

tmp title: MUSC source

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(October 28, 2015)

GEO-Example

Running head: *Geophysics* example

ABSTRACT

INTRODUCTION

Since the early developments of seismic imaging methods in the middle of 20th century, approaches and algorithms innovations are still proposed in current research projects. The improvements deal with both the qualitative imaging techniques like migration (e.g. Berkhout et al. (2012); Guofeng et al. (2013)), novel applications of quantitative imaging methods such as the first arrival tomography (e.g. Bohm et al. (2015)), or even more recent approaches like the Full Waveform Inversion (e.g. Perez Solano et al. (2014), see Virieux and Operto (2009) for a revue of this last decade). The refinements are proposed for different scales like near surface applications for civil engineering topics or more deeper investigation for example for oil prospection or crustal imaging at regional or global scales. They are mostly validated by using synthetic data, for example with well known shared benchmark (like the Marmousi case). However, the synthetic data are generally computed using the same wave propagation modeling engine used in the inverse problem process. In other terms, the synthetic data are computed with some assumptions which are the same in the inverse problem, for example the approximation of acoustic propagation, a 2D space medium, or a 2D line source. This approach, called *inverse crime* (Wirgin, 2004) is particularly useful for validating an algorithm in its early development stage but does not take into account the artefacts that can be due to the assumptions of the direct problem. Some authors tackle this issue by providing 3D data which are inverted with a 2D approach or other restrictive assumptions (e.g). But also in this case, the approach does not allow to assess the efficiency of the method for real seismic data. Moreover, because no one knows precisely the Earth interior, it is difficult to evaluate the capacity of a method to recover physical parameters and structures from real seismic data which can lead sometimes to geological misinterpretation due to numerical artifacts (Morozov, 2004). Thus, it is necessary to add

a step for which imaging methods will be tested for experimental seismic measurements
25 obtained under controlled conditions.

The best way to satisfy this need is to use Physical Small Scale Modeling Methods (noted
PSM subsequently). *PSM* were used since several years to study the propagation of waves
in various media with several stage of complexity, from acoustic wave propagation in homo-
geneous media to elastic wave propagation in three-dimensional heterogeneous anisotropic
30 media (Rieber, 1936; Howes et al., 1953; Hiltermann, 1970; French, 1974; Bishop et al., 1985;
Pratt, 1999; Favretto-Cristini et al., 2013; Sarkar et al., 2003; Isaac and Lawton, 1999), and
allow to generate experimental seismic data under well-controlled conditions. In this way,
recent studies have been conducted to simulate multi-sources and multi-receivers through
piezo-electric transducers (Wong et al., 2009). An alternative approach consists in using the
35 laser interferometry as the receiver system, as done in the MUSC Laboratory (Bretaudeau
et al., 2008, 2011, 2013), *Mesure Ultrasonore Sans Contact* in French, is one of them. This
technology, by avoiding the contact of the receivers on the model, allows to by-pass the
coupling issue of transducers that is difficult to model. In this way, the MUSC laboratory is
designed to simulate (1) wide-angle on-shore acquisitions modeling both body waves and sur-
40 face waves, (2) automatic multisource-multireceiver measurements with a high-productivity,
(3) high-precision source-receiver positioning and (4) high-precision recording of absolute
surface displacement without coupling effects.

Our objective here is to increase the potential of the MUSC system as a reliable tool
for generating experimental data which will be distributed in the scientific community.
45 Thus, we present two studies of experimental data in order to : 1) quantitatively refine the
comparison between numerical and experimental data by taking into account the 3D/2D
geometrical spreading effects through an alternative way and 2) identify the reproducibility

of the source impact and, consequently, data repeatability. These approaches will complete the knowledge of the system and facilitate the achievement of massive multi-source and multi-receiver data simulating subsurface seismic experimental campaigns. Moreover, they provide quantitative informations about the data quality for geophysicists who need to use them measurement based on reduced scale model.

In order to achieve these objectives, we used a seismic wave modeling code based on the Spectral Element Method (Komatitsch et al., 1998; Komatitsch and Tromp, 1999; Komatitsch et al., 2005; Festa and Vilotte, 2005) that allow to provide numerical signals as reference data for comparison. The Spectral Element Method (SEM) has several advantages compared to finite differences and finite elements, such as: (1) a weak formulation which can naturally take into account the free surface, (2) an explicit scheme in time domain facilitating parallelization and reducing the computational cost, (3) a spatial discretization (mesh) convenient for the representation of complex environments and (4) high precision results and low numerical dispersion.

The numerical characteristics of the code used are described in a first part below. Afterwards, the specificities of the MUSC system are explained, followed by the presentation of the models used. Finally The two coupled studies on experimental data are detailed, in the respective aims (1) of refining the comparison between numerical and experimental data by taking into account the geometrical spreading effects between two-dimensional and three-dimensional data through an alternative way, and (2) of identifying the reproducibility of the source impact to validate the data reproducibility.

METHODS

Numerical modeling: Spectral Element Method

70 Various numerical methods exist to resolve the equation of motion in arbitrary elastic media. The most widely used for seismic applications is the Finite-Differences (FD) method (Virieux, 1986; Levander, 1988; Robertsson et al., 1994; Pratt, 1990; Stekl and Pratt, 1998; Saenger and Bohlen, 2004) which estimates each derivative on a regular Cartesian grid using a Taylor development (Moczo et al., 2004) of order n . FD is simple to implement
75 and robust but quickly shows some limitations. First the Cartesian grid is defined by the minimum propagated wavelength (λ_{min}) in the full medium which conducts to a very small spatial step in case of low velocities zones it is usually the case for subsurface issues. Moreover, Saenger et al. (2000) show that 60 points by wavelength (λ) are needed to model propagation of Rayleigh wave in order $n = 2$ where only 15 points by λ are required to
80 model propagation of body waves which increases drastically the numerical cost in case of near-surface modeling experiment. Second, the Cartesian grid does not provide a suitable tool to reproduce properly complex topography and interfaces.

