

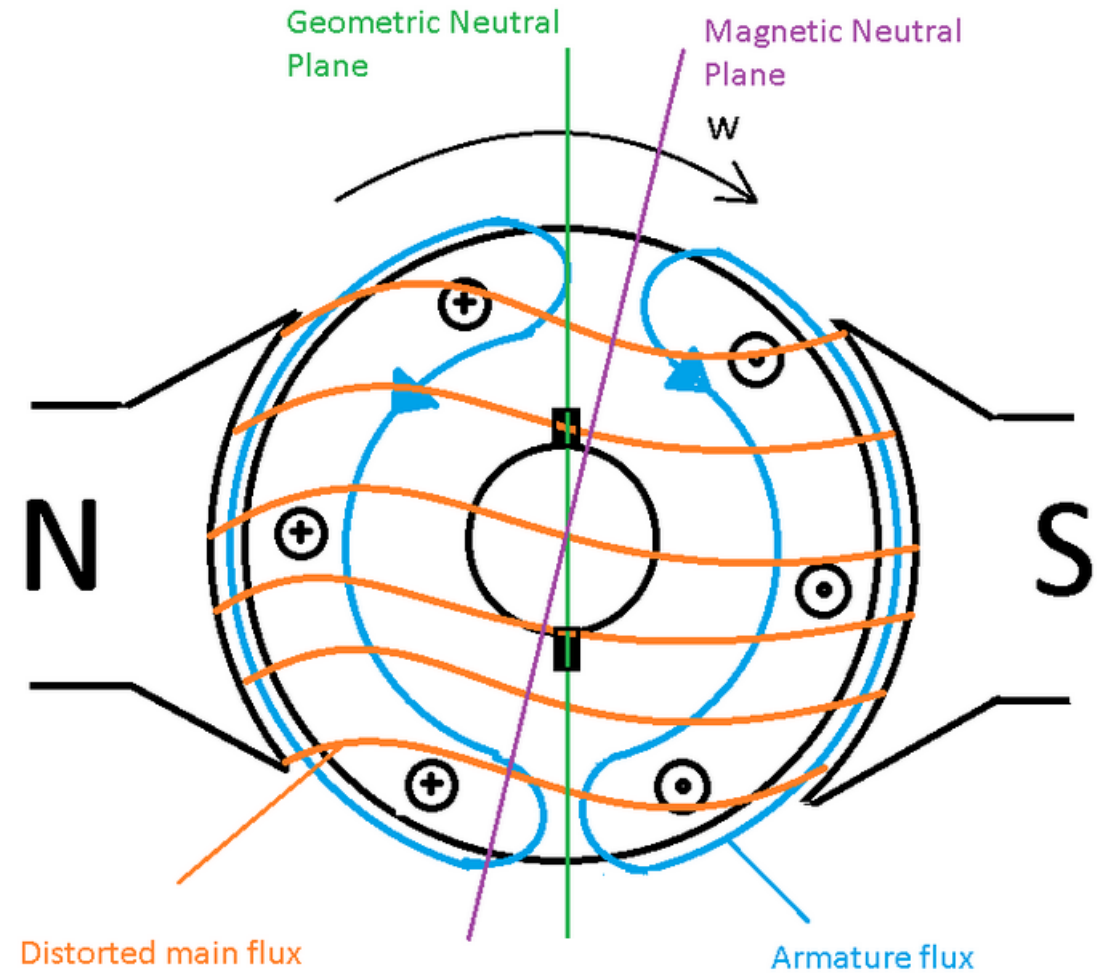
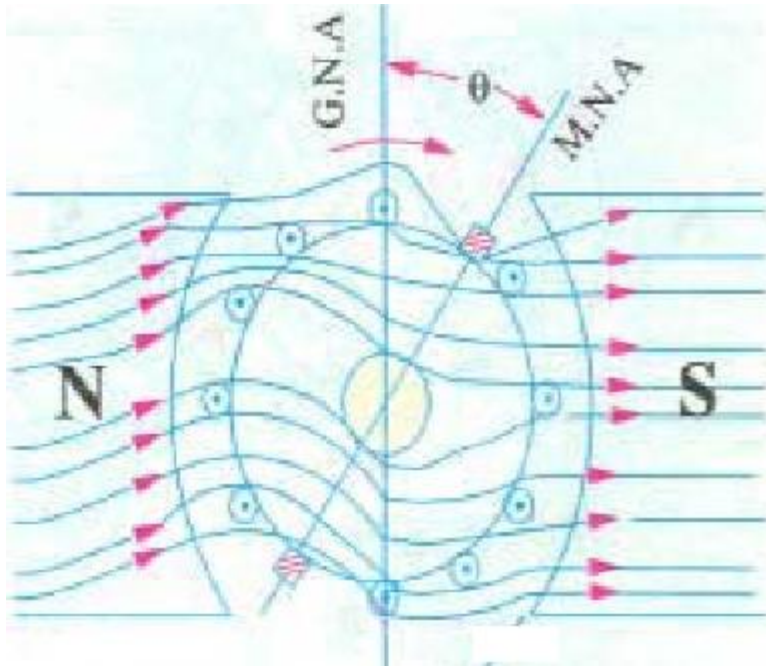
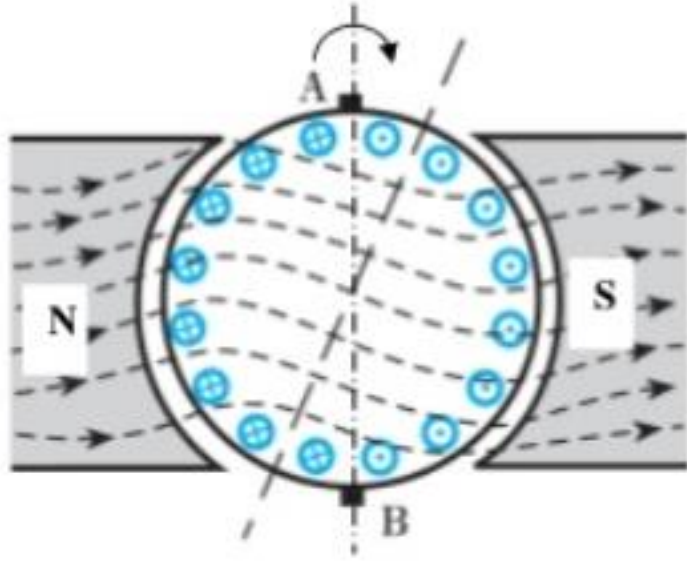
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Electrical Machines

