

Short review of activities on optical and geometrical characterization of OMSoP dish

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OMSoP demonstrative plant: INNOVA dish @ ENEA-Casaccia

- **Structure:** revamping of an old McDonnell Douglas dish
- **Mirrors:** new facets based on ALMIRR 303
- **Receiver:** original!
- **Microturbine:** original!
- **Control system:** original!

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Receiver design needs of the solar Flux profile!!!
- **Microturbine:** original!
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OMSoP demonstrative plant: INNOVA dish @ ENEA-Casaccia

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Focus position necessary for the right position of the components!!!
- **Microturbine:** original!
- **Control system:** original!

Dish OMSoP in numbers

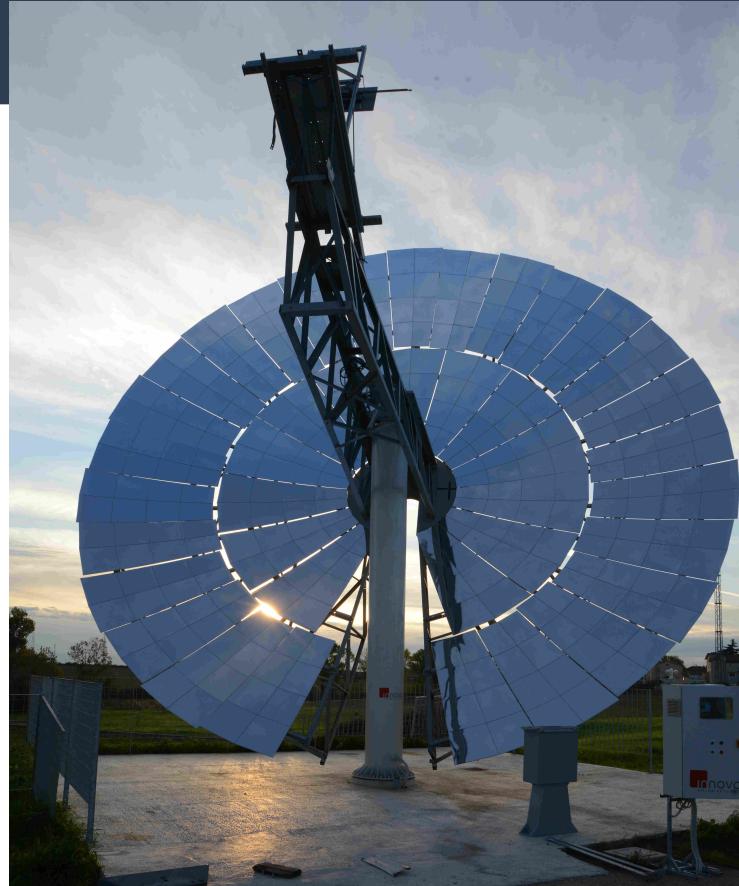
$\varnothing_{\text{outer}} \approx 12 \text{ m}$

$\varnothing_{\text{inner}} \approx 2 \text{ m}$

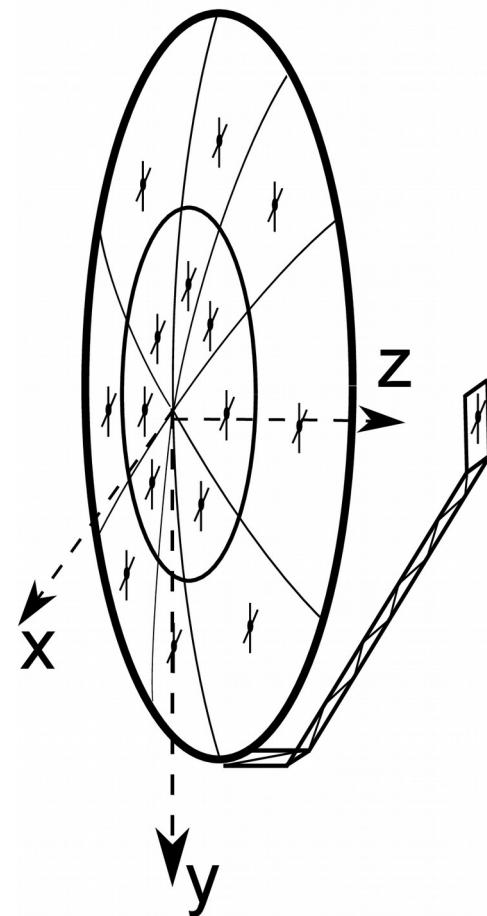
$A \approx 88 \text{ m}^2$

$P_0 = A \times \text{DNI} \approx 70.4 \text{ kW} @ 0.8 \text{ kW/m}^2$

$z = 0.25(x^2+y^2)/f \text{ con } f \approx 7 \text{ m}$



Preliminary geometrical characterization of the dish - I



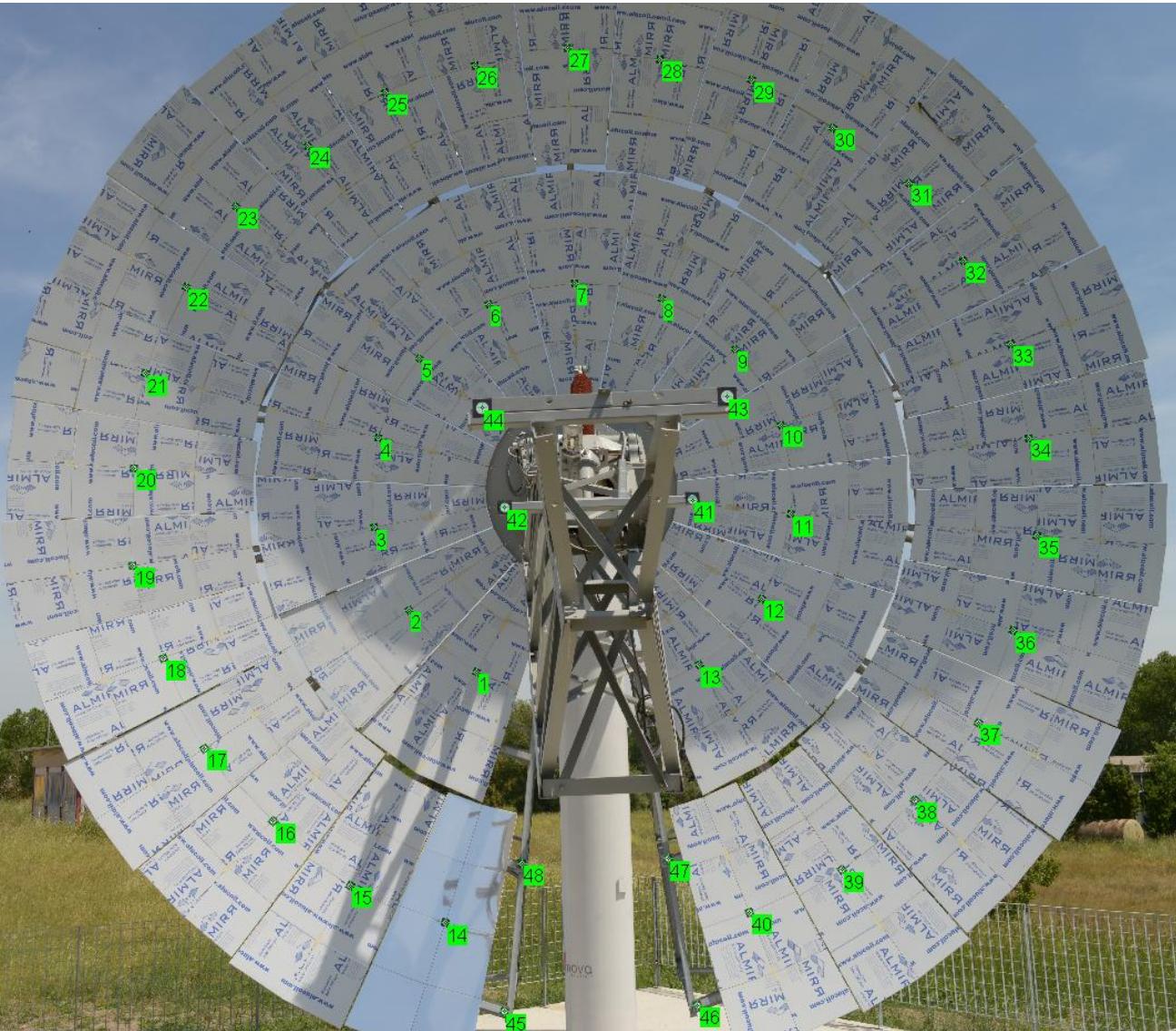
Photogrammetry

- 1 target per facet
- 4 targets on boom
- Best fit of points $\{(x_k, y_k, z_k)\}_{\text{facet}}$ with paraboloide equation

