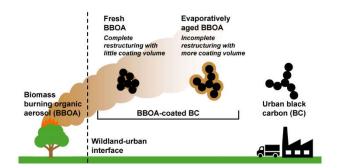
- 1 Effect of biomass burning organic aerosol on the
- 2 structure of black carbon at the wildland-urban
- 3 interface varies with evaporative aging
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## **Environmental significance**

Wildland fires are a significant source of primary organic aerosol, called biomass burning organic aerosol (BBOA). When this material crosses the wildland-urban interface (WUI), it can interact with urban black carbon (BC), uncoated aggregates with fractal, highly branched structures, emitted largely from diesel engines. Specifically, it can partition onto BC, resulting in restructuring due to surface tension and capillary forces. Here, we show in saturator-condenser experiments that fresh BBOA from sources close to the WUI is more effective by volume at restructuring BC than evaporatively aged BBOA from sources far from the WUI. The resulting morphologies dictate how the particles will interact with radiation and water vapor, interactions that govern their direct and indirect effects on climate, respectively.

## Abstract

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Biomass burning organic aerosol (BBOA) and black carbon (BC) play significant roles in climate, via their interactions with light and clouds, as well as public health. BC in the urban atmosphere, largely emitted by diesel vehicles, is initially highly branched and fractal, but it can be restructured upon coating. Urban BC aggregates can be exposed to the components of BBOA when wildfire plumes cross the wildland-urban interface (WUI), which may partition to coat the BC. Here, we investigate the effects of laboratorygenerated BBOA from pine on BC from an inverted diffusion burner. Initially 200 nm BC aggregates were selected using a differential mobility analyzer (DMA) and exposed to different volatility fractions of BBOA. These fractions were prepared by evaporative aging in the laboratory, which mimics evaporative aging with transport in the atmosphere, to give fresh, moderately aged, and most aged BBOA. The resulting mobility diameters with and without removal of the coating were determined using a second DMA. We find that an exceedingly small coating volume of fresh (i.e., higher volatility) BBOA causes complete restructuring while a significantly higher coating volume of most aged (i.e., lower volatility) BBOA is necessary for this same extent of restructuring. Our results highlight the importance of evaporative age of BBOA as wildfire plumes are transported across the WUI into urban environments.

## 1. Introduction

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Black carbon (BC) aggregates affect air quality as well as the radiative balance of the atmosphere, through interactions with light and clouds. 1 BC aggregates are composed of spherical primary particles of elemental carbon arranged in highly branched, fractal morphologies, <sup>2,3</sup> which dictate how the particles interact with light. <sup>4,5</sup> BC aggregates may also accumulate coatings that alter these interactions through lensing effects. <sup>6-8</sup> These coatings may induce restructuring of the BC aggregates, resulting in more compact, closely-packed morphologies.9 Coatings that have been observed to induce BC restructuring in laboratory experiments include water, 10,11 sulphuric acid, 12,13 and secondary organic aerosol (SOA) from a wide range of gaseous precursors: e.g., biogenic isoprene and  $\alpha$ -pinene; <sup>14–17</sup> anthropogenic benzene, <sup>18</sup> toluene, <sup>18,19</sup> ethylbenzene, <sup>18</sup> and m- and p-xylene, <sup>18,20,21</sup> and co-emitted combustion byproducts. <sup>22,23</sup> Water is important also for its ability to plasticize solid organic coatings or deliquesce solid inorganic coatings, such that the liquified coatings can go on to induce restructuring. <sup>24,25</sup> For some coatings, like water, the mechanism of restructuring is evaporation of the coating; 10,26 for others, the mechanism of restructuring is a combination of condensation and evaporation.<sup>27–29</sup> Several models of restructuring have been developed to represent the forces (e.g., capillary and surface tension) acting on the primary particles in coated BC aggregates. 20,30-<sup>32</sup> For initially monodisperse BC, the combination of restructuring and coating has been observed to result in significant absorption enhancement. 13,19,33 In the atmosphere, coated BC aggregates occur across a wide range of morphologies, differing the amount of BC (i.e., few or many primary particles), the amount of coating (i.e., thinly or thickly coated), the compactness of the BC (i.e., branched or closely packed), and the distribution of the coating on the BC (i.e., centric or acentric).<sup>34–36</sup> This wide range of morphologies further complicates the physical and optical properties of BC.<sup>37,38</sup>

