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STUDY OF THE LIQUID-VAPOR EQUILIBRIUM IN THE BPOMINE-HYDROBROMIC ACID-WATER SYSTEM

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14. Abstract

A glass ebullioscope was built and a method developed to study, at atmospheric pressure, liquid-vapour equilibria relative to the ${\rm Br}_2$ -HBr-10 system, in the concentration range of interest for evaluation of the MARK 13 cycle. Weasurements were preformed for the bromeazeotrope (HBr-H₂O) pseudo-binary system and for the ternary system at temperatures lower than 125°C and in the bromine concentration range up to 13% wt.

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STUDY OF LIQUID-GAS PHASE EQUILIBRIUM IN THE BROMINE-HYDROBROMIC ACID-WATER SYSTEM

1. INTRODUCTION

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The "Mark 13" chemical decomposition cycle of water that was analyzed at the Centre d'Ispra (and set up in a laboratory loop operating continuously and producing 100 l.h⁻¹ of hydrogen) [1] includes 3 steps:

(1)
$$Br_2 + SO_2 + 2 H_2O \longrightarrow H_2SO_4 + 2HBr$$

(2)
$$H_2SO_4 + H_2O + SO_2 + \frac{1}{2}O_2$$

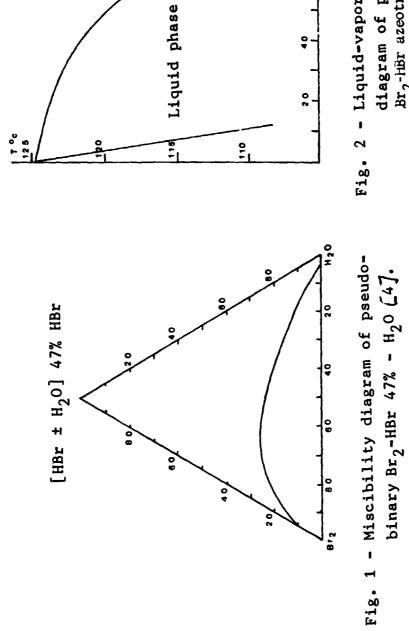
(3)
$$2HBr + Br_2 + H_2$$
 (electrolysis)

To calculate the amount of energy needed to separate the bromine produced by electrolysis from the hydrobromic acid in the presence of water through distillation, and to determine the size of the corresponding columns, it is necessary to know the concentrations at the liquid-vapor phase equilibrium of the $\rm H_2O-HBr-Br_2$ ternary system for certain ranges of interest for the process. As requested by the Ispra engineers, this equilibrium was studied at Saclay as part of a contract with the Commission of the European Communities (project $\rm H/A22$).

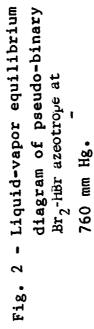
A summary of the bibliographic study concerning the $\rm H_2O-HBr-Br_2$ ternary system may be found in the reports from the preceding seminar on hydrogen organized by the CEC [2]. It is reminded that the liquid-vapor equilibrium diagram of binary system $\rm H_2O-HBr$ is known at atmospheric pressure [3]. The miscibility range of the pseudoternary bromine azeotrope ($\rm H_2O-HBr$ 47%) was defined at 20°C [4]; this is shown in Figure 1. The properties of the solutions formed by the 3 compounds were also studied in 5.

In order to determine the liquid-gas phase equilibriums of ternary system Br_2 -HBr- $\mathrm{H}_2\mathrm{O}$ we built a glass ebullioscope and designed a procedure [2]. Measurements were taken at atmospheric pressure in the concentration range of interest for the Mark 13 process.

^{*} Numbers in margin indicate foreign pagination.



Vapor phase



2. EBULLIOSCOPE AND MEASUREMENT THEORY

The ebullioscope has a dual function: first, it enables the liquid /104 and vapor phases to be put into equilibrium, with measurement of the temperature at fixed values of pressure; second, it enables the separation and taking of samples of the phases in equilibrium. The samples are then analyzed. The CATHALA ebullioscope [6] used is schematized in Figure 3. A preheated liquid and a superheated vapor flow into a mixer at a constant rate. The mixer is composed of two perforated plates and a COTTRELL nozzle equipped with VIGREUX points. The closely mixed liquid-vapor mixture wets a thermometric sheath before it completely separates into two phases which are cooled and condensed and then sent to the sampling outlets.

