

# Appendix A

## Codes for Co-Optimization and Design Process

This Appendix presents the codes for the design process discussed in Chapter 4. In this appendix, first the MATLAB script for designing and co-optimization process of magnetics and circuits is presented. 50000 designs are generated, analysed and saved in an initial file called "AllDesigns.txt". In the design process a function called OptimizeT is used for optimizing the circuit and calculating the required inductance. OptimizeT is using other functions in itself: ScaleT for calculating the scaling factor of the transistor, EstLosses for estimating the losses inside the transistor and the diode, FindInductor for finding the required inductance for the circuit at the operating frequency. Finally a MATLAB script is presented for filtering the designs based on the process presented in Section 4.2.6. Among the scripts and functions presented here, functions OptimizeT, ScaleT, EstLosses, and FindInductor are originally written by the circuit team; see Acknowledgments.

```
1 clear all;  
2 close all;  
3 tic;  
4  
5 format shortG  
6
```

```

7  %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
8  % CONSTANTS
9  %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
10
11 mu0=4*pi*1e-7;           % Permeability of Air
12 epsilon0=8.85e-12;       % Permittivity of Air
13 mu=mu0*1;                 % Permeability of Inductor Core
14
15 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
16 % CONSTANT and FIXED PARAMETERS
17 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
18
19 Vin_V=100;                % Input Voltage [V]
20 Vled_V=35.8;              % LED Voltage [V]
21 Power_W=25;               % LED Power Delivery Goal [W]
22 Height=1000e-6;           % Height of Inductor [m]
23 ConductorThickness=30e-6;
24 SigmaCopper=5.8e7;         % Conductivity of
    Copper at 25 C [S/m]
25 SigmaCopper=SigmaCopper/(1+0.0039*(100)); % Conductivity at
    125 C [S/m]
26 WindingGap=100e-6; % Gap between the winding [m]
27 X0=Height/2;              % Half of the Inductor Height [m]
28
29 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
30 % Generating Random Designs
31 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
32
33 for iRand=1:50000          % Defining Number of
    Random Designs

```

```

34
35 Ro=3.5e-3+rand*(4e-3); % Defining Outer
    Radius Range [m]
36 MinFeatureSize=90e-6+rand*80e-6; % Defining Minimum
    Feature Size Range [m]
37
38 Freq_MHz=10+rand*20; % Defining Frequency
    Range [MHz]
39 Freq_Hz=Freq_MHz*1e6; % Frequency [Hz]
40 Omega=2*pi*Freq_Hz;
41
42 Cind_F=5e-12+rand*(5e-12); % Defining Inductor
    Capacitance Range [F]
43
44 % The inductor Height can be either defined as a random
    variable or as a fixed parameter. Random Variable:
    Height=500e-6+rand*500e-6; X0=Height/2;
45
46 Cind_pF=Cind_F/1e-12;
47 Cind_F=Cind_F;
48
49 [ scaleT , P_W , PDiode_W , PSwitch_W , L_H , Ton_s ,
    Vswitch_V , Iswitch_A , Vdiode_V , Idiode_A , Vind_V ,
    Iind_A , T_s] =...
50 OptimizeT( Vin_V , Vled_V , Power_W , Freq_Hz ,
    @MITHEMT_Coss , @STPS10170C_Cj , Cind_F , 0.9 , .3 ,
    .69 , .5);
51
52 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
53 % Designing The Inductor Ro and Ri

```

```

54 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
55
56 L_nH=L_H/1e-9;      % Required Inductance from
    Optimization Code
57 Ri=Ro/4;            % Initial Value for Inner Radius
58 RoOvRi=Ro/Ri;       % Initial Value Ro Over Ri Ratio
59 for RoOvRiStep=1:10
60     RoOvRi = pi*Ro*sqrt(2)*sqrt(mu0*Height*log(RoOvRi))
        /((MinFeatureSize+GapRi)*sqrt(L_nH*1e-9*pi));
61 end
62
63 Ri=abs(Ro/RoOvRi);      % Inner
    Radius of the Inductor [m]
64 N=round(2*pi*Ri/(MinFeatureSize+GapRi)); % Number of
    Turns for Toroidal Inductor
65 MinFeaturesize=2*pi*Ri/N-WindingGap;
66
67 TopLength=Ro-Ri;
68 BottomAngle=2*pi/N;
69 BottomLength=sqrt(Ri^2+Ro^2-2*Ro*Ri*cos(BottomAngle));
70
71 Length=(BottomLength+TopLength+2*Height)*N; % Total
    Length of Windings
72
73 LRecal=(1/2)*N^2*mu0*Height*log(Ro/Ri)/pi; %
    Recalculating the value of the inductance to check if
    the solution has converged
74
75 ErrorInL=(LRecal-L_H)/L_H*100;      % Error
    between the Recalculated Inductance and Required