To overcome this limit, one can use the Finite-Elements Method (FEM) which is another popular method used for wave propagation modeling (Lysmer and Drake, 1972; Seron et al.,
85 1990; Hulbert and Hughes, 1990). FEM is based on a variational formulation of the equation of motion and gives a continuous approximate solution in space using polynomial basis functions defined on each node of each cell of the mesh. The natural boundary conditions of FEM is the free surface and the triangular (in 2D) or tetraedric (in 3D) unstructured meshes are well adapted to complex media and topography. However, low polynomial basis
90 are inadequate with fine spatial discretization and the required discretization to obtain

precise and non-dispersive solution is numerically costly.

Parallel, at the end of the 20th century, the Spectral Element Method (SEM), widely used in fluid dynamics (Patera, 1984; Korczak and Patera, 1986; Karniadakis, 1989), has been adapted to seismic wave propagation (Komatitsch et al., 1998; Komatitsch and Tromp, 1999; Komatitsch et al., 2005; Festa and Vilotte, 2005). The SEM is a variant of FEM
95 based upon a high-order piecewise polynomial approximation of the weak formulation of the wave equation which leads to a spectral convergence ratio as the interpolation order increases.

In this method, the wave-field is represented in terms of high-degree Lagrange interpolants, and integrals are computed based upon Gauss-Lobatto-Legendre (gll) quadrature. This
100 combination leading to a perfectly diagonal mass matrix leads in turn to a fully explicit time scheme which leads itself very well to numerical simulations on parallel computers.

SEM inherits the flexibility and the natural free surface condition of the FEM (Tromp et al., 2008). The typical element size that is required to generate an accurate mesh is of the order
105 of λ , λ being the smallest wavelength of waves traveling in the model. Models are meshed with quadrangles (2D) and hexaedras (3D) using the open-source software package GMSH (Geuzaine and Remacle, 2009). It is particularly well suited to handle complex geometries and interface matching conditions (Cristini and Komatitsch, 2012). In order to simulate infinite or semi-infinite domain, SEM can use Perfect Match Layers boundary conditions
110 (Bérenger, 1994; Festa and Vilotte, 2005) but are not used here.

Physical modeling: MUSC system

The MUSC system (Bretaudeau et al., 2008, 2011, 2013) is built to experimentally reproduce field seismic data with a great accuracy on reduces scale model. Figure 1 shows the bench and its components : it is composed of a honeycomb tab and two arms which control the
115 source and the receiver position with a precision of $10\ \mu\text{m}$.

The receiving system of MUSC system is a laser interferometer based on a phase shift of the reflected laser signal due to the particular displacement at the surface of the model during the seismic waves propagation in the medium. A real-time calibration value enables a continuous conversion to a nanometric displacement. The focal diameter of the laser
120 on the model surface is about several micrometers and allows a detection limit of $2.5\ \text{nm}$ (few) in the frequency range from $20\ \text{kHz}$ to $20\ \text{MHz}$. The laser interferometer constitutes a non coupled receiver which avoid the complicated modeling of the coupling effect on measurement.

But using a laser source needs more security protocols in the laboratory and up to now,
125 the seismic source in the MUSC laboratory is simulated by a piezoelectric transducer linked to a launching and synchronization system. It allows to choose the source function, i.e., a waveform like a Gauss or Ricker function, the central frequency f_0 and the time delay t_0 . For that, the source is generated by a waveform generator and is then amplified before being transmitted to the small-scale-model.

130 For the purpose of reduced scale modeling, the change of scale must keep the relationship between observables, i.e. amplitudes and time arrivals. Concerning the amplitude, the quality factor Q will be chosen to be in the same range as the materials of near surface. For the time arrivals, the key parameter is the rate between the propagated seismic wavelength

and the spatial dimensions of the experience that includes the model geometry, the spatial
135 increment between the sources and the receivers positions, but also the dimensions of the
source impact. In the framework of seismic physical modeling, this latter must be as close
as possible to a point source in order to simulate the spatial energy repartition of a weight
drop at the soil surface, i.e. with an isotropic directivity of the emitted P waves.

In the MUSC system, the main frequency bands used for reduced scale data are [20 KHz
140 ; 200 KHz] and [300 KHz; 800 KHz], respectively called here "low frequency band" and
"high frequency band". For the lower spectral band, a commercial piezo-electric transducer
is used without any coupling gel. For the higher band, the piezoelectric source is coupled
through a conical adapter which is stucked to the transducer in order to obtain the expected
impact surface. The resulting source pattern is isotropic enough in the spectral band of
145 interest (see (Bretaudeau et al., 2011) for more details).

The lower frequency band is well adapted to simulate seismic experiment applied to near
surface through the scales ratios proposed in tables 1 and 2. In the first case (table 1), a
central frequency of 100 KHz in the laboratory corresponds to a central frequency of 100
Hz on the field, whereas in the second one (table 2) a central frequency of 100 KHz in the
150 laboratory corresponds to a central frequency of 50 HZ on the field. Note that with these
propositions, the quality factor Q and the density ρ are modeled with a ratio equal to 1, i.e.
they remain the same at both of the scales. Actually small-scale models are generally made
of thermoplastic or casting epoxy resin materials (Bretaudeau et al., 2013, 2011, 2008). The
mechanical properties of these materials provide attenuation characteristics close to natural
155 soil materials of subsurface media. Their seismic velocities are about 2 times of those in
subsurface materials as proposed in table 2. The possibilities of combinations can generate
the impedance contrasts encountered in the geophysical issues.