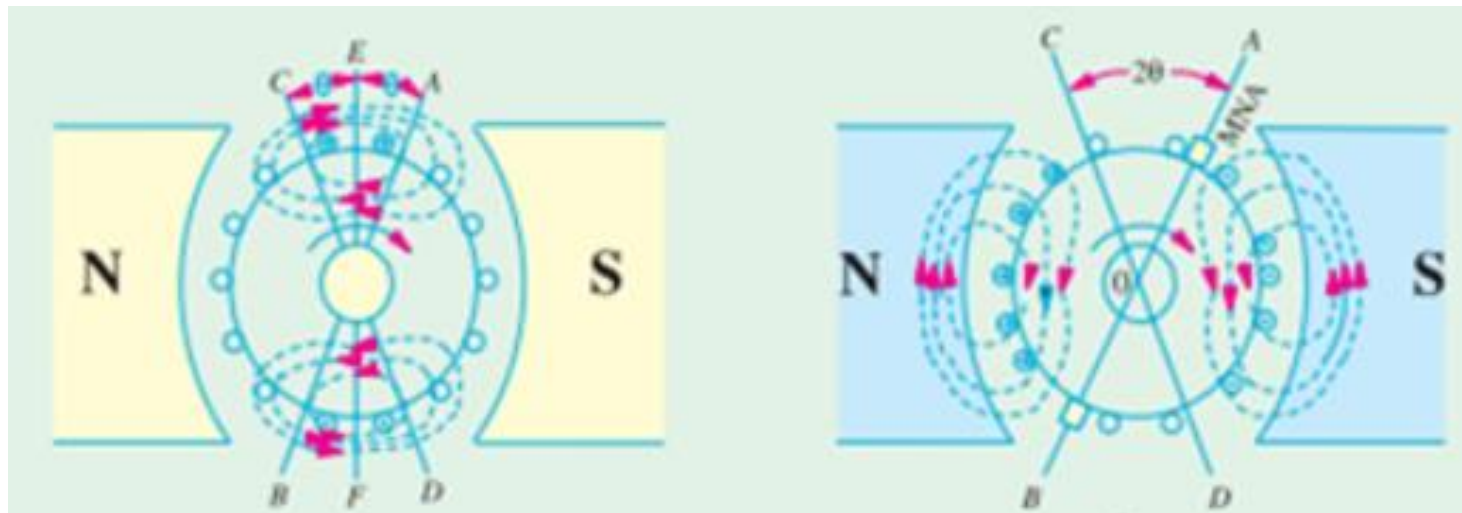
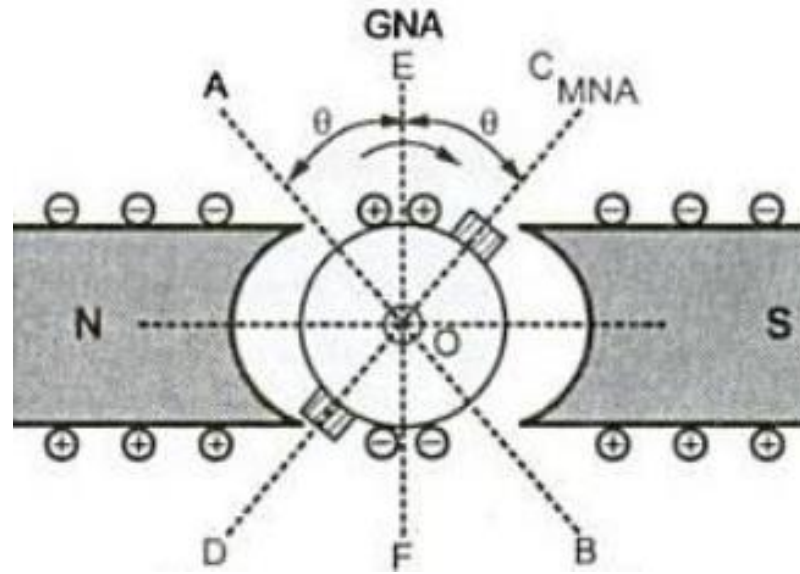
Lecture # 6

