

differentiating with respect to  $t$  we obtain

$$\frac{df}{dt}(t) = \frac{dx}{dt}(t)\bar{\psi}(t) + x(t)\frac{d\bar{\psi}}{dt}(t) = \left( \sum_{q=1}^Q qa_q t^{q-1} \right) x(t)\bar{\psi}(t) + x(t)\frac{d\bar{\psi}}{dt}(t) \quad (7)$$

Because  $\psi$  is zero outside of the interval  $[-\frac{L_t}{2}, \frac{L_t}{2}]$ , integrating  $\frac{df}{dt}(t)$  we obtain

$$\int_{-\infty}^{\infty} \frac{df}{dt}(t)dt = \sum_{q=1}^Q qa_q \int_{-\frac{L_t}{2}}^{\frac{L_t}{2}} t^{q-1} x(t)\bar{\psi}(t)dt + \left\langle x, \frac{d\bar{\psi}}{dt} \right\rangle = 0 \quad (8)$$

or, using the operator  $\mathcal{T}^\alpha$ ,

$$\sum_{q=1}^Q qa_q \langle \mathcal{T}^{q-1} x, \bar{\psi} \rangle = - \left\langle x, \frac{d\bar{\psi}}{dt} \right\rangle \quad (9)$$

Estimating coefficients  $a_q$ ,  $1 < q \leq Q$ , simply requires  $R$  atoms  $\psi_r$  with  $R \geq Q$  to solve the linear system of equations

$$\sum_{q=1}^Q qa_q \langle \mathcal{T}^{q-1} x, \bar{\psi}_r \rangle = - \left\langle x, \frac{d\bar{\psi}_r}{dt} \right\rangle \quad (10)$$

for  $1 \leq r \leq R$ .

To estimate  $a_0$  we rewrite the signal we are analysing as

$$x(t) = \exp(a_0)\gamma(t) + \epsilon(t) \quad (11)$$

where  $\epsilon(t)$  is the error signal, the part of the signal that is not explained by our model, and  $\gamma(t)$  is the part of the signal whose coefficients have already been estimated, i.e.,

$$\gamma(t) = \exp \left( \sum_{q=1}^Q a_q t^q \right) \quad (12)$$

Computing the inner product  $\langle x, \gamma \rangle$ , we have

$$\langle x, \gamma \rangle = \langle \exp(a_0)\gamma, \gamma \rangle + \langle \epsilon, \gamma \rangle \quad (13)$$

The inner product between  $\epsilon$  and  $\gamma$  is 0, by the orthogonality principle [13, ch. 12]. Furthermore, because  $\exp(a_0)$  does not depend on  $t$ , we have

$$\langle x, \gamma \rangle = \exp(a_0) \langle \gamma, \gamma \rangle \quad (14)$$

so we can estimate  $a_0$  as

$$a_0 = \log(\langle x, \gamma \rangle) - \log(\langle \gamma, \gamma \rangle) \quad (15)$$

As will be seen in subsequent sections, the DDM typically involves taking the discrete Fourier transform (DFT) of the signal windowed by both an everywhere once-differentiable function of finite support (e.g., the Hann window) and this function's derivative. A small subset of atoms corresponding to the peak bins in the DFT are used in Eq. 10 to solve for the parameters  $a_q$ .

### 3. ESTIMATING THE $a_{p,q}$ OF $P$ COMPONENTS

We examine how the mixture model influences the estimation of the  $a_{p,q}$  in Eq. 3. Consider a mixture of  $P$  components. If we define the weighted signal sum

$$g(t) = \sum_{p=1}^P x_p(t)\bar{\psi}(t) = \sum_{p=1}^P f_p(t) \quad (16)$$

and substitute  $g$  for  $f$  in Eq. 7 we obtain

$$\sum_{p=1}^P \int_{-\frac{L_t}{2}}^{\frac{L_t}{2}} \frac{df_p}{dt}(t)dt = 0 = \sum_{p=1}^P \left( \sum_{q=1}^Q qa_{p,q} \langle \mathcal{T}^{q-1} x_p, \bar{\psi} \rangle + \left\langle x_p, \frac{d\bar{\psi}}{dt} \right\rangle \right) \quad (17)$$

From this we see if  $\langle \mathcal{T}^{q-1} x_p, \bar{\psi}_r \rangle$  and  $\langle x_p, \frac{d\bar{\psi}_r}{dt} \rangle$  are small for all but  $p = p^*$  and a subset of  $R$  atoms<sup>1</sup>, we can simply estimate the parameters  $a_{p^*,q}$  using

$$\sum_{q=1}^Q qa_{p^*,q} \langle \mathcal{T}^{q-1} x_{p^*}, \bar{\psi}_r \rangle = - \left\langle x_{p^*}, \frac{d\bar{\psi}_r}{dn} \right\rangle \quad (18)$$

for  $1 \leq r \leq R$ . To compute  $a_{p^*,0}$  we simply use

$$\gamma_{p^*}(t) = \exp \left( \sum_{q=1}^Q a_{p^*,q} t^q \right) \quad (19)$$

in place of  $\gamma$  in Eq. 15.

### 4. DESIGNING THE $\psi_R$

In practice, an approximation of Eq. 4 is evaluated using the DFT on a signal  $x$  that is properly sampled and so can be evaluated at a finite number of times  $nT$  with  $n \in [0, N-1]$  and  $T$  the sample period in seconds. In this way, the chosen atoms  $\psi_\omega(t)$  are the products of the elements of the Fourier basis and an appropriately chosen window  $w$  that is once differentiable and finite, i.e.,

$$\psi_\omega(t) = w(t) \exp(-j\omega t) \quad (20)$$

Defining  $N = \frac{L_t}{T}$  and angular frequency at bin  $r$  as  $\omega_r = 2\pi \frac{r}{N}$ , the approximate inner product is then

$$\langle x, \psi_\omega \rangle \approx \sum_{n=0}^{N-1} x(nT)w(nT) \exp(-2\pi j r \frac{n}{N}) \quad (21)$$

i.e., the definition of the DFT of a windowed signal<sup>2</sup>. The DFT is readily interpreted as a bank of bandpass filters centred at normalized frequencies  $\frac{r}{N}$  and with frequency response described by

<sup>1</sup>The notation  $x^*$  will mean the value of the argument  $x$  maximizing or minimizing some function.

<sup>2</sup>Notice however that this is an approximation of the inner product and should not be interpreted as yielding the Fourier series coefficients of a properly sampled signal  $x$  periodic in  $L_t$ . This means that other evaluations of the inner product that yield more accurate results are possible. For example, the analytic solution is possible if  $x$  is assumed zero outside of  $[-\frac{L_t}{2}, \frac{L_t}{2}]$  (the  $\psi$  are in general analytic). In this case the samples of  $x$  are convolved with the appropriate interpolating sinc functions and the integral of this function's product with  $\psi$  is evaluated.