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close all; clear all; clc;

Initial Set up

```
atm2Pa = 101325;
C2K = 273;
T_ref = 298;
R_u = 8.314;
                        % [J/mol-K]
% given lambda
G1.L = 2;
G1.Pm = 1*atm2Pa;
% Mass of
M H2 = 2.016;
                                             % [q/mol]
M_{H2O} = 18.01528;
                                             % [g/mol]
% LHV, HHV of H2 from Table A-27
C.LHV_bar = 120e3 * M_H2;
                                                             % [J/g] -->
 [J/mol]
                                                             % [J/g] -->
C.HHV_bar = 141.8e3 * M_H2 ;
[J/mol]
C.coef_{H2Ov} = [32.24, 0.1923e-2, 1.055e-5, -3.595e-9];
C.coef_H2 = [29.11, -0.1916e-2, 0.4003e-5, -0.8704e-9];
C.coef_02 = [25.48, 1.520e-2, -0.7155e-5, 1.312e-9];
C.coef_N2 = [28.90, -0.1571e-2, 0.8081e-5, -2.873e-9];
% heat of formation @ STP, N2
                                                             % [J/mol]
C.h_fo_N2 = 0;
% entropy of formation @ STP, N2
C.s_o_N2 = 191.61;
% heat of formation @ STP, O2
C.h_{fo_02} = 0;
                                                             % [J/mol]
% entropy of formation @ STP, O2
                                                             % [J/mol
C.s_o_02 = 205.04;
% heat of formation @ STP, H2
                                                              % [J/mol]
C.h_fo_H2 = 0;
```

Problem 1

```
P1.T = [25:1:1000] + C2K;
P1.Psat = T2P_sat(P1.T);
P1.y max = P1.Psat./G1.Pm;
P1.N_H2O = 1; % moles of water = beta + gamma
P1.y_{test} = P1.N_{H20}/(P1.N_{H20} + 0.5*(G1.L-1) +
0.5*G1.L*3.76); %P1.N_H2O/(P1.N_H2O + 0.5*G1.L);
P1.N a = 0.5*(G1.L-1) + 0.5*G1.L*3.76;
P1.N_react = 1 + 0.5*G1.L*(1+3.76);
[P1.beta, P1.gamma] = vaporLiquidBalance (P1.T, P1.y_test,
P1.y_max, ...
                             P1.N_a, P1.N_H2O, 0);
P1.N_prod = P1.beta + 0.5*(G1.L - 1) + 0.5*(G1.L)*(3.76);
% enthalpy of N2 at T
P1.dh_bar_N2 = integral_h (C.coef_N2, P1.T); % [J/mol]
                      % [J/mol K]
% N2 on the REACTANTS side
P1.y N2 react = (.5*G1.L*3.76)./(P1.N react-1);
                                                   % mole
fraction of N2 on reactants side
P1.ds_o_N2_react = delta_s (C.coef_N2, P1.T, P1.y_N2_react); %
integral term and log term of entropy
P1.g_bar_N2react = C.h_fo_N2 + P1.dh_bar_N2 ...
           - P1.T.*(C.s_o_N2 + P1.ds_o_N2_react);
% N2 on the PROD side
N2 on PRODUCT side
P1.ds_o_N2_prod = delta_s (C.coef_N2, P1.T, P1.y_N2_prod); % integral
term and log term of entropy
P1.g_bar_N2prod = C.h_fo_N2 + P1.dh_bar_N2 ...
           - P1.T.*(C.s_o_N2 + P1.ds_o_N2_prod);
% enthalpy of O2 at T
```

```
P1.dh_bar_02 = integral_h (C.coef_02, P1.T); % [J/mol]
P1.y_O2_react = (.5*G1.L)./(P1.N_react-1);
 % mole fraction of O2 on reactants side
P1.ds_o_02_react = delta_s (C.coef_02, P1.T, P1.y_02_react); %
integral term and log term of entropy
P1.g_bar_02react = C.h_fo_02 + P1.dh_bar_02 ...
            - P1.T.*(C.s_o_02 + P1.ds_o_02_react);
%%%%% PRODUCT SIDE
P1.y_O2_prod = (0.5*(G1.L-1))./P1.N_prod;
 % mole fraction of O2 on products side
P1.ds_o_02_prod = delta_s (C.coef_02, P1.T, P1.y_02_prod);
integral term and log term of entropy
P1.g_bar_02prod = C.h_fo_02 + P1.dh_bar_02 ...
