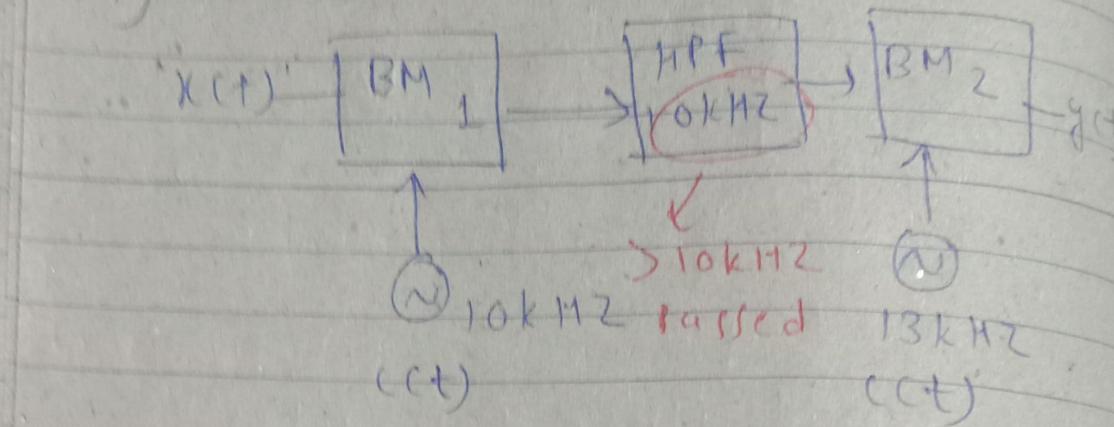
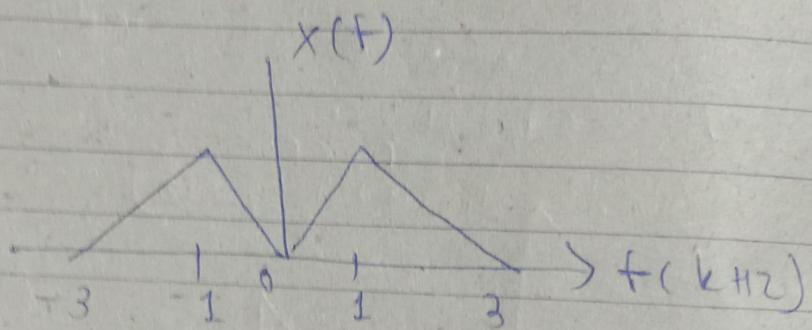


Lec 10 (Demodulation Techniques)

(Q1)



Spectrum of $x(t)$ is:



Find out the positive frequencies where $Y(f)$ has peaks?

Soln:

$$Y(f) \leftarrow Y(f)$$

$$X_f = \begin{cases} 1 \text{ kHz} \\ -1 \text{ kHz} \end{cases} \rightarrow \text{Peaks}$$

Balanced modulator = $x(t)c(t)$

$$\omega_c + \omega_m - \omega_c + \omega_m$$

$$O/P \text{ of } BM_1 = n(t) c(t)$$

$$\checkmark \\ 10 \text{ kHz}$$

= frequencies added & subtracted

$$f \left\{ \begin{array}{l} \cancel{\omega_c + \omega_m} 10 \text{ kHz} \pm 1 \text{ kHz} \\ \omega_c - \omega_m \\ 10 \text{ kHz} \pm (-1 \text{ kHz}) \end{array} \right.$$

Peaks

$$= 11 \text{ kHz}, 9 \text{ kHz}$$

$$9 \text{ kHz}, 11 \text{ kHz}$$

↓ HPF ($> 10 \text{ kHz}$)

11 kHz passed

$$O/P \text{ of } BM_2 = y(f) = 13 \text{ kHz} \pm 11 \text{ kHz}$$

Ans)

$$= 24 \text{ kHz} \\ \text{OR} \\ 2 \text{ kHz}$$

Peaks

T_x = Transmitter
R_x = Receiver

Amplitude modulation

↳ DSB-C (conventional AM)