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BC is an important component of the urban atmosphere, where it is largely emitted from diesel vehicles.<sup>39,40</sup> The initial morphology of BC from diesel engines has been investigated and shown to be highly branched. 41-43 Branched aggregates produced from diesel engines in the laboratory have been shown to be compacted upon coating. 44,45 Urban BC has also been shown to be coated and compacted in the field. 46–48 Nascent, monodisperse BC introduced into an outdoor semi-permeable chamber, where it was exposed to gaseous species in two urban atmospheres, also was coated and compacted.<sup>33</sup> The occurrence of BC in the urban atmosphere that is initially largely bare contrasts with BC in wildfire plumes that is initially internally mixed with organic aerosol, called biomass burning organic aerosol (BBOA), 49 which influences the physical and optical properties of co-emitted BC as described above. 50-53 Wildfires have been shown to influence the organic composition of suspended particles and deposited films in the urban environment;<sup>54,55</sup> for example, wildfires increase the concentration of polycyclic aromatic hydrocarbons (PAHs) in the urban atmosphere. 55 Several PAHs have been shown to restructure BC aggregates in the laboratory as sub-cooled liquids.<sup>56</sup> Consequently, when wildfire plumes cross the wildland-urban interface (WUI),<sup>57–59</sup> urban BC is exposed to the components of BBOA, which may alter the morphology of the BC aggregates. Furthermore, BBOA is a complex mixture of organic species with wide ranges of physical and chemical properties, 60-62 which may influence its interactions with urban BC.

Here, we focus on the following hypotheses: first, components of BBOA will partition to form coatings on nascent, highly branched BC aggregates and, in turn, induce restructuring to give a more compact, closely-packed morphology; and, second, the effects of BBOA on BC morphology will depend on the physical properties of this complex mixture, which change during transport in the atmosphere. BC was generated using an inverted diffusion flame, and aggregates with an initial mobility diameter of 200 nm were selected using a differential mobility analyzer (DMA). BBOA was generated by thermal degradation of pine wood in a tube furnace, and filter-collected samples were conditioned by evaporative aging. Monodisperse BC was exposed to conditioned BBOA in a saturator-condenser apparatus, and the resulting mobility diameters with and without thermal denuding were monitored using a second DMA coupled to a condensation particle counter (CPC). Our results and their atmospheric implications are discussed below.

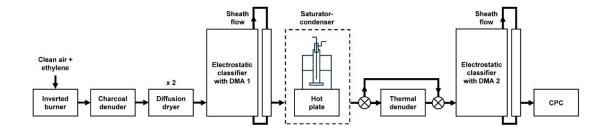
## 2. Materials and methods

#### 2.1. Generation of black carbon

BC was generated using a miniature inverted soot generator (Argonaut) with ethylene as the fuel.<sup>63,64</sup> The flowrates of ethylene (Airgas, Ultra High Purity) and air (Airgas, Ultra Zero Grade) were set to 0.1 and 10 L min<sup>-1</sup>, respectively, using mass flow controllers (Sensirion, SFM5500 Series). The flowrates were verified using a bubble-based calibrator (Sensidyne, Gilibrator 2). As shown in Fig. 1, a small fraction of the output of the soot generator, at a flowrate of 0.3 L min<sup>-1</sup>, was directed through a denuder with a length of

60 cm, consisting of stainless-steel mesh packed in granular activated carbon (Sigma-Aldrich, SBHL1410). This sample was then sent through two diffusion dryers, the first with a length of 43 cm and the second (TSI, 3062) with a length of 44 cm, both packed with indicating silica gel desiccant (Parker, DRP-14-10B). The conditioned aerosol was then directed to an electrostatic classifier (TSI, 3082), equipped with a 0.0457-cm nozzle upstream of the inertial impactor, a soft X-ray advanced aerosol neutralizer (TSI, 3088), and a long DMA (TSI, 3081). The sample and sheath flowrates of the DMA were 0.3 and 3 L min<sup>-1</sup>, respectively. The DMA voltage was set to select particles with an electrical mobility diameter of 200 nm.