Dr Atiqur Rahman

Resultant Flux



Demagnetizing & Cross-magnetizing conductors



Demagnetizing Effect

Let

Z = Total number of armature conductors

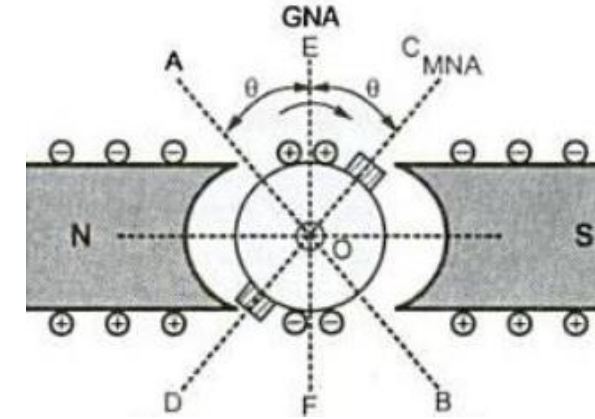
P = Number of poles

I = Armature conductor current in Amperes

= $I_a/2$ for simplex wave winding

= I_a/P for simplex lap winding

θ_m = Forward lead of brush in mechanical degrees.



Total number of armature conductors lying in angles AOC and BOD = $\frac{4\theta_m}{360} \times Z$

Since two conductors from one turn, **Total number of turns in these angles** = $\frac{1}{2} \cdot \frac{4\theta_m}{360} \times Z = \frac{2\theta_m}{360} \times Z$

$$\text{Demagnetising amp-turns} = \frac{2\theta_m}{360} \times IZ$$

$$\text{Demagnetising amp-turns / pole} = \frac{\theta_m}{360} \times IZ$$

$$\boxed{AT_d \text{ per pole} = ZI \times \frac{\theta_m}{360}}$$

Cross-magnetizing Effect

The conductor which are responsible for cross magnetizing ampere turns are lying between the angles AOD and BOC, as shown in the Fig.