The MUSC bench presented above has been studied for simulating with a great reproducibility the typical field campaigns of subsurface seismic measurement. The validation
160 was achieved by comparison between small scale measurement and numerical data (ref). Results have shown a great reproducibility of the converted and diffracted events recorded on the vertical component. The amplitudes analysis had been conducted through 2D-3D corrections and small discrepancies remained due to the difficulty of taking into account the S and P waves in the same way. For this reason, we propose here to refine the study by
165 testing a more recent correction methodology (ref) as well as providing experimental and numerical, 2D and 3D data. This study will be achieved through data carried out on two models that are presented below.

Reduced-scale models

Reduced-scale models are generally made of melted epoxy-resins. These materials have
170 several advantages: (1) they can be homogeneous and isotropic in the frequency bands of MUSC sources, (2) they have a large set of mechanical properties, close to those of natural soils, and can be modified by adding some charges, (3) they are insensitive to environmental conditions (ambient temperature, humidity) and (4) they allow to reproduce complex geometries. Table 1 presents the mechanical properties of some epoxy-resins widely
175 used to produce reduced-scale models for MUSC.

A key issue in reduced-scale modeling is the preservation of the number of propagated wavelength (N_λ) through the acquisition area between the real model and the reduced-scale model. This leads to a scale ratio k , such as: $\lambda_{real} = k^{-1}\lambda_{reduc}$, where λ_{real} and λ_{reduc} denote the wavelength propagated in the real and reduced-scale models, respectively. Given

180 the frequency bands of the MUSCs sources, the scale ratio k for near-surface experiments is typically around 1000 which means that at reduced-scale meters become millimeters en seconds become milliseconds. Table 2, from Bretaudeau et al. (2011), presents scale ratios for several parameters considering that wave-velocity in natural soil is equal to wave-velocity in reduced-scale model. Considering reduced-scale models have finite dimensions, they are
 185 generally oversized to easily separate reflected waves on boundaries from the rest of the recorded signal.

In this study, we consider two different reduced-scale models. The first one is an homogeneous model made of *F50 pure* epoxy-resin with dimensions $500 \times 504 \times 115 \text{ mm}$. This model, like other homogeneous models, is useful to calibrate the components of MUSC
 190 and validate methods in a first approach. The second model, presented in figure 3 is a two-layered model, named *BiAlt*. This model is made of F50 pure for the top layer and LAB1000 for the bottom layer and shows a central depression of few millimeters.

RESULTS

From point-source to line-source response

In the framework of wave propagation modeling and imaging methods, most of available
 195 algorithms are limited to the two-dimensional approximation especially for computational cost causes. More, a widely used way to validate imaging methods consists in inverse crime while the validity of applications on real dataset is conditioned by strong *a priori* and a weak knowledge of the target. All of these leads to a limited validation of the efficiency imaging methods to recover parameter models. Thus, it is critical for 2D inversion of field
 200 data to accurately correct the geometrical spreading.

Point-source data can be corrected from geometrical spreading using a simple two-steps signal processing: (1) convolving each trace by $\sqrt{t^{-1}}$, where t is the time, to correct the phase shift of $\pi/4$ (2) applying a taper \sqrt{t} to all traces to correct amplitudes. Some variations exist, for examples, using a linear source wavelet estimation method to correct the phase (Bre-
205 taudeau et al., 2013) or applying an offset conditioning (Tran et al., 2013). To correct some biases of these methods, Forbriger et al. (2014) and Schafer et al. (2014) have introduced, and successfully applied to synthetic data, the *hybrid method*. In the *hybrid method* the geometrical spreading correction is conditioned by: (1) the offset, (2) the knowledge of the wave propagation velocities in the medium and (3) a user defined ratio used to smoothly
210 correct amplitudes from near to far offsets. The results are thus strongly dependent of user's *a priori* and attempts. However, this kind of signal corrections are valid only for two-dimensional (x, z) medias invariant along the y -axis.

In other cases, 3D data are corrected or process *on the fly*, or used as is in algorithm using a 2.5D approximation.

215 Thus, the missing step between purely numerical validation and real data applications can be the use of experimental line-source seismograms recorded under controlled conditions.

Here, we take advantage of the experimental framework to explore an alternative approach specific to MUSC system. Figure 4 presents a schematic representation of the principle for this kind of experiment. Theoretically, the stack of all receiver with the same offset
220 will results in a pseudo line-source response. Yet, to simplify the experiment, an other way is to consider only one receiver per offset, on a line perpendicular and centered to the defined line-source. All traces of each common receiver gather are then stacked together to obtain the line-source response. In order to apply this protocol, we have to choose a line-

source's length L sufficiently great to be assimilated to a cylindrical source and above all a
 225 suitable sampling interval Δs between each point-source constituting the pseudo line-source
 to ensure applicability of the *Huygen's principle*.

For this experiment, we choose the homogeneous block of *F50 pure* epoxy-resin. Given
 the material's properties, we choose $L = 240 \text{ mm}$ and $ds = 0.5 \text{ mm}$ which leads to 481
 point-source locations. Four receiver positions have been selected: 45, 50, 55 and 60 mm
 230 offset perpendicular to the line-source. The source wavelet is a Ricker with a central fre-
 quency $f_0 = 100 \text{ kHz}$. Figures 5(a,c) show the signal recorded at one receiver for a line
 of point-sources and for both numerical (figure 5(a)) and experimental (figure 5(b)) mod-
 eling. Note that the quality factor is not took into account for the numerical modeling,
 and for the experimental result, the *PSv*-reflected wavefront is masked by the echo of the
 235 experimental source (which will be considered in the next section). Here, the point-source
 response corresponds to the central trace (distance 0 mm) and the equivalent line-source
 response is the weighted stack of all traces. Comparisons of the point-source and line-source
 responses are presented in figures 5(b) and 5(d), respectively for numerical and experimental
 modeling. Traces are here normalized to be comparable. These comparisons show clearly
 240 the attempted phase shift of $\pi/4$ between point-source and line-source responses, and some
 differences in terms of waveform, especially for the experimental results between 0.08 and
 0.10 *ms*. The same comparisons, for the four source-receiver offsets, are shown in figures
 6(a) and 6(b) for numerical modeling and experimental modeling, respectively. To validate
 our approach to produce experimental line-source responses, we have applied and calibrated
 245 the *hybrid method* (Forbriger et al., 2014; Schafer et al., 2014) on the numerical point-source
 response to obtain the equivalent line-source response. Figure 6(b) presents the compari-
 son between numerical line-source response and equivalent line-source response and shows