→ axis & vertex

Total Station
permanent points:
4 low facet supports
2 boom
For anytime measure

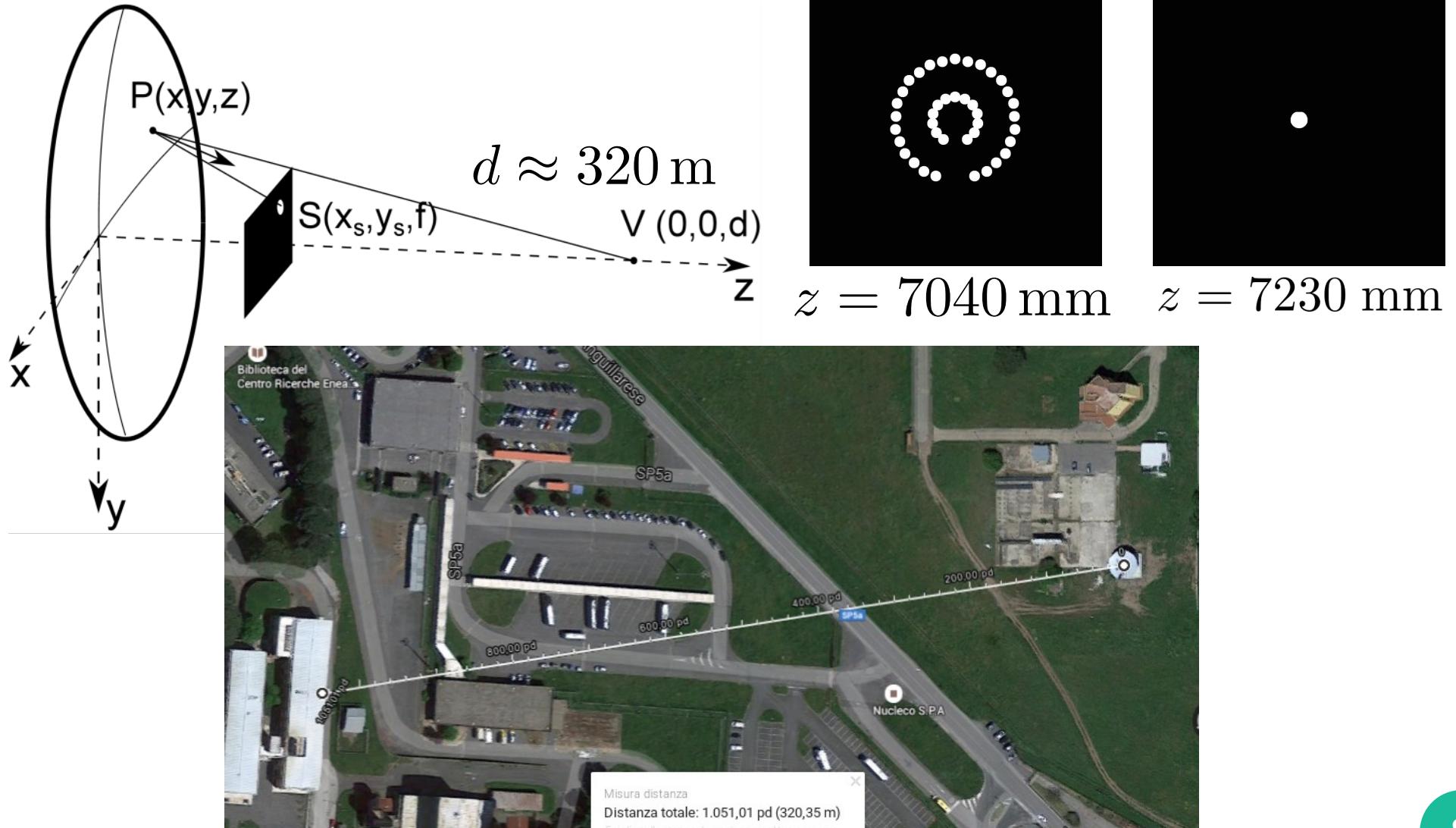
Preliminary geometrical characterization of the dish - II



→ - paraboloide axis
- vertex point
by assuming
 $f = 7040 \text{ mm}$

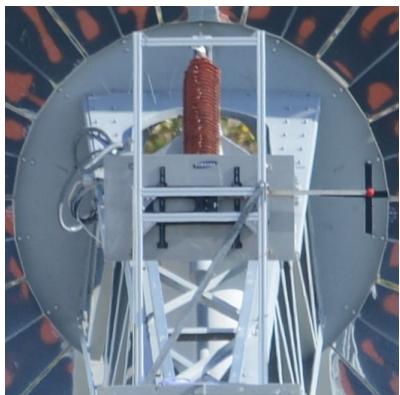
Facet canting by means the new instrument **VIStdish**