**Fig. 1.** Schematic of experimental setup for the generation, coating, and characterization of BC aggregates. The saturator-condenser apparatus consists of a glass bubbler in a sand bath on the hot plate, and the filter-collected and conditioned BBOA is placed at the base of the bubbler while the hot plate temperature is ramped during coating. DMA: differential mobility analyzer; CPC: condensation particle counter.

#### 2.2. Generation and characterization of biomass burning organic aerosol

BBOA was generated by heating pine wood in a tube furnace (Across International, STF1200), described previously.<sup>65,66</sup> A rectangular chip of pine wood was placed at the center of the 5-cm diameter quartz tube that is housed in the furnace. The average mass of pine was about 3.5 g. Air (Airgas, Ultra Zero Grade) was directed through the quartz tube at a flowrate of 1.5 L min<sup>-1</sup>. The tube furnace was programmed to increase in temperature from 25°C to 400°C in 15 min. At 350°C, the generation of BBOA began, a polycarbonate filter holder (Pall, 1119) was connected to the inlet, and BBOA was collected onto a 47-mm fiber filter (Pall, Emfab). BBOA was collected on the filter for about 1 min. The filter-collected BBOA was then stored in a freezer (Fisher, Isotemp) at -15°C for later use in the coating experiments.

In these experiments, BBOA was generated to use as a coating on BC. Three categories of BBOA were used, differing in conditioning, i.e., evaporative aging, and the resulting volatility distribution. In the first category, called fresh, BBOA collected on a filter was used without further conditioning. In the second category, called moderately aged, BBOA on the same filter after the previous experiment was subjected to evaporative conditioning, passing 3 L min<sup>-1</sup> of clean, dry air from a zero-air generator (Aadco, 747-30) over the filter in a 250-mL glass bubbler, heated to 60°C, for 48 h. In the third category, called most aged, BBOA on the same filter after the previous two experiments was subjected to further evaporative conditioning, passing 3 L min<sup>-1</sup> of clear, dry air over the filter, heated to 120°C, for 48 h. The heating was performed on a hot plate using a sand bath, in which the bubbler was immersed about 3 cm from the base. Mass losses with

each step of conditioning were determined gravimetrically using an analytical balance.

Three replicates of this sequence of conditioning were performed.

BBOA was characterized in terms of absorptivity using UV-vis spectroscopy of bulk solutions of BBOA extracted into methanol. Spectra were measured for three filter-collected samples, conditioned respectively to give fresh, moderately aged, and most aged BBOA. Each filter sample was placed in a vial containing 10 mL of methanol (Fisher, >99.8%), and the vial was placed on a roller mixer for 15 min at 60 rpm. The filter paper was removed, dried, and weighed to determine the mass concentration of BBOA in each solution. An aliquot of each solution was used in a 1-cm quartz cuvette for spectroscopic measurements via a modular fiber-optic-based spectrometer, which consists of a balanced deuterium-halogen light source (Ocean Optics, DH-2000-BAL), a cuvette holder with lenses (Thorlabs, CVH100), and a grating-based spectrometer (Ocean Insight, Flame-T-UV-vis).