that the *hybrid method* is able to produce the equivalent line-source response with a very good agreement in terms of both phase and amplitude. Finally, we have applied the same
 250 correction to the experimental signal (figure 6(d)). This last result shows a good agreement between experimental line-source and equivalent line-source responses up to 0.12 *ms*. Then, the correction of the geometrical spreading seems unable to scale correctly amplitude where echo of the source and *PSv*-reflected wave are superimposed. For the signal at 55 *mm* offset, the largest amplitude difference can be explain by a weaker *signal-to-noise* ratio than
 255 for the the three other offsets in the experimental data.

These results on our approach to generate experimental line-source responses show that the MUSC system is efficient and can produce reliable 2D experimental data suitable for migration-based methods such as FWI.

Experimental source reproducibility

260 We have shown the MUSC system is able to generate high quality 2D experimental seismograms. However, experimental data, as other, must be reproducible to be used as a reference or in an inversion process. As shown by Bretaudeau et al. (2011), the source waveform injected in the reduced-scale model by the piezo-electric source is not similar to the selected theoretical one. Figure 5(c), in previous section, shows clearly multiple wavefront following
 265 the main *P*-wave and, particularly, *S*-wave wavefronts. After Bretaudeau et al. (2011), these multiples are generated inside the conical adapter of the piezo-electric source before being injected in the model. This naturally raises question about the ability of MUSC system to provide reproducible data. To evaluate the reproducibility of the source impact, several physical modeling were performed on the same *F50 pure* homogeneous epoxy-resin block as

270 in previous section.

In a first step, ten realizations have been acquired on this model with a similar geometry setup: 120 receivers positions with an increment $\Delta r = 1 \text{ mm}$ and a minimum source-receiver offset of $o = 10 \text{ mm}$. The numerical wavelet sent to the piezoelectric transducer source is a Ricker function with a central frequency of 100 kHz . Figure 8 shows the resulting central
275 trace ($o = 70 \text{ mm}$) of each realization and **cc** gives the correlation coefficient of each trace with a mean signal calculated using central trace of each of the ten experiments. For each realization, **cc** is always greater than 0.98 which demonstrate the very high reproducibility of data generated by the MUSC system.

In a second step, a unique source wavelet is estimated using a linear source wavelet es-
280 timation method based on a stabilized deconvolution (Pratt, 1999). The source wavelet estimation takes into account the vertical components of the ten experiments together and allows to obtain a mean effective source wavelet. The resulting source wavelet is applied to the synthetic signals (figure 10). The corrected seismograms are in good agreement with the experimental seismograms (correlation coefficients > 0.96) confirms the great efficiency
285 of the wavelet source assessment process.

These last results, based on an average estimated source wavelet show that the effective impulse source emitted by the transducer in the MUSC system measurement bench is stable enough to ensure a robust reproducibility of the source. Therefore, concerning the key issue of the source knowledge, experimental data acquired in the MUSC system can be
290 efficiently processed by imaging methods like Full Waveform Inversion (FWI) with only one estimation step for all the multi-source and multi-receivers data.

However, this last result does not mean that the source will be the same for an experiment

for an other experiment on an other model. Thus, we consider now a more complex model,
called *BiAlt* (figure 3). We generate synthetic seismogram with the 2D SEM algorithm
295 and using the mean effective source wavelet estimated on homogeneous block as a source
function. Figure 11 shows that the synthetic seismogram using the effective source wavelet
is in good agreement with the experimental one...

This last result shows that the MUSC source is stable from an experiment to an other and
can be consequently injected as an input in modeling and imaging methods without any
300 pre-processing or *on the fly* source inversion.

CONCLUSIONS

These two studies allow to refine the capacity of the physical modeling designed for seismic
experiments simulation by 1) completing the validation of the measurement through com-
parison of numerical and experimental data generated by a realistic 2D source line and 2)
assessing the reproductivity of the effective source emitted in a model. These improvements
305 allow to provide and distribute experimental reduced scale data to the scientific community
as benchmark datasets.

PLOTS

Equations

Figures

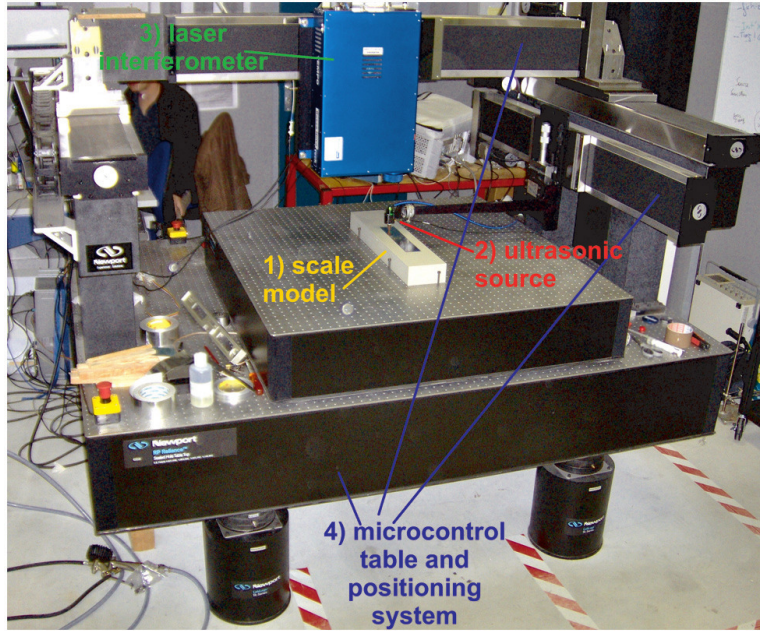


Figure 1: Photograph of the MUSC ultrasonic laboratory (from Bretaudeau et al. (2013)) with its four components: (1) a small-scale model of the underground, (2) an optical table with two automated arms moving above the model, (3) a laser interferometer recording ultrasonic wave propagation at the model surface, (4) a piezoelectric ultrasonic source generating ultrasonic waves in the model.

