# VERIFICATION OF RECOIL SEPARATOR PROPERTIES THROUGH REACTION MEASUREMENTS

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### Introduction

#### CAPTURE REACTIONS

Stellar energy production depends on the interior conditions of the star, such as the isotopic enrichment and temperature/pressure

Hydrogen burning:  $(p, \gamma)$  reactions

- · low mass energy production through pp-chains
- massive stars core and shell burning through CNO, NeNa, and MgAl cycles

Helium burning:  $(\alpha, \gamma)$  reactions

- $^{12}{
  m C}(lpha,\gamma)^{16}{
  m O}$  determines C/O ratio
- AGB stars during He burning stages are key source of neutrons for s-process (  $^{13}{\rm C}(\alpha,n)^{16}{\rm O},\,^{22}{\rm Ne}(\alpha,n)^{25}{\rm Mg}$  )
- breakout reactions from cyclic H burning (e.g.  $^{14}N(\alpha, \gamma)^{18}F$ )

#### RADIATIVE CAPTURE

Commonly studied by detecting the emitted  $\boldsymbol{\gamma}$ 

Detection is difficult due to:

- large background count rates (target impurities, background radiation)
- limited by HPGe detector efficiency
- potentially low count rates

Studied focused primarily on resonances to reduce the effect of these problems

#### **INVERSE KINEMATICS**

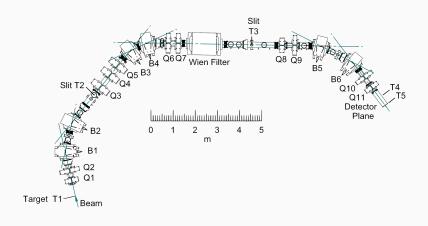
We can instead detect the heavy recoil particle using a high-efficiency detector to study complete cross sections

- Perform the reaction in inverse kinematics  $a(A, B)\gamma$
- Heavy projectile impinges on light target, heavy recoil escapes the target
- · Requires a stable H or He (commonly) target

Gain in efficiency of detector offset by complexities of distinguishing the few recoil particles from the high-intensity beam

### RECOIL SEPARATION

### St. George



Couder et al., 2008

#### MAGNETIC AND ELECTRIC RIGIDITIES

Elements within St. George are tuned for the  $B\rho$  and  $E\rho$  of the recoil particle

$$B\rho = \frac{\sqrt{2mT}}{q} \qquad E\rho = \frac{2T}{q}$$

Design limits:  $0.1 \le B\rho \le 0.45$  Tm and  $E\rho \le 5.7$  MV

#### PARTICLE SELECTION

We can uniquely identify particles by their mass, charge and energy:

#### **Magnetic Selection**

selects a single momentum:  $p = q \cdot B\rho$ 

#### **Electric Selection**

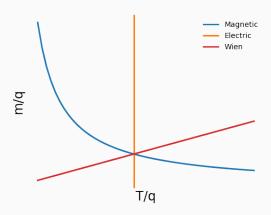
selects a single energy:  $T = q/2 \cdot E\rho$ 

#### Wien Filter Selection

selects a single velocity: v = E/B

#### PARTICLE SELECTION

Any two of the three possibilities may be combined to uniquely identify a particle



#### ANGULAR AND ENERGY ACCEPTANCE

Recoils can only be transported within defined parameter bounds

$$\Delta E/E = \pm 7.5\%$$
  $\Delta \theta = \pm 40 \,\mathrm{mrad}$ 

These bounds must hold for all possible E
ho and B
ho

#### IMPORTANCE OF ACCEPTANCES

Verifying the acceptances across a wide range of  $B\rho$  and  $E\rho$  is required in order to eliminate it as an unknown source of error Ensures that all of the produced recoils for a given reaction reach the detector plane

• The produced recoils can be extremely rare ( $10^{-15}$  per beam particle)

Once acceptances have been verified for enough  $B\rho$  and  $E\rho$  possibilities, scaling the electromagnetic elements to other rigidity values should retain the acceptance properties

# COMMISSIONING

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change the deflection of the particle at the target location

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#### Joint

adjust both at the same time

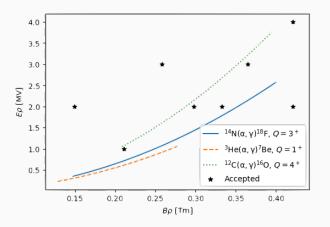
#### **ENERGY ACCEPTANCE**

For a particle beam with a given  $B\rho$  and  $E\rho$ :