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VIStdish - facet canting

Aiming

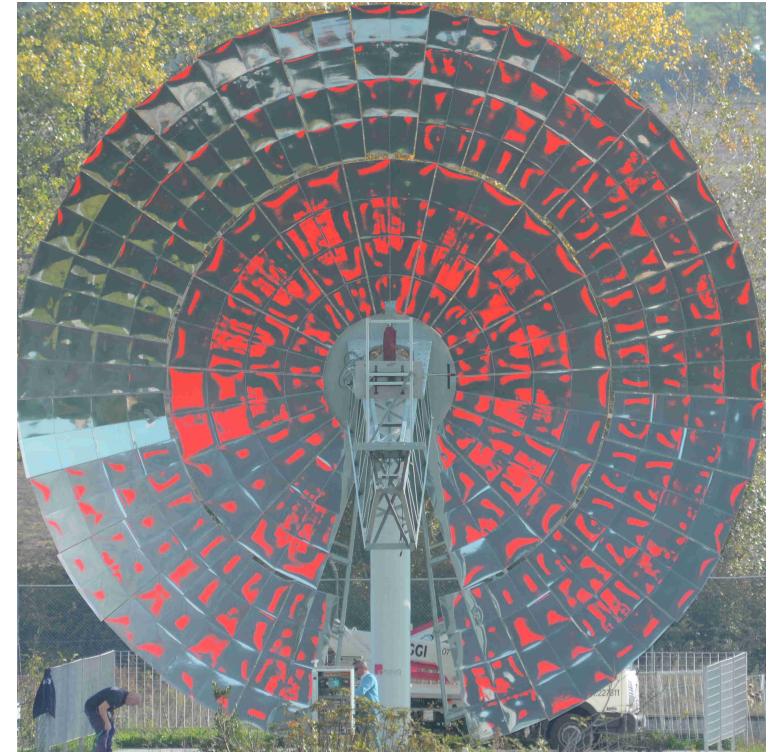


fake-monitor

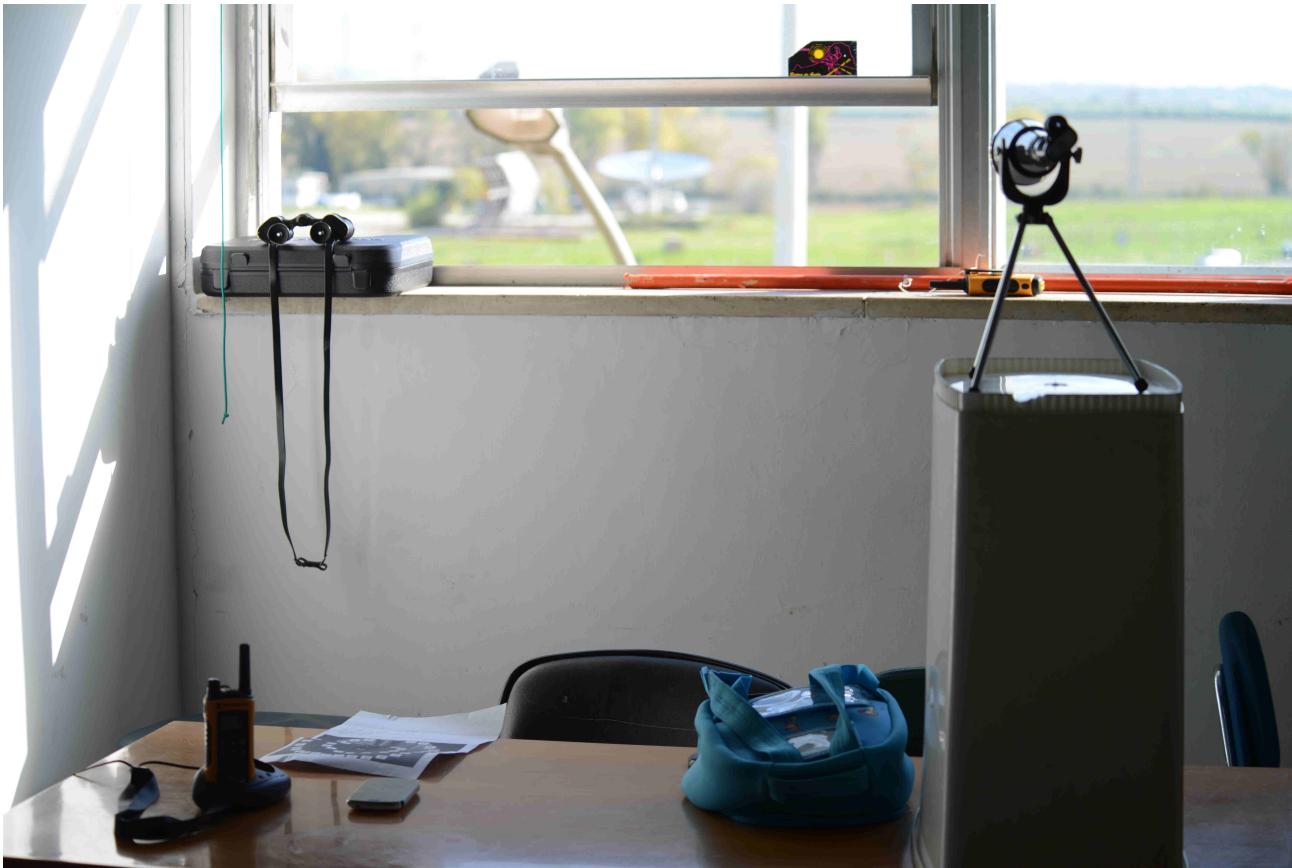


\varnothing red dot = 120 mm

Alignment at mid way



VIStdish: the observer

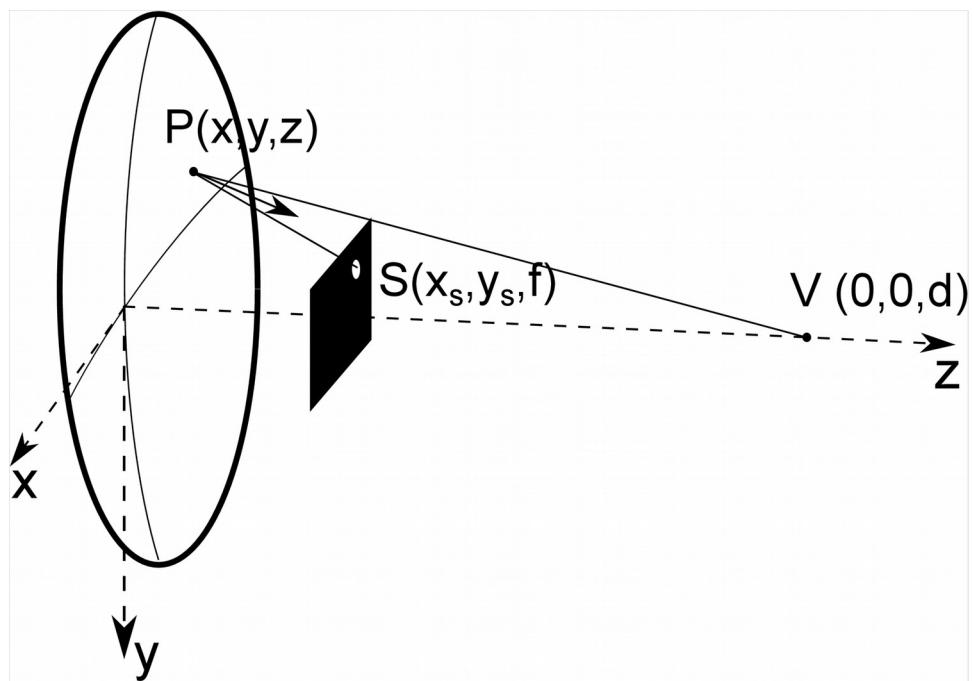


Components of VIStdish-canting:

- 1) Fake monitor**
- 2) Telescope**
- 3) Binocular**
- 4) Walkie-Talkie**

Simple & Cheap !!!

VIStdish: shape-measurement

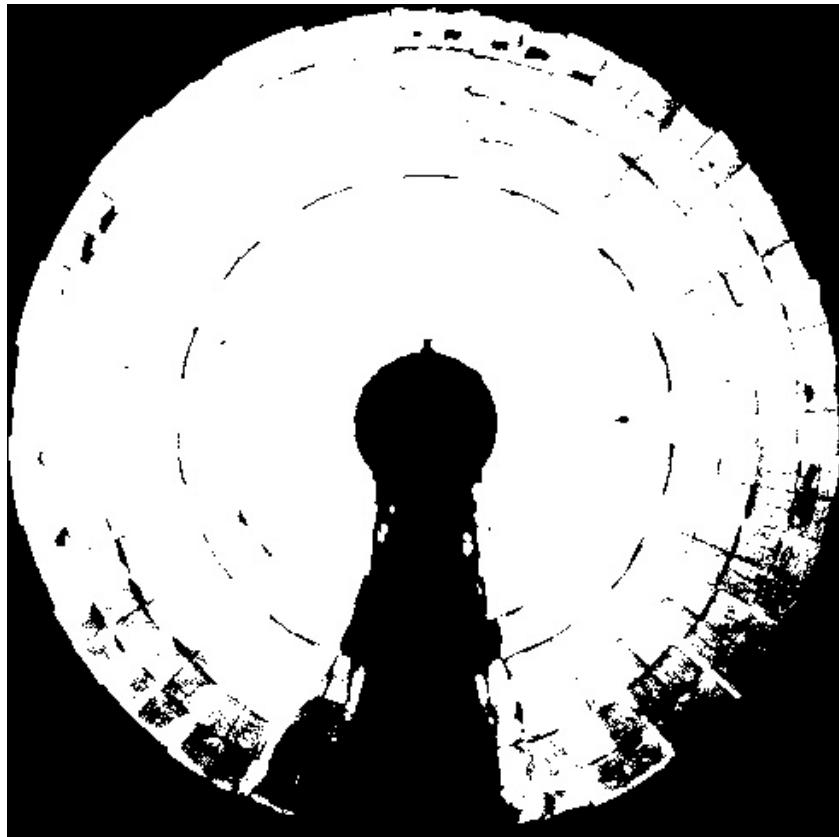


- **S is moved at step.**
- **For each position, one image is acquired by V**
- **Point, N^2 step**
- **Linee horizontal and vertical, $2N$ step !!!!**
- **Determination of the unit vector normal to the mirrored surface by image processing**