#### 2.3. Characterization of particles upon coating

BC was coated by passing it over the BBOA collected on filters. The size-selected BC was directed through a clean 250-mL glass bubbler with the selected category of filter-collected BBOA at the bottom (see Fig. 1). The flowrate through the bubbler was 0.3 L min<sup>-1</sup>. Like above, heating was performed using a sand bath. Here, the temperature was increased incrementally, up to 142°C for the most aged, least volatile category of BBOA. Downstream of the bubbler, which serves as the saturator, the sample was returned to room temperature before being directed through one of two paths, alternately. In the

first path, the sample was passed through a 1.8-m thermal denuder, constructed from 1/4" copper tubing, as described previously. 66,67 The temperature of the thermal denuder was set to 200°C. The particles were then directed to a second DMA, which was equipped the same as the first and operated at the same flowrates, and a CPC (TSI, 3750). The sample flowrate of the CPC is 1 L min<sup>-1</sup>, so the difference of 0.7 L min<sup>-1</sup> was sampled from the laboratory through a particle filter. In the second path, the sample bypassed the thermal denuder. In a control experiment, BBOA was also used to coat spherical monodisperse polystyrene latex particles, and sheath flowrates of 3, 4.5, and 6 L min<sup>-1</sup> on the second DMA gave the same mobility diameters for coated particles (see Fig. S1), suggesting that evaporation between the condenser and DMA was insignificant.

## 3. Results and discussion

The filter-collected BBOA was conditioned by preparatory evaporation, flowing clean, dry air through the filters, to produce BBOA differing in evaporative aging and, in turn, volatility and absorptivity. The mass of fresh BBOA collected on the filters was  $110 \pm 10$  mg. After the first step of conditioning, to produce what is here called moderately aged BBOA,  $0.61 \pm 0.02$  of the fresh BBOA mass remained. After the second step of conditioning, to produce the most aged BBOA,  $0.33 \pm 0.04$  of the fresh BBOA mass remained. The fraction remaining for the most aged BBOA closely matches the largest increment used in recent studies of the effects of evaporative aging on the viscosity and absorptivity of BBOA, where this fraction was called PO<sub>3</sub> to denote the volume was reduced by a factor of three from that of the initial pyrolysis oil. 60,68 This preparatory

evaporation mimics in the laboratory the partitioning of BBOA components downwind of a fire, 61,69 and is similar to approaches used previously to simulate evaporative aging. 66,70 Increased evaporative aging is known to result in decreased BBOA volatility. 60,68 The mass absorption coefficient (MAC; see ESI) of the remaining BBOA also increased with evaporative aging, as shown in Fig. 2 for solutions in methanol. All but 0.1 mg of each sample was soluble in methanol. At 365 nm, MAC was 0.26, 0.57, and 0.73 m<sup>2</sup> g<sup>-1</sup> for fresh, moderately aged, and most aged BBOA. The mass of the most aged BBOA is precisely one third that of the fresh, and the MAC at 365 nm of the fresh is just slightly greater than one third that of the most aged. At 405 nm, MAC was 0.07, 0.18, and 0.32 m<sup>2</sup> g<sup>-1</sup> for fresh, moderately aged, and most aged BBOA. The significant increase in MAC with evaporative aging indicates that the most volatile components of BBOA, which partition out of the particle phase, are much less absorptive than the components that remain in the particle phase. This observation is consistent with previous observations for BBOA produced from hardwood pellets and eastern red cedar. 60,66 The variable absorptivity of BBOA will result in different effects on the optical properties of BC aggregates upon coating. 52,53,71

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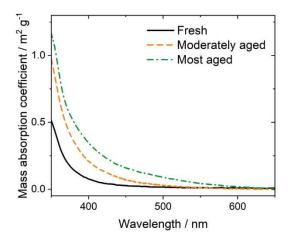
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**Fig. 2.** Mass absorption coefficients for differently conditioned BBOA fractions in methanol solutions.