Total armature-conductors / pole = Z/P

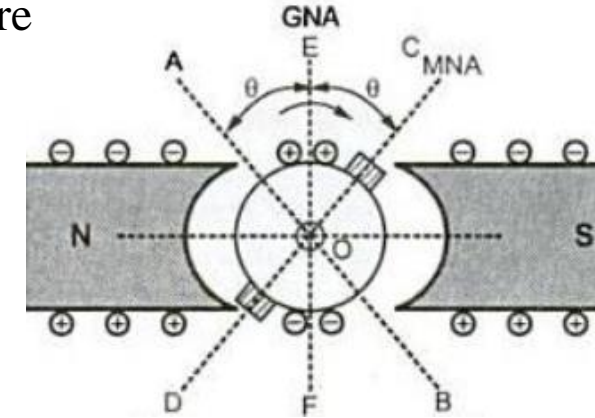
$$\text{Demagnetising conductors / pole} = Z = \frac{2\theta_m}{360}$$

$$\text{Cross magnetising conductors/pole} = \frac{Z}{P} - Z \frac{2\theta_m}{360} = Z \left[\frac{1}{P} - \frac{2\theta_m}{360} \right]$$

$$\text{Cross magnetising amp-conductors / pole} = ZI \left[\frac{1}{P} - \frac{2\theta_m}{360} \right]$$

Since two conductors from one turn,


$$\text{Cross magnetising amp-turns / pole} = \frac{1}{2} \cdot ZI \left[\frac{1}{P} - \frac{2\theta_m}{360} \right] = ZI \left[\frac{1}{2P} - \frac{\theta_m}{360} \right]$$

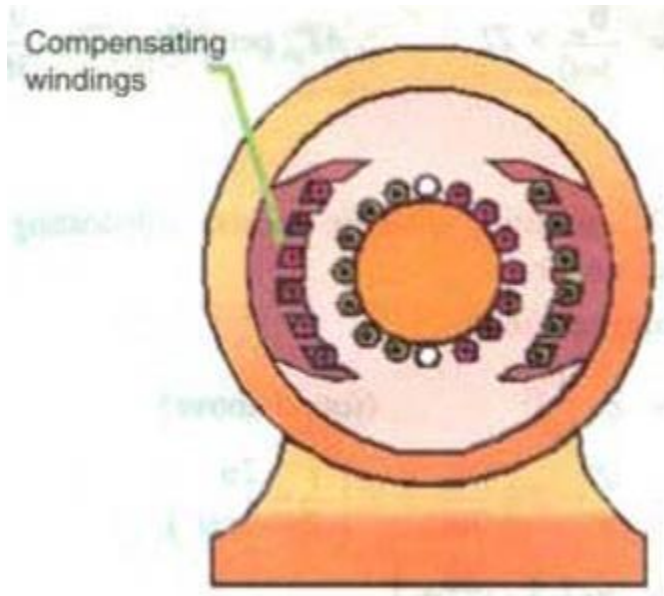


$$\text{AT}_c \text{ per pole} = ZI \left[\frac{1}{2P} - \frac{\theta_m}{360} \right]$$

Remedy for De/Cross-Magnetizing Effect

✓ Demagnetizing effect  Additional field turns

✓ Cross-Magnetizing effect  Compensating winding



Compensating winding

Compensating Winding (CW)

- Windings are embedded in slots in the pole shoe and are connected in series with the armature.
- Used for large DC machines which are subject to large fluctuations in load.
- In the absence of compensating winding, the flux will be shifting forward and backward with every change in load.
- This change in flux causes statically induced emf in armature coil and thus results in **sparking between commutator segments**.

