

# Chapter 4 - Integral Form for a Control Volume

## Lecture 9 Section 4.2

### Introduction to Fluid Mechanics

Mechanical Engineering and Materials Science  
University of Pittsburgh



# Student Learning Objectives

Chapter 4 - Integral  
Form for a Control  
Volume

MEMS 0071

Learning Objectives

4.2 Reynolds  
Transport Theorem

Students should be able to:

- ▶ Understand the Material Derivative
- ▶ Use the conservation equations and understand their formulation through the Reynolds Transport Theorem using a Control Volume formulation



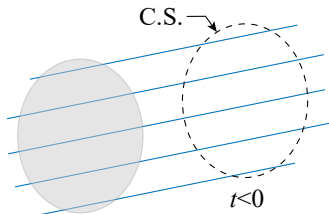
# What is RTT?

- ▶ The relationship between the time rate of change of an extensive property for a system, and for a control volume, which contains our system of interest, is known as the **Reynolds Transport Theorem (RTT)**
- ▶ Osborne Reynolds (1842-1912) - by the end of this course, his name will be ingrained in your memory



# Definition of C.S.

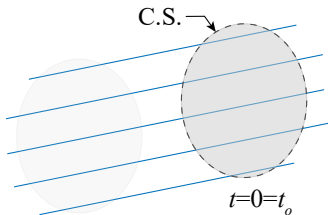
- Consider a Control Surface, C.S., that defines our Control Volume, C.V.



- Before a time  $t_o$ , a quantity of our system is approaching the C.S., following a streamline, a concept we will later introduce

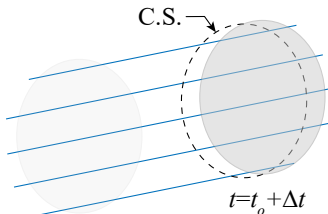


- At time  $t_o$ , the system is completely within the C.S., establishing a C.V.



# Change of System of Interest

- ▶ After some small time interval,  $\Delta t$ , the system moves in the direction of flow and moves out of the C.V.

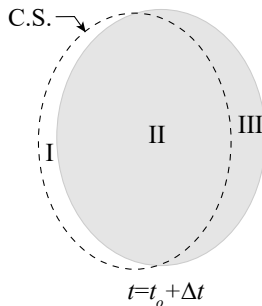


- ▶ We have three quantities: that of which the C.V. is not occupied by the system, that which the system is still in the C.V., and that which the system left the C.V.



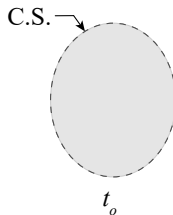
# Definition of Regions

- ▶ Regions I and II are within the C.V. for some  $t$ , however, at time  $t_o + \Delta t$ , the part of the system within the C.V. is only within region II
- ▶ Region III is the part of the system that is outside the C.V. at time  $t_o + \Delta t$



- ▶ If we represent our extensive property as  $B$  (say, banana), we can express  $B$  of the system at times  $t_o$  and  $t_o + \Delta t$
- ▶ At time  $t_o$ , the extensive property of the system is the same as that of the control volume

$$B_{sys}|_{t_o} = B_{C.V.}|_{t_o}$$





# Change of $B$ with $\delta t$

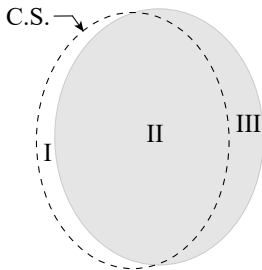
- ▶ At time  $t_o + \Delta t$ , the extensive property of the system is that of regions II and III

$$B_{sys}|_{t_o + \Delta t} = B_{II}|_{t_o + \Delta t} + B_{III}|_{t_o + \Delta t}$$

- ▶ Region II is the C.V. less region I

$$B_{II}|_{t_o + \Delta t} = B_{C.V.}|_{t_o + \Delta t} - B_I|_{t_o + \Delta t}$$

$$\Rightarrow B_{sys}|_{t_o + \Delta t} = (B_{C.V.} - B_I + B_{III})|_{t_o + \Delta t}$$



$t = t_o + \Delta t$

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- ▶ Recalling the definition of a derivative

$$\left. \frac{dB}{dt} \right|_{sys} = \lim_{\Delta t \rightarrow 0} \frac{B_{sys}|_{t_o+\Delta t} - B_{sys}|_{t_o}}{\Delta t}$$

