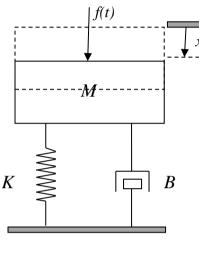
# 4. State-space representation

#### 4.1 Introduction

- When the differential equations governing the system are linear, the model can be described in terms of a Laplace transfer function.
- Consider for example the spring-mass damper system:



Physical model

$$M\frac{d^2x}{dt^2} + B\frac{dx}{dt} + Kx = f(t)$$

$$G(s) = \frac{X(s)}{F(s)} = \frac{1}{Ms^2 + Bs + K}$$

- While transfer functions are compact and have several advantages in relation to analysis of dynamical systems, they also have a number of weaknesses as follows:
  - They do not handle initial conditions (assumed to be zero).
  - Information about internal variables is lost ( $\frac{dx}{dt}$  in the case of the above example).
  - For general *m*-input, *p*-output systems, we would need a total of *m* x *p* transfer functions to fully describe the system.
- An alternative model representation, known as a state-space model, overcomes these weaknesses.
- The basic idea behind state-space modelling is to write down a set of first-order differential equations in terms of the system state(s) and input(s).

• **Example 4.1:** Develop a state-space model for the second-order differential equation model of the spring-mass damper system:

$$M\frac{d^2x}{dt^2} + B\frac{dx}{dt} + Kx = f(t)$$

#### **Solution**

We proceed as follows:

Firstly we have a **second-order** differential equation; hence we define two states  $x_1$  and  $x_2$ :

$$x_1 = x$$
,  $x_2 = \frac{dx}{dt}$ 

When we do it this way we get the CONTROLLABLE CANONICAL FORM state-space model.

We then obtain expressions for  $\frac{dx_1}{dt}$  and  $\frac{dx_2}{dt}$ :

$$\frac{dx_1}{dt} = \frac{dx}{dt} \qquad \frac{dx_2}{dt} = \frac{d^2x}{dt^2} = \frac{1}{M} \left( f(t) - B \frac{dx}{dt} - Kx \right)$$

Note that the latter expression is obtained from the original mathematical model.

We can rewrite these equations in terms of the states  $x_1$  and  $x_2$  only, by replacing x and  $\frac{dx}{dt}$  with their state equivalent. Hence:

$$\frac{dx_1}{dt} = x_2 \qquad \frac{dx_2}{dt} = \frac{1}{M} (f(t) - Bx_2 - Kx_1)$$

Now, we combine these into matrix form as follows:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{K}{M} & -\frac{B}{M} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{M} \end{bmatrix} f(t)$$

Finally, let us define the output as y = x. Hence  $y = x_I$  giving:

$$[y] = [1 \quad 0] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + [0] f(t) \Rightarrow [y] = [1 \quad 0] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

Our state-space model is expressed, in full, as:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{K}{M} & -\frac{B}{M} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{M} \end{bmatrix} f(t)$$

$$\begin{bmatrix} y \end{bmatrix} = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

### 4.2 Formal definitions

- The commonly used terms associated with state-space representation are as follows:
- **State** the state of a dynamic system is the smallest set of variables (called state variables) such that knowledge of these variables at  $t = t_0$ , together with knowledge of the input for  $t \ge t_0$ , completely determines the behaviour of the system for  $t \ge t_0$ .
- **State variables** the variables that make up the state as defined above.
- **State vector** when there is more than one state variable, they are normally collected together into a vector called a state vector.
- **State-space** the *n*-dimensional state vector can be viewed as a point moving around in *n*-dimensional space. This *n*-dimensional space is known as state-space.