```

```

76      Inductance .
77
78      LengthOver2=((2*pi*((Ro+Ri)/2)/N)-WindingGap)/2; % Half
      of Conductor Width (Y/2)
79
80      %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
81      % Voltage and Current Waveforms at the Inductor
82      %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
83
84      V0=(max(Vind_V)-min(Vind_V))/2; %
      Amplitude of First Harmonic of Voltage Waveform
85      IMaxAC=(max(Iind_A(:,1))-min(Iind_A(:,1)))/2; %
      Amplitude of First Harmonic of Current Waveform
86      I0DC=(max(Iind_A(:,1))+min(Iind_A(:,1)))/2; %
      Amplitude of the DC Component of the Current Waveform
87
88      %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
89
90      IMax=1; %
      Amplitude of a 1-Ampere single harmonic current
91
92      %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
93      % Calculating AC Loss By Energy Models + Diffusion
      Equations
94      %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
95
96      %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
97      % Defining Solved Free Parameters Equations:
98      %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

```

99

100  $Asinyc = -(2 * X0 + \pi * WindingGap) / (2 * WindingGap) ;$ 101  $Asinyt = (12.0 * WindingGap^2 * (-8 * WindingGap^3 + 2 * X0 * \pi * WindingGap^2 + \dots$ 102  $\pi^2 * WindingGap^3 + 2 * \pi * X0^3 + \pi^2 * X0^2 * WindingGap) / (\pi * \dots$ 103  $(-12 * \pi * X0^5 + 5 * \pi^3 * X0^3 * WindingGap^2 + \pi^2 * X0^2 * WindingGap^3 + \dots$ 104  $6 * \pi * X0^3 * WindingGap^2 - 18 * X0 * \pi * WindingGap^4 - 24 * WindingGap^5 + \dots$ 105  $3 * \pi^2 * WindingGap^5 + 2 * \pi^3 * X0^5 + \pi^4 * X0^2 * WindingGap^3 + \dots$ 106  $\pi^4 * X0^4 * WindingGap + 3 * \pi^3 * X0 * WindingGap^4) ) ;$ 107  $Bsinx1 = (-48.0 * WindingGap^3 * X0^2 / (\pi * (-12 * \pi * X0^5 + 5 * \pi^3 * X0^3 * \dots$ 108  $WindingGap^2 + \pi^2 * X0^2 * WindingGap^3 + 6 * \pi * X0^3 * WindingGap^2 - \dots$ 109  $18 * X0 * \pi * WindingGap^4 - 24 * WindingGap^5 + 3 * \pi^2 * WindingGap^5 + \dots$ 110  $2 * \pi^3 * X0^5 + \pi^4 * X0^2 * WindingGap^3 + \pi^4 * X0^4 * WindingGap + \dots$ 111  $3 * \pi^3 * X0 * WindingGap^4) ) ;$ 112  $betaly = (1.0 * \pi / X0) ;$ 113  $betatx = (1.0 * \pi / WindingGap) ;$ 

114

115  $Ralpha = (1/2) * \sqrt{2} * \sqrt{\Omega * \mu_0 * \text{SigmaCopper}} ;$ 116  $RalphaL = Ralpha * 2 * \text{LengthOver2} ;$ 117  $RalphaT = Ralpha * \text{ConductorThickness} ;$ 

118

```

119 k0=Asinyt*pi/((-2*Asinyt*pi*(-1+exp(-betatx*
      ConductorThickness))...
120 /(betatx*WindingGap)+(2*(-Bsinx1*pi+betaly*
      LengthOver2+Bsinx1*...
121 pi*exp(-betaly*LengthOver2)))/(betaly*X0))*
      WindingGap);
122 DenkL=(-2*Asinyt*pi*(-1+exp(-betatx*ConductorThickness))
      /...
123 (betatx*WindingGap)+(2*(-Bsinx1*pi+betaly*
      LengthOver2+...
124 Bsinx1*pi*exp(-betaly*LengthOver2)))/(betaly*X0))*X0
      ;
125 RalphaBTh=Ralpha*ConductorThickness;
126
127 LossShortEdges= -(1/4)*Ralpha*k0^2*(2*cos(RalphaL)*sinh(
      RalphaL)+...
128 2*cosh(RalphaL)*sin(2*Ralpha*LengthOver2)+sinh(4*
      Ralpha*...
129 LengthOver2)+sin(4*Ralpha*LengthOver2))*(-1+exp(-2*
      betatx*...
130 ConductorThickness))/((sinh(2*Ralpha*LengthOver2)
      ^2*...
131 cos(RalphaL)^2+cosh(2*Ralpha*LengthOver2)^2*...
132 sin(RalphaL)^2)*SigmaCopper*betatx);
133
134 LossLongEdge= -(1/16)*Ralpha*(-Bsinx1^2*pi^2+4*Bsinx1*pi
      +...
135 Bsinx1^2*pi^2*exp(-2*betaly*LengthOver2)-4*Bsinx1*pi
      *...