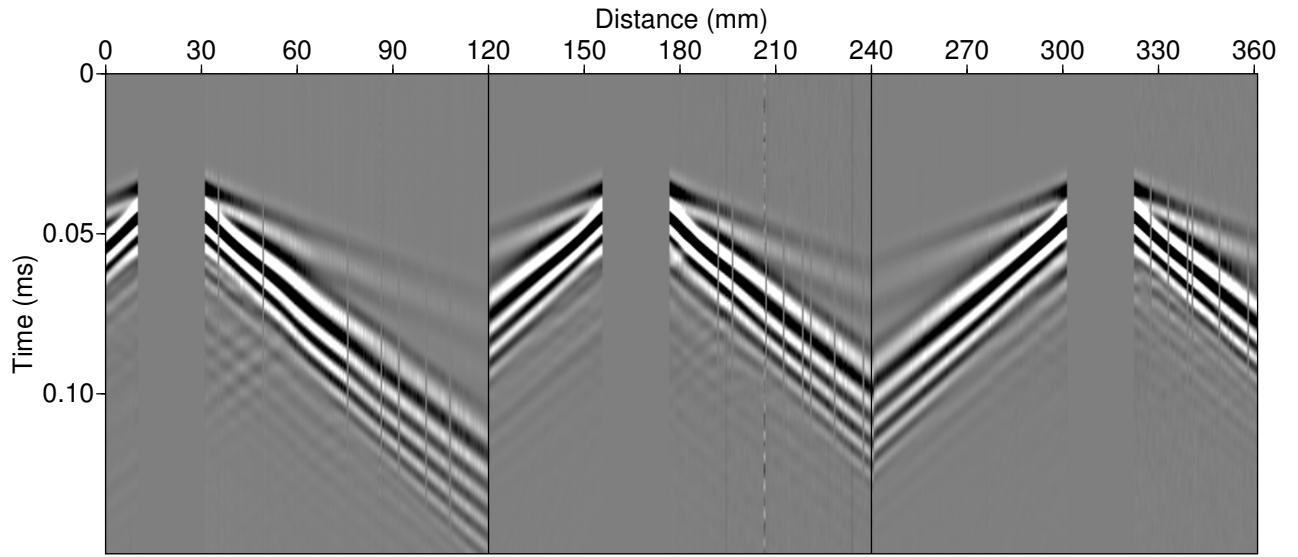


Figure 2: Example of multi-source multi-receiver record on the MUSC system for a two-layer model (balt).

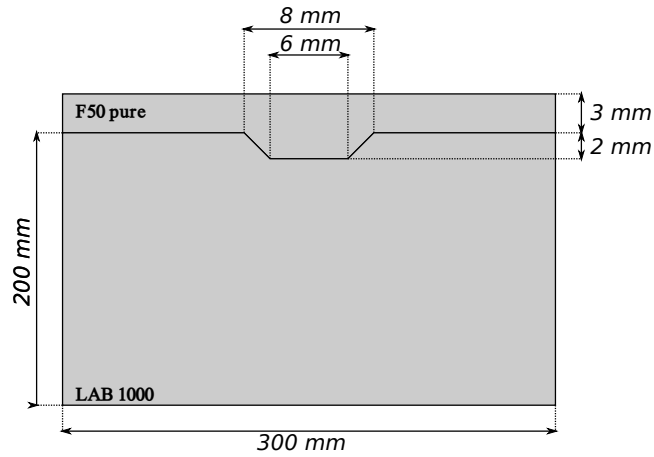


Figure 3: Schematic representation of the so-called *BiAlt* model.

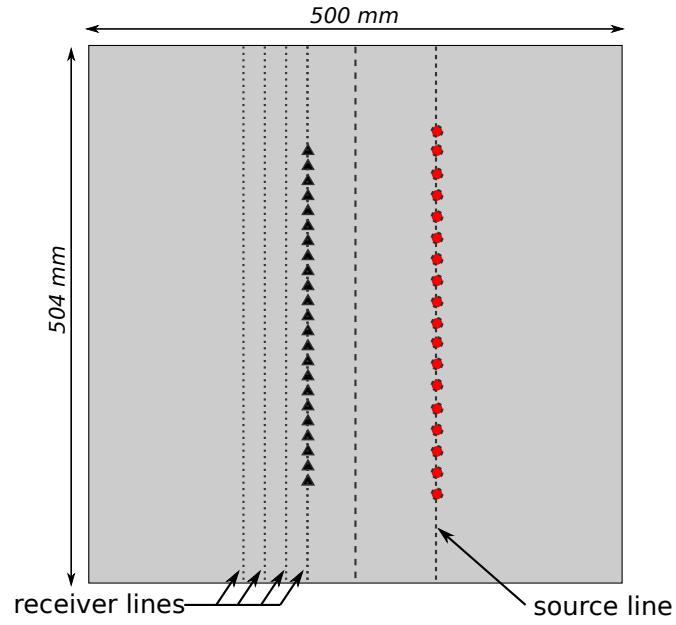


Figure 4: Schematic representation of the acquisition geometry used to generate experimental line-source, *i.e.* an equivalent of cylindrical source use in two-dimensional modeling. Black triangle and red circle represent receivers and sources, respectively.

