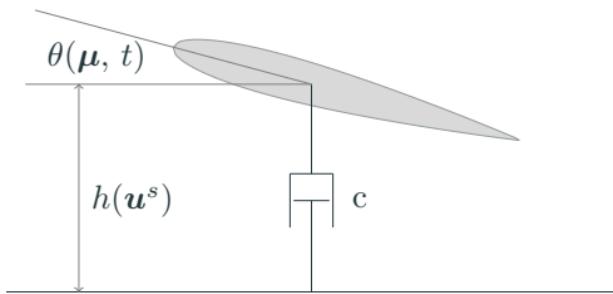


Optimal energy harvesting from foil-damper system

Goal: Maximize energy harvested from foil-damper system

$$\underset{\boldsymbol{\mu}}{\text{maximize}} \quad \frac{1}{T} \int_0^T (c h^2(\mathbf{u}^s) - M_z(\mathbf{u}^f) \dot{\theta}(\boldsymbol{\mu}, t)) dt$$

- Fluid: Isentropic Navier-Stokes on deforming domain (ALE)
- Structure: Force balance in y -direction between foil and damper
- Motion driven by *imposed* $\theta(\boldsymbol{\mu}, t) = \mu_1 \cos(2\pi ft)$



$$\mu_1^* \approx 45^\circ$$

Summary and future work

Summary

- Extended standard fully discrete adjoint framework to partitioned, high-order multiphysics setting
- Demonstrated on simple optimal energy harvesting model problem

Future work

- Extend structure model to fully deformable continuum model
 - High-order, energy conserving load transfer from fluid to structure
 - Handle discontinuities between fluid elements that arise from DG discretization
- Study optimal 3D flapping with deformable wing

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