```

```

136     exp(- betaly * LengthOver2)+2*log ( exp(- betaly *
        LengthOver2))) * ...
137     ( exp(4* RalphaT)*cos ( RalphaT )^2+exp(4* RalphaT)+8*cos (
        RalphaT) * ...
138     sin ( RalphaT)*exp(2* RalphaT)-cos ( Ralpha*
        ConductorThickness)^2 - ...
139     1+exp(4* RalphaT)*sin ( RalphaT)^2- sin ( RalphaT)^2)*exp
        (-2* RalphaT) / ...
140     (( sinh ( RalphaBTh)^2*cos ( RalphaBTh)^2+ cosh ( RalphaBTh)
        ^2 * ...
141     sin ( RalphaBTh)^2)*DenkL^2* SigmaCopper* betaly );
142
143     ACLossForOneAmperSingleHarmonicPerMeter=LossShortEdges+
        LossLongEdge ;
144     Rac=ACLossForOneAmperSingleHarmonicPerMeter / (0.5 * IMax^2)
        *Length ; % IMax =1
145
146     TotalACLoss=Rac*(IMaxAC^2*0.5) ; % Using Inductor Current
        Waveform
147
148     %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
149     % Calculating DC Loss
150     %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
151     SF=1+(pi*Ri/N/(Ro-Ri))^2 ;
152     RDC=1/SigmaCopper*N^2/ ConductorThickness*(( Height-2*
        ConductorThickness)/(2*pi*Ri-N*WindingGap)+( Height-2*
        ConductorThickness)/(2*pi*Ro-N*WindingGap)+SF/pi*log
        ((2*pi*(Ro)-N*WindingGap)/(2*pi*(Ri)-N*WindingGap))) ;
153     LossDC=RDC*I0DC^2 ;
154

```



```

155     TotalLossOnGlass=PDiode_W+PSwitch_W+LossDC+TotalACLoss ;
156     CircuitEfficiencyGlass =25/(25+ TotalLossOnGlass ) ;
157
158     AreaOfInductor=pi*Ro^2;
159     InductorPowerDensityWPmSq=25/ AreaOfInductor ;
160
161     Qac=L_H*Omega/Rac ;
162
163     % Operating Frequency
164     InitialDesignTable (iRand ,1)=Freq_MHz ;
165
166     % Designed Inductor Geometry
167     InitialDesignTable (iRand ,2)=N;
168     InitialDesignTable (iRand ,3)=Ri/1e-3;
169     InitialDesignTable (iRand ,4)=Ro/1e-3;
170     InitialDesignTable (iRand ,5)=Height/1e-6;
171     InitialDesignTable (iRand ,6)=ConductorThickness/1e-6;
172     InitialDesignTable (iRand ,7)=WindingGap/1e-6;
173     InitialDesignTable (iRand ,8)=BottomLength ;
174     InitialDesignTable (iRand ,9)=TopLength ;
175     InitialDesignTable (iRand ,10)=MinFeaturesize ;
176
177     % Optimized Transistor Area:
178     InitialDesignTable (iRand ,11)=scaleT ;
179
180     % Design Material Properties
181     InitialDesignTable (iRand ,12)=mu/mu0; % Core Relative
        Permeability
182     InitialDesignTable (iRand ,13)=SigmaCopper ;
183

```

```

184 % R, L, C Values
185 InitialDesignTable(iRand,14)=L_nH;
186 InitialDesignTable(iRand,15)=RDC;
187 InitialDesignTable(iRand,16)=Rac;
188 InitialDesignTable(iRand,17)=Qac;
189 InitialDesignTable(iRand,18)=ErrorInL;
190 InitialDesignTable(iRand,19)=Cind_pF;
191
192 % Waveforms at The Inductor
193 InitialDesignTable(iRand,20)=V0;
194 InitialDesignTable(iRand,21)=IMaxAC;
195 InitialDesignTable(iRand,22)=I0DC;
196
197 % Inductor , Switch and Diode Loss
198 InitialDesignTable(iRand,23)=TotalACLoss;
199 InitialDesignTable(iRand,24)=LossDC;
200 InitialDesignTable(iRand,25)=LossDC+TotalACLoss;
201 InitialDesignTable(iRand,26)=PDiode_W;
202 InitialDesignTable(iRand,27)=PSwitch_W;
203 InitialDesignTable(iRand,28)=P_W;
204 InitialDesignTable(iRand,29)=TotalLossGlass;
205
206 % Circuit Efficiency and Inductor Power Density
207 InitialDesignTable(iRand,30)=CircuitEfficiencyGlass;
208 InitialDesignTable(iRand,31)=InductorPowerDensityWPmSq;
209
210 end
211
212 RandomSortedLossGlass=sortrows(InitialDesignTable,29);

```

```

213 dlmwrite('AllDesigns.txt', RandomSortedLossGlass, 'delimiter
      ', '\t', ...
214       'precision', 5);
215
216 toc
217
218 function [ scaleT, P_W, PDiode_W, PSwitch_W, L_H, Ton_s,
      Vswitch_V, Iswitch_A, Vdiode_V, Idiode_A, Vind_V, Iind_A,
      T_s] = ...
219 OptimizeT( Vin_V, Vled_V, Power_W, Freq_Hz, Coss_F, Cj_F,
      Cind_F, Rsw_Ohm, TranCRes_Ohm, DiodeDrop_V, DiodeCRes_Ohm
      )
220 % Inputs
221 % Vin_V – scalar – Input supply voltage [Volts]
222 % Vled_V – scalar – LED string voltage [Volts]
223 % Power_W – scalar – LED power delivery goal [Watts]
224 % Freq_Hz – scalar – Operating frequency goal [Hz]
225 % Cj_F – function – Incremental diode capacitance versus
      reverse voltage
226 % [Volts to Farads]
227 % Coss_F – function – Incremental transistor output
      capacitance versus
228 % drain source voltage [Volts to Farads]
229 % Cind_F – scalar – Inductor capacitance to ground [Farads
      ]
230 % Rsw_Ohm – scalar – Transistor on resistance [Ohms]
231 % TranCRes_Ohm – scalar – resistance in series with the
      FET capacitance [Ohms]
232 % DiodeDrop_V – scalar – diode voltage drop [Volts]