The conditioned BBOA was used to coat BC aggregates, which were first selected by size at a mobility diameter of 200 nm from the polydisperse size distribution characteristic of the burner and combustion conditions. <sup>63,63</sup> The miniature inverted soot generator produced a stable size distribution of BC, as shown in Fig. S2. We note that the particles selected at 200 nm occur to the right, i.e., higher mobility diameter, than the geometric mean diameter. This choice of initial diameter ensures that singly charged particles are the most abundant, as opposed to doubly or multiply charged particles with larger dimensions. Monodisperse, size-selected particles were monitored using the second DMA in combination with the CPC, stepping through voltages and measuring the resulting number concentration. Representative size spectra are shown in Fig. S3. Changes in morphology upon coating and restructuring were determined by monitoring the monodisperse particles. Each size spectrum was fit to a lognormal peak. The center

of the peak was used to quantify the change in mobility diameter, and the geometric standard deviation was used to ensure the particles remained monodisperse. 72,73

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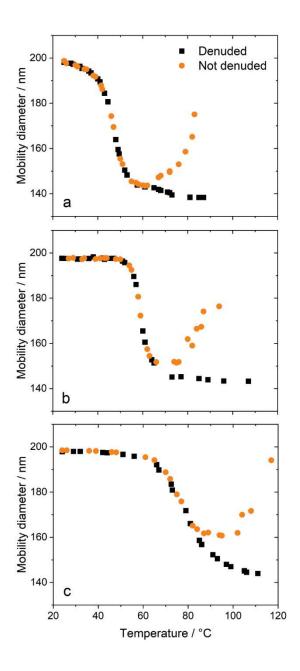
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A representative coating experiment with the moderately aged BBOA is shown in Fig. 3b, in terms of the mobility diameters of both denuded (i.e., coated-uncoated) and non-denuded (i.e., coated) particles as a function of the saturator temperature. The experiment can be divided into three stages. In the first stage, between 20 and 50°C, the denuded and non-denuded particles exhibited the same morphology as the initial sizeselected aggregates. For these saturator temperatures and this BBOA volatility fraction (i.e., moderately aged), the vapor pressures of the components were too low to result in partitioning onto the BC. During the second stage, between 50 and 70°C, the mobility diameters of both classes of particles began decreasing. The denuded particles decreased in diameter throughout this stage, until they approached a plateau for the final, fully restructured aggregates, resulting in a sigmoidal curve. The non-denuded particles (i.e., with coating intact) also decreased in diameter initially during this stage, demonstrating that condensation rather than evaporation is driving most of the restructuring in BBOAcoated BC. This is not the case for all coatings; for example, water is known to cause significant restructuring only upon evaporation, a distinction that may be attributed to whether a coating effectively wets the BC surface or not. 10 This observation also demonstrates that the BBOA coating was a liquid. Fresh BBOA has previously been shown to be liquid. 62,66 While evaporative aging is known to increase the viscosity of BBOA, 60,74 here it was still sufficiently low-viscosity to restructure the aggregates on the experimental timescale, i.e., the residence time between the saturator and the second DMA. The non-denuded particles followed the trend of the denuded particles until a saturator temperature of about 65°C, at which point they diverged, reaching a minimum and beginning to grow. During the third stage of the experiment, between 70 and 110°C, the mobility diameter of the denuded particles reached its plateau, i.e., the aggregates could not restructure further, no matter how much coating material partitioned onto the BC. The mobility diameter of the non-denuded particles continued increasing, as more material was added to the coating, according to the temperature dependence of the vapor pressures of the BBOA components (i.e., governed by the Clausius-Clapeyron equation).<sup>75,76</sup>



**Fig. 3.** Representative experiments with (a) fresh, (b) moderately aged, and (c) most aged BBOA, showing evolution of the mobility diameter of particles with and without thermal denuding as a function of increasing saturator temperature, which drives partitioning of BBOA components onto the BC aggregates.