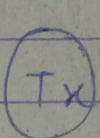


$$x_{AM}(t) = c(t) + m(t)c(t)$$

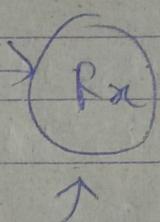
↳ DSB-SC

↳ only 2SB ($m(t)c(t)$)

↳ SSB-SC = only 1SB, carrier suppressed



$x_{AM}(t)$



Demodulation takes

place here

DEMODULATION/DETECTION OF AM

SIGNALS

① Envelope detection (Aynchronous / Non-coherent detector)

② Synchronous / Coherent detection

③ Square law detector

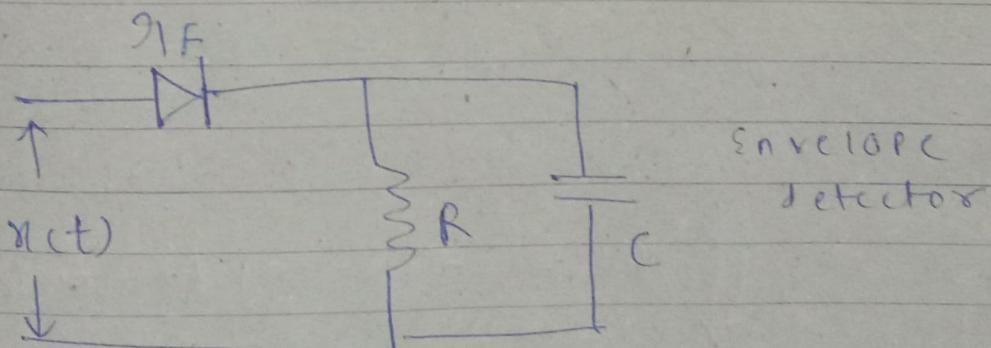
ENVELOPE DETECTION

→ used for conventional AM type of signal

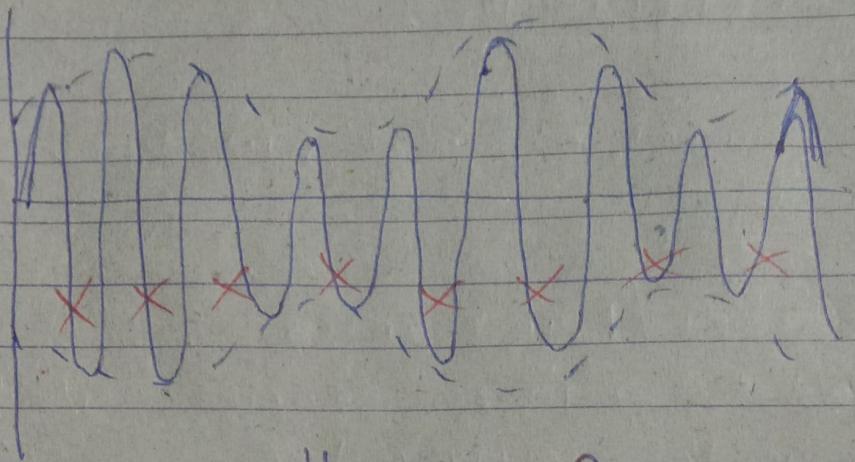
→ non-coherent / Asynchronous
(does not require carrier signal at the receiver for detection)