```

```

233 % DiodeCRes_Ohm – scalar – resistance in series with the
    diode capacitance [Ohms]
234 %
235 % Outputs
236 % scaleT – scalar – optimum scaling factor of the
    transistor die
237 % P_W – scalar – amount of power lost in both the diode
    and transistor
238 % PDiode_W – scalar – power loss in the diode
239 % PSwitch_W – scalar – power loss in the transistor
240 % L_H – scalar – required inductor value [Henries]
241 % Ton_s – scalar – on time [seconds]
242 % Vswitch_V – vector – switch drain voltage [Volts]
243 % Vdiode_V – vector – diode reverse voltage [Volts]
244 % Iind_A – matrix – inductor current – first column is
    inductive
245 % current , second column is capacitive current from Cind [
    Amperes]
246 % Idiode_A – matrix – inductor current – first column is
    forward
247 % current , second column is capacitive current from Cj [
    Amperes]
248 % Iswitch_A – matrix – switch current – first column is on
    -state
249 % current , second column is capacitive current from Coss [
    Amperes]
250 % T_s – vector – time [seconds]
251
252 [ scaleT ,P_W] = fminbnd(@(x) ScaleTLoss( Vin_V , Vled_V ,
    Power_W , Freq_Hz , Coss_F , Cj_F , Cind_F , Rsw_Ohm ,

```

```

TranCRes_Ohm , DiodeDrop_V , DiodeCRes_Ohm , x) ,0.01 ,10);
253 [~, PDiode_W , PSwitch_W , L_H , Ton_s , Vswitch_V , Iswitch_A ,
    Vdiode_V , Idiode_A , Vind_V , Iind_A , T_s] = ScaleTLoss(
    Vin_V , Vled_V , Power_W , Freq_Hz , Coss_F , Cj_F , Cind_F ,
    Rsw_Ohm , TranCRes_Ohm , DiodeDrop_V , DiodeCRes_Ohm , scaleT
    );
254
255 end
256
257 function [ P_W , PDiode_W , PSwitch_W , L_H , Ton_s , Vswitch_V ,
    Iswitch_A , Vdiode_V , Idiode_A , Vind_V , Iind_A , T_s] =
    ScaleTLoss( Vin_V , Vled_V , Power_W , Freq_Hz , Coss_F , Cj_F
    , Cind_F , Rsw_Ohm , TranCRes_Ohm , DiodeDrop_V ,
    DiodeCRes_Ohm , scaleT)
258 % ESTLOSSES Finds the losses total from scaling the
    transistor using the proper inductor.
259 %
260 % Inputs
261 % Vin_V – scalar – Input supply voltage [Volts]
262 % Vled_V – scalar – LED string voltage [Volts]
263 % Power_W – scalar – LED power delivery goal [Watts]
264 % Freq_Hz – scalar – Operating frequency goal [Hz]
265 % Cj_F – function – Incremental diode capacitance versus
    reverse voltage
266 % [Volts to Farads]
267 % Coss_F – function – Incremental transistor output
    capacitance versus
268 % drain source voltage [Volts to Farads]
269 % Cind_F – scalar – Inductor capacitance to ground [Farads
    ]

```

```

270 %   Rsw_Ohm – scalar – Transistor on resistance [Ohms]
271 %   TranCRes_Ohm – scalar – resistance in series with the
    FET capacitance [Ohms]
272 %   DiodeDrop_V – scalar – diode voltage drop [Volts]
273 %   DiodeCRes_Ohm – scalar – resistance in series with the
    diode capacitance [Ohms]
274 %   scaleT – scalar – amount the transistor die area is
    increased
275 %
276 %   Outputs
277 %   P_W – scalar – amount of power lost in both the diode
    and transistor
278 %   PDiode_W – scalar – power loss in the diode
279 %   PSwitch_W – scalar – power loss in the transistor
280 %   L_H – scalar – required inductor value [Henries]
281 %   Ton_s – scalar – on time [seconds]
282 %   Vswitch_V – vector – switch drain voltage [Volts]
283 %   Vdiode_V – vector – diode reverse voltage [Volts]
284 %   Iind_A – matrix – inductor current – first column is
    inductive
285 %   current , second column is capacitive current from Cind [
    Amperes]
286 %   Idiode_A – matrix – inductor current – first column is
    forward
287 %   current , second column is capacitive current from Cj [
    Amperes]
288 %   Iswitch_A – matrix – switch current – first column is on
    –state
289 %   current , second column is capacitive current from Coss [
    Amperes]