# **General state-space form**

• The dynamics of a general  $n^{th}$  order linear dynamical system, with m inputs, is completely described by a  $n^{th}$  order state-space equation of the form:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} & \cdots & a_{1n} \\ a_{21} & a_{22} & \cdots & a_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ a_{n1} & a_{n2} & \cdots & a_{nn} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} + \begin{bmatrix} b_{11} & \cdots & b_{1m} \\ b_{21} & \cdots & b_{2m} \\ \vdots & \ddots & \vdots \\ b_{n1} & \cdots & b_{nm} \end{bmatrix} \begin{bmatrix} u_1 \\ \vdots \\ u_m \end{bmatrix}$$

$$\equiv \frac{d\mathbf{x}}{dt} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$$
 state equation

with a set of initial conditions (one for each state):

$$\mathbf{x}(0) = \begin{bmatrix} x_1(0) \\ x_2(0) \\ \vdots \\ x_n(0) \end{bmatrix} = \mathbf{x_0}$$
 initial conditions

The model output(s) are given by a linear combination of the states and the inputs. Given p outputs, we obtain:

$$\begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_p \end{bmatrix} = \begin{bmatrix} c_{11} & c_{12} & \cdots & c_{1n} \\ c_{21} & c_{22} & \cdots & c_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ c_{p1} & c_{p2} & \cdots & c_{pn} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} + \begin{bmatrix} d_{11} & \cdots & d_{1m} \\ d_{21} & \cdots & d_{2m} \\ \vdots & \ddots & \vdots \\ d_{p1} & \cdots & d_{pm} \end{bmatrix} \begin{bmatrix} u_1 \\ \vdots \\ u_m \end{bmatrix}$$

$$\equiv$$
  $\mathbf{y} = \mathbf{C}\mathbf{x} + \mathbf{D}\mathbf{u}$  output equation

Together, these two equations describe the state-space model of a system.

$$\frac{d\mathbf{x}}{dt} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u} \qquad , \mathbf{x}(0) = \mathbf{x}_0$$
$$\mathbf{y} = \mathbf{C}\mathbf{x} + \mathbf{D}\mathbf{u}$$

The matrices A, B, C and D are called the state matrix, input matrix, output matrix and direct transmission matrix respectively:

A - state matrix (n x n)
B - input matrix (n x m)
C - output matrix (p x n)
D - direct transmission matrix (p x m)

## 4.3 State - space representations are not unique

State-space representations are NOT unique.

Consider the following system

$$\frac{d^2y(t)}{dt^2} + 4\frac{dy(t)}{dt} + 3y(t) = 2f(t)$$

# Controllable canonical form state-space representation

Form the transfer function

$$G(s) = \frac{Y(s)}{F(s)} = \frac{2}{s^2 + 4s + 3}$$

Let  $x_{1c}(t) = y(t)$  and  $x_{2c}(t) = \frac{dy(t)}{dt}$ .

One needs two equations – one for the time derivative of state 1 and one for the time derivative of state 2.

$$\frac{dx_{1c}}{dt} = \frac{dy(t)}{dt} = x_{2c}$$

$$\frac{d^2y}{dt^2} + 4\frac{dy}{dt} + 3y = 2f$$
$$\frac{d^2y}{dt^2} = -4\frac{dy}{dt} - 3y + 2f$$

Now put in the states

$$\frac{d^2y}{dt^2} = \frac{dx_{2c}}{dt} = -4x_{2c} - 3x_{1c} + 2f$$

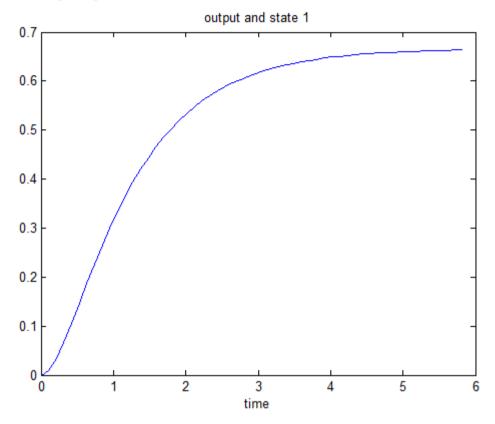
Put in matrix formation

$$\frac{d}{dt} \begin{bmatrix} x_{1c}(t) \\ x_{2c}(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -3 & -4 \end{bmatrix} \begin{bmatrix} x_{1c}(t) \\ x_{2c}(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 2 \end{bmatrix} f(t)$$