Since carrier signal already present in ~~X_{AM}(t)~~

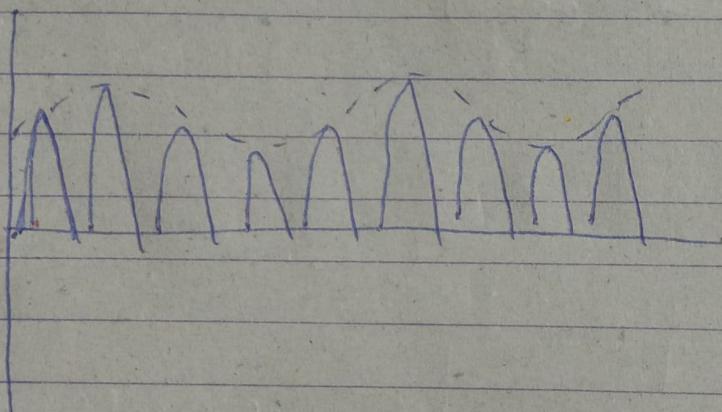
CIRCUIT:



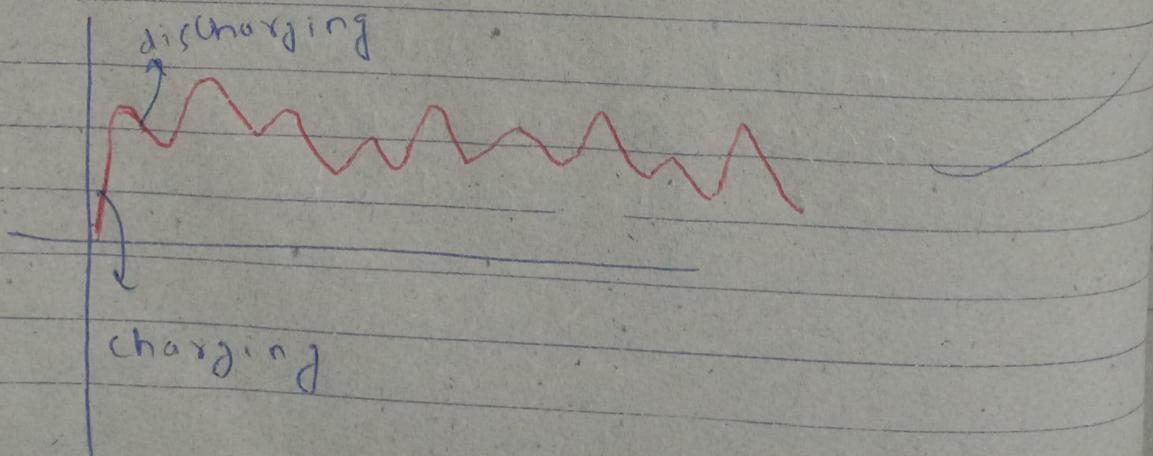
- * simple & cheap detector
- * consists of inexpensive discrete elements like diode, R, C.



↓ diode. (all negative polarities removed)



↓ RC = charging / discharging circuit



charge
d
of
m(t)