The instrument underwent a preliminary calibration to determine:

- The flow rates not to be exceeded in order to prevent droplets of liquid from being drawn along with the vapor;
- The amount of time the fluids remain in the space between the thermocouple sheaths and the bleed valves.

The various equilibrium points are studied by varying the supply flows, the temperatures, and the concentrations of the entering liquids.

Proper operation of the ebullioscope greatly depends upon the supply conditions.

The primary problems encountered were due to the highly active nature of the fluids studied. Only viton and teflon should be used for the flexible connections of the instrument. Beyond 100°C teflon does not withstand prolonged contact with the liquid phases.

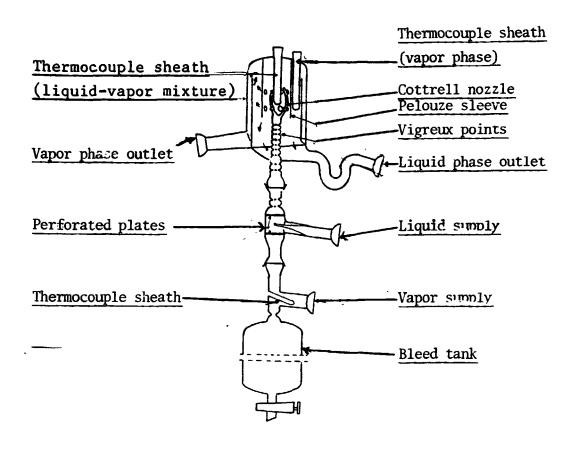


Fig. 3 - CATHALA ebullioscope

N _{HBr}	N _{Br2}	Density	ABr % mass	Br ₂ % mass
HBr/1	eq. Br/1			_
8,04	3,53	1,653	39,30	17,06
6,04	12,93	2,104	23,40	49,47
8,44	1,91	1,584	43,12	9,62
7,22	7,71	1,865	31,56	33,28
4,81	3,66	1,487	26,24	19,72
7,95	4,02	1,682	38,33	19,14
5,70	5,33	1,634	28,30	26,14
5,50	7,95	1,776	25,14	35,89
	8,04 6,04 8,44 7,22 4,81 7,95 5,70	8,04 3,53 6,04 12,93 8,44 1,91 7,22 7,71 4,81 3,66 7,95 4,02 5,70 5,33	R. HBr/1 eq. Br/1 8,04 3,53 1,653 6,04 12,93 2,104 8,44 1,91 1,584 7,22 7,71 1,865 4,81 3,66 1,487 7,95 4,02 1,682 5,70 5,33 1,634	8,04 3,53 1,653 39,30 6,04 12,93 2,104 23,40 8,44 1,91 1,584 43,12 7,22 7,71 1,865 31,56 4,81 3,66 1,487 26,24 7,95 4,02 1,682 38,33 5,70 5,33 1,634 28,30

3. DENSITIES OF SOLUTIONS

Proportioning of the liquid and vapor phases in equilibrium leads to determination of the number of moles of hydrobromic acid and bromine per liter of solution. These molarities are linked to mass percentages W by the densities of the corresponding solutions according to the following formulas:

$$W_{HBr} = \frac{8.092 \text{ M}_{HBr}}{d}$$
 $W_{Br_2} = \frac{15.9808 \text{ M}_{Br_2}}{d}$

where M represents the molar concentrations of HBr and Br_2 in the solution of density d.

We had first used density values evaluated according to documentation based on the empirical law: $d = A(N_{HBr} + N_{Br_2}) + B$, where A and B are constants and N_{HBr} and N_{Br_2} are normalities of the solution; density is expressed linearly depending on the total number of bromine equivalents contained in a liter of solution, with the bromine equivalents originating from the HBr or Br₂ having the same "weight".

For cross-checking purposes, and in order to more closely evaluate the mass percentages, we performed some experimental determinations of the density of the HBr - Br_2 - H_2O solutions. In order to do this we worked at ambient temperature using pycnometers whose volumes were determined at the temperature considered in relation to water at $4^{\circ}C$.

The results, according to the temperature and normality of the solutions, are given in Table I. Within the limits of experimental accuracy, our results agree with those of the existing documentation.