```

```

290 %   T_s – vector – time [seconds]
291
292 [ L_H, Ton_s, ~ ] = FindInductor(Vin_V, Vled_V, Power_W,
    Freq_Hz, @(Vds) Coss_F(Vds)*scaleT, Cj_F, Cind_F);
293 [ Vswitch_V, Iswitch_A, Vdiode_V, Idiode_A, Vind_V, Iind_A,
    T_s ] = SimulateWaveforms( Vin_V, Vled_V, Ton_s, L_H, @(
    Vds) Coss_F(Vds)*scaleT, Cj_F, Cind_F, Rsw_Ohm/ scaleT);
294 [PDiode_W, PSwitch_W] = EstLosses( Iswitch_A, Idiode_A, T_s,
    DiodeDrop_V, DiodeCRes_Ohm, Rsw_Ohm/ scaleT, TranCRes_Ohm
    );
295 P_W = PDiode_W + PSwitch_W;
296
297
298 end
299
300 function [ L_H, Ton_s, T_s ] = FindInductor( Vin_V, Vled_V,
    Power_W, Freq_Hz, Coss_F, Cj_F, Cind_F)
301 %FindInductor – This function gives you the inductance,
    diode scaling
302 %factor, and switch on–time necessary for the provided
    operating conditions
303 %
304 %   Inputs
305 %   Vin_V – scalar – Input supply voltage [Volts]
306 %   Vled_V – scalar – LED string voltage [Volts]
307 %   Power_W – scalar – LED power delivery goal [Watts]
308 %   Freq_Hz – scalar – Operating frequency goal [Hz]
309 %   Cj_F – function – Incremental diode capacitance versus
    reverse voltage
310 %   [Volts to Farads]

```

```

311 % Coss_F – function – Incremental transistor output
    capacitance versus
312 % drain source voltage [Volts to Farads]
313 % Cind_F – scalar – Inductor capacitance to ground [Farads
    ]
314 %
315 % Output
316 % L_H – scalar – required inductor value [Henries]
317 % T_s – scalar – cycle time [seconds]
318 % Ton_s – scalar – on time [seconds]
319
320 Cnode_F = @(V) (( Coss_F(V)+Cj_F(Vin_V–V)+Cind_F));
321
322 tRingScaled_s_rootH = RingTime( Vin_V , Vled_V , Cnode_F);
323
324 QSum_C = reimann( Cnode_F , 0 , Vin_V , 100);
325
326 L_H=800e–9;
327
328 Tgoal_s=1/Freq_Hz;
329 Igoal_A=Power_W / Vled_V;
330 Qtot_C=Igoal_A * Tgoal_s;
331
332 while 1==1
333     Ton_s=sqrt( Qtot_C / ( Vin_V^2/(2*L_H*Vled_V)–Vin_V/(2*L_H))
        );
334     Ipk_A=Ton_s*( Vin_V–Vled_V )/L_H;
335     Toff_s=Ipk_A*L_H/ Vled_V;
336     Trise_s=QSum_C/ Ipk_A;
337     Tring_s=sqrt( L_H)*tRingScaled_s_rootH;

```



```

338     T_s = Ton_s+Toff_s+Trise_s+Tring_s;
339     scaleT = T_s/Tgoal_s;
340     if (0.995 < scaleT && scaleT < 1.05)
341         break;
342     else
343         L_H=L_H/scaleT;
344     end
345 end
346
347
348 end
349
350
351 function [ Vswitch_V , Iswitch_A , Vdiode_V , Idiode_A , Vind_V ,
        Iind_A , T_s ] = ...
352 SimulateWaveforms( Vin_V , Vled_V , Ton_s , L_H , Coss_F , Cj_F ,
        Cind_F , Rsw_Ohm)
353 %SimulateWaveforms Simulate a complete single cycle of the
        circuit
354 %
355 %   Inputs
356 %   Vin_V – scalar – Input supply voltage [Volts]
357 %   Vled_V – scalar – LED string voltage [Volts]
358 %   Ton_s – scalar – on time [nanoseconds]
359 %   L_H – scalar – Inductor inductance [nanoHenries]
360 %   Coss_F – function – Incremental transistor output
        capacitance versus
361 %   drain source voltage [Volts to Farads]
362 %   Cj_F – function – Incremental diode capacitance versus
        reverse voltage

```

```

363 %    [ Volts to Farads]
364 %    Cind_F – scalar – Inductor capacitance to ground [Farads
    ]
365 %    Rsw_Ohm – scalar – Transistor on resistance [Ohms]
366 %
367 %    Outputs
368 %    V_switch_V – vector – switch drain voltage [Volts]
369 %    V_diode_V – vector – diode reverse voltage [Volts]
370 %    I_ind_A – matrix – inductor current – first column is
    inductive
371 %    current , second column is capacitive current from Cind [
    Amperes]
372 %    I_diode_A – matrix – inductor current – first column is
    forward
373 %    current , second column is capacitive current from Cj [
    Amperes]
374 %    I_switch_A – matrix – switch current – first column is
    on–state
375 %    current , second column is capacitive current from Coss [
    Amperes]
376 %    T_s – vector – time [seconds]
377 %    Vzvs – scalar – voltage at which switching is occuring [
    Volts]
378
379 Cnode_F = @(V) (( Coss_F(V)+Cj_F(Vin_V–V)+Cind_F));
380
381
382 [ Vring_V , Iring_A , Tring_s ] = SimulateRing( Vin_V , Vled_V ,
    Cnode_F , L_H , 0);
383