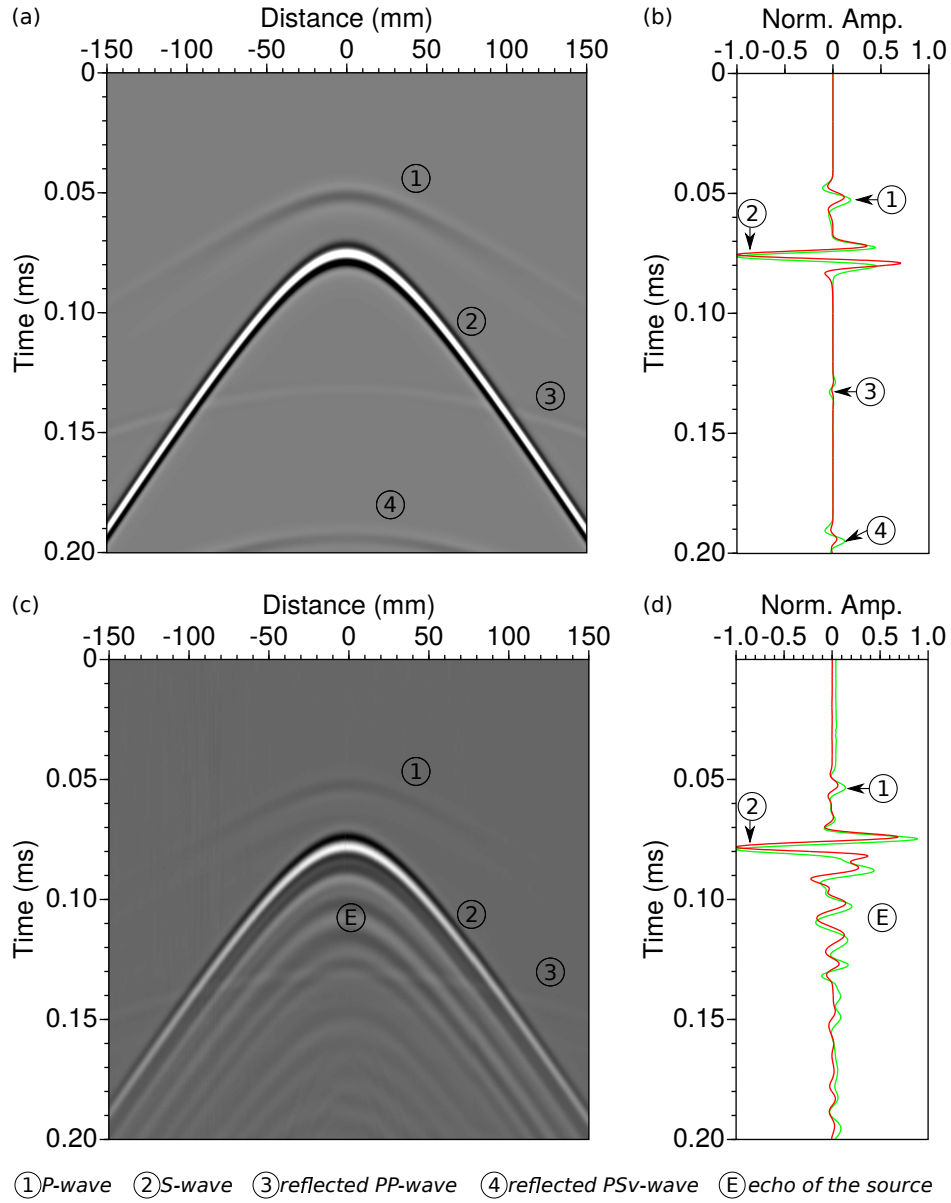


Figure 5: (a,b) Numerical modeling. (a) Resulting seismogram at one receiver position for the experimental line-source. (b) Comparison between point-source response in red (central trace of (a)) and line-source response in green (stack of (a)). (c,d) Same as (a) and (b) but for experimental modeling.