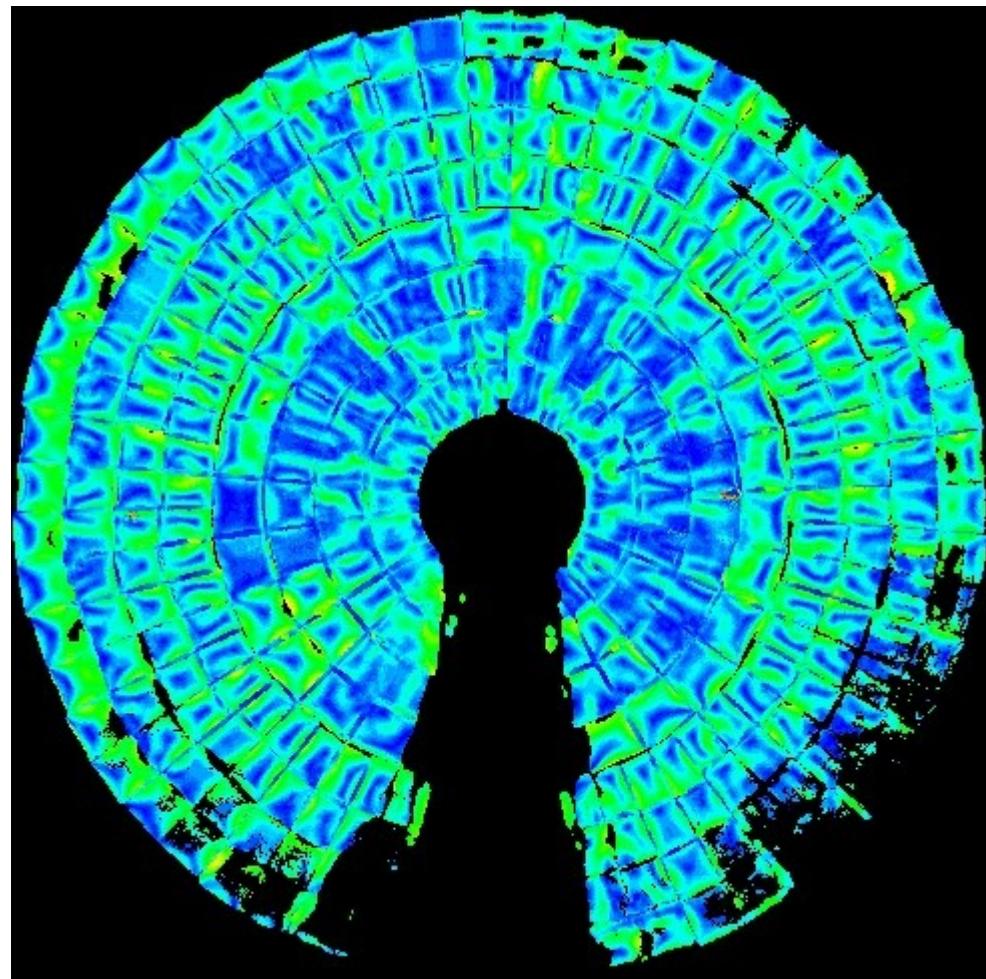
Results dish shape

Sample surface: 83.25 m² of 88 m²

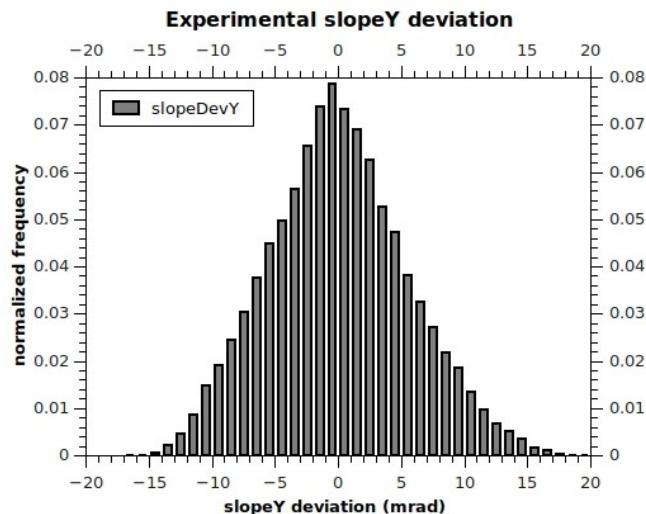
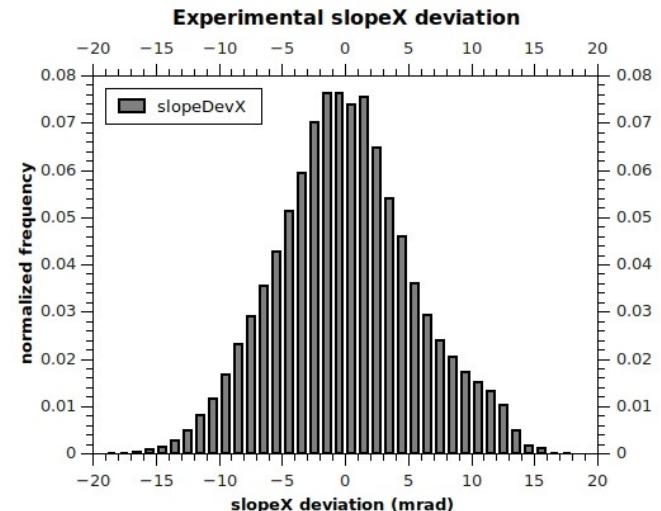
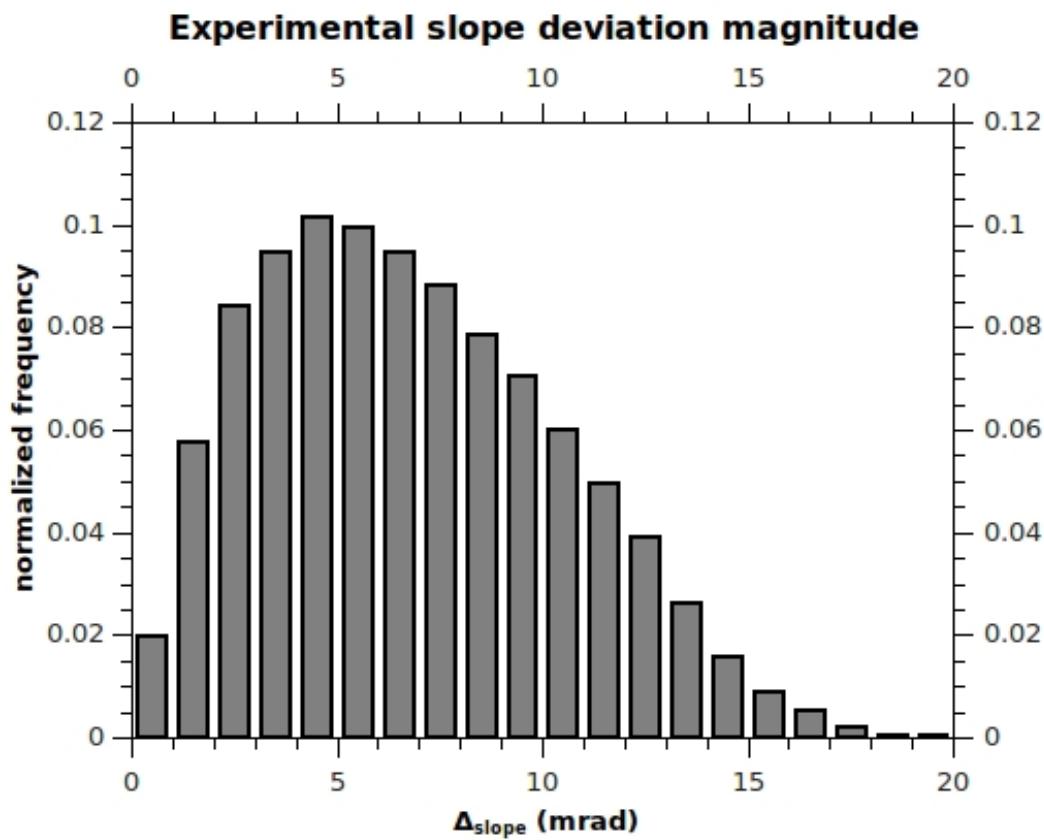
- The used TV LCD was too much small
- Frost on the mirrors



Slope deviation contour map

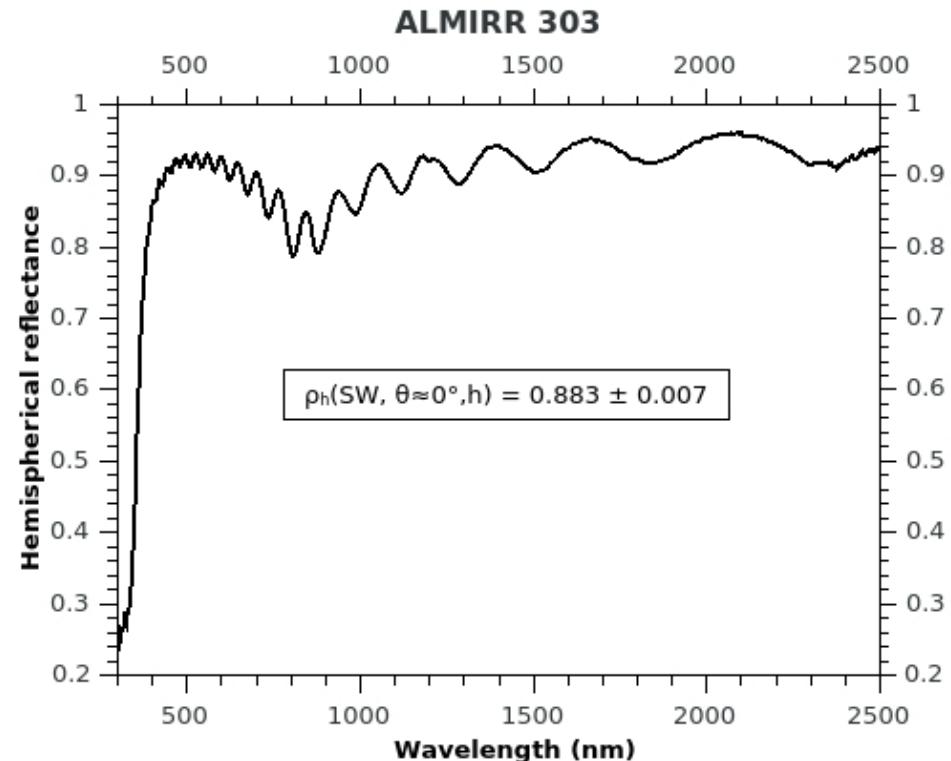
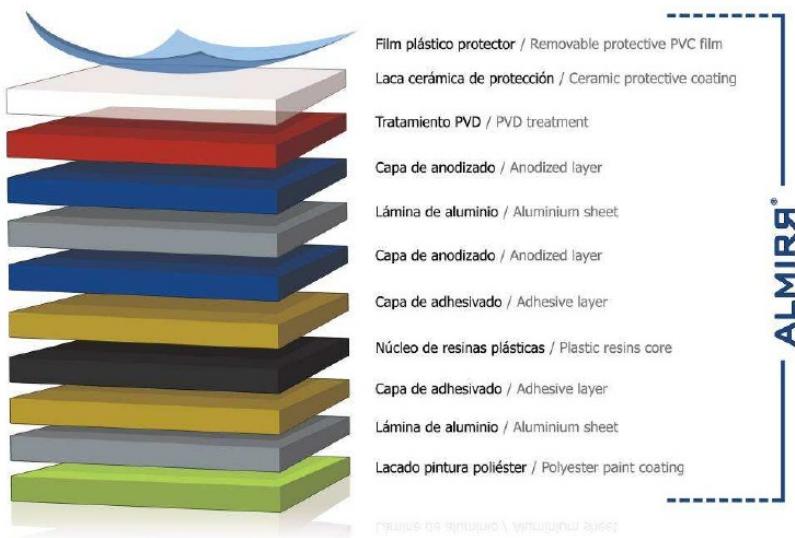


Slope deviation dish OMSoP



ALMIRR 303 solar mirror

Multilaminar Aluminium Mirrors, Almirr®, consist of two aluminium sheets and a plastic resin core.

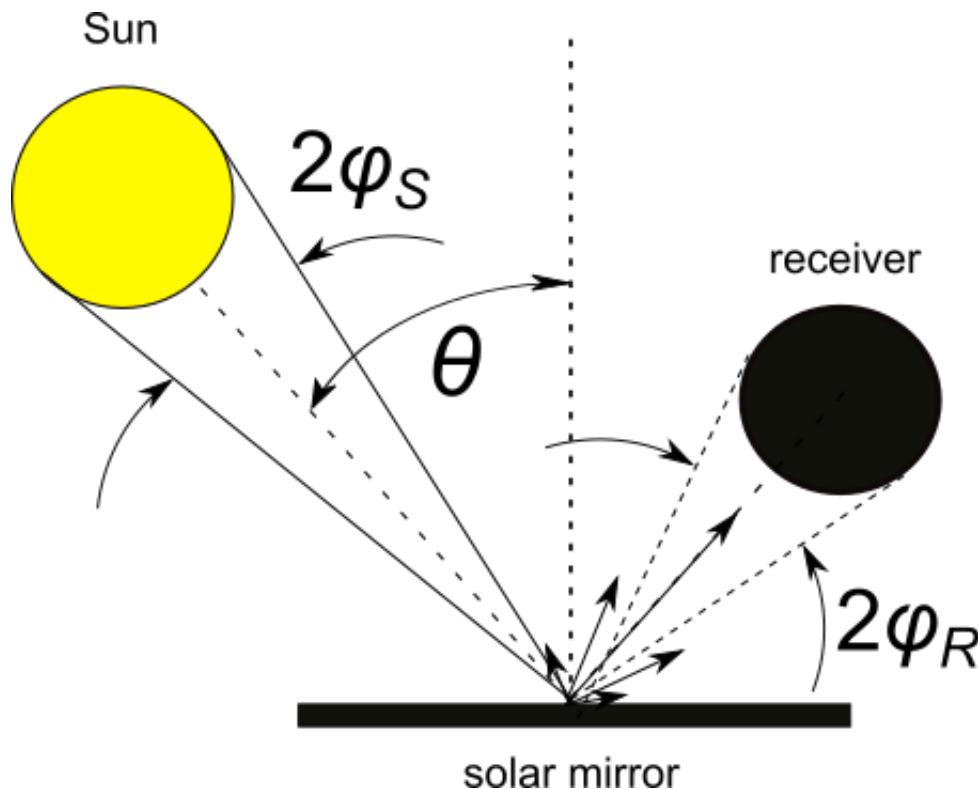


Perkin Elmer L950, integrating sphere 15 cm,
first surface Al reference mirror

$$\rho_h(SW, \theta \approx 0^\circ, h) = 0.883 \pm 0.007$$

$$A = 0.117$$

MIRRORS IN CSP and SCR(θ, φ)



Sun is not a point source infinitely far.