```

```

384 [ Vdisc_V , IdiscR_A , Idisc_A , Tdisc_s ] =SimulateDisc( Vin_V
    , Vled_V , Cnode_F, L_H, Rsw_Ohm, Vring_V(end) , Iring_A(
    end) , Tring_s(end));
385
386 [ Von_V, Ion_A , Ton_s ] = SimulateOn( Vin_V , Vled_V , Ton_s ,
    L_H, Idisc_A(end) , Tdisc_s(end));
387
388 [ Vrise_V , Irise_A , Trise_s ] = SimulateRise( Vin_V , Vled_V ,
    Cnode_F, L_H, Ion_A(end) , Ton_s(end));
389
390 [ Voff_V , Ioff_A , Toff_s ] = SimulateOff( Vin_V , Vled_V , L_H
    , Irise_A(end) , Trise_s(end));
391
392
393
394 Vswitch_V = [ Vring_V; Vdisc_V(2:end); Von_V; Vrise_V(2:end);
    Voff_V ];
395 Vdiode_V = Vin_V-Vswitch_V;
396 Vind_V = Vin_V-Vled_V-Vswitch_V;
397
398
399 ICind_A = -Cind_F./( Cnode_F(Vswitch_V)).*[ Iring_A; Idisc_A
    (2:end); 0 ; 0 ; Irise_A(2:end); 0 ;0];
400 ICswitch_A = Coss_F(Vswitch_V)./( Cnode_F(Vswitch_V)).*[
    Iring_A; Idisc_A(2:end); 0 ; 0 ; Irise_A(2:end); 0 ; 0];
401 ICdiode_A = Cj_F(Vdiode_V)./( Cnode_F(Vswitch_V)).*[ Iring_A;
    Idisc_A(2:end); 0 ; 0 ; Irise_A(2:end); 0 ; 0];
402
403 T_s = [Tring_s; Tdisc_s(2:end); Ton_s; Trise_s(2:end);
    Toff_s ];

```

```

404
405 Iind_A = [Iring_A' Idisc_A(2:end)' Ion_A' Irise_A(2:end)'
           Ioff_A' ; ICind_A']';
406 Iswitch_A = [zeros(size(Iring_A')) IdiscR_A(2:end)' Ion_A'
               zeros(size([Irise_A(2:end)' Ioff_A'])) ; ICswitch_A']';
407 Idiode_A = [zeros(size([Iring_A' Idisc_A(2:end)' Ion_A'
                           Irise_A(2:end)'])) Ioff_A' ; ICdiode_A']';
408
409 end
410
411 function [ PDiode_W, PSwitch_W ] = EstLosses( Iswitch_A ,
         Idiode_A , T_s , DiodeDrop_V , DiodeCRes_Ohm , TranRon_Ohm ,
         TranCRes_Ohm )
412 % ESTLOSSES Find the losses in the devices given the current
         waveforms
413 %
414 % Inputs
415 % I_switch_A – matrix – switch current – first column is
         on–state
416 % current , second column is capacitive current from Coss [
         Amperes]
417 % I_diode_A – matrix – inductor current – first column is
         forward
418 % current , second column is capacitive current from Cj [
         Amperes]
419 % T_s – vector – time [seconds]
420 % DiodeDrop_V – scalar – diode voltage drop [Volts]
421 % DiodeCRes_Ohm – scalar – resistance in series with the
         diode capacitance [Ohms]
422 % TranRon_Ohm – scalar – FET on resistance [Ohms]

```

```

423 %   TranCRes_Ohm – scalar – resistance in series with the
      FET capacitance [Ohms]
424 %
425 %   Outputs
426 %   PDiode_W – scalar – power loss in the diode
427 %   PSwitch_W – scalar – power loss in the transistor
428
429
430
431 DT_s=T_s(2:end) – T_s(1:end-1);
432
433 PswitchCap_W = ((Iswitch_A(2:end,2))'.^2)*DT_s*TranCRes_Ohm)
      /T_s(end);
434 PswitchCond_W = (((Iswitch_A(1:end-1,1))'.^2+(Iswitch_A(2:
      end,1))'.*(Iswitch_A(1:end-1,1))'+(Iswitch_A(2:end,1))
      ').^2)/3*DT_s*TranRon_Ohm)/T_s(end);
435 PDiodeDrop_W = ((Idiode_A(2:end,1))'+(Idiode_A(1:end-1,1))')
      *DT_s*DiodeDrop_V/2/T_s(end);
436 PDiodeCap_W = ((Iswitch_A(2:end,2))'.^2)*DT_s*DiodeCRes_Ohm)
      /T_s(end);
437
438 PSwitch_W = PswitchCap_W + PswitchCond_W;
439 PDiode_W = PDiodeDrop_W + PDiodeCap_W;
440
441
442 end
443
444
445 function [ Coss ] = MITHEMT_Coss( Vds )