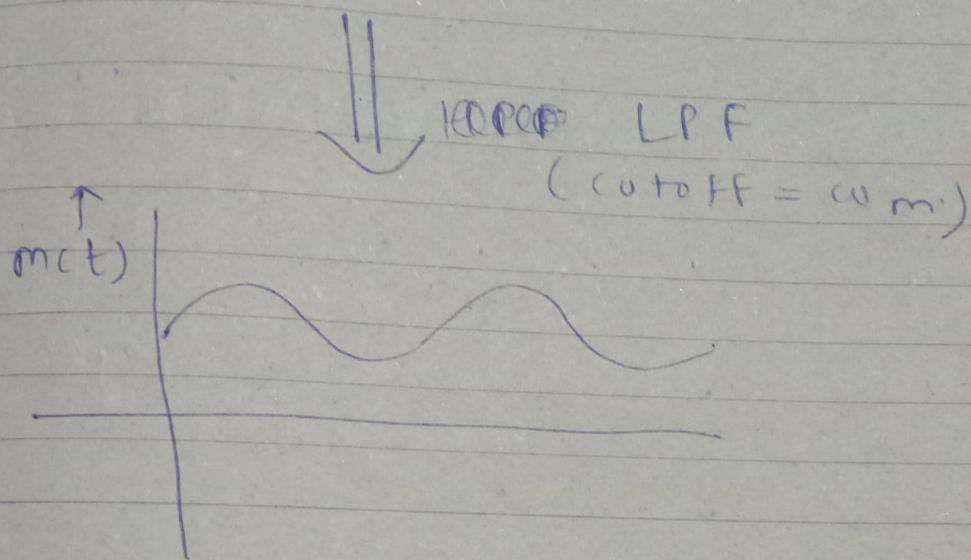
CHAR

9f

char

τ_{ch}

charging / discharging = leads to
distorted envelope consisting
of high frequency components



CHARGING TIME CONSTANT

r_f = forward bias resistance

charging through ~~route~~ diode $\rightarrow C$

$$\tau_{\text{charging}} = r_f C$$

$$r_f C \ll \frac{1}{f_c}$$

DISCHARGING TIME CONSTANT

* DSB -

~~Techn~~

$$\tau_{\text{discharge}} = R \times C$$

$$\text{discharging through path} = \text{parallel combination} \rightarrow R$$

This cannot be too low / too high
to properly detect the envelope.

It should be moderate.

$$RC \gg \frac{1}{f_c}$$

$$\text{Results } RC \ll \frac{1}{f_m}$$

$$\left[\frac{1}{f_c} \ll RC \ll \frac{1}{f_m} \right]$$

If not this, then discharge very quickly, may lead to distorted envelope

* DSB-C / conventional Am used for
~~broadcasting~~ broadcasting since detection
technique very cheap

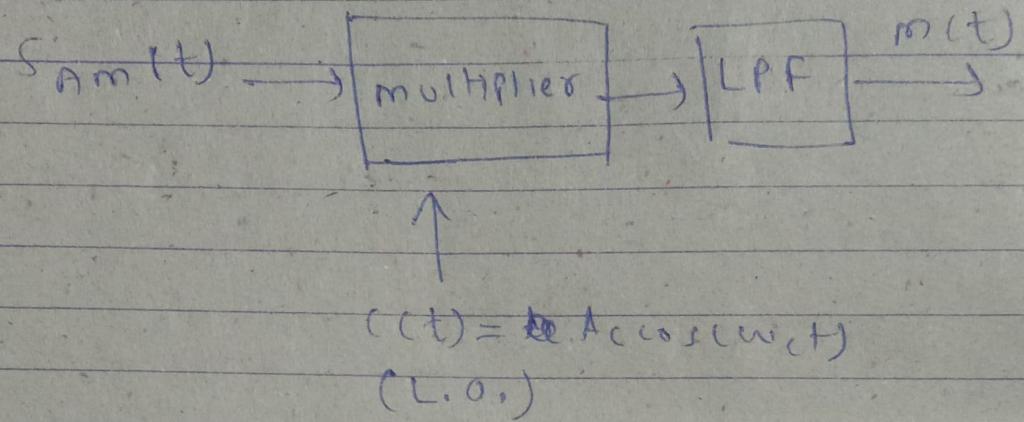
~~secret~~

high
c.

ry
d

SYNCHRONOUS DETECTION

(Locally generated carrier signal $s_{am}(t)$)



* $c(t)$ should be perfectly synchronized in phase & frequency to the $c(t)$ at the transmitter end.

