



SCHOOL OF COMPUTING AND ENGINEERING SCIENCES
BACHELOR OF SCIENCE IN ELECTRICAL AND ELECTRONICS ENGINEERING
2nd SEMESTER 2025/2026
BEE 5214: Multivariate Control Lab_4

DATE: February, 2026

1. Title:

Simulation and practical implementation of CKF + PI Control of a Quadcopter (X Configuration)

2. Objective:

- 2.1 Implement the quadcopter digitized EOM and allocator for quadcopter X configuration.
- 2.2 Use fixed step forward Euler to simulate CKF + PI controller for (i) altitude-only hover and (ii) cascaded altitude + attitude for the quadcopter.
- 2.3 Implement fixed step forward Euler CKF + PI controller for (i) altitude-only hover and (ii) cascaded altitude + attitude for the quadcopter.

3. Learning Outcomes:

By completing this laboratory, students will be able to:

- 3.1 Build body/world dynamics and the mixer A_X from geometry.
- 3.2 Assemble an X quadcopter
- 3.3 Simulate attitude CKF + PI loops with anti-windup and saturation
- 3.4 Simulate attitude and altitude CKF + PI loops with anti-windup and saturation
- 3.5 Understand bandwidth separation between inner attitude and outer altitude loops for the quadcopter.
- 3.6 Implement attitude CKF + PI loops with anti-windup and saturation

4.0 Homework

Print the quadcopter motor mounting chassis and arms and assemble the quadcopter as shown in Fig. 4.2.

Quadcopter (X)

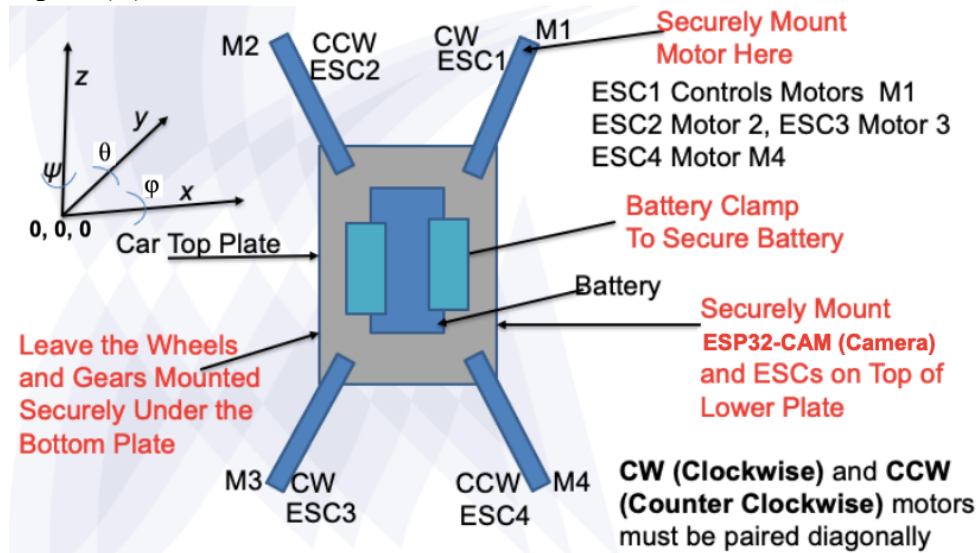


Fig. 4.1 Quadcopter geometry



Fig. 4.2 X Quadcopter assembly

60 Marks

4.1 X Quadcopter EOM

Flying Car (Drone) X Configuration

Body Frame - Refer to Fig. 4.1

- $x \rightarrow$ East $y \rightarrow$ North $z \rightarrow$ Up
- Roll about x Pitch about y Yaw about z

Rigid body states

Position (3) $[x, y, z]$ Velocity (3) $[v_x, v_y, v_z]$

Motor

Motor Input Voltages (4) $[V_1, V_2, V_3, V_4]$ **Motor Currents (4)** $[i_1, i_2, i_3, i_4]$

