

TITLE

Please change the title to a new one, not using the same as for the conference paper published in 2015.

Yes, it is done.

1-INTRODUCTION

1.1 The manuscript motivates controlled experimental measurements by noticing that both synthetic benchmarks and validations of imaging techniques are generally limited. This is an important aspect, however it would be great to provide further motivation and background about small-scale physical modeling by the MUSC laboratory.

We have reorganized introduction and the section about MUSC laboratory .

In introduction, the following lines have been added :

lines 88 to 90

Lines 91 to line 106.

Line 119

In the section concerning the MUSC laboratory, different parts have been added to answer to the remarks below (see the indicated lines).

1.2 When introducing small-scale physical modeling (page 3), it omitted references to many previous studies using thin-plate models for this same purpose. I think it would still be worthwhile to mention some of this work (sometimes referred to two-dimensional, plate wave or Lamb wave modelling), like Oliver et al. (1954), Angona (1960), Healy and Press (1960), O'Brien and Symes (1971), Pant et al. (1988) or more recent Mo et al. (2015).

References have been added in the corrected manuscript.

1.3 A short explanation about the differences and limitations of 2-D versus 3-D physical modeling would be great to provide, in order to motivate the setup chosen of the MUSC laboratory.

It is done in the corrected version in Introduction, line 98 to line 106.

1.4 Also, the nomenclature and abbreviation used of "Physical small-scale Modeling Methods (PSM)" is somewhat new, where most other literature uses terms like "physical scale model", "physical modeling" or "scale model data". Thus, it would rather be "Small-scale physical modeling methods". The abbreviation PSM in the manuscript is hardly used and could be omitted altogether.

We use "Small-scale physical modeling methods" in the corrected version.

1.5 You mention modeling surface waves as a reason not to immerse the model in say a water tank. However, you do not further discuss this important topic and the results presented in this study omit showing surface waves. It would be great to list limitations in physical modeling of surface waves and clarify what you refer to as "reflection echoes", mentioned in the conclusions.

Concerning « ommit showing surface waves »

55 Surface waves are presented but labeled as S-wave. Indeed, in a homogeneous medium, the direct S-wave propagating along the free-surface is a non-dispersive Rayleigh wave. It is corrected in the corrected version.

Concerning "reflection echoes"

60 Our words were wrongly chosen here, "reflected echoes" in the conclusion refers to ringing effects of the source in fact. This ringing effect carried by the direct P and S/Rayleigh waves interfere with direct S/Rayleigh wave and reflected-wave arrivals respectively. This is corrected in the new version.

65 **The findings presented on page 4 could be further structured. The manuscript mainly lists the following problem items addressed in this study: (1) line-source versus point-source modeling, (2) geometrical spreading corrections, (3) effective source time function, that is the transducer influence, (4) reproducibility of the experiment/measurement. These items could be separated into challenges related to the "forward problem" of modeling wave propagation in 2-D (items**
70 **1,2), the "inverse problem" of retrieving the correct source and model parameters (item 3), and finally the robustness, stability and precision of the measurement apparatus (item 4).**

Line 120 to line 140. This part has been restructured in the corrected manuscript taking into account the difficulties in organizing the results. We understand this remark but splitting into challenges
75 would require, from our point of view, to rewrite largely the result sections. Indeed, these challenges are strongly linked to each other: (1) 3D-2D spreading correction and point-source versus line source, and (2) source reproducibility and source time function estimation. However, we try to clarify at best these different results and we now differentiate them in the introduction.

80 **2-METHODS**

2.1 Since the focus of the study is on physical modeling, it would make sense to start presenting the MUSC laboratory (section 2.2) rather than the numerical method used for comparison (section 2.1).