Solar radiation does not travel as plane wave: $2\varphi_S = 9.46$ mrad in a clear-sky day.

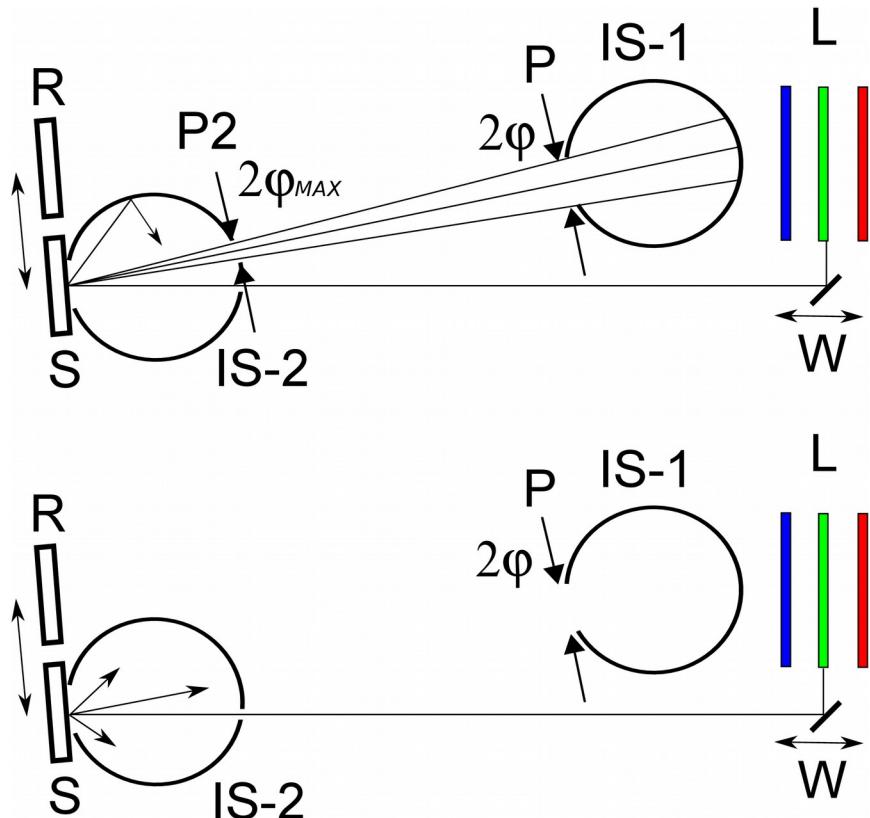
Then *reflectance* concept does not properly fit the typical CSP conditions!!!

This is the first reason for introducing the new parameter:
Sun-radiation Conic Reflectance (SCR)

i.e. rate of solar energy reflected by the mirror and intercepted by the receiver viewed under $2\varphi_R$ from the reflection point.

SMQ set-up (ENEA)

Designed to measure the near-specular reflectance (no deconvolution)!



Main features:

- low divergent laser beams (< 1 mrad)
- no lenses
- small beam size (< 1 mm)
- \Rightarrow spatial selection of φ (3-20 mrad)
- data processing based on TIS and EMA returning the solar near-specular reflectance

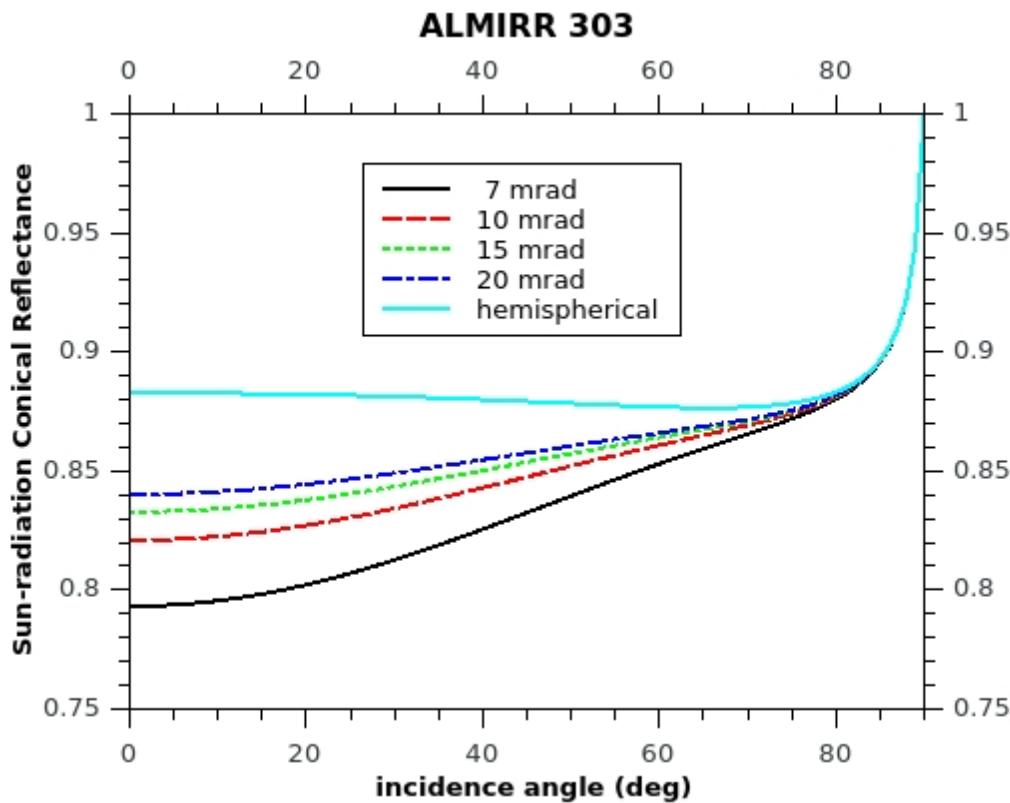
$$\rho_s(SW, \theta, \varphi)$$

given

$$\rho_h(\lambda, 0^\circ, h)$$

The continuous spectral measurement can not be achieved by SMQ because the beam must have *low divergence* (< 1 mrad) and *small spot* (< 1 mm) \Rightarrow **laser beam!!!**