Problem # 1

A 4-pole generator has a wave-wound armature with 722 conductors, and it delivers 100 A on full load. If the brush lead is 8° , calculate the armature demagnetising and cross-magnetising ampere turns per pole.

$$I = I_a / 2 = 100 / 2 = 50 \text{ A}; Z = 722; \theta_m = 8^\circ$$

$$AT_d / \text{pole} = ZI \cdot \frac{\theta_m}{360} = 722 \times 50 \times \frac{8}{360} = 802$$

$$\begin{aligned} AT_c / \text{pole} &= ZI \cdot \left(\frac{1}{2P} - \frac{\theta_m}{360} \right) \\ &= 722 \times 50 \left(\frac{1}{2 \times 4} - \frac{8}{360} \right) = 37/8 \end{aligned}$$

Problem # 2

An 8-pole generator has an output of 200 A at 500 V, the lap-connected armature has 1280 conductors, 160 commutator segments. If the brushes are advanced 4-segments from the no-load neutral axis, estimate the armature demagnetizing and cross-magnetizing ampere-turns per pole.

$$I = 200/8 = 25 \text{ A}, Z = 1280, \theta_m = 4 \times 360 / 160 = 9^\circ ; P = 8$$

$$AT_d / \text{pole} = ZI\theta_m/360 = 1280 \times 25 \times 9/360 = 800$$

$$AT_c / \text{pole} = ZI \left(\frac{1}{2p} - \frac{\theta_m}{360} \right) = 1280 \times 25 \left(\frac{1}{2 \times 8} - \frac{9}{360} \right) = 1200$$

Problem # 3

A 4-pole generator supplies a current of 143 A. It has 492 armature conductors (a) wave-wound (b) lap-wound. When delivering full load, the brushes are given an actual lead of 10° . Calculate the demagnetising amp-turns/pole. This field winding is shunt connected and takes 10 A. Find the number of extra shunt field turns necessary to neutralize this demagnetisation.

$$Z = 492 ; \theta_m = 10^\circ ; AT_d / \text{pole} = Z I \times \frac{\theta_m}{360}$$

$$I_a = 143 + 10 = 153 \text{ A} ; I = 153/2 \quad (\text{wave winding})$$
$$= 153/4 \quad (\text{Lap winding})$$

$$(a) \therefore AT_d / \text{pole} = 492 \times \frac{153}{2} \times \frac{10}{360} = 1046 \text{ AT}$$

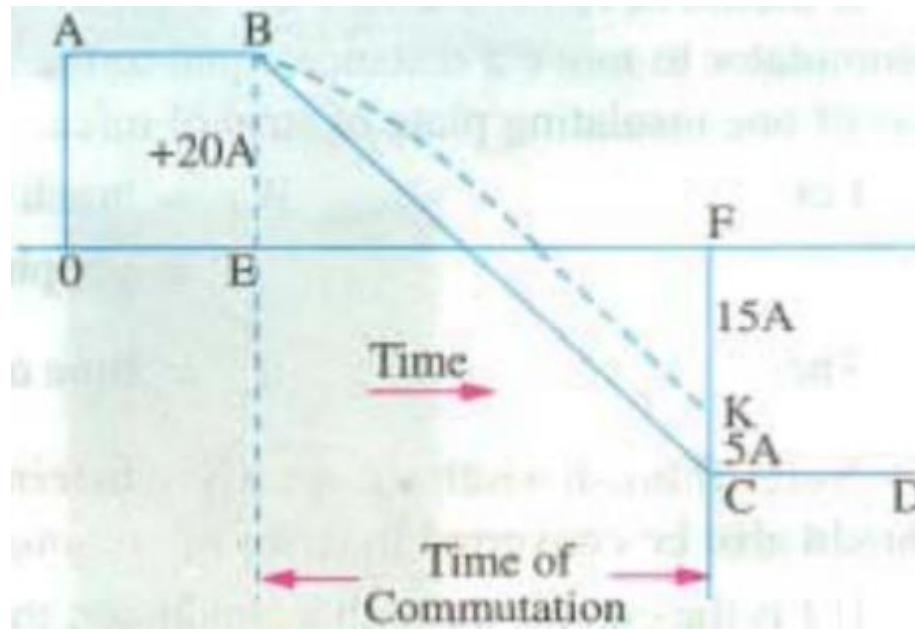
$$\text{Extra shunt field turns} = 1046/10 = 105 \text{ (approx.)}$$

$$(b) AT_d / \text{pole} = 492 \times \frac{153}{4} \times \frac{10}{360} = 523$$

