

# EEN1047

# CONTROL SYSTEMS ANALYSIS

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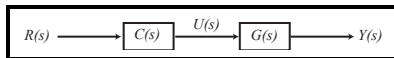
Semester 1 2024-2025

# Section 4

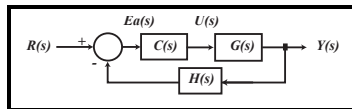
## Sensitivity

## 4.1 Linear Feedback Control Systems

- A **Control System** is a set of interconnected systems designed to provide a desired system response.
- **Open Loop System**



- Has no feedback.
  - The output is generated directly by the input.
- **Closed Loop System**



- Has a feedback loop; is error based.
  - Compares the output with the desired response.
  - Often  $H(s) = 1$ , called a **unity feedback** system.
  - Feedback reduces the **sensitivity** of the control system to model inaccuracies and disturbances.

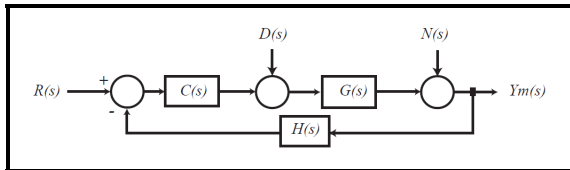
## 4.2 A Benefit of Feedback

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- Feedback facilitates the reduction of **System Sensitivity**.
  - A process, represented by a transfer function  $G(s)$ , undergoes changes over time due to aging and/or variations in its environment.
  - The original transfer function will give an inaccurate result in an **open-loop** configuration.
  - A **closed-loop** system will measurement changes in the output due to the changes in  $G(s)$  and will attempt to correct the output.
  - The degree to which changes in system parameters affect the transfer function is called **sensitivity**.
  - If changes in system parameters have no effect on the transfer function, the system is said to have zero sensitivity (ideal).
  - The greater the system sensitivity, the larger the effect that system parameter changes will have on the transfer function.

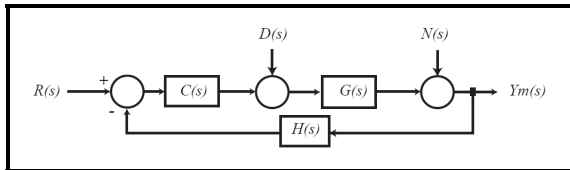
## 4.3 Disturbance Signals

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- Note that we have assumed that there is no pre-conditioning filter  $P(s)$  in the system.
- There are two **signals** indicated in the model.
  - $D(s)$  is a disturbance that affects the input of the process.
  - $N(s)$  is a disturbance that affects the output of the process, it is usually a measurement noise introduced by the output sensor.

## 4.4 Open Loop Variations

- In order to examine the effects of parameter variations on the transfer function, we will assume that  $D(s) = N(s) = 0$ .
- As the system is linear, for simplicity, assume that  $C(s) = 1$ .
- Taking the open-loop case and letting  $\Delta$  denote 'a change in':

### Open-loop

$$Y(s) = G(s).R(s)$$

$$G_{alt}(s) = G(s) + \Delta G(s)$$

$$\Rightarrow Y_{new}(s) = Y(s) + \Delta Y(s) = [G(s) + \Delta G(s)].R(s)$$

$$\Delta Y(s) = \Delta G(s).R(s)$$

- The change in output is directly related to the change in the process; if there is a big change in the process, there will be a big change in the output (may be undesirable!).

## 4.5 Closed Loop Variations

- If there is a change in a model  $G(s)$  that is in a closed-loop configuration:

### Closed-loop

$$Y(s) = \frac{G(s)}{1 + GH(s)} \cdot R(s)$$

$$G_{alt}(s) = G(s) + \Delta G(s)$$

$$Y_{new} = Y(s) + \Delta Y(s) = \frac{G(s) + \Delta G(s)}{1 + GH(s) + \Delta G(s)H(s)} \cdot R(s)$$

$$\Delta Y(s) = \left[ \frac{G(s) + \Delta G(s)}{1 + GH(s) + \Delta GH(s)} - \frac{G(s)}{1 + GH(s)} \right] \cdot R(s)$$

$$\Delta Y(s) = \frac{\Delta G(s)}{(1 + GH(s))(1 + GH(s) + \Delta GH(s))} \cdot R(s)$$

$$\Delta Y(s) \approx \frac{\Delta G(s)}{[1 + GH(s)]^2} R(s) \quad \text{If } GH(s) \gg \Delta GH(s)$$



## 4.5 Closed Loop Variations

- The change in output depends on the change in the model **and** on  $G(s)$  and  $H(s)$ .