The output is y(t) which is the first state

$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_{1c}(t) \\ x_{2c}(t) \end{bmatrix}$$

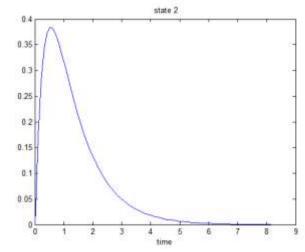
The unit-step response is as follows



Suppose you wanted to see what the second state looks like

$$o(t) = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} x_{1c}(t) \\ x_{2c}(t) \end{bmatrix}$$

Then you could plot this.

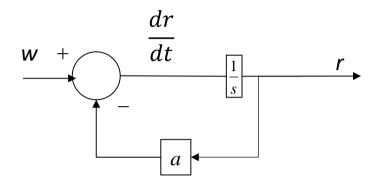


# Series form representation

Express G(s) as the product of  $\frac{1}{s+a}$  terms.

$$G(s) = \frac{2}{s^2 + 4s + 3} = 2\left(\frac{1}{s+1}\right)\left(\frac{1}{s+3}\right)$$

The block diagram for  $\frac{1}{s+a}$  is



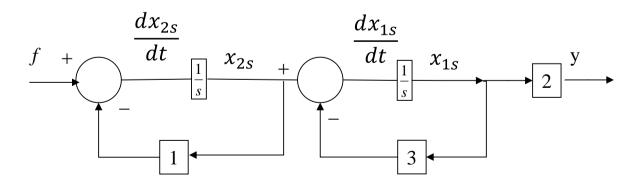
$$\frac{dr}{dt} = w - ar$$

$$sR(s) = W(s) - aR(s)$$

$$\frac{R(s)}{W(s)} = \frac{1}{s+a}$$

So G(s) can be represented in block diagram form as follows

$$G(s) = \frac{2}{s^2 + 4s + 3} = 2\left(\frac{1}{s+1}\right)\left(\frac{1}{s+3}\right)$$



$$\frac{dx_{1s}}{dt} = -3x_{1s} + x_{2s}$$

$$\frac{dx_{2s}}{dt} = -x_{2s} + f$$
$$y = 2x_{1s}$$

Now write the state-space representation in matrix form

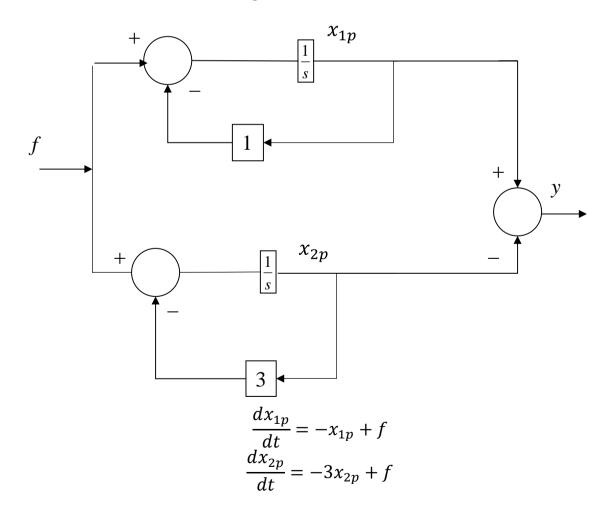
$$\frac{d}{dt} \begin{bmatrix} x_{1s}(t) \\ x_{2s}(t) \end{bmatrix} = \begin{bmatrix} -3 & 1 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} x_{1s}(t) \\ x_{2s}(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} f(t)$$
$$y(t) = \begin{bmatrix} 2 & 0 \end{bmatrix} \begin{bmatrix} x_{1s}(t) \\ x_{2s}(t) \end{bmatrix}$$