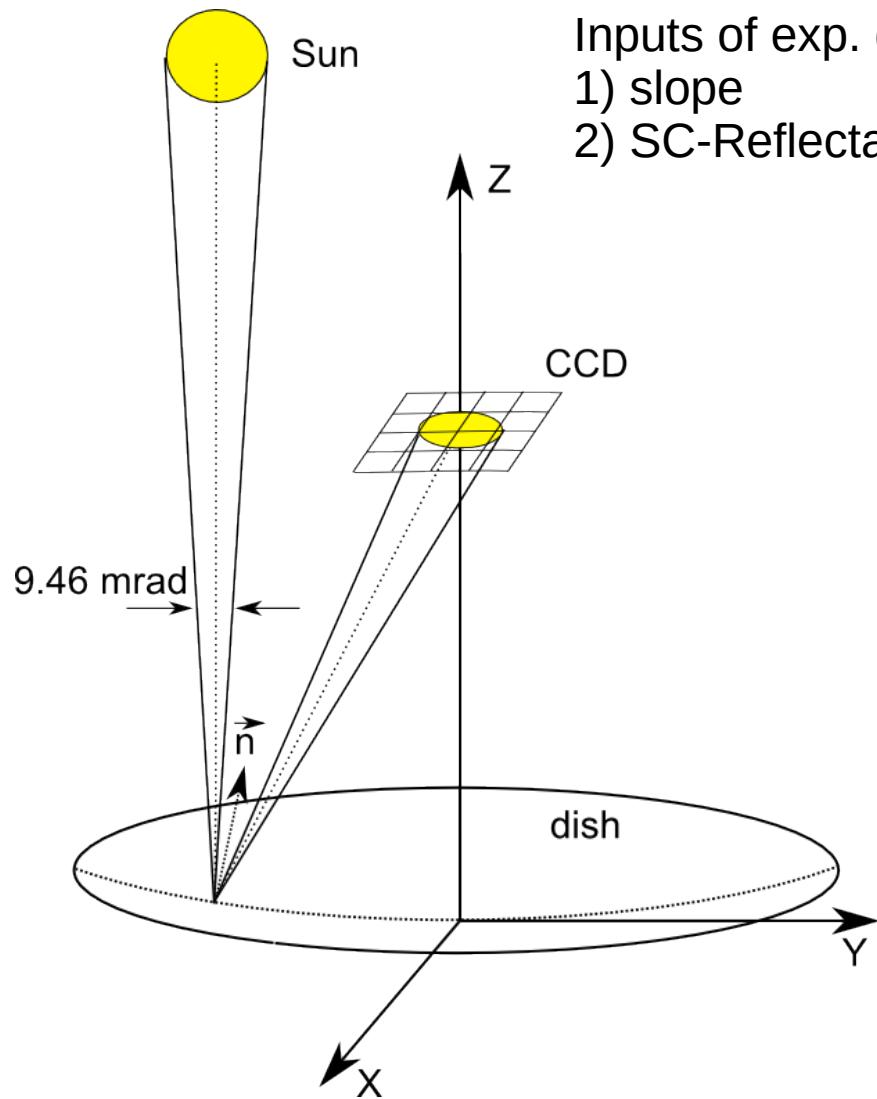
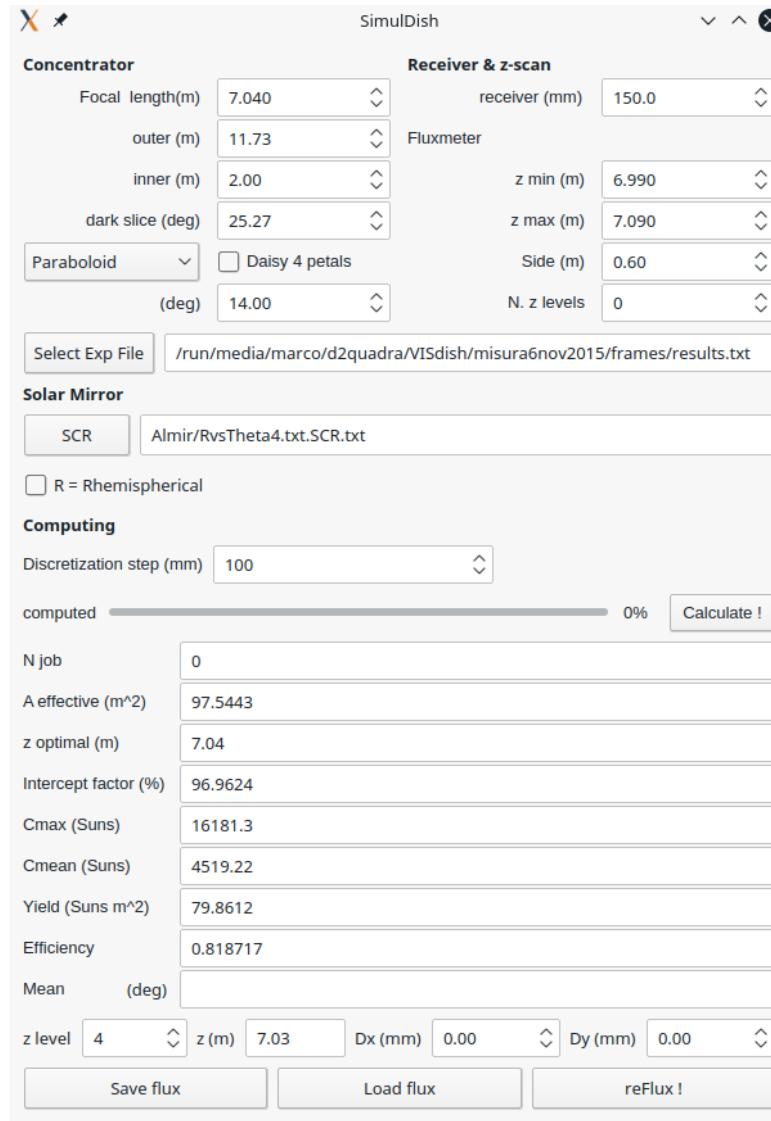
SCR of ALMIRR 303



Low performance
SCR(15 mrad)≈83%
(thin glass Ag > 95 %)