- ▶ Substituting in our expressions for  $B_{sys}|_{t_o}$  and  $B_{sys}|_{t_o+\Delta t}$  (red boxes)

$$\left. \frac{dB}{dt} \right|_{sys} = \lim_{\Delta t \rightarrow 0} \frac{(B_{C.V.} - B_I + B_{III})|_{t_o+\Delta t} - B_{C.V.}|_{t_o}}{\Delta t}$$



- ▶ The limit of a sum is equal to the sum of the limit such that

$$\begin{aligned} \left. \frac{dB}{dt} \right|_{sys} &= \overbrace{\lim_{\Delta t \rightarrow 0} \frac{B_{C.V.}|_{t_o+\Delta t} - B_{C.V.}|_{t_o}}{\Delta t}}^{\text{term 1}} \\ &+ \underbrace{\lim_{\Delta t \rightarrow 0} \frac{B_{III}|_{t_o+\Delta t}}{\Delta t}}_{\text{term 2}} - \underbrace{\lim_{\Delta t \rightarrow 0} \frac{B_I|_{t_o+\Delta t}}{\Delta t}}_{\text{term 3}} \end{aligned}$$

- ▶ Let us look at each individual term



# ROC of $B$ to Integral Formulation

- ▶ The first term

$$\lim_{\Delta t \rightarrow 0} \frac{B_{C.V.}|_{t_o+\Delta t} - B_{C.V.}|_{t_o}}{\Delta t} = \frac{\delta B_{C.V.}}{\delta t}$$

is merely the time rate of change of the property,  
by the definition of a derivative

- ▶ It is our goal to take system rate equation and convert it into a control volume equation
- ▶ The intensive property of our system, on a per mass basis,  $b=B/M$ , can be expressed as

$$B_{sys} = \int_{M_{sys}} b \, dM = \int_{V_{sys}} b \, \rho \, dV$$



- ▶ Thus, the first term can be expressed as

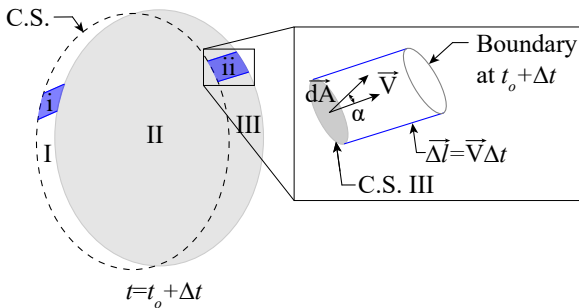
$$\frac{\delta B_{C.V.}}{\delta t} = \frac{\delta}{\delta t} \int_{C.V.} b \rho dV$$

- ▶ The time rate of change of our system property  $B$  is equal to the time rate of change of the total amount of the property within the control volume.
- ▶ If the term is positive, our system property  $B$  is increasing, and vice versa



# Outflux Through C.S.

- ▶ Term II is solved for by analyzing subregion ii:



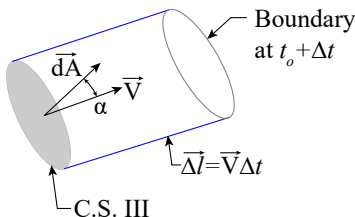
- ▶ This is the net rate of outflow from the C.V. through the control surface, C.S. III
- ▶ The flow with velocity  $\vec{V}$  is crossing the differential area  $dA$ , which has a unit normal  $\vec{n}$ , which can be represented as the area vector  $d\vec{A}$ , at some angle  $\alpha$