In addition, we calculated, through the method of the least squares, the equations that are likely to correlate with greater accuracy than the linear law, the densities given at 20°C by the documentation and the normalities of the bromine and hydrobromic acid solutions.

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TABLE II

Experimental results for pseudo-binary mixture $\rm Br_2$ - azeotrope HBr, $\rm H_2^{0}$

	Br ₂ % mass		20'18	77' 57	16,72	*0,*6	CO 07	43,27	47,24	16,79	25,44	50,03	66,39	67,91	69,90	73,0	72,76	73,57
	HBr % mass	27 23	5 96	36,00					99,49	56,85	26'61	36,98	14,45	14,08	13,18	11,84	11,62	11,02
or phase	Moles Br ₂ /1	1.6954	1 7368	1 7803	18881	1.9265	2.0840	01001	9190'7	2,0012	9//1/2	7,2376	2,4074	2,4489	2,5006	2,5889	2,5668	2,5794
Vapor	Moles Br ₂ /1	2.2105		3.042	3.06	4.66	2, R.S.	900		16110	667	671'6	10,03	10,41	10,94	11,83	11,687	11,875
	Moles HBr/1	7.80	7.74	7.64	7.1	6.90	7.7	77. 9	200	2, 2		67'6	£ / 4	4,26	4,07	3,79	3,68	3,51
	Br ₂ % mass	, 0,964	1.16		1,83	2,17	2,83	70° E	81.6	A. A.	700	6110	6,63	6,87	7,65	. 87	8,91	9,56
	HBr % mass	46,98	46.62	46,31	46,61	46,13	45,94	46.05	45.97	45.28	44.49		91'55	44,47	44,22	42,95	43,01	43,11
Liquid phase	Density	1,4986	1,4962	1,4957	1,5070	1,5050	1,5131	1,5181	1,5192	1,5332	1,5280	1.5482	1 5516	1,00,1	100011	1,00,1	1,1630	1,3040
Liqu	Moles Br ₂ /1	0,0904	0,1083	0,1337	0,173	0,204	0,269	0,288	0,3029	0,449	0,491	0.642	62			20,0	0,000	0,240
	Moles HBr/1	0.70	8,62	8,56	89'8	8,58	8,59	8,64	8,63	8,58	8.40	8.45	8		2, 6	76.0	, «	7 .
	T°C	123,6	123,4	123,1	122,3	121,8	121,3	120,5	120,1	118,6	118,0	116.0	115.6	2 4 1	113.4	112 0	112.5	

TABLE III

Experimental results for ternary system ${\rm Br}_2$ - ${\rm HBr}$ - ${\rm H}_2{\rm O}$ range of low concentrations of bromine

	Liq	quid phase	ase					Vapo	Vapor phase	
T°C	Moles HBr/·]	Moles Br ₂ / l	Density	HBr & mass.	HEr & mass, Br ₂ & mass, Moles	Moles HBr/l	Moles Br ₂ /1	Density	HBr & mass.	Br 2 & mass.
124,7	8,70	0,0105	1,4894	47,27	0,112	8,55	0,195	1,5023	46,05	2,07
124,6	8,63	0,0120	1,4856	47,01	0,129	7,79	0,2326	1,4642	43,05	2,54
124,0	_	0,0217	1,4527	45,36	0,237	5,59	0,5145	1,374	32,92	8,98
124,0		0,0580	1,4937	47,02	0,620	7,78	1,423	1,6011	39,32	14,20
123,1		0,0397	1,4419	43,72	0,4399	3,90	1,306	1,3718	23,00	15,21
122,7		0,0224	1,4360	43,50	0,2493	2,72	0,5465	1,2117	18,07	7,17
122,3		0,0190	1,4401	43,83	0,2108	2,98	0,4945	1,2262	19,66	6.44
121,8	7,50	0,0297	1,4246	42,60	0,3332	0,53	0,5875	1,1001	3,89	6,531
119,9		0,0344	1 4022	40,91	0,3905	1,3	0,703	1,1568	60'6	9.71
118,1		0,0344	1,3798	39,19	86 £ '0	0,79	0,6795	1,1257	89,8	6,65
117,4	6,70	0,0337	1,3803	39,28	0,390	0,68	0,711	1,1232	06.4	10,11
112,0*	5,44	0,0239	1,3088	33,63	0,292	0,110	0,110 0,161	1,0271	0,86	2,50
107,4 m	4,22	0,0307	1,2415	27,51	0,395	0,025	0,025 0,099	1,0151	0,199	1,56

* Presence of another liquid phase with a high concentration of bromine when the vapor phase undergoes condensation.