```

```

446 %This function shows the voltage/capacitance relationship
      for an MIT FET
447 Coss = (-8e-5*Vds.^2+0.0074*Vds+7.118)*1e-11;
448 end
449
450
451 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
452 % This script filters the designs generated in the first
      step. All generated designs have been saved in the file "
      AllDesigns.txt". Here, all of those designs are checked
      for the filtering process. First the hard requirements
      are checked. Next the Pareto-Filtering process is used to
      keep only the superior designs. See the filtering
      process in "Chapter 4: Inductor Design" of the thesis.
453 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
454
455 clear all;
456 close all;
457
458 load('AllDesigns.txt')
459 Sorted=AllDesigns;
460
461 BudgetVectStp1=2.5-Sorted(:,28); % Budget loss for the
      magnetics considering a total loss budget of 2.5 Watts.
462 MinFeatureSizeStp1=Sorted(:,10); % Minimum feature size of
      the inductor
463 InductorLossStp1=Sorted(:,25); % AC and DC loss for the
      inductor
464 LossVectStp1=Sorted(:,29); %Total circuit loss

```

```

465 ErrorInLStp1=abs(Sorted(:,18)); %Error in calculating
    inductor
466
467 HRStep=0; % A counter for the designs that pass the hard
    requirements
468
469 % The following loop checks that the designs satisfy the
    hard requirements and have numerically converged in
    calculating the inductor value and losses.
470
471 for i=1:size(LossVectStp1)
472     if ( (InductorLossStp1(i)<(1.5*BudgetVectStp1(i)) )
        &&...
473         (ErrorInLStp1(i)<5) ) &&...
474         (BudgetVectStp1(i)<2.5)
475         % (MinFeatureSizeStp1(i)>75e-6) )
476         HRStep=HRStep+1;
477         PassedHardReq(HRStep,:)=Sorted(i,:); % Only the
            designs that pass the hard requirements are saved
            in "PassedHardReq"
478     end
479 end
480
481 BudgetVect=2.5-PassedHardReq(:,28);
482 MinFeatureSize=PassedHardReq(:,10);
483 InductorLoss=PassedHardReq(:,29);
484 LossVect=PassedHardReq(:,18);
485 FreqMHz=PassedHardReq(:,1); % Operating Frequency [MHz]
486 RoVect=PassedHardReq(:,4); % Outer Radius [mm]
487 ConvEfficiency=PassedHardReq(:,30);

```

```

488
489 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
490 % The following loop is for the Pareto-Filtering process.
491 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
492
493 for i=1:HRStep
494     jStep=0;
495
496     for j=[1:(i-1),(i+1):HRStep]
497
498         if ( (LossVect(i)>LossVect(j)) &&...
499             (RoVect(i)>RoVect(j)) ) &&...
500             (MinFeatureSize(i)<MinFeatureSize(j)) )
501             jStep=jStep+1;
502         end
503     end
504
505     if( (jStep == 0) )
506
507         kStep=kStep+1;
508         Filtered(kStep,:)=PassedHardReq(i,:);
509         % OptMu(kStep)=muVect(i); ADD THIS LINE FOR RANDOM
510         % MU
511
512     end
513
514 end
515 dlmwrite('FilteredDesigns.txt', Filtered, 'delimiter', '\t',
516         ...

```



```

516     'precision', 5); % Saving the filtered results in a file.
517
518 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
519 % Here, the filtered designs are divided into 3 categories
    based on the minimum feature size: 1) Between 90 um to
    110 um, 2) between 110 um to 130 um, 3) between 130 um to
    170 um
520 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
521
522 FirstMFS=110e-6;
523 SecondMFS=130e-6;
524
525 AboveSecondStep=0;
526 BelowFirstStep=0;
527 BtwFirstandSecondStep=0;
528
529 for i=1:size(Filtered(:,10),1)
530     if Filtered(i,10)<FirstMFS
531         BelowFirstStep=BelowFirstStep+1;
532         BelowFirst(BelowFirstStep,:)=Filtered(i,:);
533     else
534         if Filtered(i,10)<SecondMFS
535             BtwFirstandSecondStep=BtwFirstandSecondStep+1;
536             BtwFirstandSecond(BtwFirstandSecondStep,:)=
                Filtered(i,:);
537         else
538
539             AboveSecondStep=AboveSecondStep+1;
540             AboveSecond(AboveSecondStep,:)=Filtered(i,:);
541         end