- Tune the test beam to a given energy, and tune St. George for that energy
- · Verify 100 % transmission, adjust the tune if necessary
- Adjust the beam energy within the energy acceptance bounds and measure transmission
- Adjust the tune if necessary to have 100 % transmission for all possible energy changes within the acceptance bounds

#### **ENERGY ACCEPTANCE**

Energy acceptance completed for a subset of  $B\rho$  and  $E\rho$  test particles (100 % transmission found through current measurements)



#### JOINT ACCEPTANCE

All experiments will have an angular and energy spread, so must confirm that the acceptances can be achieved at the same time Can use a degrader foil to create an angular and energy spread at the same time

- New central energy based on energy loss
- Target material and thickness extremely important to understand well
- "Fuzziness" of beam spot may still make it difficult to tune

# REACTION MEASUREMENTS

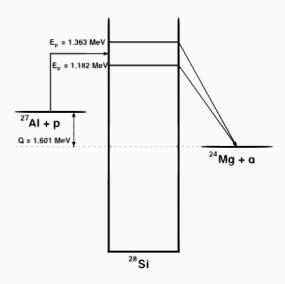
#### JUSTIFICATION FOR REACTION MEASUREMENTS

Joint acceptance measurements are costly to cover all of the possibilities

Reactions can be used to "bootstrap" the process

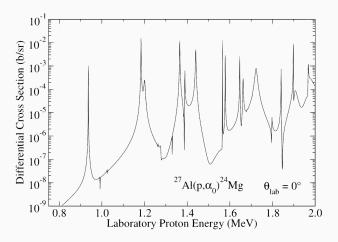
- Reactions have a known cross section, angular and energy spread, etc.
- If all of the expected produced recoils reach the detector, the separator is performing optimally

# The $^{27}\mathbf{Al}(\mathbf{p},\alpha)^{24}\mathbf{Mg}$ Reaction



## The $^{27}\mathbf{Al}(\mathbf{p},\alpha)^{24}\mathbf{Mg}$ Reaction

Cross section is well-known, reducing it as an uncertainty in the measurements



#### **ALTERNATE TUNE**

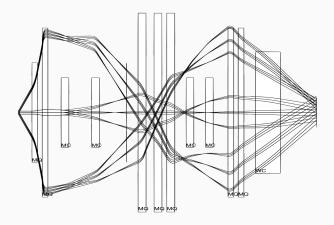
Since the last segment of St. George has not been fully commissioned (full angular acceptance not yet verified), we can use the focal plane after the Wien filter to perform cross section measurements

For  $(p, \alpha)$  reactions, the expected beam suppression is sufficient to reject the high-intensity incident beam

The beam spot at this focal plane needs to be adjusted to direct the reaction products to the detector

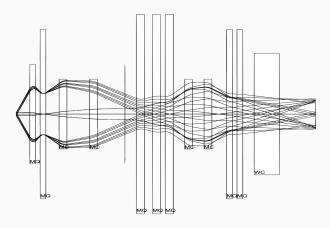
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Determined expected field strengths using COSY and verified with direct particle transport before the experiment



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#### ANGULAR ACCEPTANCE MEASUREMENT

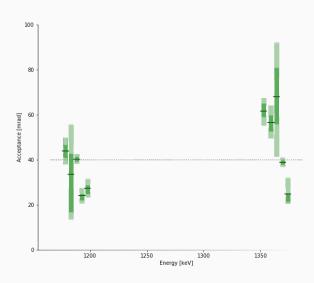
The reaction  $^{27}\mathrm{Al}(\mathrm{p},\alpha)^{24}\mathrm{Mg}$  emits the  $\alpha$  particles within an isotropic angular distribution

- target cup restricts us to  $\approx$  40 mrad acceptance
- $\cdot$  we will attempt to transport all lpha particles to the detector

Tuning the beginning of the separator to transport the particles to the Wien filter focal plane is an alternative to a full angular acceptance measurement

Ability to fine-tune and have confidence in the properties of the separator are required

#### **ACCEPTANCE MEASUREMENTS**



#### ACCEPTANCE UNCERTAINTY

We can attribute the uncertainty at each measurement to the underlying variables within our control: energy, current, time, and target thickness

- · On-resonance: dominated by current uncertainty
- · Below resonance: dominated by energy uncertainty
- · Attribution through a hybrid Monte Carlo/Bayesian approach

Final irreducible uncertainty comes from the underlying cross section, particle count rate, potential non-uniformity, etc.