TABLE IV

Experimental results for ternary system ${\rm Br}_2$ - ${\rm HBr}$ - ${\rm H}_2{\rm O}$ Bromine concentration range greater than 1%

Liquid phase	hase		-			Vapor p	por p	'n	se		Point	, C
Moles Moles Density HBr & Br $^{\circ}$ Moles Moles HBr/1 Br $_2/1$ mass. mass. HBr/1 Br $_2/1$	Density HBr & Br ₂ Moles mass. mass. HBr/1	HBr & Br & Moles mass. mass. HBr/1	Br ₂ e Moles maßs. HBr/1	Moles HBr/1		Mole Br ₂ /	7.8	Density	HBr.	Br.2. mass.	1	2
0,133 1,4795 45,23 1,44	1,4795 45,23 1,44 4,93	45,23 1,44 4,93	1,44 4,93	4,93		2,9	1	1,6227	24,58	29,29		
0,180 1,4810 44,80	1,4810 44,80 1,94 3,99	44,80 1,94 3,99	1,94 3,99	3,99		3,6		1,6468	19,60	35,22		
1,4 -7 43,61 2,10	1,4 7 43,61 2,10 2,98	43,61 2,10 2,98	2,10 2,98	2,98		3,6	2	1,6133	14,95	37,84	m	
0,625 1,5309 43,21 6,52 3,89	1,5309 43,21 6,52 3,89	43,21 6,52 3,89	6,52 3,89	3,89		6	9,75	2,3526	13,38	66,21	3	
3,10 1,50	1,4794 43,48 3,10 1,50	43,48 3,10 1,50	3,10 1,50	1,50	_	S	5,14	1,6863	7, 20	948,76	s	
0,237 1,4535 42,25 2,60 2,12	1,4535 42,25 2,60 2,12	42,25 2,60 2,12	2,60 2,12	2,12		•	90'1	1,5938	10,76	40,71	9	
0,419 1,4874 42,54	1,4874 42,54 4,50	42,54 4,50	4,50		2,27		7,06	1,9526	9,43	57,82	٠	
0,402 1,4826 42,41 4,33	1,4826 42,41 4,33	42,41 4,33	4,33		2,62		6,45	1,9000	11,18	54,25	•	
0,584 1,4336 40,18 3,25	1,4336 40,18 3,25	40,18 3,25	3,25		1,07		5,16	1,6645	5,20	49,54	σ.	
0,414 1,4712 41,47 4,49	1,4712 41,47 4,49	41,47 4,49	4,49		9,0		6,81	1,8315	2,65	59,42	10	
0,631 1,5196 42,38 6,63	1,5196 42,38 6,63	42,38 6,63	6,63		2,84		7,71	2,0596	11,17	59,85	11	
0,305 1,4307 39,81 3,41	1,4307 39,81 3,41	39,81 3,41	3,41		0,77		5,67	1,7078	3,65	53,06	12	
0,674 1,4294 39,34 3,77	1,4294 39,34 3,77	39,34 3,77	3,77		0,82		99'5	1,7092	3,88	52,92	13	
0,335 1,4213 38,8i	1,4213 38,81 3,76	38,81 3,76	3,76		0,52		5,82	1,7114	2,46	54,34	1	
1,4529 37,65	1,4529 37,65 6,95	37,65 6,95	6,95		1,64		7,67	1,9894	69'9	61,65	1.5	
0,826 1,5210 40,33 8,68	1,5210 40,33 8,68	40,33 8,68	8,68		1,47		98'6	2,2349	5,32	70,50	16	
6,54 0,398 1,4129 37,45 4,44 0,39	1,4129 37,45 4,44	37,45 4,44	4,44	_	0,39		5,94	1,7191	1,84	55,26	17	
			_									

TABLE IV (Cont'd)

Experimental results for ternary system ${\rm Br}_2{\rm ^{-}HBr^{-}H}_2^0$ Bromine concentration range greater than 1%.