            - P1.T.*(C.s_o_02 + P1.ds_o_02_prod);
P1.dh_bar_H2 = integral_h (C.coef_H2, P1.T); % [J/mol]
P1.y_H2 = 1./P1.N_react;
P1.ds_o_H2 = delta_s (C.coef_H2, P1.T, 1); % integral term and
log term of entropy
P1.q bar H2 = C.h fo H2 + P1.dh bar H2 \dots
           - P1.T.*(C.s_o_H2 + P1.ds_o_H2);
% H2O vapor
P1.dh bar H2Ov = integral h (C.coef H2Ov, P1.T);
                                                            % [J/
mol1
P1.y_H2Ov = P1.beta./P1.N_prod;
P1.ds_o_H2Ov = delta_s (C.coef_H2Ov, P1.T, P1.y_H2Ov);
integral term and log term of entropy
Pl.g_bar_H2Ov = C.h_fo_H2Ov + Pl.dh_bar_H2Ov ...
                    - P1.T.*(C.s o H2Ov + P1.ds o H2Ov);
P1.dh_bar_H2Ol = C.cp_bar_H2Ol*(P1.T - T_ref);
                                                % [J/mol]
P1.y_H2Ol = P1.gamma./P1.N_prod;
P1.ds o H2Ol = C.cp bar H2Ol.*log(P1.T/T ref);
P1.g_bar_H20l = C.h_fo_H20l + P1.dh_bar_H20l ...
                        - P1.T.*(C.s_o_H2Ol + P1.ds_o_H2Ol);
% P1.DG = Delta G [J]
P1.DG = P1.beta .* P1.g_bar_H20v ...
       + P1.gamma .* P1.g_bar_H201 ...
       + 0.5 *(G1.L - 1).* Pl.g bar O2prod ...
        + (.5*G1.L*3.76).* Pl.g_bar_N2prod...
                                                           % N H2 = 1
        - P1.g_bar_H2...
       - 0.5*G1.L*P1.g_bar_02react...
N_02_react = 1 = 1/2 * 2
        - (.5*G1.L*3.76).* P1.g_bar_N2react;
```

```
P1.Dh_bar = P1.beta.*(P1.dh_bar_H2Ov + C.h_fo_H2Ov) ...
        + P1.gamma.*(P1.dh bar H201 + C.h fo H201) ...
        + .5*(G1.L-1)*(P1.dh_bar_O2 + C.h_fo_O2) ...
        - 1*(P1.dh bar H2 + C.h fo H2) ...
        - .5*G1.L*(P1.dh_bar_O2 + C.h_fo_O2);
                                                             % [J/mol]
                                                             % [mol]
P1.N_fuel = 1;
P1.DH = P1.Dh bar * P1.N fuel;
                                                             % [J]
                                                            % [J]
P1.LHV = C.LHV bar * P1.N fuel;
                                                            % [J]
P1.HHV = C.HHV_bar * P1.N_fuel;
P1.E_HHV = (-P1.DG)./(P1.HHV);
P1.E LHV = (-P1.DG)./(P1.LHV);
P1.E_DH = (P1.DG)./(P1.DH);
% Carnot Efficiency = 1 - TL/TH
P1.E_c = 1 - (25 + C2K)./(P1.T);
% Plots for part 1
figure('units','normalized','outerposition',[0 0 .75 .75]); % for
larger plot
hold on;
plot(P1.T,P1.E_HHV,'LineWidth',2,'MarkerSize',10);
plot(P1.T,P1.E LHV,'LineWidth',2,'MarkerSize',10);
plot(P1.T,P1.E_DH,'LineWidth',2,'MarkerSize',10);
plot(P1.T,P1.E c,'LineWidth',2,'MarkerSize',10);
xlabel('Temperature, [K]','FontSize',18,'FontWeight','bold');
ylabel('First Law Efficiency,
 \eta_I', 'FontSize', 18, 'FontWeight', 'bold');
P1.leg = legend('HHV','LHV','H_{rxn}', 'Carnot
Efficiency', 'Location', 'best');
P1.leq.FontSize = 18;
set(gca,'FontSize',18);
```

Problem 2

```
P2.L = linspace(1,10,100);
% mole numbers are unique to each Lambda
P2.N_{H20} = 1;
                    % moles of water = beta + gamma
P2.y test = P2.N H20./(P2.N H20 + 0.5*(P2.L-1) +
0.5*P2.L*3.76); %P1.N_H2O/(P1.N_H2O + 0.5*G1.L);
P2.N_a = 0.5*(G1.L-1) + 0.5*G1.L*3.76;
P2.N_react = 1 + 0.5*P2.L*(1+3.76);
P2.T = [80, 220, 650, 800] + C2K; % 80 + C2K; %
figure('units','normalized','outerposition',[0 0 .75 .75]); % for
 larger plot
hold on;
for j = 1:length(P2.T)
    P2.Psat = T2P_sat(P2.T(j));
                                                % unique to each temp
    P2.y_max = P2.Psat./G1.Pm;
                                                % unique to each temp
```

```
[P2.beta, P2.gamma] = vaporLiquidBalance (P2.T(j), P2.y_test,
P2.y max,...