# Parallel form state-space representation

Express G(s) as the sum or difference of  $\frac{1}{s+a}$  terms.

$$G(s) = \frac{2}{s^2 + 4s + 3} = \left(\frac{1}{s+1}\right) - \left(\frac{1}{s+3}\right)$$

This can be shown in block diagram format as follows



$$\frac{d}{dt} \begin{bmatrix} x_{1p}(t) \\ x_{2p}(t) \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -3 \end{bmatrix} \begin{bmatrix} x_{1p}(t) \\ x_{2p}(t) \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} f(t)$$

$$y(t) = \begin{bmatrix} 1 & -1 \end{bmatrix} \begin{bmatrix} x_{1p}(t) \\ x_{2p}(t) \end{bmatrix}$$

Note that the state matrix is diagonal. This is important for computations as solution of the state equations (to be dealt with in a later lecture) involves exponentials of the state matrix and it is much easier to get the exponential of a diagonal matrix.

# 4.4 Transforming system models to state-space form

Derivation of the state-space model from the transfer function model of the system.

# **4.4.1** Transfer function $\rightarrow$ State space Case 1: when the input does *not* involve derivatives

• Consider the following third-order transfer function:

$$G(s) = \frac{Y(s)}{U(s)} = \frac{k}{s^3 + a_2 s^2 + a_1 s + a_0}$$

• Converting this to the time domain gives:

$$\frac{d^{3}y}{dt^{3}} + a_{2}\frac{d^{2}y}{dt^{2}} + a_{1}\frac{dy}{dt} + a_{0}y = ku$$
or
$$\frac{d^{3}y}{dt^{3}} = -a_{2}\frac{d^{2}y}{dt^{2}} - a_{1}\frac{dy}{dt} - a_{0}y + ku$$

• We simply define the states as  $x_1 = y$ ,  $x_2 = \frac{dy}{dt}$  and  $x_3 = \frac{d^2y}{dt^2}$ , leading to the following state model:

$$\frac{dx_1}{dt} = \frac{dy}{dt} = x_2$$

$$\frac{dx_2}{dt} = \frac{d^2y}{dt^2} = x_3$$

$$\frac{dx_3}{dt} = \frac{d^3y}{dt^3} = -a_2x_3 - a_1x_2 - a_0x_1 + ku$$

$$y = x_1$$

giving:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -a_0 & -a_1 & -a_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ k \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

# **4.4.2** Transfer function → State space Case 2: when the input does involve derivatives

• Consider the following third-order transfer function:

$$G(s) = \frac{Y(s)}{U(s)} = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{s^3 + a_2 s^2 + a_1 s + a_0}$$

• Firstly, we split the transfer function into two parts by defining an intermediate variable Z(s) as follows:

$$\frac{Z(s)}{U(s)} = \frac{1}{s^3 + a_2 s^2 + a_1 s + a_0} \quad \text{and} \quad \frac{Y(s)}{Z(s)} = b_3 s^3 + b_2 s^2 + b_1 s + b_0$$

$$\begin{array}{c|c}
U(s) & \hline
 & 1 & \\
\hline
 & s^3 + a_2 s^2 + a_1 s + a_0
\end{array}$$

$$Z(s) & \hline
 & b_3 s^3 + b_2 s^2 + b_1 s + b_0$$

$$Y(s)$$

• Converting to the time domain gives:

$$\frac{d^3z}{dt^3} + a_2 \frac{d^2z}{dt^2} + a_1 \frac{dz}{dt} + a_0 z = u$$

and

$$b_3 \frac{d^3 z}{dt^3} + b_2 \frac{d^2 z}{dt^2} + b_1 \frac{dz}{dt} + b_0 z = y$$

• Setting the states as  $x_1 = z$ ,  $x_2 = \frac{dz}{dt}$  and  $x_3 = \frac{d^2z}{dt^2}$ , we get the state equation as follows:

$$\frac{dx_1}{dt} = x_2$$
Once again, we have the **controllable canonical form**.
$$\frac{dx_2}{dt} = x_3$$

$$\frac{dx_3}{dt} = -a_2x_3 - a_1x_2 - a_0x_1 + u$$

giving:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -a_0 & -a_1 & -a_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$$