# Volume Outflux $d\mathcal{V}$ Through C.S.

- ▶ The amount of fluid (magnitude) crossing C.S. III, which can be represented as a volume  $d\mathcal{V}$ , is the differential length of the projection of the C.S. at time  $t_o$  to  $t_o + \Delta t$ ,  $\Delta \vec{l}$ , times (dot product) the differential area vector  $d\vec{A}$

$$d\mathcal{V} = \Delta \vec{l} \cdot d\vec{A}$$



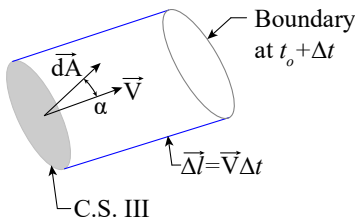
# Magnitude of $d\mathcal{V}$

- ▶ The differential length is simply the velocity of the fluid  $\vec{V}$  times the time interval  $\Delta t$

$$\Delta \vec{l} = \vec{V} \Delta t$$

- ▶ Thus, the amount of fluid crossing C.S. III is

$$d\mathcal{V} = \vec{V} \cdot d\vec{A} \Delta t$$





- ▶ Thus, reconstructing the second term

$$\begin{aligned}B_{\text{III}}|_{t_o+\Delta t} &= \int_{C.\forall.} b\rho\forall|_{t_o+\Delta t} \\ \implies dB_{\text{III}}|_{t_o+\Delta t} &= b\rho d\forall|_{t_o+\Delta t} \\ \implies dB_{\text{III}}|_{t_o+\Delta t} &= b\rho\vec{V} \cdot d\vec{A}\Delta t\end{aligned}$$

- ▶ We need to integrate over C.S. III to determine the total amount of the property leaving the C. $\forall$ .

$$\begin{aligned}\lim_{\Delta t \rightarrow 0} \frac{B_{\text{III}}|_{t_o+\Delta t} - B_{\text{III}}|_{t_o}}{\Delta t} &= \lim_{\Delta t \rightarrow 0} \frac{\int_{\text{C.S. III}} B_{\text{III}}|_{t_o+\Delta t} - B_{\text{III}}|_{t_o}}{\Delta t} = \\ \lim_{\Delta t \rightarrow 0} \frac{\int_{\text{C.S. III}} b\rho\vec{V} \cdot d\vec{A}\Delta t}{\Delta t} &= \int_{\text{C.S. III}} b\rho\vec{V} \cdot d\vec{A}\end{aligned}$$



- Therefore

$$\lim_{\Delta t \rightarrow 0} \frac{B_{\text{III}}|_{t_o+\Delta t}}{\Delta t} = \int_{\text{C.S. III}} b\rho \vec{V} \cdot d\vec{A}$$

- The same approach can be applied to a subregion of region I.
- It is noted the velocity vector is into the C.V., opposing the unit normal of  $dA$ , thus

$$\lim_{\Delta t \rightarrow 0} \frac{B_{\text{I}}|_{t_o+\Delta t}}{\Delta t} = - \int_{\text{C.S. I}} b\rho \vec{V} \cdot d\vec{A}$$



- Combining our expressions for terms 1 through 3, we have the following

$$\left. \frac{dB}{dt} \right|_{sys} = \frac{\delta}{\delta t} \int_{C.V.} b\rho dV + \int_{C.S. III} b\rho \vec{V} \cdot d\vec{A} - \int_{C.S. I} b\rho \vec{V} \cdot d\vec{A}$$

- Noting C.S. I and C.S. III constitute the entire control surface, we are left with RTT:

$$\left. \frac{dB}{dt} \right|_{sys} = \frac{\delta}{\delta t} \int_{C.V.} b\rho dV + \int_{C.S.} b\rho \vec{V} \cdot d\vec{A}$$



$$\left. \frac{dB}{dt} \right|_{sys} = \frac{\delta}{\delta t} \int_{C.V.} b \rho dV + \int_{C.S.} b \rho \vec{V} \cdot d\vec{A}$$

- ▶ The LHS is the rate of change of the extensive property of system
- ▶ The first term on the RHS is the rate of change of the extensive property of the system within the C.V.
- ▶ The second term on the RHS is the rate at which the extensive property of the system is exiting the C.V. through the C.S.



# Application to Conservation Laws

- ▶ RTT is used to derive our conservation equations
- ▶  $B=M, b=1 \implies$  Conservation of Mass (COM)
- ▶  $B=\vec{P}, b=\vec{V} \implies$  Conservation of Linear Momentum (COLM)
- ▶  $B=\vec{H}, b=\vec{r} \times \vec{V} \implies$  Conservation of Angular Momentum (COAM)
- ▶  $B=E, b=e \implies$  Conservation of Energy (COE),  
1<sup>st</sup> Law of Thermodynamics
- ▶  $B=S, b=s \implies$  2<sup>nd</sup> Law of Thermodynamics