Large diffuse portion
4.3% beyond 20 mrad

SIMUL-DISH: simulation software

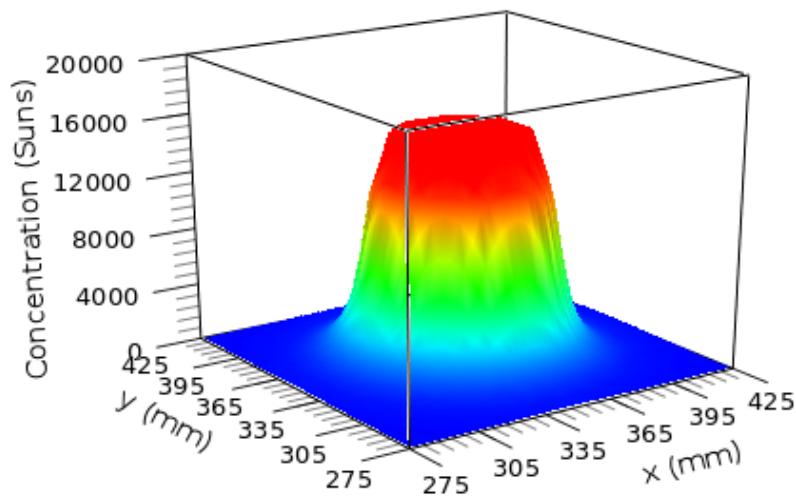


Inputs of exp. data:
1) slope
2) SC-Reflectance

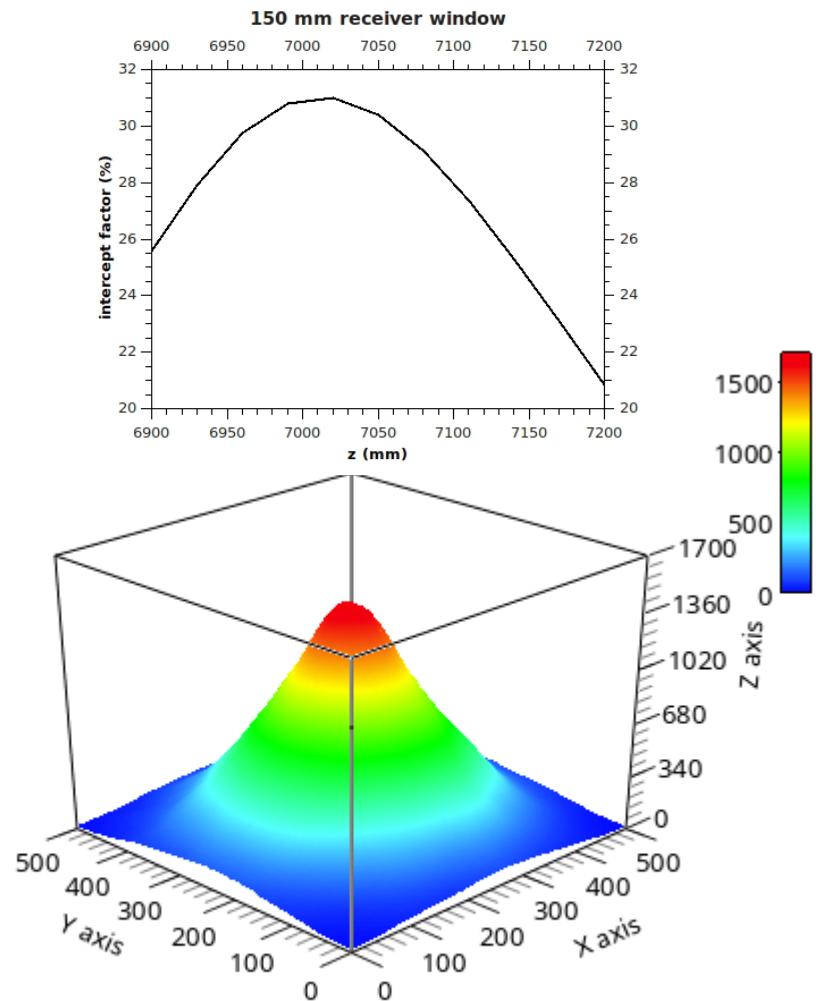
Results

$$f = 7020 \pm 10 \text{ mm}$$

$$IF_{150 \text{ mm}} = 31.0\%$$



ALMIRR & ideal shape
Cmax \approx 16'000 Suns



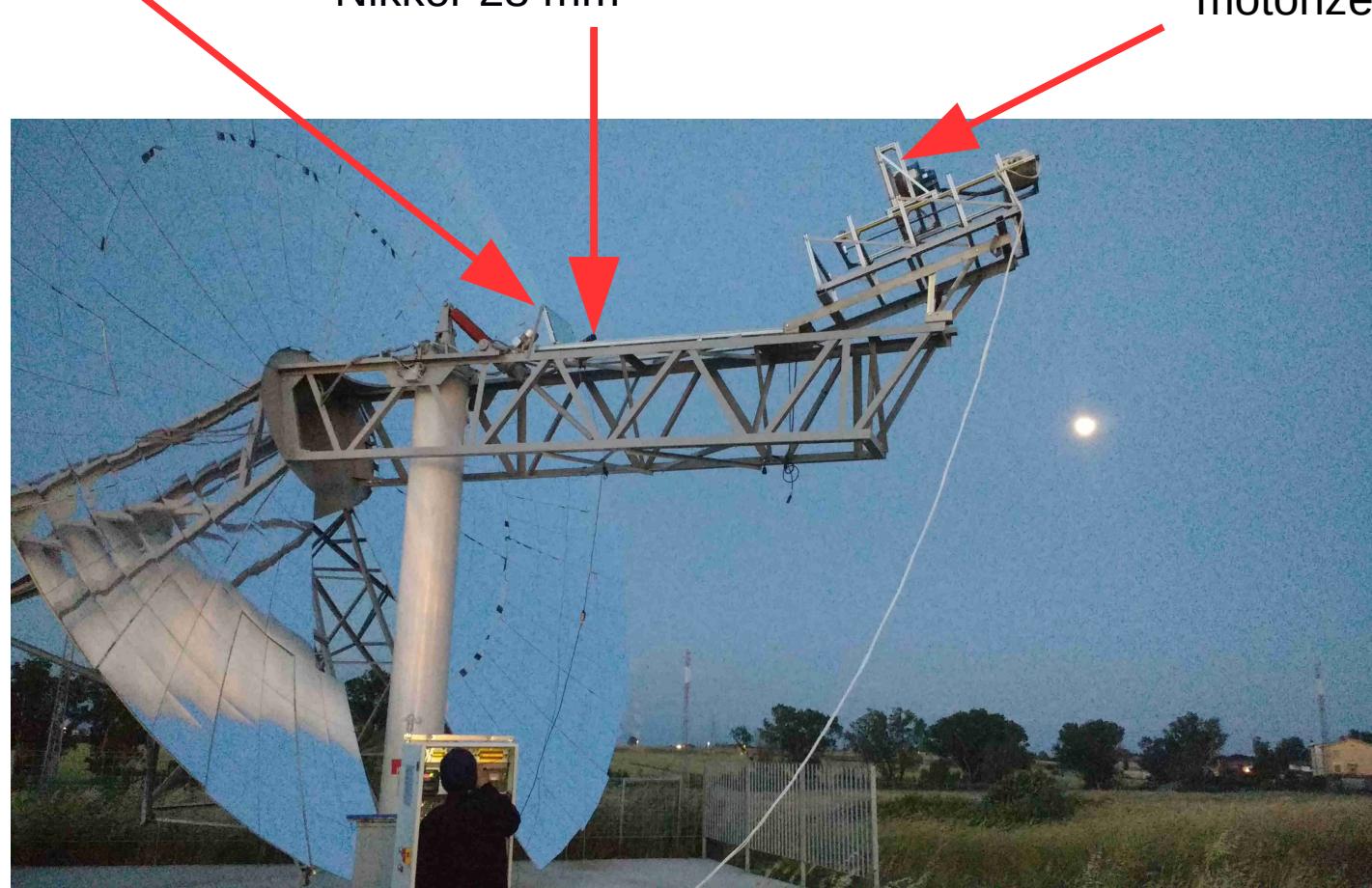
ALMIRR & exp .slope by VISdish
Cmax \approx 1'680 Suns

FluxMapper: experimental measurement of flux profile

Flat mirror (reference)
1 Sun

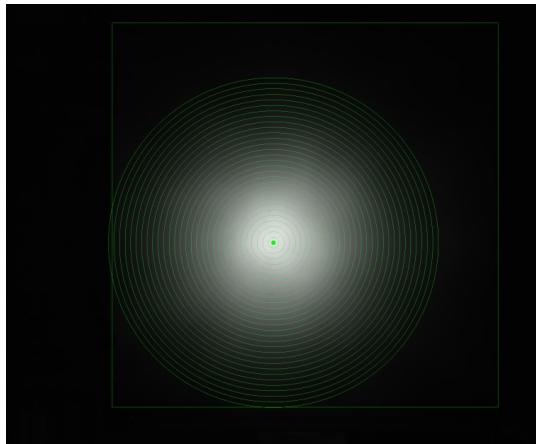
Camera Prosilica GT Allied Vision
2448×2050 pixels
14 bit depth
Nikkor 28 mm

Diffusive screen
Alumined copper
cooler
motorized

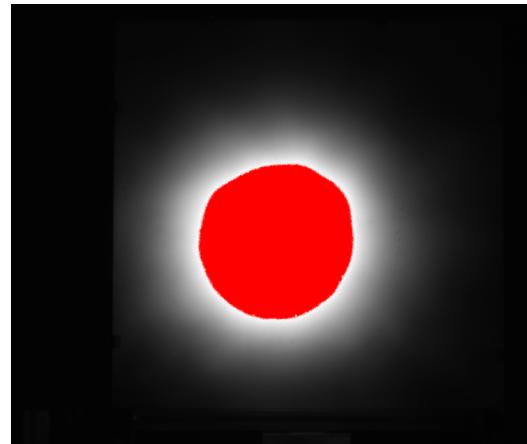


FluxMapper: Moon-tracking 20th May 2016 (99% lunar disc)

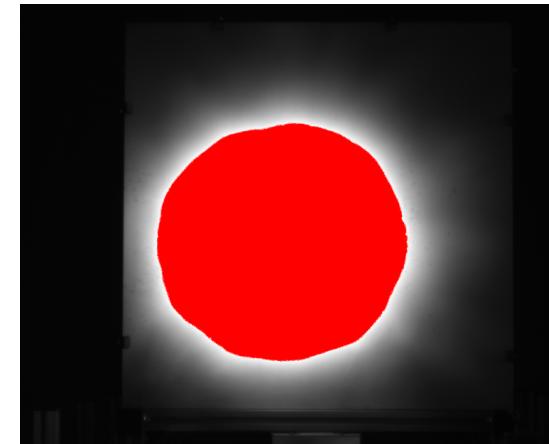
$$z = 7016 \pm 5 \text{ mm}$$



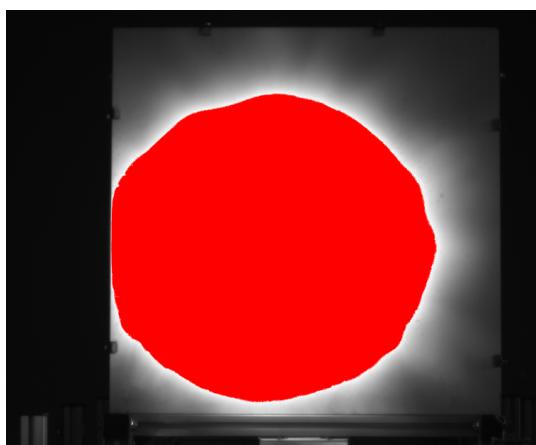
10 ms



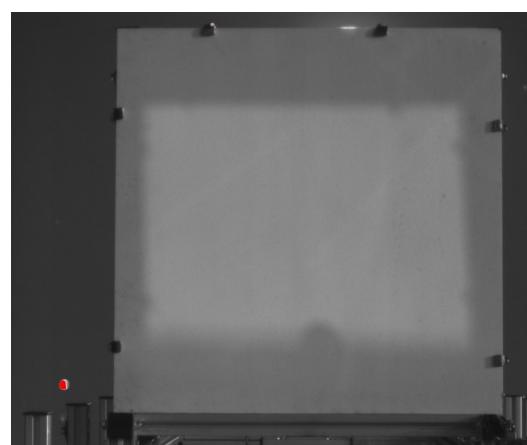
30 ms



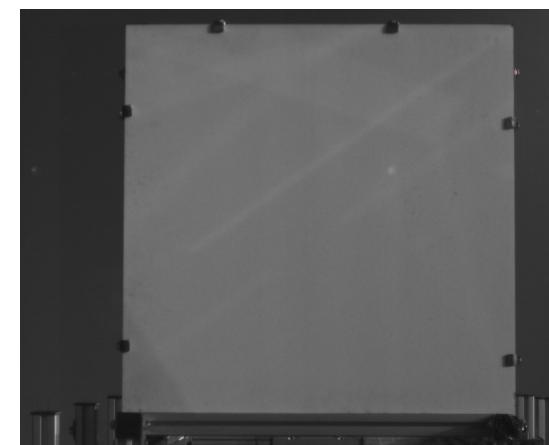
90 ms



270 ms



1 Sun at 270 ms



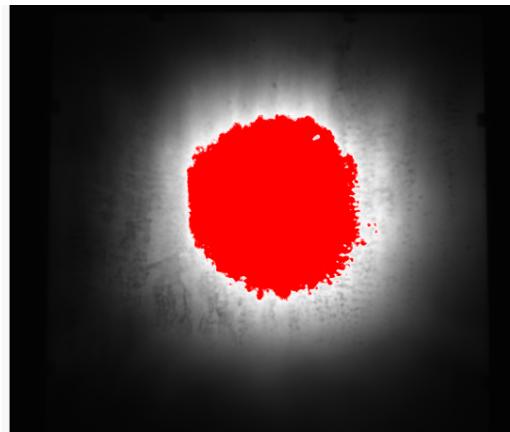
Background at 270 ms

FluxMapper + 10 Big stop Lee filter: Sun-tracking 17th May 2017

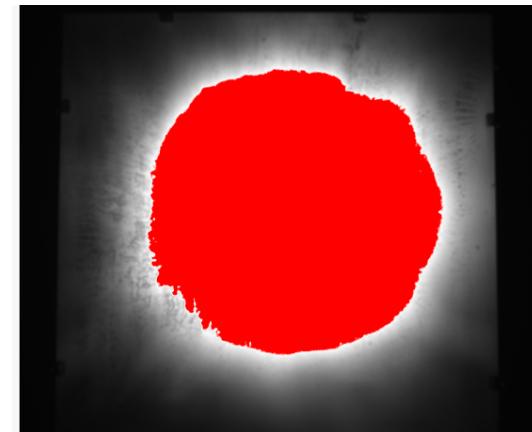
$$z = 7016 \pm 5 \text{ mm} \quad \text{Confirmed!!!!}$$