### Closed-loop

$$Y(s) = \frac{G(s)}{1 + GH(s)} \cdot R(s)$$

$$G_{alt}(s) = G(s) + \Delta G(s)$$

$$Y_{new} = Y(s) + \Delta Y(s) = \frac{G(s) + \Delta G(s)}{1 + GH(s) + \Delta G(s)H(s)} \cdot R(s)$$

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## 4.6 Closed-Loop Variations - Equation

### Closed-loop

$$\Delta Y(s) \approx \frac{\Delta G(s)}{[1 + GH(s)]^2} \cdot R(s)$$

- Comparing the open-loop and closed-loop expressions for the change in output, it can be seen that the closed-loop expression features elements of the original system dynamics.
- If the expression  $[1 + GH] > 1$ , then the effect of the change in  $G(s)$  is reduced.
- If  $[1 + GH] > 1$ , then  $[1 + GH]^2 \gg 1$  and the reduction effect is greater.
- This factor *is* usually much greater than unity in most practical cases.
- Thus, the feedback loop (even with  $H(s) = 1$ ) reduces the effect of changes in system dynamics on the output.

## 4.7 Parameter Variations - Example Changes

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- Take an example of a first order motor model with gain  $K_m = 20$  and time constant  $\tau_m = 0.6$  (s).

$$G_m(s) = \frac{K_m}{\tau_m s + 1} = \frac{20}{0.6s + 1}$$

- Assume that  $C(s) = 1$  and  $H(s) = 0.45$  in the closed-loop configuration:
  - Calculate the open-loop steady-state gain of the system:

$$G_m(0) = 20$$

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  - Calculate the open-loop steady-state gain of the system:

$$G_m(0) = 20$$

- Calculate the CLTF of the system:

$$T(s) = G_{CL}(s) = \frac{G(s)}{1 + GH(s)} = \frac{20}{0.6s + 10}$$

- Calculate the closed-loop steady-state gain of the system:

$$T(0) = G_{CL}(0) = \frac{20}{10} = 2$$

## 4.8 Parameter Variations - Example Changes

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- It is now assumed that some change has occurred in the motor model; the effect of this change is that the motor gain value changes to  $K_m^* = 15$ , i.e. a 25% reduction.
  - Calculate the open-loop steady-state gain of the new system:

$$G_m^*(0) = 15 \quad \text{versus} \quad G_m(0) = 20$$

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$$G_m^*(0) = 15 \quad \text{versus} \quad G_m(0) = 20$$

- Calculate the CLTF of the changed system:

$$T^*(s) = G_{CL}^*(s) = \frac{G^*(s)}{1 + G^*H(s)} = \frac{15}{0.6s + 7.75}$$

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- Calculate the CLTF of the changed system:

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- Calculate the closed-loop steady-state gain of the system:

$$T^*(0) = G_{CL}^*(0) = \frac{15}{7.75} = 1.9355 \quad \text{versus} \quad T(0) = 2$$

- The closed-loop system does not experience a change of 25% - this is due to feedback.

## 4.9 Sensitivity - Definition

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- **Sensitivity** is defined as the ratio of the percentage change in the function to the percentage change in the parameter as the percentage change in the parameter approaches zero.



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- The sensitivity function of a function  $F$  to a change in parameter  $p$  is:

### Definition

$$\begin{aligned} S_p^F &= \lim_{\Delta p \rightarrow 0} \frac{\% \text{ change in } F}{\% \text{ change in } p} \\ &= \lim_{\Delta p \rightarrow 0} \frac{\Delta F / F}{\Delta p / p} = \lim_{\Delta p \rightarrow 0} \frac{p \Delta F}{F \Delta p} \end{aligned}$$

$$S_p^F = \frac{p}{F} \frac{\delta F}{\delta p}$$

## 4.10 System Sensitivity - Definition

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- The system sensitivity of a CLTF  $T$  to a change in process  $G$  is:

### Definition

$$\begin{aligned} S_G^T &= \lim_{\Delta G \rightarrow 0} \frac{\Delta T / T}{\Delta G / G} \\ &= \lim_{\Delta G \rightarrow 0} \frac{G \Delta T}{T \Delta G} \end{aligned}$$

$$S_G^T = \frac{G}{T} \frac{\delta T}{\delta G}$$

## 4.11 System Sensitivity - Expression

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- Taking the general closed-loop system with  $P(s) = C(s) = 1$  and  $N(s), D(s) = 0$ :

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### General Expression

$$\begin{aligned}T(s) &= \frac{G(s)}{1 + GH(s)} \\S_G^T &= \frac{G}{T} \frac{\delta T}{\delta G} = \frac{G}{\frac{G}{1+GH}} \cdot \frac{\delta G (1 + GH)^{-1}}{\delta G} \\&= \frac{G (1 + GH)}{G} \cdot \frac{(1 + GH) \cdot 1 - GH}{(1 + GH)^2} \\&= \frac{G (1 + GH)}{G} \cdot \frac{1}{(1 + GH)^2} \\&= \frac{1}{1 + GH}\end{aligned}$$