                      P2.N_a, P2.N_H2O, 0);
P2.N \text{ prod} = P2.beta + 0.5*(P2.L - 1) + 0.5*(P2.L)*(3.76);
% enthalpy of N2 at T
% N2 on the REACTANTS side
P2.y_N2_react = (.5*G1.L*3.76)./(P2.N_react-1);
                                                    % mole
fraction of N2 on reactants side
P2.ds_o_N2_react = delta_s (C.coef_N2, P2.T(j), P2.y_N2_react); %
integral term and log term of entropy
P2.g_bar_N2react(j,:) = C.h_fo_N2 + P2.dh_bar_N2 ...
                          - P2.T(j).*(C.s_o_N2 + P2.ds_o_N2_react);
% N2 on the PROD side
P2.y_N2_prod = (.5*G1.L*3.76)./P2.N_prod;
                                               % mole fraction of
N2 on PRODUCT side
P2.ds_o_N2_prod = delta_s (C.coef_N2, P2.T(j), P2.y_N2_prod); %
integral term and log term of entropy
P2.q bar N2prod(j,:) = C.h fo N2 + P2.dh bar N2 ...
           - P2.T(j).*(C.s_o_N2 + P2.ds_o_N2_prod);
% enthalpy of O2 at T
P2.dh_bar_02 = integral_h (C.coef_02, P2.T(j)); % [J/mol]
P2.y O2 react = (.5*P2.L)./(P2.N react-1); % mole fraction of
02 on reactants side
P2.ds_o_O2_react = delta_s (C.coef_O2, P2.T(j), P2.y_O2_react); %
integral term and log term of entropy
P2.q bar O2react(j,:) = C.h fo O2 + P2.dh bar O2 ...
           - P2.T(j).*(C.s_o_O2 + P2.ds_o_O2_react);
P2.y O2 prod = (0.5*(P2.L-1))./P2.N prod;
                                                       % mole
fraction of O2 on products side
for k = 1:length(P2.y_02_prod)
   if P2.y O2 prod(k) == 0
       P2.g_bar_02prod(j,:) = 0;
   else
       P2.ds_o_02_prod = delta_s (C.coef_02, P2.T(j),
P2.y_O2_prod(k)); % integral term and log term of entropy
       P2.q bar O2prod(j,k) = C.h fo O2 + P2.dh bar O2 ...
                      - P2.T(j).*(C.s_o_O2 + P2.ds_o_O2_prod);
   end
end
P2.y_H2 = 1./P2.N_react;
```

```
P2.ds_o_H2 = delta_s (C.coef_H2, P2.T(j), 1); % integral term and
 log term of entropy
P2.g_bar_H2(j,:) = C.h_fo_H2 + P2.dh_bar_H2 ...
                - P2.T(j).*(C.s_o_H2 + P2.ds_o_H2);
% H20 Vapor
P2.dh_bar_H2Ov = integral_h (C.coef_H2Ov, P2.T(j)); % [J/mol]
P2.y H2Ov = P2.beta./P2.N prod;
P2.ds_o_H2Ov = delta_s (C.coef_H2Ov, P2.T(j), P2.y_H2Ov);
integral term and log term of entropy
P2.g_bar_H2Ov(j,:) = C.h_fo_H2Ov + P2.dh_bar_H2Ov ...
                    - P2.T(j).*(C.s o H2Ov + P2.ds o H2Ov);
% H2O liquid
                                                              % [J/
P2.dh_bar_H2Ol = C.cp_bar_H2Ol*(P2.T(j) - T_ref);
P2.ds_o_H2Ol = C.cp_bar_H2Ol.*log(P2.T(j)/T_ref);
P2.q bar H2Ol(j,:) = ones(size(P2.L)).*(C.h fo H2Ol +
P2.dh_bar_H201 ...
                         - P2.T(j).*(C.s_o_H2Ol + P2.ds_o_H2Ol));
P2.DG(j,:) = P2.beta .* P2.g_bar_H2Ov(j,:) ...