* generation of carrier signal
= complex task

ANALYSIS

Case 1: Perfect synchronization of $c(t)$

$$s_{am}(t) = \cancel{A_m} \cos(w_c t) + A_c m(t) \cos(w_c t)$$

$$\cos(\omega_c t) = 2 \cos^2(\omega_c t) - 1$$

$$S_{Am}(t) \times c(t) = [A_c \cos(\omega_c t) + A_c m(t)] \cos(\omega_c t)$$

$$= A_c^2 \cos^2(\omega_c t) + A_c^2 m(t) \cos^2(\omega_c t)$$

$$= \frac{A_c^2}{2} [1 + \cos(2\omega_c t)] + \frac{A_c^2 m(t)}{2}$$

$$(1 + \cos(2\omega_c t))$$

↓ LPF (cwm)

$$\frac{A_c^2}{2} \cos(2\omega_c t) \quad \times$$

$$\frac{A_c^2 m(t)}{2} \quad \checkmark$$

$$\frac{A_c^2 m(t)}{2} \cos(2\omega_c t) \quad \times$$

$$\frac{A_c^2 m(t)}{2} \Rightarrow \text{required signal} = m(t)$$

we are getting

100% scaled version
of $m(t)$, scaling
factor can be removed

L.O. (t) = Locally generated carrier signal

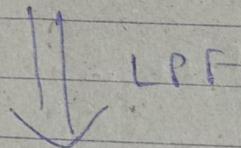
Case 2:

$$L.O. (t) = A_c \cos(\omega_c t + \phi)$$

$$S_{am}(t) \times A_c \cos(\omega_c t + \phi)$$

$$= (A_c \cos(\omega_c t + \phi) \text{ rect}(t) + A_c m(t)) \cos(\omega_c t + \phi)$$

$$A_c \cos(\omega_c t + \phi)$$



$$\left(\frac{A_c^2}{2} m(t) \right) \cos \phi \rightarrow \text{distortion}$$

in demodulated

signal

~~varied~~

varied
in

accordance
to ϕ

scaled

factor of $m(t)$

SQVA

$x_{am}(t)$

V

WAVE

LP

{ if $\phi = 90^\circ$,

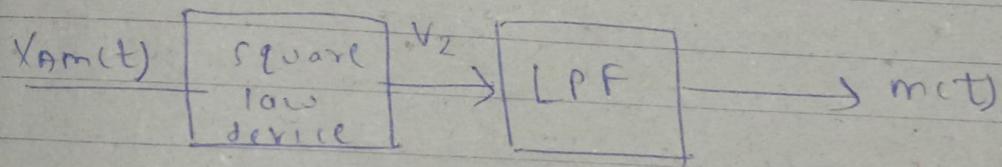
$\cos 90^\circ = 0$, hence total loss
of signal.

∴ This condition is called

Quadrature null effect

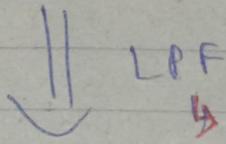
orthogonal phase ↴
total loss
of $m(t)$)

SQUARE LAW DETECTOR



$$V_2 = a_1 X_{Am}(t) + a_2 [X_{Am}(t)]^2$$

↓



↳ eliminates all

high frequency
components

& keeps lower
frequency

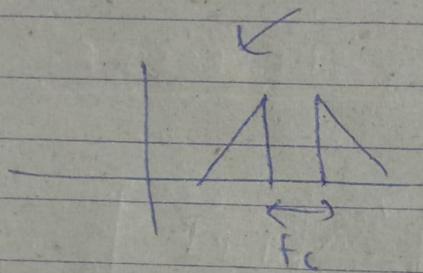
$$\text{LPF}_{out} = \frac{a_2^2 A_c^2}{2} m(t)$$

VSB = vestigial side band modulation

SSB-SC = better in case of Power efficiency & Radio Transmission efficiency.

demodulation circuit is complex.