These three stages of evolution are also observed for BC aggregates coated with fresh and most aged BBOA, but the temperatures associated with the three stages are different. For fresh BBOA, the first stage occurs only at very low temperatures. Already at 30°C, sufficient BBOA begins to partition to result in some restructuring (see Fig. 3a). Again, the trends for denuded and non-denuded particles overlap, indicating that the restructuring occurs during condensation rather than evaporation of the coating in the thermal denuder. For most aged BBOA, the temperature required for restructuring to begin is about 60°C (see Fig. 3c). For fresh BBOA, the two series overlap for the duration of the second stage of restructuring. It is only when the BC cores are fully restructured, reaching the plateau at the final extent of restructuring, that the two series diverge (see Fig. 3a). In other words, very little coating is required to fully restructure the BC aggregates for fresh BBOA. For most aged BBOA, the two datasets diverge halfway through the second stage of evolution (see Fig. 3c), well before the aggregates are fully restructured, indicating that the coating required to induce complete restructuring is higher for this less volatile fraction of BBOA. During the third stage of the experiments, the exponential increase in mobility diameter of the fully restructured aggregates with coating intact is an indication that these particles were spherical. The fully restructured aggregates without coating are known to be not quite spherical, with mass-mobility exponents (see ESI) of about 2.7-2.8 (i.e., less than the value of 3 expected for spheres), 9,18,45 but in an approximation they are taken as spherical here, such that their volume may be estimated from their mobility diameter.

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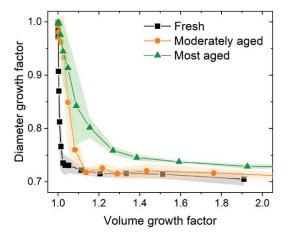
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To estimate the volume of coating, we take the difference between the volume of the coated particles and volume of the restructured cores, with coating removed, both calculated according to their respective mobility diameters (see ESI). This difference is shown in Fig. S4 for a representative experiment with the fresh BBOA, the same as depicted in Fig. 3a. The subtraction of volumes assumes spherical geometries, an approximation that is only reasonable after the BC cores approach their final diameter, during the third stage of the coating experiment, described above. Another constraint is that, at the initial saturator temperature, no BBOA partitioning onto BC occurs, so the coating volume is zero at 25°C. Fitting an exponential function, meant to capture the temperature dependence of the vapor pressures of the BBOA components, to these first and third stages of the coating experiment, we obtain the curve shown in Fig. S4. From this fit, coating volume at any temperature can be estimated by interpolation.

When the diameter growth factor of the restructured BC aggregates without coating is plotted as a function of the volume growth factor of the aggregates with coating intact (see ESI), differences between the BBOA volatility fractions are further evident. As shown in Fig. 4, fresh BBOA (i.e., without any evaporative conditioning before the coating experiment) induced significant restructuring at very low coating volumes. At a volume growth factor of 1.1 (i.e., when the coating volume is 10% of the initial aggregate volume), the diameter growth factor was already approaching its final value of about 0.70. For moderately aged BBOA, the diameter growth factor at the same volume growth factor is about 0.75. In other words, at the same coating volume, this fraction is less effective at restructuring the BC aggregates than the fresh BBOA. For most aged BBOA, the same

volume growth factor of 1.1 leads to a diameter growth factor of only 0.85, about halfway between the initially branched and fully restructured aggregates. To reach the plateau for completely restructured BC aggregates with most aged BBOA, the coating volume must approach 100% of the initial aggregates volume, ten times greater than for fresh BBOA.



**Fig. 4.** Diameter growth factor of coated-denuded BC aggregates as a function of volume growth factor of coated particles for differently conditioned BBOA coatings. Experiments were performed in triplicate, and the shaded regions depict inter-experiment variance in terms of one standard deviation. The individual replicate experiments are shown in Fig. S5.

How can these differences between the volatility fractions of BBOA in terms of their ability to induce restructuring of BC aggregates be rationalized? Based on their study of pure liquid coatings, Chen et al. proposed a single-parameter framework of soot aggregate restructuring.<sup>30</sup> The single parameter,  $\chi$ , is expressed as follows:

$$\chi = \frac{l_{\rm K}}{R_{\rm s}} \frac{1}{\zeta}$$

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where  $l_{\rm K}$  is the Kelvin length,  $R_{\rm S}$  is the radius of the spherical primary particles, and  $\zeta$  is the reduced (i.e., dimensionless) vapor supersaturation of the coating species. In our experiments, the conditions were carefully controlled to give the same initial aggregate morphology,  $^{45}$  so the value of  $R_s$  is expected to be consistent between experiments. The Kelvin length varies with the surface tension of the coating species; however, this effect is smaller than the effect of volatility, through changes in  $\zeta$ . When  $\chi$  is much less than unity, the coating partitions uniformly across the surface of the soot aggregates; when  $\chi$ approaches unity, the coating partitions preferentially into the junctions between neighbouring primary particles, i.e., constituent spherules of the aggregates.<sup>30</sup> By volume, coatings following this latter pathway are more effective at inducing restructuring of BC aggregates. As volatility increases,  $\chi$  increases, as well. Consequently, pure high-vaporpressure coatings (e.g., triethylene glycol and tetradecane) caused aggregates to restructure to their final morphology already at mass growth factors of less than 1.1. In contrast, pure low-vapor-pressure coatings (e.g., dioctyl sebacate and oleic acid) caused aggregates to restructure only partially at the same mass growth factors, a few percent opposed to the final diameter growth factor of 0.80 observed for the high-vapor-pressure coatings. Note the final extent of restructuring is highly dependent on the initial morphology of the soot aggregates, including the size and number of primary particles, <sup>45</sup> so it is not surprising that the final diameter growth factor in our experiments, about 0.70, is different than those reported in the earlier study with pure liquid coatings. More importantly, the relationship between coating volatility and its distribution on the BC aggregates allows us to rationalize our current results: fresh BBOA components on average have higher vapor pressures than evaporatively aged BBOA components, so they partition preferentially in the junctions between primary particles, inducing complete restructuring with little volume.

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#### 4. Atmospheric implications

Our results have broad implications on the interactions between BBOA from wildland fires and BC from urban sources at the WUI. Each volatility fraction of BBOA induced restructuring of BC aggregates upon partitioning, with the coating intact, demonstrating that compaction occurs without coating evaporation. This observation stands in contrast with restructuring induced by water, which requires evaporation, <sup>10</sup> and it is an important feature of the interactions between BBOA and BC, since many BBOA components, with lower volatilities, would not be expected to partition from the coated aggregates back into the gas phase. The restructuring induced by the most aged BBOA also demonstrates that even the most viscous volatility fraction acts as a liquid in the internally mixed particles.<sup>24,56</sup> Furthermore, the differences observed between the fresh, moderately aged, and most aged BBOA demonstrate that volatility largely governs the impact of BBOA coatings on BC aggregate morphology. Fresh BBOA, emitted from wildfires near the WUI, is most effective at restructuring BC aggregates; i.e., coating volumes as little as 10% of the initial BC volume are sufficient to induce complete restructuring of BC aggregates to their final, most closely-packed morphology. As the evaporative age of BBOA increases, for emissions of wildfires at increasing distances from the WUI, the BBOA becomes less effective at inducing soot restructuring. For the most aged BBOA investigated here, 33% by mass of the initial BBOA, coating volumes about 100% of the initial BC volume (i.e., doubling the total particle volume) are required to induce complete restructuring of BC aggregates to their final morphology. Not only is more coating required, less BBOA (i.e., primary) material is available to partition upon dilution of the plume of wildfire emissions. 61,69 This dependence on BBOA volatility can be rationalized in the context of the single-parameter framework of soot restructuring; 30 by volume, less fresh BBOA is required for complete restructuring because this material partitions preferentially into the junctions between neighbouring BC primary particles, whereas aged BBOA partitions more uniformly across the BC aggregate surface. This application of the single-parameter framework to complex mixtures of atmospherically relevant organic species, specifically those emitted from wildland fires, further emphasizes the utility of this framework.<sup>30</sup> As wildfires continue to increase in frequency and severity in many regions, 77,78 wildfire plumes of BBOA are more likely to interact with urban BC at the WUI. The morphology of coated BC aggregates influences their interactions with solar and terrestrial radiation, water vapor, and the respiratory tract, so these volatility-dependent impacts on morphology will influence the effects of BC on human health through climate and air quality.

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## **Conflicts of interest**

There are no conflicts to declare.

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