        + P2.gamma .* P2.g bar H2Ol(j,:) ...
        + 0.5 *(P2.L - 1).* P2.g_bar_02prod(j,:) ...
        + (.5*P2.L*3.76).* P2.g_bar_N2prod(j,:)...
        - 1.*P2.g_bar_H2(j,:)...
        - 0.5*P2.L.*P2.g_bar_02react(j,:)...
        - (.5*P2.L*3.76).* P2.g_bar_N2react(j,:);
% These are the values that the book gives; Table A-27
P2.LHV_bar = 120e3 * M_H2;
                                                             % [mol]
P2.N fuel = 1;
P2.LHV = P2.LHV_bar * P2.N_fuel;
P2.E LHV(j,:) = (-P2.DG(j,:))./(P2.LHV);
plot(P2.L,P2.E LHV(j,:),'LineWidth',2,'MarkerSize',10);
end
xlabel('Air Fuel Ratio, \lambda','FontSize',18,'FontWeight','bold');
ylabel('First Law Efficiency,
 \eta_I', 'FontSize', 18, 'FontWeight', 'bold');
P2.leg =
 legend('80^oC', '220^oC', '650^oC', '800^oC', 'Location', 'best');
P2.leg.FontSize = 18;
set(qca,'FontSize',18);
```

Deliverable 3, Problem 2 - Part 2

```
P3.y_{test} = P3.N_{H20}/(P3.N_{H20} + 0.5*(G1.L-1) +
0.5*G1.L*3.76); %P1.N H2O/(P1.N H2O + 0.5*G1.L);
P3.N a = 0.5*(G1.L-1) + 0.5*G1.L*3.76;
P3.N_react = 1 + 0.5*G1.L*(1+3.76);
P3.T = [80, 220, 650, 800] + C2K;
P3.Psat = T2P sat(P3.T);
                                        % unique to each temp
figure('units','normalized','outerposition',[0 0 .75 .75]); % for
larger plot
hold on;
for j = 1:length(P3.T)
P3.y max = P3.Psat(j)./P3.Pm;
                                             % unique to each temp
[P3.beta, P3.gamma] = vaporLiquidBalance (P3.T(j), P3.y_test,
P3.y_max,...
                            P3.N a, P3.N H2O, 0);
P3.N_prod = P3.beta + 0.5*(G1.L - 1) + 0.5*(G1.L)*(3.76);
% enthalpy of N2 at T
P3.dh bar N2 = integral h (C.coef N2, P3.T(j)); % [J/mol]
% N2 on the REACTANTS side
P3.y_N2_react = (.5*G1.L*3.76)./(P3.N_react-1);
                                                        % mole
fraction of N2 on reactants side
P3.p_rat_N2_react = P3.y_N2_react.*P3.Pm ./ P3.P_ref;
P3.ds_o_N2_react = delta_s (C.coef_N2, P3.T(j), P3.p_rat_N2_react); %
integral term and log term of entropy
P3.g_bar_N2react = C.h_fo_N2 + P3.dh_bar_N2 ...
            - P3.T(j).*(C.s_o_N2 + P3.ds_o_N2_react);
% N2 on the PROD side
P3.y_N2_prod = (.5*G1.L*3.76)./P3.N_prod; % mole fraction of
N2 on PRODUCT side
P3.p_rat_N2_prod = P3.y_N2_prod.*P3.Pm ./ P3.P_ref;
P3.ds_o_N2_prod = delta_s (C.coef_N2, P3.T(j), P3.p_rat_N2_prod); %
integral term and log term of entropy
P3.g_bar_N2prod = C.h_fo_N2 + P3.dh_bar_N2 ...
            - P3.T(j).*(C.s_o_N2 + P3.ds_o_N2_prod);
% enthalpy of O2 at T
P3.dh_bar_O2 = integral_h (C.coef_O2, P3.T(j)); % [J/mol]
                                                  % mole fraction of
P3.y_O2_react = (.5*G1.L)./(P3.N_react-1);
02 on reactants side
P3.p_rat_02_react = P3.y_02_react .* P3.Pm ./ P3.P_ref;
P3.ds_o_O2_react = delta_s (C.coef_O2, P3.T(j), P3.p_rat_O2_react); %
integral term and log term of entropy
```

```
P3.g_bar_02react(j,:) = C.h_fo_02 + P3.dh_bar_02 ...
