

# Summary of TTK4115

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## 1 Matrix stuff

**Nullity**  $\text{nul}(A) = \text{No. of columns of } A - \text{rank}(A)$

**Positive definite** A symmetric  $n \times n$  real matrix  $M$  is *positive definite* if all its eigenvalues are positive. (Or if  $\mathbf{z}^T M \mathbf{z} > 0$  for every non-zero vector  $\mathbf{z}$  of  $n$  real numbers.) It is positive *semidefinite* if all eigenvalues are positive or zero.

**Singularity** A square matrix is singular if it is not invertible, i.e. if its determinant is 0.

**Matrix exponential (diagonal)**

$$A = \begin{bmatrix} a_1 & \cdots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \cdots & a_n \end{bmatrix} \implies e^{At} = \begin{bmatrix} e^{a_1 t} & \cdots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \cdots & e^{a_n t} \end{bmatrix}$$

**Matrix exponential (Cayley-Hamilton Method)**

$$e^{At} = \sum_{k=0}^{n-1} \alpha_k A^k \quad \text{with } \alpha_0 \cdots \alpha_{n-1} \text{ determined by } e^{\lambda_i t} = \sum_{k=0}^{n-1} \alpha_k \lambda_i^k$$

**Matrix exponential (Laplace method)**

$$e^{At} = \mathcal{L} \left\{ (sI - A)^{-1} \right\}$$

**Matrix exponential (Jordan form)**

$$e^{At} = Q e^{\bar{A}t} Q^{-1} \quad \text{where } \bar{A} = Q^{-1} A Q$$

**Matrix exponential (series expansion)**

$$e^A = I + A + \frac{1}{2}A^2 + \frac{1}{6}A^3 + \cdots + \frac{1}{(q-1)!}A^{q-1} \quad \text{where } A^q = 0$$

**Controllability matrix**

$$C = [B \quad AB \quad A^2B \quad \dots \quad A^{n-1}B]$$

**Observability matrix**

$$O = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

**Minimal realisation** Given a transfer function; a state-space model that is controllable and observable, and has the same input-output behaviour as the function, is minimal.

## 2 Eigen stuff

**Eigenvalues** Values of  $\lambda$  such that  $\Delta(\lambda) = |\lambda I - A| = 0$ .

**Eigenvectors** Vectors  $\mathbf{v}$  such that  $(A - \lambda I)\mathbf{v} = 0$ .

## 3 Stability

**Asymptotic stability** Occurs if all poles have strictly negative real parts.

**Instability** Occurs if one or more poles have positive real parts.

**Marginal stability** Occurs when the real part of every pole is non-positive, at least one pole has zero real value, and there are no repeated poles on the imaginary axis.

**BIBO stability** If bounded input  $\rightarrow$  bounded output. Defined for the zero-state response (initially relaxed system). See Section 4.

**Lyapunov stability** If every finite initial state gives a finite response. I.e. the zero-input response.

## 4 BIBO Stability

### 4.1 BIBO Stability for Continuous Systems

A continuous system is BIBO stable *iff*:

- (SISO)  $g(t)$  is absolutely integrable in  $[0, \infty)$  or  $\int_0^\infty |g(t)| dt \leq M < \infty$  for some constant  $M$ .
- (SISO/MIMO) Every pole of every transfer function in  $\hat{G}(s)$  or  $\hat{g}(s)$  has a negative real part.

## 4.2 BIBO Stability for Discrete Systems

A discrete system is BIBO stable iff:

- Every pole of every transfer function in  $\hat{G}(s)$  or  $\hat{g}(s)$  has magnitude less than 1.

## 4.3 Lyapunov Stability for Linear Systems

An LTI system  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x}$  is stable if there exists a *symmetric* positive definite matrix  $\mathbf{P}$  that satisfies the Lyapunov Equation

$$\mathbf{A}^T \mathbf{P} + \mathbf{P} \mathbf{A} = -\mathbf{N}$$

Where  $\mathbf{N}$  is an arbitrary positive definite matrix.