	Liqui	Liquid phas	e					Vapor	phase		Foint N	No.
T°C	Moles HBr/l	Moles Br ₂ /1	Densité	HBr & mass.	Br28 māss.	Moles HBr/l	Moles Br ₂ /1	Densité	HBr & mass.	Br ₂ e mass.		
111,2	6,55	085'0	1,4357	36,92	6,51	0,41	7,94	1,9541	1,72	64,97	1.9	
108,7	5,48	0,400	1,3552	32,72	4,77	0,08	6,50	1,7728	0,04	59,04	19	
108,7	7,03	1,280	1,5431	36,86	13,27	0,61	12,03	2,4427	2,02	78,74	2.0	
107,1	2,60	0,517	1,3749	32,96	6,01	80'0	7,16	1,8431	0,37	61,99	2 1	
105,3	4.79	0,335	1,3049	29,70	3,72	0,032	5,38	1,6338	0,16	52,67	2 2	
104,2	3,14	0,182	1,1987	21,19	2,43	0,15	3,82	1,4573	0,83	41,89	2 3	
104,0	3,95	0,258	1,2528	25,51	3,29	0,02	6,01	1,7064	60'0	56,29	24	
104,0		0,571	1,3460	29,88	6,78	0,05	7,36	1,8662	0,20	63,07	2.5	
103,8		0,749	1,3934	31,65	8,59	0,04	8,9	2,0516	0,18	69,72	26	
107,0	3,01	0,161		20,48	2,16	9,01	3,59	1,4160	0,03	39,89	2.7	
100,7	2,50	0,151	1,1595	1.7,44	5,09	0,004	3,64	1,4282	0,02	40,73	28	
100,2	3,76	0,496		23,96	6,24	0,04	7,11	1,8370	0,20	61,89	2.9	
1,66	2,36	0,256	1,1638	16,40	3,51	0,03	4,91	1,5789	0,17	49,74	30	
8,76	3,48	0,664	1,2738	22,11	8,33	90.0	8,20	1,9648	0,25	69'99	3.1	
					_	_						

It appears that the best correlation is of the following type:

$$d = A.N_{HBr} + B.N_{Br_2} + C.N_{HBr}.N_{Br_2} + D$$
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In this formula the bromine equivalents no longer have the same influence, depending on whether they come from hydrobromic acid or bromine; nevertheless their respective weights are very similar, with constants A and B being very close. For information purposes the values of the constants are as follows:

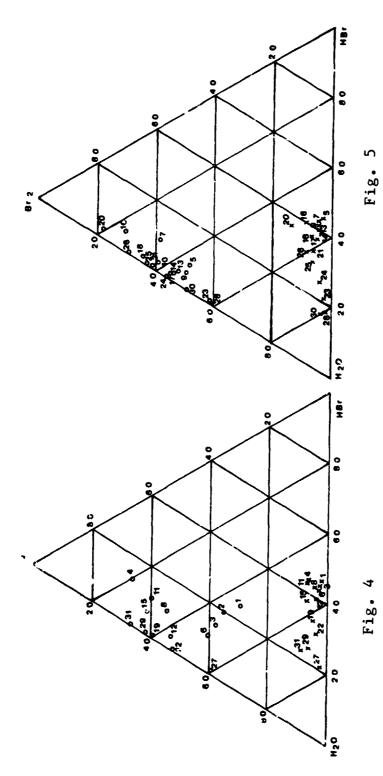
$$A = 5.5859 10^{-2}$$
 $B = 5.8489 10^{-2}$
 $C = -9.7082 10^{-5}$
 $D = 1.0052$

4. EXPERIMENTAL RESULTS

The results of the ebullioscope measurements for the pseudo-binary mixture of Br_2 -azeotrope (HBr-H $_2$ O) are grouped together in Table II and represented in Figure 2. The experimental results of the phase equilibrium study for ternary system Br_2 -HBr-H $_2$ O are shown in Table III for small concentrations of bromine and in Table IV for larger concentrations.

The experimental points of Table IV were located in a ry diagram: in Figures 4 and 5 the points bearing the same numbers (defining the experiment - refer to Table IV) correspond to the phases in equilibrium; the points represented by circles give the composition of the vapor phase, whereas those represented by a cross give the cimental points makes any representation on a ternary diagram.

The compositions of the liquid and vapor phases in equilibrium are shown for different temperature values T (°C) (first column). The results given in the other columns are described as follows:



Ternary diagram of $\mathrm{H_20\textsc{-}Br_2\textsc{-}HBr}$ for the range of bromine concentrations greater than 1% in the liquis phase.