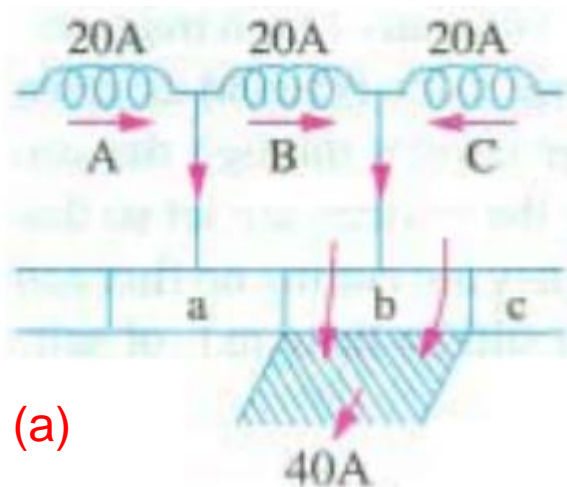
$$\text{Extra shunt field turns} = 523/10 = 52 \text{ (approx.)}$$

Problem in Commutation

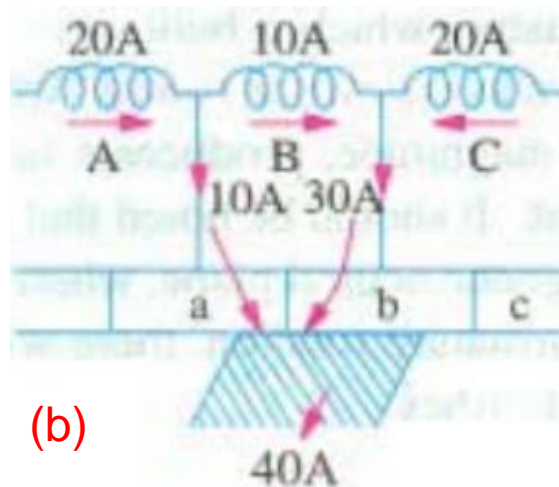
- ✓ The process by which the current in the short circuited coil is reversed while it crosses the MNA is called **commutation**.
- ✓ Time taken to complete the process is called **commutation period**.
- ✓ If current reversal is not complete by that time, sparking occurs between brush and commutator segment



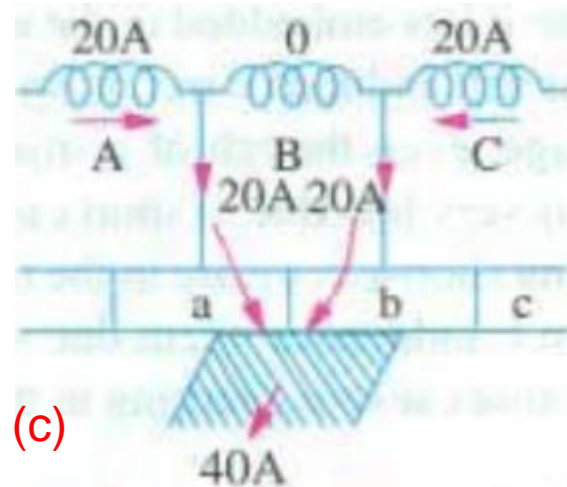
Commutation problem demonstration



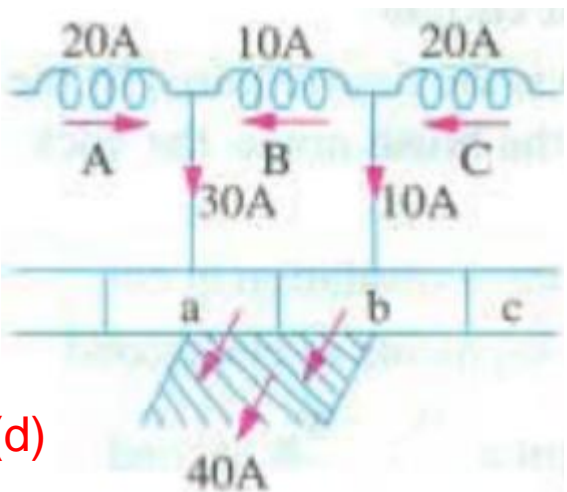
(a)