## 5 Discretisation

$$\mathbf{A}_d = e^{\mathbf{A}T}, \quad \mathbf{B}_d = \int_0^T e^{\mathbf{A}\tau} d\tau \mathbf{B}, \quad \mathbf{C}_d = \mathbf{C}, \quad \mathbf{D}_d = \mathbf{D}$$

## 6 Similarity transform

A linear change of coordinates where the original object is expressed with respect to a different basis. The representation of  $\mathbf{x}$  with respect to the basis  $\{\mathbf{q}_1, \dots, \mathbf{q}_n\}$  is  $\bar{\mathbf{x}}$  and with  $\mathbf{Q} = [\mathbf{q}_1, \dots, \mathbf{q}_n]$ , the similarity transform is

$$\mathbf{x} = \mathbf{Q}\bar{\mathbf{x}}.$$

The system originally expressed as

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$$

$$\mathbf{y} = \mathbf{C}\mathbf{x} + \mathbf{D}\mathbf{u}$$

is transformed to

$$\dot{\bar{\mathbf{x}}} = \bar{\mathbf{A}}\bar{\mathbf{x}} + \bar{\mathbf{B}}\mathbf{u}$$

$$\mathbf{y} = \bar{\mathbf{C}}\bar{\mathbf{x}} + \bar{\mathbf{D}}\mathbf{u}$$

where

$$\bar{\mathbf{A}} = \mathbf{Q}^{-1} \mathbf{A} \mathbf{Q}, \quad \bar{\mathbf{B}} = \mathbf{Q}^{-1} \mathbf{B}, \quad \bar{\mathbf{C}} = \mathbf{C} \mathbf{Q}, \quad \bar{\mathbf{D}} = \mathbf{D}$$

## 7 Jordan canonical form

General strategy:

1. Find all eigenvectors corresponding to an eigenvalue of  $\mathbf{A}$ .
2. The number of L.I. eigenvectors is the number of Jordan blocks.
3. For each eigenvector  $\mathbf{q}$ , solve  $(\lambda \mathbf{I} - \mathbf{A})\mathbf{v} = \mathbf{q}$  for the vector  $\mathbf{v}$ .

## 8 Statistics

**Expected value**  $E[X] = \int_{-\infty}^{\infty} xf(x) dt$

**Variance**  $\text{Var}(X) = E[(X - E[X])^2] = E[X^2] - (E[X])^2$

**Autocorrelation**  $R_X(t_1, t_2) = E[X(t_1)X(t_2)]$

**Wide-sense stationary process**  $X(t)$  is WSS if its mean and autocorrelation functions are time invariant:  $E[X(t)] = \nu$  and  $R_X(t_1, t_2) = f(t_2 - t_1)$ .

**Spectral density function**  $S_X(j\omega) = \mathcal{F}\{R_X(\tau)\}$

**Gauss–Markov process** A stationary Gaussian process  $X(t)$  that has an exponential autocorrelation is called a *Gauss–Markov* process.

$$R_X(\tau) = \sigma^2 e^{-\beta|\tau|}$$

$$S_X(j\omega) = \frac{2\sigma^2\beta}{\beta^2 + \omega^2} \quad \text{or} \quad S_X(s) = \frac{2\sigma^2\beta}{\beta^2 - s^2}$$

## 9 Linear-quadratic regulator

A system is given as

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$$

with a state feedback  $\mathbf{u} = -\mathbf{K}\mathbf{x}$  chosen to minimise the cost function

$$J = \int_0^{\infty} \mathbf{x}^T \mathbf{Q} \mathbf{x} + \mathbf{u}^T \mathbf{R} \mathbf{u} dt$$

where  $\mathbf{Q}$  is symmetric and positive semidefinite,  $\mathbf{R}$  is symmetric and positive definite, and  $\mathbf{K} = \mathbf{R}^{-1}\mathbf{B}^T\mathbf{P}$ . The matrix  $\mathbf{P}$  is found by solving

$$\mathbf{A}^T\mathbf{P} + \mathbf{P}\mathbf{A} - \mathbf{P}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^T\mathbf{P} + \mathbf{Q} = \mathbf{0}$$