 $^{\circ}$ - Compositions of vapor phases in mass %

x - Compositions of liquid phases in mass $\ensuremath{\chi}$

An identical reference number corresponds to a phase equilibrium (refer to Table IV).

- "Moles HBr/l" represents the molarity of HBr in the liquid or vapor phase at ambient temperature. This molarity is obtained by metric acid-base pH proportioning. $^{/113}$
- "Moles $\mathrm{Br}_2/1$ " represents the molari+" of Br_2 in the liquid or vapor phase at ambient temperature. This molarity is obtained by potentiometric oxydation-reduction proportioning of iodine by sodium hyposulfite according to the following reaction:

$$2 S_{2}O_{3}^{2-} + I_{2} \longrightarrow S_{4}O_{6}^{2-} + 2 I^{-}$$

The bromine, which is a stronger oxydizer than iodine, oxydizes the thiosulfate into sulfate under variable conditions. This is why the proportion of bromine is controlled by adding excess KI before titrating the released iodine with thiosulfate

$$Br_2 + 2 I^- \longrightarrow I_2 + 2Br^-$$

In a very acid environment, since the iodine can be oxidized by the oxygen in the air, proportioning is performed in an argon atmosphere and in a solution adjusted to a pH number of 5 (acetate solution).

"Density" represents the mass per unit volume in g/cm³ of the liquid or vapor phases at ambient temperature.

"HBr mass %" represents the mass of HBr contained in 100 grams of solution, either in the liquid or vapor phase, at ambient temperature.

This value is calculated using the molar mass of HBr, the molarity determined experimentally, and the density ϵ aluated according to the documentation.

"Br $_2$ % mass" likewise represents the weight titre of the solution in Br_2 .

The concentrations of HBr and Br_2 given for the vapor phase represent

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an average concentration of two liquid phases generally obtained after condensation of the vapor. The maximum concentration obtained for the liquid phase does not exceed 13.3 % bromine

5. DISCUSSION

In the course of this work about sixty different liquid-vapor phase equilibrium points for the HBr-Br₂-H₂O system were determined for the corresponding temperatures. However, only a limited area of the ternary diagram was explored.

If one wished to extend the study of this diagram, two major difficulties would be encountered: the existence of a vast zone of partial mixing in the liquid phase and the extremely corrosive nature of the products.

Since the gaseous phase in equilibrium with the liquid phase is very rich in bromine, in order to extend the realm of study it would be necessary to modify the Cathala ebullioscope to enable injection of a liquid phase having a similar composition to that desired, as well as two gaseous phases in suitable proportions - one rich in Br_2 and therefore very poor in HBr and $\mathrm{H}_2\mathrm{O}$, the other very poor in Br_2 and with an HBr concentration such that, when the two gaseous phases are mixed, a gas of similar composition to that of the gaseous phase in equilibrium with the added liquid phase is obtained. In this case the Cathala ebullioscope would be equipped with a preheated-liquid input and two quartz atomizers with different heating capacities. The input lines should be welded to avoid having couplings in The other products should be supplied without pulsations by a nonvermicular proportioning pump; flexible lines are quickly deteriorated by concentrated bromine solutions (in some of the experiments the hoses were damaged in less than 6 hours).

6. CONCLUSION

As part of the studies concerning the cyclical Mark 13 process of hydrogen production, the isobaric diagram of liquid-vapor equilibrium for the Br₂-HBr-H₂O system was analyzed at atmospheric pressure and at temperatures greater than 300 K. The concentration range studied, which is of interest for the process, is limited by a large range of partial mixing of the system at ambient temperature and by the aggressive nature of the mixtures. Another ebullioscope would have to be designed to complete analysis of the system.

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After careful examination of the results, observations concerning the separation of bromine, hydrobromic acid, and water after electrolysis, may be made (step 3 of the cycle - refer to §1). As the gaseous phase in equilibrium is very rich in bromine when compared to the liquid phase, separation should be easy and energy consumption moderate provided it is acceptable that the hyrobromic acid recycled into electrolysis still contain a little bromine at a concentration of a few thousandths. However, elimination of this small amount of bromine appears to be difficult, especially as the composition of the mixture becomes similar to that of the azeotrope HBr-H₂O.

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