# \_\_\_\_

**FUTURE DIRECTIONS** 

#### **EXPERIMENTAL OUTCOME**

St. George has been shown to have the following acceptances:

- $\Delta E/E \geq 7.5\%$
- $\Delta E/E = 3$  % and  $\Delta \theta = 40$  mrad (to WF)

Preliminary beam reduction measurements on the order of 10<sup>12</sup>

St. George can be used to study an additional class of reactions

Separation properties and beam currents are suitable for low-energy and off-resonance cross section measurements

#### THE FUTURE OF ST. GEORGE

- St. George can be used for a restricted subset of experiments
- Ability to fine-tune the separator and verify its properties over a range of  $B\rho$  and  $E\rho$  values essential for future experiments
- Diagnostic equipment and procedures developed to be applied to future separators (SECAR)
- Final parts of the St. George system (HIPPO supersonic jet gas target, full detector system, additional diagnostics, etc) will unlock the full range of experimental work

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#### 95 % CONTRIBUTIONS

ACCEPTANCE BOUNDS WITH HELD VARIABLES,  $95\,\%$ 

Held	241	234	$260^{\dagger}$	255	248	288	282	277	$270^{\dagger}$	264
$E_{\rm p}~[{ m MeV}]$	1.178	1.183	1.188	1.193	1.198	1.353	1.359	1.364	1.369	1.374
$\delta E$	49.4	7.5	101.1	75.8	93.0	64.1	39.6	13.2	102.4	50.9
$\delta t$	101.8	95.3	101.3	99.8	99.6	102.7	101.0	97.9	99.0	107.6
$\delta i$	86.6	97.3	26.8	51.1	66.3	77.7	93.9	93.6	26.5	102.0
$\delta\Delta$	95.4	98.2	101.4	80.4	82.9	98.7	104.2	95.8	103.5	75.8
$\delta E,\delta t$	47.4	7.2	96.7	73.4	93.4	63.8	39.6	13.2	101.4	50.2
$\delta E,\delta i$	12.0	1.7	23.0	18.1	55.5	20.1	12.5	3.0	24.0	42.7
$\delta E,\delta \Delta$	46.8	7.6	100.3	72.0	73.8	60.4	38.0	12.9	103.5	20.6
$\delta t,\delta i$	88.0	97.2	13.4	50.1	64.6	78.2	96.8	96.9	15.2	94.7
$\delta t, \; \delta \Delta$	98.5	98.3	98.2	86.7	83.5	99.4	102.0	98.8	99.8	75.9
$\delta i,\delta \Delta$	87.7	95.9	26.6	29.7	29.1	76.9	93.4	93.5	25.6	72.9
$\delta E,\delta t,\delta i$	11.1	1.0	8.1	18.6	54.0	17.8	11.5	1.5	8.3	43.5
$\delta E,\delta t,\delta \Delta$	47.4	7.2	96.8	70.1	76.0	59.9	39.0	12.9	99.4	20.4
$\delta E,\delta i,\delta \Delta$	7.9	1.6	21.4	8.4	5.0	8.4	7.4	2.7	22.4	4.6
$\delta t,\delta i,\delta \Delta$	86.2	98.6	13.1	29.6	27.0	78.2	94.2	96.5	14.5	68.0
All	5.4	1.0	4.0	2.8	3.8	6.6	5.2	0.9	3.7	1.3

†: Denotes runs at resonance energy

#### **INITIAL TEST REACTIONS**

Table 1

Inverse  $(\alpha, \gamma)$  reactions of astrophysical interest

Beam	Recoil	Beam $E_{lab}$ (MeV)	$E_{\rm cm}$ (MeV)	Recoil $E_{lab}$ (MeV)	Recoil <i>Q</i> [14]	Recoil abund. (%)	Half angle (mrad)	E range ±%	Mom. $p$ (MeV/ $c$ )	<i>Β</i> ρ (T m)
6O 2	<sup>20</sup> Ne	5.8	1.16	4.64	5	42	14.2	2.8	415.7	0.277
		12.5	2.5	10.02	6	40	11.8	2.4	610.9	0.340
<sup>18</sup> O <sup>22</sup>	<sup>22</sup> Ne	1.94	0.35	1.59	3	38	39.2	7.8	177.1	0.284
		3.3	0.60	2.70	4	42	30.9	6.2	332.6	0.277
	38Ar	10.0	1.05	8.95	8	32	10.4	2.1	795.7	0.332
		38.0	4.00	34.00	12	32	7.2	1.4	1551.0	0.431
<sup>36</sup> Ar <sup>40</sup> C	<sup>40</sup> Ca	12.5	1.25	11.25	9	31	9.1	1.8	915.3	0.339
		40.0	4.00	36.00	13	30	6.7	1.3	1638.0	0.420