The relative values of the elements of  $\mathbf{Q}$  and  $\mathbf{R}$  enforce tradeoffs between the magnitude of the control action and the speed of the response. The equilibrium can be shifted from  $\mathbf{0}$  to  $\mathbf{x}_{\text{eq}}$  by instead using  $\mathbf{u} = \mathbf{P}\mathbf{x}_{\text{eq}} - \mathbf{K}\mathbf{x}$ .

## 10 Kalman filter

The system is given as:

$$\mathbf{x}_{k+1} = \mathbf{A}\mathbf{x}_k + \mathbf{B}\mathbf{u}_k + \mathbf{w}_k$$

$$\mathbf{z}_k = \mathbf{H}_k\mathbf{x}_k + \mathbf{v}_k$$

The Kalman measurement update equations are:

$$\mathbf{K}_k = \mathbf{P}_k^- \mathbf{H}_k^T (\mathbf{H}_k \mathbf{P}_k^- \mathbf{H}_k^T + \mathbf{R}_k)^{-1}$$

$$\hat{\mathbf{x}}_k = \hat{\mathbf{x}}_k^- + \mathbf{K}_k (\mathbf{z}_k - \mathbf{H}_k \hat{\mathbf{x}}_k^-)$$

$$P_k = (\mathbf{I} - \mathbf{K}_k \mathbf{H}_k) P_k^- (\mathbf{I} - \mathbf{K}_k \mathbf{H}_k)^T + \mathbf{K}_k \mathbf{R}_k \mathbf{K}_k^T$$

And the time update equations are:

$$\hat{\mathbf{x}}_{k+1}^- = \mathbf{A} \hat{\mathbf{x}}_k + \mathbf{B} \mathbf{u}_k$$

$$P_{k+1}^- = \mathbf{A} P_k \mathbf{A}^T + \mathbf{Q}_k$$

## 11 Extended Kalman filter

The system is given as:

$$\mathbf{x}_{k+1} = \mathbf{f}(\mathbf{x}_k, \mathbf{u}_k) + \mathbf{w}_k$$

$$\mathbf{y}_k = \mathbf{h}(\mathbf{x}_k) + \mathbf{v}_k$$

The Kalman measurement update equations are:

$$\mathbf{K}_k = P_k^- C_k^T (C_k P_k^- C_k^T + \mathbf{R})^{-1}$$

$$\hat{\mathbf{x}}_k = \hat{\mathbf{x}}_k^- + \mathbf{K}_k \left( \mathbf{y}_k - \mathbf{h}(\hat{\mathbf{x}}_k^-) \right)$$

$$P_k = (\mathbf{I} - \mathbf{K}_k C_k) P_k^- (\mathbf{I} - \mathbf{K}_k C_k)^T + \mathbf{K}_k \mathbf{R}_k \mathbf{K}_k^T$$

And the time update equations are:

$$\hat{\mathbf{x}}_{k+1}^- = \mathbf{f}(\hat{\mathbf{x}}_k, \mathbf{u}_k)$$

$$P_{k+1}^- = \mathbf{A}_k P_k \mathbf{A}_k^T + \mathbf{Q}_k$$

Where:

$$\mathbf{A}_k = \left. \frac{\partial \mathbf{f}}{\partial \mathbf{x}_k} \right|_{\mathbf{x}_k = \hat{\mathbf{x}}_k} \quad \text{and} \quad \mathbf{C}_k = \left. \frac{d\mathbf{h}}{d\mathbf{x}_k} \right|_{\mathbf{x}_k = \hat{\mathbf{x}}_k^-}$$