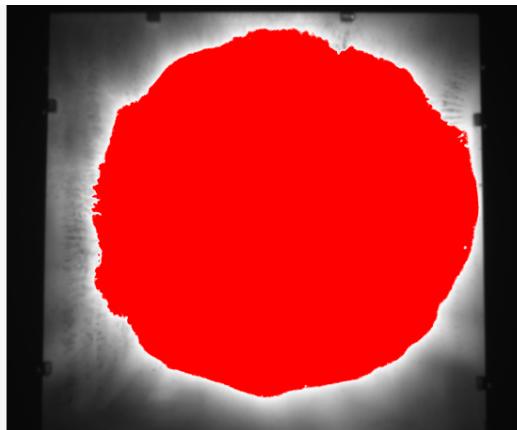
1.4 ms



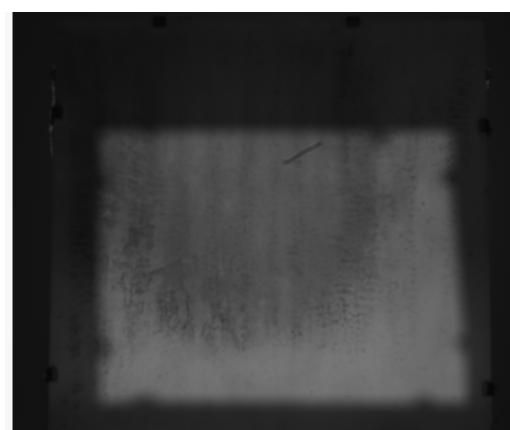
4.2 ms



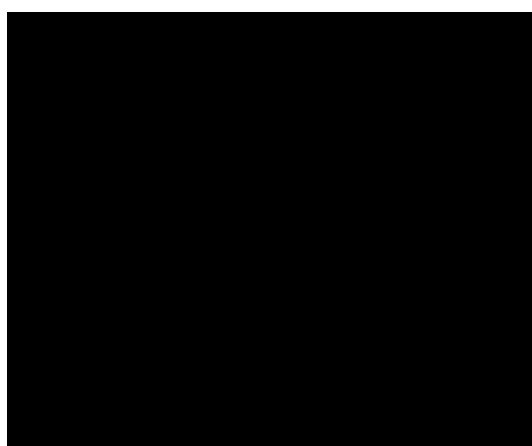
12.6 ms



37.8 ms

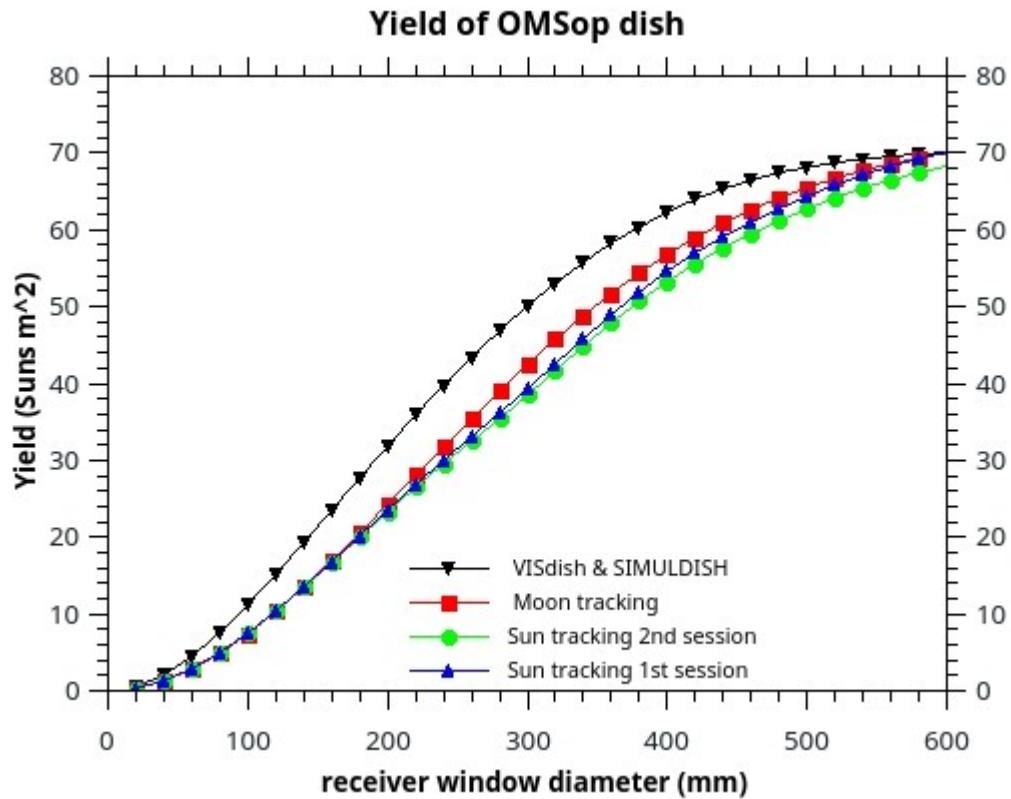


1 Sun at 340 ms



Background at 340 ms

Dish-yield from different methods



Experimental measurements with *Flux-mapper* give flux profile more spread than the simulated one based on **VISdish & SCReflectance!**

With DNI 800 Wm⁻², in a window of diameter 220 mm

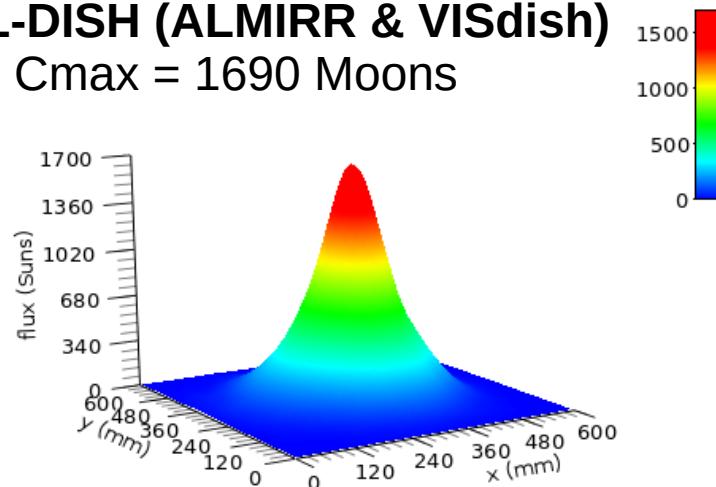
Pin = 22.4 kW

Pout = 33.6 kW

Flux profile comparison

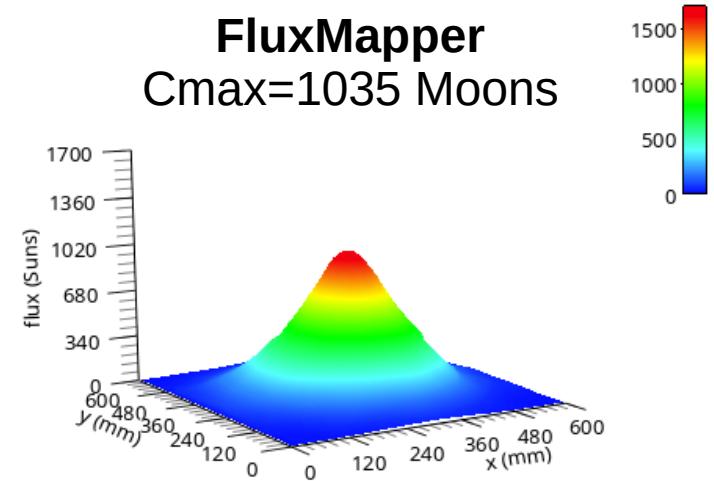
SIMUL-DISH (ALMIRR & VISdish)

Cmax = 1690 Moons

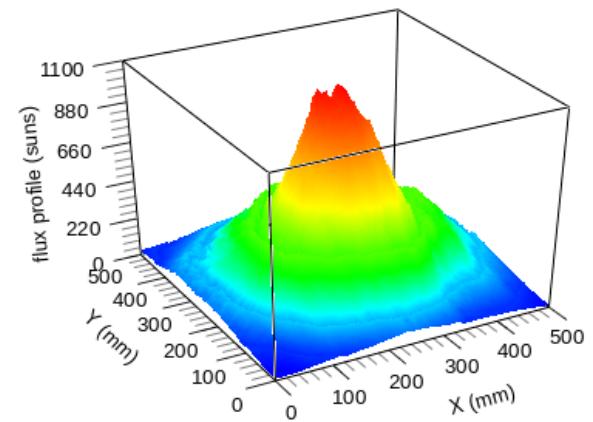


FluxMapper

Cmax=1035 Moons



FluxMapper
Cmax=1100 Suns



Results & Conclusions

- ✓ Optical axis z e focal length (7020 mm) have been determined
- ✓ ALMIRR 303 SCReflectance was measured: $\text{SCR}(15 \text{ mrad}) \approx 83\%$
- ✓ Facet-shape deviation was measured: $\sigma \approx 5.4 \text{ mrad}$
- ✓ Flux-profile by simulation (VISdish&SCR&SIMUL-DISH): **in 220 mm 28.9 kW**
- ✓ Flux-profile by FluxMapper: **in 220 mm 22.4 kW**
- The low quality of facets of SCReflectance and mainly of shape greatly reduces the concentration performance of the OMSoP dish
- **33.6 kW goes out 220 mm \Rightarrow shielding is needed**