Motor Speeds (4) $[\omega_1, \omega_2, \omega_3, \omega_4]$

Flying Car (Drone) Model Parameters and Difference Equations

Drone mass M

Motor constants J_m , b_m , k_t , k_b , L , R , τ

Drone angular momentum in x, y, z reference frame I_x (roll) I_y (pitch) I_z (Yaw)

Drone velocity damping coefficients in x, y, z reference frame k_{dx} , k_{dy} , k_{dz}

Drone propeller viscous damping coefficients k_θ , k_ϕ , k_ψ

The drone assembly shown in Fig. 4.2 may have upto 24 state variables;

- (i) Drone position and velocity in x, y, z coordinates - 6 state variables,
- (ii) Drone angular position and speed in x, y and z axis – 6 state variables
- (iii) Drone motor input voltage, current, propeller speed
- 3 state variables for each motor making a total of 12 state variables for 4 motors.

Motor M_1 /Propeller Parameters

R_i Winding resistance	0.1 Ω
L_i Winding inductance	0.002H
k_{bi} Back EMF Constant	0.01 Vs/rad
k_{ti} Torque Constant	0.01 N/A
b_{mi} Motor damping coefficient.	0.00009Ns/rad
J_{mi} Motor/Propeller inertia	0.0004 kgm ²
k_{Qi} Propeller aerodynamic drag coefficient = $C_{Qi}\rho A_i R_i^3$	0.000002 Ns ² /rad ²
k_{Ti} Propeller thrust coefficient = $C_{Ti}\rho A_i R_i^2$	0.000018 Ns ² /rad ²
$k_{dx} = k_{dy}$ Velocity damping	0.15 Ns/m
k_{dz} Velocity damping	0.25 Ns/m
$k_\theta = k_\phi$ Viscous damping	0.002 Ns/rad
k_ψ Viscous damping	0.003

Motor M_1 /Propeller Parameters

C_{Ti} Propeller thrust constant	
C_{Qi} Propeller drag constant	
R_i Propeller radius	
$A_i = \pi R_i^2$ Propeller disc area	
ρ Air density	
l Drone arm	0.1m
Variables	
i_1 Motor current.	20A (Max)
ω_i Propeller speed	
V_i Input voltage	12V (Max)
m Drone mass	1.5 kg
$I_x = I_y$	0.02 kgm ²
I_z Angular momentum	0.04 kgm ²
T_s Sampling time	0.004s
g Gravity acceleration	9.81 ms ⁻²

Motor Electrical Dynamics

$$L_i \frac{di_i}{dt} = -R_i i_i - k_{bi} \omega_i + V_i$$

Motor Mechanical Dynamics

$$J_{mi} \dot{\omega}_i = k_{ti} i_i - b_{mi} \omega_i - k_{Qi} \omega_i^2$$

Thrust and Torques

$$T = \sum_{i=1}^4 k_{Ti} \omega_i^2$$

X-configuration torques:

$$\begin{aligned} \tau_\phi &= \frac{l}{\sqrt{2}} (k_{T2} \omega_2^2 + k_{T3} \omega_3^2 - k_{T1} \omega_1^2 - k_{T4} \omega_4^2) \\ \tau_\theta &= \frac{l}{\sqrt{2}} (k_{T1} \omega_1^2 + k_{T2} \omega_2^2 - k_{T3} \omega_3^2 - k_{T4} \omega_4^2) \\ \tau_\psi &= k_{Q1} \omega_1^2 - k_{Q2} \omega_2^2 + k_{Q3} \omega_3^2 - k_{Q4} \omega_4^2 \end{aligned}$$

Translational Dynamics

$$\begin{aligned} \dot{x} &= v_x & \dot{y} &= v_y & \dot{z} &= v_z \\ m \dot{v}_x &= T(\cos\phi \sin\theta \cos\psi + \sin\phi \sin\psi) - k_{dx} v_x \\ m \dot{v}_y &= T(\cos\phi \sin\theta \sin\psi - \sin\phi \cos\psi) - k_{dy} v_y \\ m \dot{v}_z &= T(\cos\phi \cos\theta) - mg - k_{dz} v_z \end{aligned}$$