            - P3.T(j).*(C.s o O2 + P3.ds o O2 react);
P3.y O2 prod = (0.5*(G1.L-1))./P3.N prod;
                                                            % mole
 fraction of O2 on products side
P3.p_rat_02_prod = P3.y_02_prod .* P3.Pm ./ P3.P_ref;
for k = 1:length(P3.y 02 prod)
    if P3.y_02_prod(k) == 0
        P3.g_bar_02prod(j,:) = 0;
    else
        P3.ds_o_O2_prod = delta_s (C.coef_O2, P3.T(j),
 P3.p rat O2 prod(k)); % integral term and log term of entropy
        P3.g_bar_02prod(j,k) = C.h_fo_02 + P3.dh_bar_02 ...
                    - P3.T(j).*(C.s_o_O2 + P3.ds_o_O2_prod);
    end
end
P3.dh bar H2 = integral h (C.coef H2, P3.T(j));
                                                     % [J/mol]
P3.y_H2 = 1./P3.N_react;
P3.p_rat_H2 = P3.Pm ./ P3.P_ref;
P3.ds_o_H2 = delta_s (C.coef_H2, P3.T(j), P3.p_rat_H2);
integral term and log term of entropy
P3.g_bar_H2(j,:) = C.h_fo_H2 + P3.dh_bar_H2 ...
                    - P3.T(j).*(C.s_o_H2 + P3.ds_o_H2);
P3.dh_bar_H2Ov = integral_h (C.coef_H2Ov, P3.T(j)); % [J/mol]
P3.y_H2Ov = P3.beta./P3.N_prod;
P3.p_rat_H2Ov = P3.y_H2Ov .* P3.Pm ./ P3.P_ref;
P3.ds_o_H2Ov = delta_s (C.coef_H2Ov, P3.T(j), P3.p_rat_H2Ov);
        % integral term and log term of entropy
P3.g_bar_H2Ov(j,:) = C.h_fo_H2Ov + P3.dh_bar_H2Ov ...
                    - P3.T(j).*(C.s_o_H2Ov + P3.ds_o_H2Ov);
% H2O liquid
P3.dh_bar_H2Ol = C.cp_bar_H2Ol*(P3.T(j) - T_ref);
                                                              % [J/
mol]
P3.y H2Ol = P3.gamma./P3.N prod;
P3.ds_o_H2Ol = C.cp_bar_H2Ol.*log(P3.T(j)/T_ref);
P3.g_bar_H2Ol(j,:) = ones(size(G1.L)).*(C.h_fo_H2Ol +
P3.dh_bar_H201 ...
                         - P3.T(j).*(C.s_o_H2Ol + P3.ds_o_H2Ol));
P3.DG(j,:) = P3.beta .* P3.g_bar_H2Ov(j,:) ...
        + P3.gamma .* P3.g_bar_H20l(j,:) ...
        + 0.5 *(G1.L - 1).* P3.g_bar_O2prod(j,:) ...
        + (.5*G1.L*3.76).* P3.g_bar_N2prod...
        - (.5*G1.L*3.76).* P3.g_bar_N2react...
        - 1.*P3.g_bar_H2(j,:)...
 N H2 = 1
        - 0.5*G1.L.*P3.g_bar_02react(j,:);
```

```
P3.E_LHV(j,:) = (-P3.DG(j,:))./(P1.LHV);

plot(P3.Pm/atm2Pa,P3.E_LHV(j,:),'LineWidth',2,'MarkerSize',10);
end

xlabel('Pressure, [atm]','FontSize',18,'FontWeight','bold');
ylabel('First Law Efficiency,
  \eta_I','FontSize',18,'FontWeight','bold');
P3.leg =
  legend('80^oC', '220^oC', '650^oC', '800^oC', 'Location', 'best');
P3.leg.FontSize = 18;
set(gca,'FontSize',18);
```

Deliverable 4, Problem 3 - inlet RH vs temperature required for a saturated outlet air stream

```
% RH = mv/mg = (mass of vapor)/(mass at sat.)