85 We have reorganized the manuscript to present the MUSC laboratory first.

2.2 Furthermore, when presenting the MUSC laboratory it would be helpful for readers to mention limitations which are expected. For example, it is known that ultrasonic transducers
90 **are resonant and narrow-band due to the physical properties of these devices. Also, the transducers are in general large compared to the minimum wavelength of the simulation, thus can impose directivity effects. Some of these effects have been studied by Francois Breteau et al. (2011) already, but it would be great to further mention and justify the selected frequency-bandwidths of 20 - 200 kHz and 300 - 800 kHz.**

95 These remarks are tackled in the corrected version in 3 separated parts as following :

1) For example, it is known that ultrasonic transducers are resonant and narrow-band due to the physical properties of these devices.

100 piezo-electrics components are indeed resonant. One of the difficulty to avoid the resonant effect is the impedance adaptation of the transducer to the propagating medium. However, in MUSC, we use transducers who have been built with well-adapted shape, backing element and suited material for the contact to the medium, in order to be adapted to the impedance of the material that we use, as

105 much as possible (for exemple, they are not adapted to alluminium blocks). That is specially the
case of those adapted to a central frequency of 100 KHz in the paper. In the case of the higher
frequency one (not used in the tests described here), a conical adaptator in resin between the
transducer and the model allow to weak the resonant effect. This aspect is already described in
110 (Bretaudeau et al, 2011) and, to our mind, it should not be repeated with long developments in the
present paper. However, it is recalled in the corrected version as recommended in lines 161 to 163.

Moreover, even if the resonnant effect are avoided, the response of the transducer remains as a
filtering effect to the electrical signal injected in input. This aspect is a critical point tackled in the
present proposed article. We have added sentences lines 163 to 168

115 **Concerning the narrow-band aspect**, lines 238 to 242 have been added.

120 **2) Also, the transducers are in general large compared to the minimum wavelength of the
simulation, thus can impose directivity effects. Some of these effects have been studied by
Fran,cois Bretaudeau et al. (2011) already, but it would be great to further mention**

Precisions about this have been added in the corrected version lines 178 to 188

125 **3) and justify the selected frequency-bandwidths of 20 - 200 kHz and 300 - 800 kHz.**

It has been clarified in the corrected version through the text lines 188 to 196

130 **2.3 Also, it would be great to evaluate the precision achieved of the measurements in the
MUSC laboratory. For example, the precision of the positioning of the receiver position is
stated as $\pm 10\mu\text{m}$ which for a shortest wavelength of 1mm amounts to a precision of 1%. So
does the vertical offset measurement by a laser beam with a $20\mu\text{m}$ diameter, thus the
135 measurement is not exactly a point measurement but an average over a small surface fraction.
One could briefly present for the chosen setups what error of the measurement would be
expected. Since this is one of the advantages of laboratory settings, you could put error bars
on the traces.**

140 It has been clarified in the corrected version through the lines 152 to 154 and Lines 227 to 237.

145 **2.4 The same consideration also holds for the ringing of the transducers which will likely look
different at different central frequencies. One could present the ringing for different central
frequencies of the source, to better highlight in which frequency regime the transducers affect
measurements and need to be treated more carefully as is then done in the following of this
study.**

150 The frequencial effects of the transducer is tackled thorough the entire waveform, as indicated in the
modified version 168 to 170

3-RESULTS

155 **3.1 It would help to start clarifying which 2-D numerical result is compared against which 3-D
experimental data and somehow introduce nomenclature for 3-D experimental point-source,
3-D experimentally constructed line-source and 2-D numerical line-source.**

This has been taken into account and the proposed nomenclatures are now incorporated in the corrected version.

3.2 Section 3.2 would be great to further subdivide into new sub-sections: The first part deals with reproducing single measurements to validate the reproducibility of the source. The second part deals with the effective source time function estimation, starting at page 14, line 29 ("In the second step ..."). The third part introduces the new 2-layer model called BiAlt, thus deals with a new experimental setup (page 15, line 8) and comparison. It would help to put these into different sub-sections and discuss each result separately.

For convenience, the RESULTS section has been reorganized into three separate parts, hoping that this will allow for better understanding of the results.