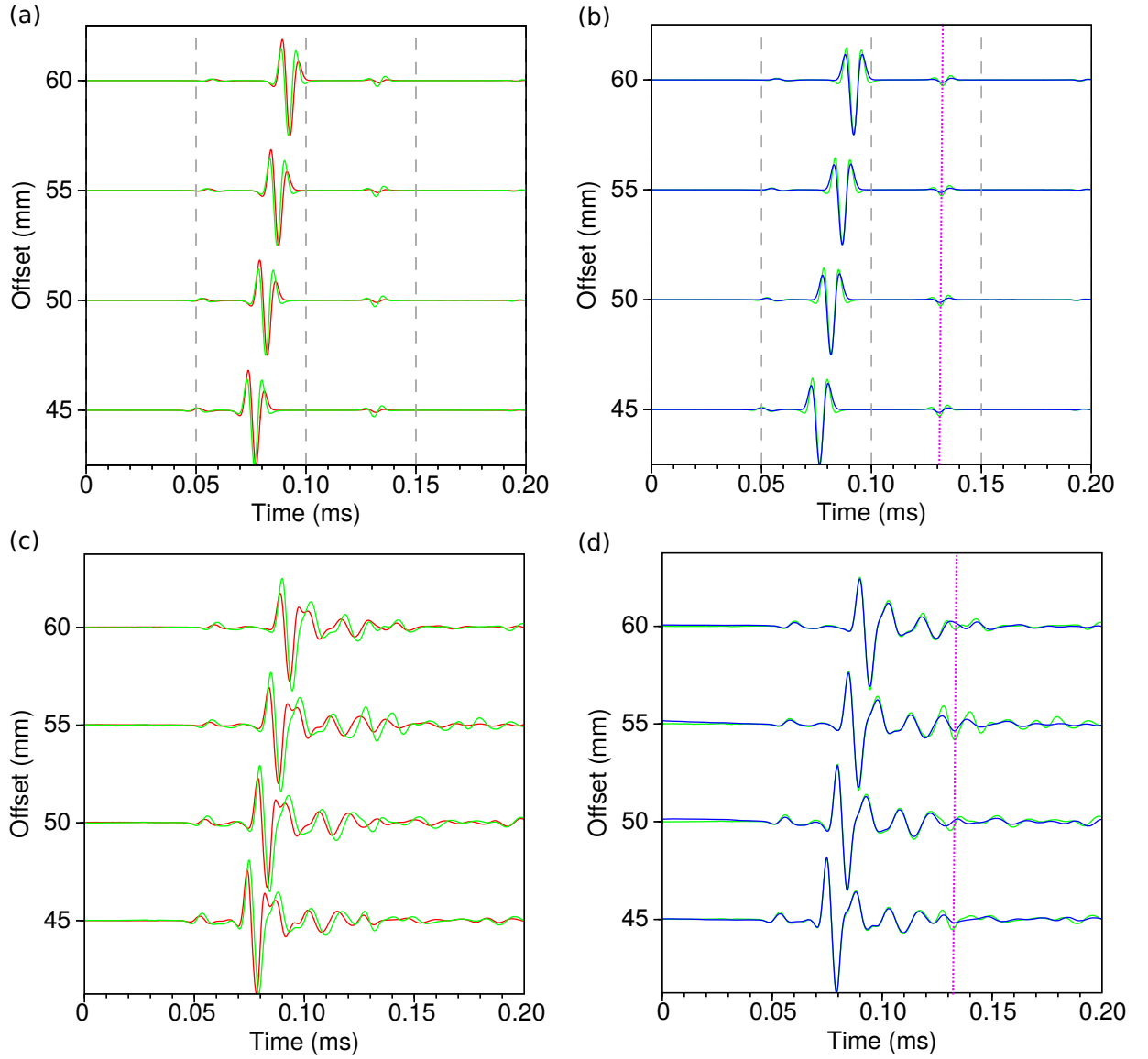


Figure 6: (a,b) Numerical modeling. (a) Comparison between synthetic seismograms for a point-source (red) and for a line source (green), for 45, 50, 55 and 60 mm source-receiver offsets respectively. (b) Comparison between synthetic seismograms for a line-source (green), and a point-source response corrected from geometrical spreading (blue) for same source-receiver offsets as (a). (c,d) Same as (a) and (b) for experimental modeling. The light-purple dotted lines pick PSv -wavefront.

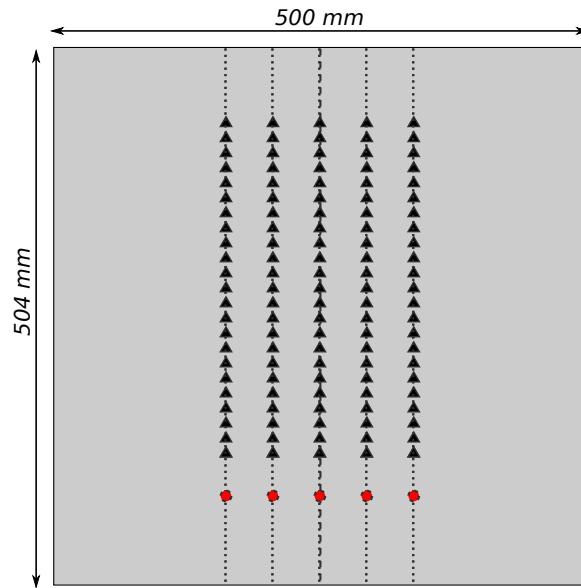


Figure 7: Schematic representation of the acquisition geometry used to assess the data reproducibility using the MUSC system. Black triangle and red circle represent receivers and sources, respectively.

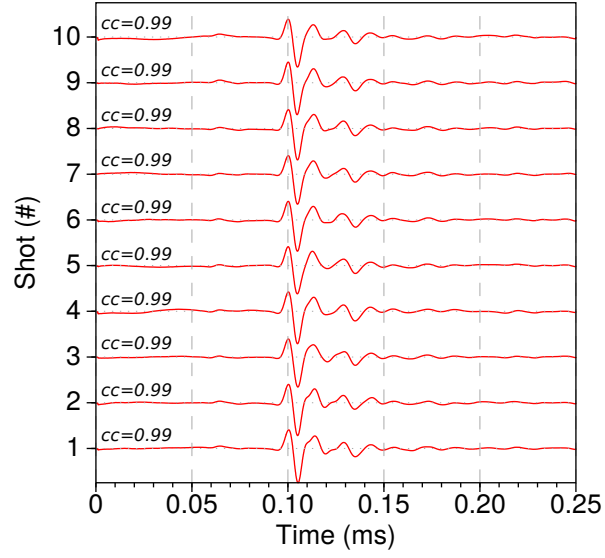


Figure 8: Central trace for each of the ten analogic experiment. **cc** gives the correlation factor of each central trace with respect to a mean trace.

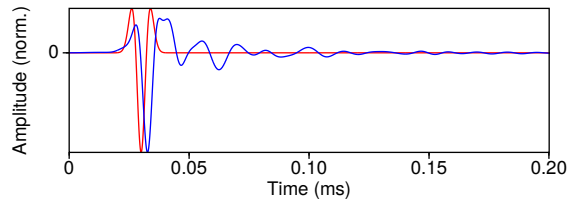


Figure 9: Comparison between the theoritical Ricker source send to the transducer and the effective source wavelet injected in the model.