Limited to voice-signal



sufficient guard band between USB & LSB, so easier to detect

VSB = variation of SSB-SC

* smaller

power

amplitude

so

* helps

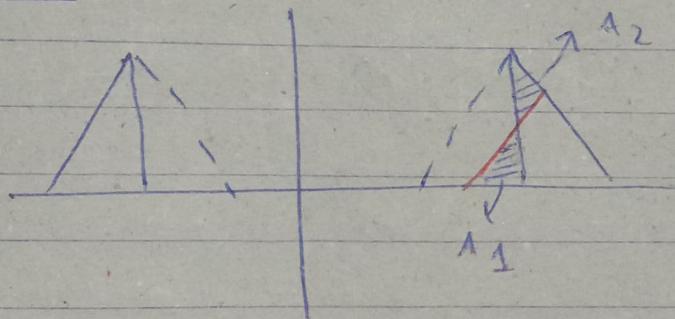
from

VSB

① B.W requirement is almost same as the bandwidth of SSB-SC and also allows video signal transmission

- * freq. range = 4.5 MHz
- * no guard band between side bands

VSB



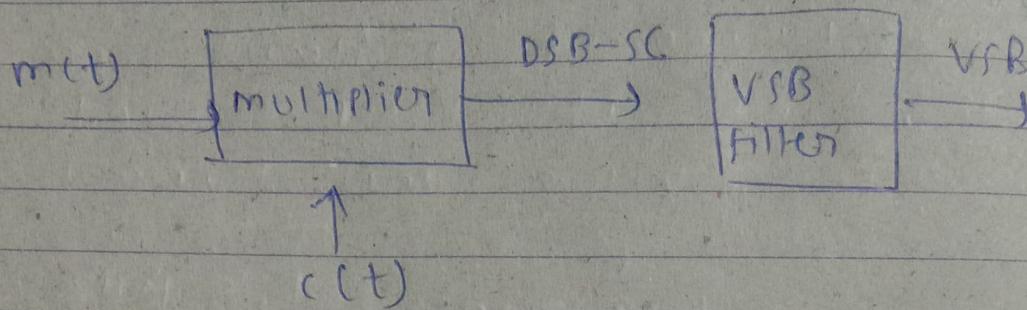
$$\text{area } A_1 = \text{area } A_2$$

* small part of vestige unwanted
Rear sideband added & equal amount of desired sideband subtracted,
so no loss of information

* helps us to use practical filtering process

GENERATION OF VSB

Power



DSB -

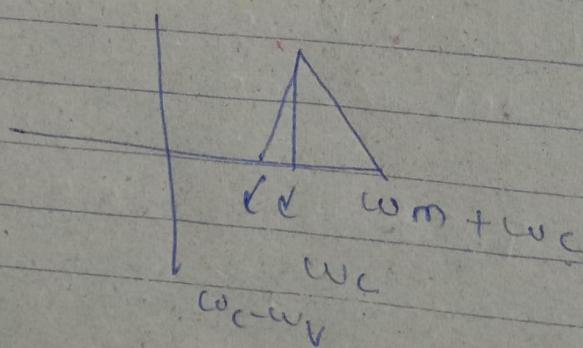
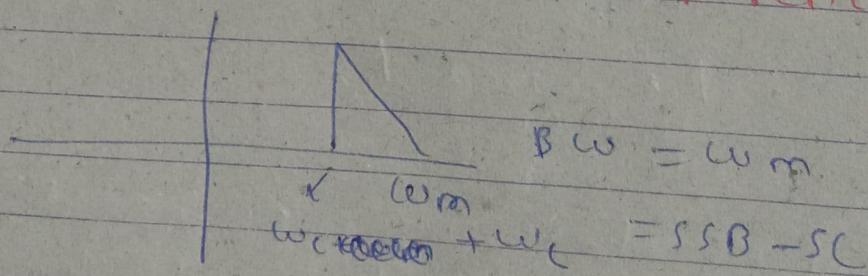
∴ VSB -

Bandwidth requirement

DSB-C < DSB-SC > VSB > SSB-SC

($2\omega_m$)

but slight difference



$Bw = \omega_m + \omega_v$

$\omega_v = \text{small}$

Power requirement

DSB-C > DSB-SC > (VSB &
SCB-SC)
Power
= same

∴ VSB-SC = efficient technique