% RH = Pv/Pg
% beta + gamma = 1 + alpha
P4.Pm = G1.Pm;
P4.L = 2;
P4.T = [25:1:100] + C2K;
P4.Psat = T2P_sat(P4.T);
P4.y_max = P4.Psat./P4.Pm;
P4.beta = P4.y_max./(1-P4.y_max)*(0.5*(P4.L-1) + 0.5*3.76*P4.L);
for i = 1:length(P4.beta)
    if P4.beta(i) < 1
        P4.alpha(i) = 0;
        P4.gamma(i) = 1-P4.beta(i);
        P4.alpha(i) = P4.beta(i) - 1;
        P4.gamma(i) = 0;
    end
end
P4.Pv = P4.alpha./(0.5*P4.L+0.5*P4.L*3.76+P4.alpha).*P4.Pm;
P4.Pg = P4.Psat;
P4.RH = P4.Pv./P4.Pg;
figure('units','normalized','outerposition',[0 0 .75 .75]); % for
larger plot
plot(P4.T,P4.RH,'LineWidth',2,'MarkerSize',10);
xlabel('Temperature, [K]','FontSize',18,'FontWeight','bold');
ylabel('Inlet RH', 'FontSize', 18, 'FontWeight', 'bold');
set(gca,'FontSize',18);
```

Deliverable 5

```
P5.L = 2;
P5.T = [25:1:100] + C2K;
P5.Pm = 1*atm2Pa;
figure('units','normalized','outerposition',[0 0 .75 .75]); % for
larger plot
hold on
% Line (1): dry hydrogen and dry air,
P5.DG = P1.DG(P1.T \le 100 + C2K);
P5.E LHV = (-P5.DG)./(P1.LHV);
plot(P5.T,P5.E LHV, 'LineWidth', 2, 'MarkerSize', 10);
%%%%%%%% shared constants in parts 2 and 3: %%%%%%%%%%%%%%%%%%%
% enthalpy of N2 at T
P5.dh bar N2 = integral h (C.coef N2, P5.T);
% enthalpy of O2 at T
P5.dh_bar_O2 = integral_h (C.coef_O2, P5.T);
                                                 % [J/mol]
%%%%%% H2O %%%%%%%%
% H2O vapor
P5.dh_bar_H2Ov = integral_h (C.coef_H2Ov, P5.T); % [J/mol]
P5.dh_bar_H2Ol = C.cp_bar_H2Ol*(P5.T - T_ref);
%%%%%%% N2 %%%%%%%%%%%
P5.dh_bar_H2 = integral_h (C.coef_H2, P5.T);
                                                 % [J/mol]
% Line (2): dry hydrogen and air with 100% relative humidity at cell
inlet
% conditions,
P5.Psat = T2P_sat(P5.T);
P5.y max = P5.Psat./P5.Pm;
P5.alpha2 = P5.y_max./(1-P5.y_max).*(0.5*P5.L*(1+ 3.76));
P5.N \text{ a prod2} = 0.5*(P5.L-1) + 0.5*P5.L*3.76;
P5.N_H2O_prod2 = 1 + P5.alpha2;
P5.y_test_prod = P5.N_H2O_prod2 ./ (P5.N_H2O_prod2 + 0.5*(P5.L-1) +
0.5*P5.L*3.76);
[P5.beta2, P5.gamma2] = vaporLiquidBalance (P5.T, P5.y_test_prod, ...
                       P5.y_max, P5.N_a_prod2, P5.N_H2O_prod2,
P5.alpha2);
P5.N_prod2 = P5.beta2 + 0.5*(P5.L-1) + 0.5*(P5.L)*3.76;
P5.N react2 = 0.5*(P5.L)*(1+3.76) + P5.alpha2;
% N2 on the REACTANTS side
```

```
P5.y_N2_react2 = (.5*G1.L*3.76)./(P5.N_react2);
                                                                % mole
 fraction of N2 on reactants side
P5.ds_o_N2_react2 = delta_s (C.coef_N2, P5.T, P5.y_N2_react2);
 integral term and log term of entropy
P5.g_bar_N2react2 = C.h_fo_N2 + P5.dh_bar_N2 ...
            - P5.T.*(C.s_o_N2 + P5.ds_o_N2_react2);
% N2 on the PROD side
P5.y_N2_prod2 = (.5*G1.L*3.76)./P5.N_prod2;
mole fraction of N2 on PRODUCT side
P5.ds_o_N2_prod2 = delta_s (C.coef_N2, P5.T, P5.y_N2_prod2);
 integral term and log term of entropy
P5.q bar N2prod2 = C.h fo N2 + P5.dh bar N2 ...
            - P5.T.*(C.s_o_N2 + P5.ds_o_N2_prod2);
P5.y_O2_react2 = (.5*P5.L)./(P5.N_react2);
  % mole fraction of O2 on reactants side
P5.ds_o_02_react2 = delta_s (C.coef_02, P5.T, P5.y_02_react2); %
integral term and log term of entropy
P5.g_bar_02react2 = C.h_fo_02 + P5.dh_bar_02 ...