• In terms of the output equation:

- if 
$$b_3 = 0$$
 then:  $y = b_2 \frac{d^2 z}{dt^2} + b_1 \frac{dz}{dt} + b_0 z = b_2 x_3 + b_1 x_2 + b_0 x_1$ 

giving: 
$$y = \begin{bmatrix} b_0 & b_1 & b_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

(Note, the D matrix is 0 in this case)

- if 
$$b_3 \neq 0$$
 then:  $y = b_2 x_3 + b_1 x_2 + b_0 x_1 + b_3 \frac{d^3 z}{dt^3}$ 

but: 
$$\frac{d^3z}{dt^3} = \frac{dx_3}{dt} = -a_2x_3 - a_1x_2 - a_0x_1 + u$$

giving:  

$$y = (b_2 - b_3 a_2) x_3 + (b_1 - b_3 a_1) x_2 + (b_0 - b_3 a_0) x_1 + b_3 u$$

therefore:

$$y = [(b_0 - b_3 a_0) \quad (b_1 - b_3 a_1) \quad (b_2 - b_3 a_2)] \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + [b_3] u$$

• Note that the state matrix (i.e. matrix A) is exactly the same for both types of transfer function models.

$$G(s) = \frac{Y(s)}{U(s)} = \frac{k}{s^3 + a_2 s^2 + a_1 s + a_0}$$

$$G(s) = \frac{Y(s)}{U(s)} = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{s^3 + a_2 s^2 + a_1 s + a_0}$$

• This implies that the dynamics depend on the transfer function denominator only.

## 4.5 Obtaining transfer functions from state-space models

- In section 4.4, we saw how to go from a transfer function model to a state-space model (known as the **controllable canonical form**).
- It is also possible to go from a state-space model to a transfer function model as follows:

### **4.5.1** Continuous-time state-space model → transfer function

• Consider the following single-input-single-output continuous-time statespace model:

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$$
$$y(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}u(t)$$

• Taking the Laplace transform gives:

$$s\mathbf{X}(s) = \mathbf{A}\mathbf{X}(s) + \mathbf{B}U(s)$$
  
 $Y(s) = \mathbf{C}\mathbf{X}(s) + \mathbf{D}U(s)$ 

• Rearranging the state equation gives:

$$(sI - \mathbf{A})\mathbf{X}(s) = \mathbf{B}U(s)$$

$$\Rightarrow \mathbf{X}(s) = (sI - \mathbf{A})^{-1}\mathbf{B}U(s)$$

• Substituting this equation into the output equation gives:

$$Y(s) = \mathbf{C}(sI - \mathbf{A})^{-1}\mathbf{B}U(s) + \mathbf{D}U(s)$$

• Hence, the transfer function is defined in terms of the state-space equation matrices as:

$$G(s) = \frac{Y(s)}{U(s)} = \mathbf{C}(sI - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}$$

• Example 4.2: Determine the transfer function for the following system:

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 2 \\ -3 & 5 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u(t), \quad y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \mathbf{x}(t)$$

**Solution** 

$$G(s) = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}$$

$$= \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{pmatrix} \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 2 \\ -3 & 5 \end{bmatrix} \end{pmatrix}^{-1} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} s & -2 \\ 3 & s - 5 \end{bmatrix}^{-1} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$= \frac{\begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} s - 5 & 2 \\ -3 & s \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix}}{s^2 - 5s + 6}$$

$$= \frac{\begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} s - 5 \\ -3 \end{bmatrix}}{s^2 - 5s + 6} = \frac{s - 5}{s^2 - 5s + 6}$$

Hence: 
$$G(s) = \frac{Y(s)}{U(s)} = \frac{s-5}{s^2 - 5s + 6}$$

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