Thermal expansion calculations:

For a mirror:

I assume the optical axis is \hat{z} , for transversal axis I choose y.

For a mirror, we have from Jeremy's paper:

$$R_{\rm th}^{-1} = -N\frac{\alpha P}{\kappa w^2}$$

And

$$\left[\frac{1}{m} = \frac{\frac{1}{K} \cdot \frac{1}{k}}{\frac{1}{M} \cdot \frac{1}{K} \cdot \frac{1}{M}} = \frac{1}{m}\right] \checkmark$$

$$R^{-1} = R_0^{-1} + R_{\text{th}}^{-1}$$

For a lens:

I will calculate everything for every facet of the lens independently.

Let us start by calculating the relation between the optical length $\xi\left(y,z\right)$, $[\mathbf{m}]$ and R,n of one facet of the lens:

The facet of the lens is defined be:

$$z^2 + y^2 = R^2 \setminus -y^2$$

$$z^2 = R^2 - y^2 \setminus \sqrt{}$$

$$z = \sqrt{R^2 - y^2} \setminus \text{Simplify}$$

$$z = R\sqrt{1 - \frac{y^2}{R^2}}$$

To leading order this equals:

$$z = R\left(1 - \frac{y^2}{2R^2}\right)$$

Multiplying it be n we get (all is up to an additive constant):

$$\xi = n \cdot z\left(y\right) = nR\left(1 - \frac{y^2}{2R^2}\right)$$

And also it is useful to write:

$$\frac{d^2\xi}{dy^2} = \frac{d^2}{dy^2} \left[nR \left(1 - \frac{y^2}{2R^2} \right) \right] \label{eq:delta_fit}$$

$$\frac{d^2\xi}{dy^2} = \frac{n\cancel{R}}{R^{\cancel{2}}} = \frac{n}{R}$$

$$\left\lceil \frac{1}{m} = \frac{1}{m} \right\rceil \checkmark$$

An important note is that $\frac{d^2\xi}{dy^2}=\propto n, R^{-1}$, and so if we later find that $\frac{d^2\xi}{dy^2}$ should be increased by a we can either transform $n\to n+aR$ (such that the new $\frac{d^2\xi}{dy^2}$ is

$$\frac{d^2\xi_{\text{new}}}{dy^2} = \frac{n+aR}{R} = \frac{n}{R} + a \tag{1}$$

) or transform $R \to R' = \frac{nR}{n+aR}$ (so that the new

)

$$\frac{d^2\xi_{\text{new}}}{dy^2} = \frac{n}{R'} = \frac{\varkappa}{\frac{\sqrt{R}}{n'+aR}} = \frac{n+aR}{R} = \frac{n}{R} + a\sqrt{2}$$
(2)

more generally, the total optical length is (up to a constant):

$$\xi(y) = \int_{0}^{z(y)} n(y, z) dz$$

Where z(y) is like before, the location of the end of the lens.

And so ξ can be modified by changing n(y, z) or by changing z(y).

As said before, this is the change due to the thermal effects only in one side of the lens:

The change ξ due to the change in n: This size can be expressed as:

$$\Delta \xi_{n} = \int_{0}^{z(y)} \Delta n(y, z) dz = \int_{0}^{z(y)} \frac{\delta n(y, z)}{\delta T} \cdot \delta T(y, z) dz$$

For an approximately constant $\frac{\delta n}{\delta T}$ we can write:

$$\Delta \xi_{n} = \frac{\delta n}{\delta T} \int_{0}^{z(y)} \delta T(y, z) dz$$

The change in ξ due to the change in the thickness of the lens We start by writing an expression for how much the thickness z(y) changes due to the heating:

$$\Delta z(y) = \alpha \cdot \frac{1+\nu}{1-\nu} \cdot \int_{0}^{z(y)} \delta T(y,z) dz$$
(3)

$$\left[\mathbf{m} = \frac{1}{K} \cdot \mathbf{1} \cdot \mathbf{K} \cdot \mathbf{m} = \mathbf{m} \right] \checkmark$$

$$\Delta \xi_{d} = n \cdot \Delta z (y) = n \cdot \alpha \cdot \frac{1+\nu}{1-\nu} \cdot \int_{0}^{z(y)} \delta T (y,z) dz$$

Assuming:

$$\int\limits_{0}^{z(y)} \delta T\left(y,z\right) dz \propto \left(T_{\max} - T_{0}\right) \cdot w \cdot F\left(y,\sigma = w\right) \tag{4}$$

For some dimensionless symmetrical function F with typical width of w, mean of 0, and maximum of w (like $we^{-\frac{y^2}{w^2}}$). The typical width of w is there because the wider the beam is, the wider the heating profile, and the typical height of w is because the wider it is, the deeper the heat will go into the lens before dissipating.