            - P5.T.*(C.s_o_02 + P5.ds_o_02_react2);
% O2, PROD side
P5.y_O2_prod2 = (0.5*(P5.L-1))./P5.N_prod2;
   % mole fraction of O2 on reactants side
P5.ds_o_02_prod2 = delta_s (C.coef_02, P5.T, P5.y_02_prod2); %
integral term and log term of entropy
P5.g_bar_02_prod2 = C.h_fo_02 + P5.dh_bar_02 ...
            - P5.T.*(C.s_o_02 + P5.ds_o_02_prod2);
% H2, reactants
P5.y_H2 = 1./P5.N_react2;
P5.ds_o_H2 = delta_s (C.coef_H2, P5.T, 1); % integral term and
log term of entropy
P5.g_bar_H2 = C.h_fo_H2 + P5.dh_bar_H2 \dots
            - P5.T.*(C.s_o_H2 + P5.ds_o_H2);
% H2O vapor reactants
P5.y_H2Ov_react2 = P5.alpha2./P5.N_react2;
P5.ds_o_H2Ov_react2 = delta_s (C.coef_H2Ov, P5.T, P5.y_H2Ov_react2);
      % integral term and log term of entropy
P5.g_bar_H20v_react2 = C.h_fo_H20v + P5.dh_bar_H20v ...
                    - P5.T.*(C.s_o_H2Ov + P5.ds_o_H2Ov_react2);
% H2O vapor products
P5.y_H2Ov_prod2 = P5.beta2./P5.N_prod2;
P5.ds_o_H2Ov_prod2 = delta_s (C.coef_H2Ov, P5.T, P5.y_H2Ov_prod2);
    % integral term and log term of entropy
P5.g_bar_H2Ov_prod2 = C.h_fo_H2Ov + P5.dh_bar_H2Ov ...
```

```
- P5.T.*(C.s_o_H2Ov + P5.ds_o_H2Ov_prod2);
% H2O Liquid products
P5.ds_o_H2Ol_prod2 = C.cp_bar_H2Ol.*log(P5.T/T_ref);
P5.g_bar_H20l_prod2 = C.h_fo_H20l + P5.dh_bar_H20l ...
                        - P5.T.*(C.s_o_H2Ol + P5.ds_o_H2Ol_prod2);
% P5.DG = Delta G [J]
P5.DG2 = P5.beta2 .* P5.g_bar_H20v_prod2 ...
       + P5.gamma2 .* P5.g_bar_H2Ol_prod2 ...
       + 0.5 *(P5.L - 1).* P5.g_bar_02_prod2 ...
       + (.5*P5.L*3.76).* P5.g_bar_N2prod2...
        - P5.q bar H2...
                                                          % N H2 = 1
       - 0.5*P5.L*P5.g_bar_02react2...
N 02 react = 1 = 1/2 * 2
       - (.5*P5.L*3.76).* P5.g_bar_N2react2...
        - P5.alpha2.*P5.g_bar_H2Ov_react2;
P5.P H20 v = P5.alpha2./(P5.alpha2+.5.*P5.L.*(1+3.76)).*P5.Pm;
P5.RH = P5.P_H2O_v./P5.Psat;
P5.E_LHV2 = (-P5.DG2)./(P1.LHV);
plot(P5.T,P5.E_LHV2, ':','LineWidth',2,'MarkerSize',10);
% Line (3): dry hydrogen and air with just enough input humidity added
% maintain saturation conditions at the exit.
P5.alpha3 = P4.alpha;
P5.beta3 = P4.beta;
P5.gamma = P4.gamma;
P5.N_react3 = 0.5*P5.L*(1+3.76) + P5.alpha3;
P5.N_prod3 = P5.beta3 + 0.5*(P5.L - 1) + 0.5*(P5.L)*(3.76);
% entropy of N2 at T, P
% N2 on the REACTANTS side
P5.y_N2_react = (.5*P5.L*3.76)./(P5.N_react3);
                                                      % mole
fraction of N2 on reactants side
P5.ds_o_N2_react = delta_s (C.coef_N2, P5.T, P5.y_N2_react); %
integral term and log term of entropy
P5.g_bar_N2react = C.h_fo_N2 + P5.dh_bar_N2 ...
           - P5.T.*(C.s_o_N2 + P5.ds_o_N2_react);
% N2 on the PROD side
P5.y_N2_prod = (.5*G1.L*3.76)./P5.N_prod3;
                                                 % mole fraction of
N2 on PRODUCT side
P5.ds_o_N2_prod = delta_s (C.coef_N2, P5.T, P5.y_N2_prod); % integral
term and log term of entropy
P5.g bar N2prod = C.h fo N2 + P5.dh bar N2 ...