## 4.12 Sensitivity - CLTF to H

- For the same closed-loop configuration, the sensitivity of  $T(s)$  to changes in  $H(s)$  can be calculated:

### General Expression

$$\begin{aligned}T(s) &= \frac{G(s)}{1 + GH(s)} \\S_H^T &= \frac{H \delta T}{T \delta H} = \frac{H}{\frac{G}{1+GH}} \cdot \frac{\delta G (1 + GH)^{-1}}{\delta H} \\&= \frac{H(1 + GH)}{G} \cdot \left( -G(1 + GH)^{-2} \cdot G \right) \\&= \frac{H(1 + GH)}{G} \cdot \frac{-G^2}{(1 + GH)^2} \\&= \frac{-GH}{1 + GH}\end{aligned}$$

## 4.13 Sensitivity - CLTF to p

- The sensitivity of the closed-loop system to a particular parameter of the open-loop system can be defined using the chain rule:

Sensitivity to parameter  $\alpha$

$$\begin{aligned} S_{\alpha}^T &= \frac{\alpha}{T} \frac{\delta T}{\delta \alpha} \\ &= \frac{G}{T} \frac{\alpha}{G} \cdot \frac{\delta T}{\delta G} \frac{\delta G}{\delta \alpha} \\ &= \frac{G}{T} \frac{\delta T}{\delta G} \cdot \frac{\alpha}{G} \frac{\delta G}{\delta \alpha} \\ &= S_G^T S_{\alpha}^G \end{aligned}$$

- Even if the chain rule is not used, the same result should be found using the general definition

## 4.14 Sensitivity Definition Example

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- Recall the first order motor model Section 4.7 with gain  $K_m$  and time constant  $\tau_m$ . Assume that  $C(s) = 1$  and  $H(s) = K_h$  in the closed-loop configuration.

$$G_m(s) = \frac{K_m}{\tau_m s + 1}$$



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- Recall the first order motor model Section 4.7 with gain  $K_m$  and time constant  $\tau_m$ . Assume that  $C(s) = 1$  and  $H(s) = K_h$  in the closed-loop configuration.

$$G_m(s) = \frac{K_m}{\tau_m s + 1}$$

### Example

$$\begin{aligned} T(s) = G_{CL} &= \frac{K_m}{\tau_m s + 1 + K_m K_h} \\ S_{K_m}^T &= \frac{K_m}{T} \frac{\delta T}{\delta K_m} \\ &= \frac{K_m}{\frac{K_m}{\tau_m s + 1 + K_m K_h}} \cdot \left[ \frac{(\tau_m s + 1 + K_m K_h) \cdot 1 - K_m \cdot K_h}{(\tau_m s + 1 + K_m K_h)^2} \right] \\ &= \frac{\tau_m s + 1}{\tau_m s + 1 + K_m K_h} \end{aligned}$$

## 4.15 Sensitivity Example - Chain Rule

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- The sensitivity function can also be calculated using the chain rule representation.

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### Example

$$\begin{aligned}S_{K_m}^T &= S_G^T \cdot S_{K_m}^G \\&= \frac{1}{1 + GH} \cdot \frac{K_m}{G} \cdot \frac{\delta G}{\delta K_m} \\&= \frac{\tau_m s + 1}{\tau_m s + 1 + K_m K_h} \cdot \frac{K_m}{\frac{K_m}{\tau_m s + 1}} \cdot \frac{1}{\tau_m s + 1} \\&= \frac{\tau_m s + 1}{\tau_m s + 1 + K_m K_h} \cdot (\tau_m s + 1) \cdot \frac{1}{\tau_m s + 1} \\&= \frac{\tau_m s + 1}{\tau_m s + 1 + K_m K_h}\end{aligned}$$

## 4.16 Sensitivity Example with Values

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- Checking what this means with numerical values,  $\Delta K_m = 25\%$ ,  $\tau = 0.6$  s,  $K_h = 0.45$ :

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### Example

$$\begin{aligned} S_{K_m}^T &= \frac{\tau_m s + 1}{\tau_m s + 1 + K_m K_h} \\ &= \frac{0.6s + 1}{0.6s + 1 + 0.45(15)} \\ &= \frac{1}{7.75} \Big|_{s=0} = 0.129 \\ S_{K_m}^T &= \lim_{\Delta K_m \rightarrow 0} \frac{\% \text{ change in } T}{\% \text{ change in } K_m} \\ &= \frac{\frac{2 - 1.9355}{2} * 100}{25} \quad (\text{from earlier}) \\ &= \frac{3.225}{25} = 0.129 \end{aligned}$$