Rotational Dynamics (gyroscopic)

$$\begin{aligned} I_x \dot{p} &= \tau_\phi + (I_y - I_z)qr - k_\phi p \\ I_y \dot{q} &= \tau_\theta + (I_z - I_x)pr - k_\theta q \\ I_z \dot{r} &= \tau_\psi + (I_x - I_y)pq - k_\psi r \end{aligned}$$

Euler Kinematics

$$\dot{\phi} = p + q \sin \phi \tan \theta + r \cos \phi \tan \theta$$

$$\dot{\theta} = q \cos \phi - r \sin \phi$$

$$\dot{\psi} = \frac{q \sin \phi + r \cos \phi}{\cos \theta}$$

Hover equilibrium: $\phi = \theta = 0 \quad p = q = r = 0 \quad v_x = v_y = v_z = 0. \quad \omega_i = \omega_h$ (hover speed)

$$\text{Hover condition:} \quad 4k_T \omega_h^2 = mg \quad \omega_h = \frac{1}{2} \sqrt{\frac{mg}{k_T}}$$

State vector:

$$X = [i_1, i_2, i_3, i_4, \omega_1, \omega_2, \omega_3, \omega_4, x, y, z, v_x, v_y, v_z, \phi, \theta, \psi, p, q, r]^T$$

Control inputs (Motor voltages):

$$U = [V_1, V_2, V_2, V_2]^T$$

4.2 Forward Euler Discretization

Motor Dynamics

Electrical:

$$i_{i,k+1} = i_{i,k} + \frac{T_s}{L_i} (-R_i i_{i,k} - k_{bi} \omega_{i,k} + V_{i,k})$$

Mechanical:

$$\omega_{i,k+1} = \omega_{i,k} + \frac{T_s}{J_{mi}} (k_{ti} i_{i,k} - b_{mi} \omega_{i,k} - k_{Qi} \omega_{i,k}^2)$$

Translational Dynamics

$$\begin{aligned} v_{x,k+1} &= v_{x,k} + \frac{T_s}{m} [T_k (\cos \phi_k \sin \theta_k \cos \psi_k + \sin \phi_k \sin \psi_k) - k_{dx} v_{x,k}] \\ v_{y,k+1} &= v_{y,k} + \frac{T_s}{m} [T_k (\cos \phi_k \sin \theta_k \sin \psi_k - \sin \phi_k \cos \psi_k) - k_{dy} v_{y,k}] \\ v_{z,k+1} &= v_{z,k} + \frac{T_s}{m} [T_k (\cos \phi_k \cos \theta_k) - mg - k_{dz} v_{z,k}] \end{aligned}$$

Position update:

$$x_{k+1} = x_k + T_s v_{x,k}, \quad y_{k+1} = y_k + T_s v_{y,k}, \quad z_{k+1} = z_k + T_s v_{z,k}$$

Body Rotational Dynamics

$$\begin{aligned} p_{k+1} &= p_k + \frac{T_s}{I_x} [\tau_{\phi,k} + (I_y - I_z)q_k r_k] - k_\phi p_k \\ q_{k+1} &= q_k + \frac{T_s}{I_y} [\tau_{\theta,k} + (I_z - I_x)p_k r_k] - k_\theta q_k \\ r_{k+1} &= r_k + \frac{T_s}{I_z} [\tau_{\psi,k} + (I_x - I_y)p_k q_k] - k_\psi r_k \end{aligned}$$

Euler Angle Kinematics

$$\phi_{k+1} = \phi_k + T_s[p_k + q_k \sin \phi_k \tan \theta_k + r_k \cos \phi_k \tan \theta_k]$$

$$\theta_{k+1} = \theta_k + T_s[q_k \cos \phi_k - r \sin \phi_k]$$

$$\psi_{k+1} = \psi_k + T_s \left[\frac{q_k \sin \phi_k + r \cos \phi_k}{\cos \theta_k} \right]$$

4.3 Write Python code to simulate and plot CKF-PI Altitude/Hover

Initial Conditions:

All states initialized to zero

Motors initialized to hover speed:

$$\omega_h = \frac{1}{2} \sqrt{\frac{mg}{k_T}}$$

$$\omega_h > 450 \text{ rad/s}$$

Total Thrust

$$T_k = \sum_{i=1}^4 k_T \omega_{i,k}^2$$

PI Attitude Control

$$u_\phi = K_{p\phi} e_\phi + K_{i\phi} \int e_\phi dt$$

$$u_\theta = K_{p\theta} e_\theta + K_{i\theta} \int e_\theta dt$$

$$u_\psi = K_{p\psi} e_\psi + K_{i\psi} \int e_\psi dt$$

Where:

$$e_\phi = \phi_{ref} - \hat{\phi}$$

CKF-estimated states are used.

Motor Voltage Mixing (X Configuration)

$$\mathbf{V} = \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix} = V_{hover} + M^{-1} \begin{bmatrix} u_\phi \\ u_\theta \\ u_\psi \\ 0 \end{bmatrix}$$

Cubature Kalman Filter (CKF)

State Model

$$x_{k+1} = f(x_k, u_k) + w_k$$

Measurement Model

$$y_k = [z \quad \phi \quad \theta \quad \psi]^T + v_k$$

CKF Algorithm

For n states:

- (i) Generate $2n$ cubature points:

$$\xi_i = \sqrt{n} e_i$$

- (iii) Time update:

- Propagate cubature points through nonlinear dynamics.
- Compute predicted mean and covariance.

- (iv) Measurement update:

- (v) Propagate cubature points through measurement equation.

- (vi) Compute Kalman gain.

Required Plots

- (i) Motor voltages V_1-V_4
- (ii) Motor currents i_1-i_4
- (iii) Propeller speeds $\omega_1-\omega_4$
- (iv) Height $z(t)$
- (v) Roll, pitch, yaw response

40 Marks

4.4 Write Python to simulate CKF + PI Attitude + Altitude Control with velocity (v_x)

Altitude PI Controller

$$u_z = K_{pz}e_z + K_{iz}\int e_z dt$$

$$e_z = z_{ref} - \hat{z}$$

Thrust Command

$$T_{cmd} = mg + u_z$$

Desired hover speed:

$$\omega_{cmd} = \sqrt{\frac{T_{cmd}}{4k_T}}$$

Forward Velocity Generation

$$\theta_{ref} = K_v(v_{x,ref} - \hat{v}_x)$$

Cascaded control structure:

Altitude \rightarrow Thrust \rightarrow Velocity \rightarrow Pitch \rightarrow Torque \rightarrow Motor Voltages

Required Plots

- (i) Motor voltages
- (ii) Motor currents
- (iii) Propeller speeds
- (iv) Height $z(t)$
- (v) Forward velocity $v_x(t)$
- (vi) Pitch angle response

Tune attitude and altitude PI controller gains to achieve

Performance Metric	Requirement
Height overshoot	$< 10\%$
Settling time	< 3 s
Forward velocity tracking	$< 5\%$ error
Attitude steady state error	≈ 0

50 Marks

5 Practical

5.1 Implement the CKF-PI Altitude/Hover Controller

Convert the and run the Python code written in 4.3 with actual propeller speed measurement on the drone assembled in 4.0 and shown in Fig. 4.2

Take a video of your drone hovering.

6. Lab Report

20 Marks

6.1 Use these guidelines

<https://drive.google.com/drive/u/2/folders/11saKDjuLBwEa5uQg5ynakZ3JinBQyGKl>
to write and upload your individual lab report detailing your journey through items 1 to 6.

6.2.1 Questions

- (i) Why is CKF preferred over EKF for this system
- (ii) What happens if motor dynamics are ignored?
- (iii) How does Euler discretization affect stability?
- (iv) What happens if sampling time increases?

References

1. S. Skogestad and I. Postlethwaite, *Multivariable Feedback Control: Analysis and Design*, 2nd ed., Wiley.
2. K. J. Åström and R. M. Murray, *Feedback Systems: An Introduction for Scientists and Engineers*, Princet