           - P5.T.*(C.s_o_N2 + P5.ds_o_N2_prod);
```

```
%%%%% REACTANT SIDE, O2 %%%%%%
P5.y O2 react = (.5*G1.L)./(P5.N react3);
  % mole fraction of O2 on reactants side
P5.ds_o_02_react = delta_s (C.coef_02, P5.T, P5.y_02_react); %
 integral term and log term of entropy
P5.g_bar_02react = C.h_fo_02 + P5.dh_bar_02 ...
            - P5.T.*(C.s_o_02 + P5.ds_o_02_react);
%%%%%% PRODUCT SIDE, O2 %%%%%%
P5.y_02_prod = (0.5*(G1.L-1))./P5.N_prod3;
   % mole fraction of O2 on products side
P5.ds o O2 prod = delta s (C.coef O2, P5.T, P5.y O2 prod);
integral term and log term of entropy
P5.g_bar_02prod = C.h_fo_02 + P5.dh_bar_02 ...
            - P5.T.*(C.s_o_O2 + P5.ds_o_O2_prod);
%%%% REACTANT SIDE, H2 %%%%%%%%
P5.ds_o_H2 = delta_s (C.coef_H2, P5.T, 1); % integral term and
log term of entropy
P5.g_bar_H2 = C.h_fo_H2 + P5.dh_bar_H2 \dots
            - P5.T.*(C.s_o_H2 + P5.ds_o_H2);
%%%%%% PRODUCT SIDE, H2O vapor %%%%%%%%%
P5.y H2Ov prod = P5.beta3./P5.N prod3;
P5.ds_o_H2Ov_prod = delta_s (C.coef_H2Ov, P5.T, P5.y_H2Ov_prod);
  % integral term and log term of entropy
P5.g_bar_H2Ov_prod = C.h_fo_H2Ov + P5.dh_bar_H2Ov ...
                    - P5.T.*(C.s_o_H2Ov + P5.ds_o_H2Ov_prod);
% H2O liquid
P5.y_H2Ol = P5.gamma./P5.N_prod3;
P5.ds_o_H2Ol = C.cp_bar_H2Ol.*log(P5.T/T_ref);
P5.g bar H201 = C.h fo H201 + P5.dh bar H201 ...
                         - P5.T.*(C.s_o_H2Ol + P5.ds_o_H2Ol);
%%%%%%% REACTANT SIDE H2O %%%%%%%%%%%
P5.y H2Ov r = P5.alpha3./P5.N react3;
for i = 1:length(P5.y_H2Ov_r)
    if P5.y H2Ov r(i) == 0
        P5.ds_o_H2Ov_r(i) = 0;
    else
        P5.ds_o_H2Ov_r(i) = delta_s (C.coef_H2Ov, P5.T(i),
                   % integral term and log term of entropy
 P5.y_H2Ov_r(i));
    end
end
P5.g_bar_H2Ov_react = C.h_fo_H2Ov + P5.dh_bar_H2Ov ...
                    - P5.T.*(C.s_o_H2Ov + P5.ds_o_H2Ov_r);
% P5.DG = Delta G [J]
P5.DG_sat_out = P5.beta3 .* P5.g_bar_H2Ov_prod ...
        + P5.gamma .* P5.g_bar_H201 ...
```

```
+ 0.5 *(G1.L - 1).* P5.g_bar_02prod ...
        + (.5*G1.L*3.76).* P5.g_bar_N2prod...
        - P5.g_bar_H2...
                                                            % N H2 = 1
        - 0.5*G1.L*P5.g_bar_02react...
N_02_react = 1 = 1/2 * 2
        - (.5*G1.L*3.76).* P5.g_bar_N2react...
        - P5.alpha3.* P5.g_bar_H2Ov_react;
P5.E_sat_out = -(P5.DG_sat_out)./(P1.LHV);
plot(P5.T,P5.E_sat_out, ':','LineWidth',2,'MarkerSize',10);
xlabel('Temperature, [K]','FontSize',18,'FontWeight','bold');
ylabel('First Law Efficiency,
\eta_I','FontSize',18,'FontWeight','bold');
P5.leg = legend('Dry H_2, Dry Air', 'Saturated Inlet Air', 'Saturated
Exit Air','Location', 'best');
P5.leg.FontSize = 18;
set(gca,'FontSize',18);
```

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