```

```

542
543     end
544 end
545
546 %
547 figure ;
548 plot( BelowFirst(:,4), BelowFirst(:,29), 'k^', BtwFirstandSecond
        (:,4), BtwFirstandSecond(:,29), 'rs', AboveSecond(:,4),
        AboveSecond(:,29), '.b' );
549 title( 'Min Feature Size: Black 90–110 um; Red: 110–130 um;
        Blue: 130–170 um' );
550 xlabel( 'Ro[mm]' );
551 ylabel( 'Circuit Loss [W]' );
552 grid on;
553 grid(gca, 'minor');
554
555 %
556 figure ;
557 plot( BelowFirst(:,4), BelowFirst(:,1), 'k^', BtwFirstandSecond
        (:,4), BtwFirstandSecond(:,1), 'rs', AboveSecond(:,4),
        AboveSecond(:,1), '.b' );
558 title( 'MinFeatSize black 90–110 um; Red: 110–130 um; Blue:
        130–170 um' );
559 xlabel( 'Ro[mm]' );
560 ylabel( 'Frequency [MHz]' );
561 grid on;
562 grid(gca, 'minor');
563
564 BelowFirst(:,4);
565 %

```

```

566 figure ;
567 plot ( BelowFirst (: ,4) ,BelowFirst (: ,11) , 'k^' ,BtwFirstandSecond
        (: ,4) ,BtwFirstandSecond (: ,11) , 'rs' ,AboveSecond (: ,4) ,
        AboveSecond (: ,11) , '.b' );
568 title ( 'MinFeatSize black 90–110; red: 110–130; blue: 130–170
        um' );
569 xlabel ( 'Ro[mm]' );
570 ylabel ( 'ScaleT' );
571 grid on ;
572 grid ( gca , 'minor' );
573
574 figure ;
575 plot ( BelowFirst (: ,30) ,BelowFirst (: ,31) , 'k^' ,
        BtwFirstandSecond (: ,30) ,BtwFirstandSecond (: ,31) , 'rs' ,
        AboveSecond (: ,30) ,AboveSecond (: ,31) , '.b' );
576 title ( 'MinFeatSize black 90–110; red: 110–130; blue: 130–170
        um' );
577 xlabel ( 'Converter Efficiency' );
578 ylabel ( 'Inductor Power Density [W/m^2]' );
579 grid on ;
580 grid ( gca , 'minor' );

```



# Appendix B

## Four Components of Inductance

```
1 % LAP : Equivalent inductance for poloidal magnetic fields
   inside air
2 % LAT : Equivalent inductance for toroidal magnetic fields
   inside air
3 % LWP : Equivalent inductance for poloidal magnetic fields
   inside the winding
4 % LWT : Equivalent inductance for toroidal magnetic fields
   inside the winding
5 % Ro : Outer radius
6 % Ri : Inner radius
7 % T : Conductor thickness
8 % D : Inductor Height
9 % Freq: Frequency of calculating the inductance
10 % sigma: Conductivity of Copper
11
12 omega=2*pi*Freq;
13 Ralpha=(1/2)*sqrt(2)*sqrt(omega*mu0*sigma)
14 LAP= (1/2)*(Ro+Ri)*mu0*(log((8*(Ro+Ri))/(Ro-Ri))-2);
15 LAT=(1/2)*mu0*N^2*(-log(Ri+T)+log(Ro-T))*(D)/pi;
```

16 LWP=0;

17 LWT=2\*((1/128)\*mu0\*N^2\*(2\*pi\*Ri-N\*Delta)\*(exp(4\*Ralpha\*T)\*  
cos(Ralpha\*T)^2+exp(4\*Ralpha\*T)-8\*cos(Ralpha\*T)\*sin(  
Ralpha\*T)\*exp(2\*Ralpha\*T)-cos(Ralpha\*T)^2-1+exp(4\*Ralpha\*  
T)\*sin(Ralpha\*T)^2-sin(Ralpha\*T)^2)\*exp(-2\*Ralpha\*T)\*D/(  
pi^2\*(Ri+T)^2\*(sinh(Ralpha\*T)^2\*cos(Ralpha\*T)^2+cosh(  
Ralpha\*T)^2\*sin(Ralpha\*T)^2)\*Ralpha)+(1/128)\*mu0\*N^2\*(2\*  
pi\*Ro-N\*Delta)\*(exp(4\*Ralpha\*T)\*cos(Ralpha\*T)^2+exp(4\*  
Ralpha\*T)-8\*cos(Ralpha\*T)\*sin(Ralpha\*T)\*exp(2\*Ralpha\*T)-  
cos(Ralpha\*T)^2-1+exp(4\*Ralpha\*T)\*sin(Ralpha\*T)^2-sin(  
Ralpha\*T)^2)\*exp(-2\*Ralpha\*T)\*D/(pi^2\*(Ro-T)^2\*(sinh(  
Ralpha\*T)^2\*cos(Ralpha\*T)^2+cosh(Ralpha\*T)^2\*sin(Ralpha\*T  
)^2)\*Ralpha)-(1/16)\*mu0\*N^2\*(-exp(4\*Ralpha\*T)+4\*cos(  
Ralpha\*T)\*sin(Ralpha\*T)\*exp(2\*Ralpha\*T)+1)\*exp(-2\*Ralpha\*  
T)\*(-log(Ri+T)+log(Ro-T))/(pi\*(sinh(Ralpha\*T)^2\*cos(  
Ralpha\*T)^2+cosh(Ralpha\*T)^2\*sin(Ralpha\*T)^2)\*Ralpha));