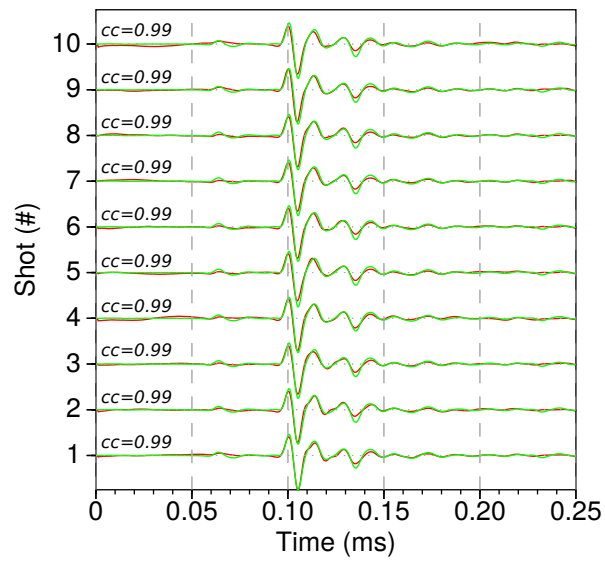


Figure 10: Comparison between analogic central traces (grey) and numerical traces corrected from the estimated effective source (black) for each experiment. **cc** gives the correlation coefficient.

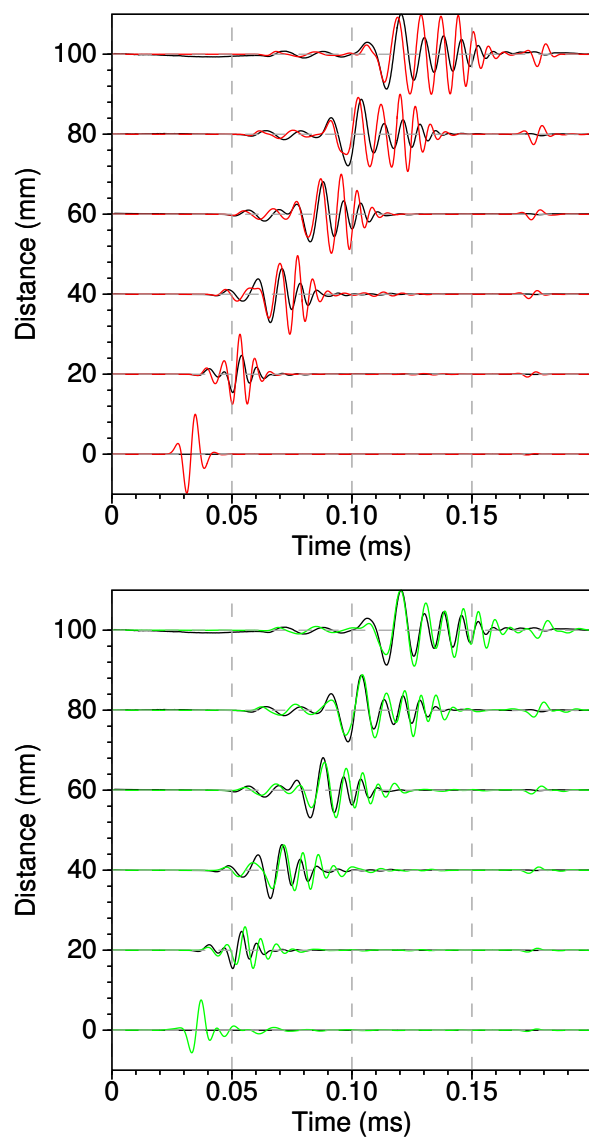


Figure 11: .

Tables

material	V_P (m/s)	V_S (m/s)	V_R (m/s)	ρ (kg/m ³)	Q
Aluminium	5630	3225	–	2700	–
F50 pure	2300	1030	965	1300	30
F50 200%	2820	1425	1328	1766	–
F50 240%	2968	1496	1388	1822	–
LAB1000	2850	1400	1310	1500	75

Table 1: Physical properties of some materials used to build small scale models. V_P , V_S and V_R are the P-wave velocity, S-wave and the Rayleigh wave velocity, respectively. ρ is the density and Q is the quality factor.

Distance	d_{real} (m)	\rightarrow	$k^{-1}d_{reduc}$ (mm)
Wavelength	λ_{real} (m)	\rightarrow	$k^{-1}\lambda_{reduc}$ (mm)
Time	t_{real} (s)	\rightarrow	$k^{-1}t_{reduc}$ (ms)
Velocity	V_{real} (m.s ⁻¹)	\rightarrow	V_{reduc} (m.s ⁻¹)
Density	ρ_{real} (kg.m ⁻³)	\rightarrow	ρ_{reduc} (kg.m ⁻³)
Quality factor	Q_{real}	\rightarrow	Q_{reduc}
Particule displacement	a_{real} (m)	\rightarrow	$k^{-1}a_{reduc}$ (mm)
Particule velocity	c_{real} (m.s ⁻¹)	\rightarrow	c_{reduc} (m.s ⁻¹)

Table 2: Scale ratio between viscoelastic parameters at the real scale and at a scale reduced by a coefficient k (after Bretaudeau et al. (2011)).

	90 mm	95 mm	100 mm	105 mm
$cc1_{init}$	0.702	0.725	0.728	0.728
$rms1_{init}$	0.794	0.760	0.762	0.774
$cc1_{final}$	0.940	0.953	0.951	0.949
$rms1_{final}$	0.358	0.317	0.325	0.343
$cc2_{init}$	0.954	0.987	0.988	0.988
$rms2_{init}$	0.304	0.162	0.155	0.154
$cc2_{final}$	—	—	—	—
$rms2_{final}$	—	—	—	—

Table 3: .

ACKNOWLEDGMENTS

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