3.3 Also, in your comparisons between different traces you use a correlation coefficient over the whole trace length. Since you already see and discuss different effects on P-, S-, PP- and PS-phases, it would make sense to further separate the comparisons into just comparing a single phase. This would make it clearer in how well a P-wave, S-wave or PP- or PS-reflection is treated in the geometrical spreading and 2D line-source approximations.

Additional correlation coefficients for P-, S/Rayleigh- and PP-reflected waves have been added to figures 8 and 9 (figures 9 and 10 in the previous version). Psv-reflected wave is difficult to locate on real data, so the correlation coefficient has not been calculated for it. Results are discussed.

Line 442 to line 446 and from line 462 to line 465.

4-CONCLUSIONS

4.1 Would it be that you verified experimentally that you can construct a line-source using the MUSC laboratory? or would it be that the geometrical spreading transformation applied to 3-D data is only accurate for P- and S-phases, but not reflected ones like PP- or PS-phases?

We think that the most important result is the 3D constructed line-source since other publications have already shown limitations of geometrical spreading correction methods.

4.2 The very last sentence mentions the addition of new measurements in the MUSC laboratory by Valensi et al. (2015). It would be great to shortly explain this addition in the introduction and why it hasn't been used for this study.

Valensi et al. (2015) have introduced horizontal component in the MUSC laboratory. However, when this study was realized the horizontal component was not fully calibrated and signal-noise ratio issues were persistent. Furthermore, some data were generated before the improvement of the laser interferometer. Consequently, we use only the vertical component.

comment – It is a work in progress that will require a little more time before being fully finalized.

5- OTHER REMARKS

Manuscript text

page 2, line 2: "2 D and 3 D" please see if 2D and 3D or 2-D and 3-D could be used in a more coherent way throughout the text.

205 It's done.

page 2, line 49: "algorithms innovations" just use e.g. "algorithms".

It's done.

210

page 3, line 56: "sharp similarities" maybe better "close ..".

OK.

215 **page 4, line 33: "It is based on the following findings." awkward ending of a paragraph.**

Yes, it's awkward...corrected.

220 **page 4, line 38: "3D/2D geometrical spreading effects" it would be clearer saying "3D-to-2D geometrical spreading corrections".**

OK.

225 **page 6, line 56: "Since the wave equation is linear" the sentence sounds a bit odd, maybe "For the linearized wave equation, .."**

It's done.

h

230 **page 8, line 24: "finely" ? could be omitted**

OK.

235 **"In the far-field approximation, .." You show the single-velocity transformation in eq. (10) and then state "is recommended for small offsets". This seems to contradict with the initial far-field assumption. Maybe you could clarify it.**

240 We have no physical explanation for this. We can just refer to Schafer (2014) and Forbirger (2014) who have shown, on the basis of numerical tests, that single-velocity transformation is better for small-offset while direct-wave transform is better for large-offset. This "clarification" has been added to the manuscript (see appendix line 695 to line 698).

page 15, line 57: "..to inverse crime." the sentence sounds strange.

Indeed...

245

Figures

250 ***Figure 2:* This figure is not referenced in the text. There is also no explanation of why the traces lack in the middle (closest to the source). Furthermore, the images all show glitches at different offsets which are not apparent in for example figure 6 (c). It would be nice to explain in the manuscript text what is shown here.**

255 Figure 2 shows three multireceiver acquisition for the BiAlt model. The traces lack in the middle is related to the position of the laser over the piezo-electric source so that no trace can be recorded.

The glitches on figure 2 which are not present on other figures are related to interferometer wear during acquisitions shown in figure 2.

260 **Figure 3 and 4: The figures only show the BiAlt model. It would be great to also show the first model used which is the homogeneous one next to it, in both figures. This would make it clearer that the study is conducting experiments on two different models.**

Done for figure 3, figure 4 from the previous version has been removed.

265 **Figure 9: there is no need to additionally label the image with (a) or reference it as Fig. 9(a). It then is just figure 9.**

It's done. Figure 9 is now Figure 8.

270 **References**

Please note that in many references on page 17 - 19, the usage of 2D, 3-D or CO2 became 2d, 3-d and co2 and would need to be corrected.

275 It is done.