Moreover, $(T_{\text{max}} - T_0)$ should go like

$$(T_{\rm max} - T_0) \propto \frac{\beta P_{\rm Laser}}{\kappa w_{\rm on lens}} \Rightarrow$$

$$(T_{\text{max}} - T_0) = C \cdot \frac{\beta P_{\text{Laser}}}{\kappa w_{\text{on lens}}}$$

$$\left[K = 1 \cdot \frac{1 \cdot \frac{1}{s}}{\frac{f \cdot \mathcal{M}}{s \pi^2 \cdot K}} = K\right] \checkmark$$

Where C is some dimensionless constant, β is the absorption coefficient on the face of the lens $[\beta] = 1$, κ is the heat conductivity $[\kappa] = \frac{\frac{J}{2} \cdot m}{m^2 \cdot K}$. $w_{\text{on lens}}$ is the width of the laser $[w_{\text{on lens}}] = m$ and P_{laser} is the laser power $[P_{\text{laser}}] = \frac{J}{s}$. Plugging it back to (4):

$$\int_{0}^{\infty} \delta T\left(y,z\right) dz \approx C \cdot \frac{\beta P_{\text{Laser}}}{\kappa \underline{w_{\text{on tens}}}} \cdot \underline{w_{\text{on tens}}} \cdot F\left(y\right) \tag{4}$$

$$[K\cdot m=K\cdot m]\checkmark$$

And so

$$\frac{d^2\Delta\xi}{dy^2} = \frac{d^2\Delta\xi_n}{dy^2} + \frac{d^2\Delta\xi_d}{dy^2} \approx \frac{C \cdot \frac{\beta P_{\text{Laser}}}{\kappa}}{w_{\text{on lens}}^2} \left(\underbrace{\frac{\delta n}{\delta T}}_{\text{change in refractive index term}} + \underbrace{n \cdot \alpha \cdot \frac{1+\nu}{1-\nu}}_{\text{change in thickness term}} \right) = C \cdot \frac{\beta P_{\text{Laser}}}{\kappa w_{\text{on lens}}^2} \left(\frac{\delta n}{\delta T} + n \cdot \alpha \cdot \frac{1+\nu}{1-\nu} \right)$$

$$\left[\frac{1}{m} = \frac{m}{m^2} = 1 \cdot \frac{1 \cdot \frac{1}{s}}{\frac{s}{m^2 \cdot K} \cdot m^2} \cdot \left(\frac{1}{K}\right) = \frac{1}{m}\right] \checkmark$$

Where $\frac{\delta n}{\delta T}$, ν , α , n_0 , k, P_{laser} , κ , $w_{\text{on lens}}$, β are constants of the system.

Having this, we can substitute back to (1) and (2):

$$n \rightarrow n' = n + aR = n + C \cdot \frac{\beta P_{\text{Laser}}}{\kappa w_{\text{on lens}}^2} \cdot \frac{\delta n}{\delta T} \cdot R$$

$$R \to R' = \frac{nR}{n + aR} = \frac{nR}{n + \left(C \cdot \frac{\beta P_{\text{Laser}}}{\kappa W_{\text{an lens}}^2} n \cdot \alpha \cdot \frac{1 + \nu}{1 - \nu}\right) R}$$

The new origin of the sphere will be:

$$z'\left(0\right) - R'$$

where $z'\left(0\right)$ is the new position of the edge of the lens, which is

$$z'\left(0\right) \stackrel{\text{\tiny{(3)}}}{=} z\left(0\right) + C \cdot \frac{\beta P_{\text{Laser}}}{\kappa w_{\text{on lens}}^2} \alpha \cdot \frac{1 + \nu}{1 - \nu}$$