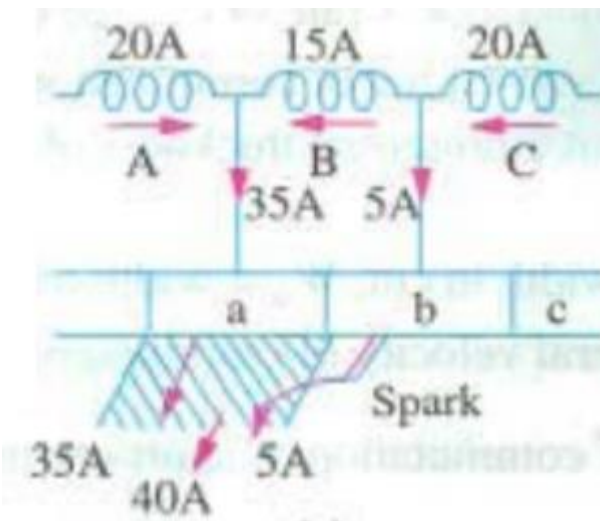
(b)



(c)



(d)



(e)

Cause of Commutation problem

- ✓ Self induced emf in the armature coil that prevents currents from reversing on time.
- ✓ Or, the inductive property of the armature coil prevents current from reversing.

Techniques to improve commutation

- i. Resistance commutation
- ii. EMF commutation

Resistance commutation

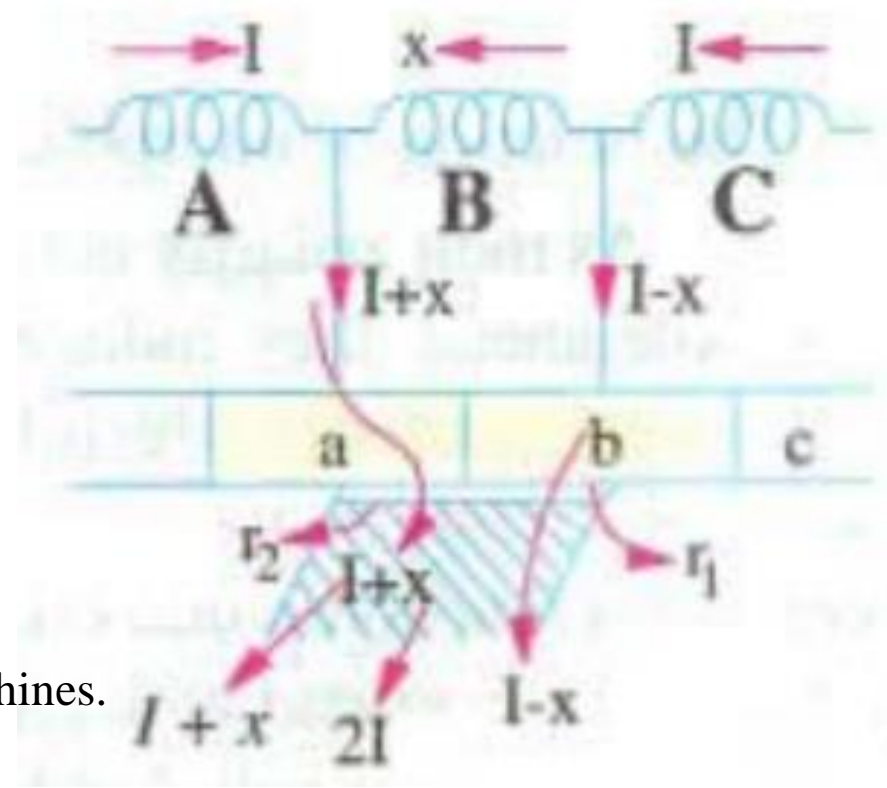
- This method of improving commutation involves replacing low resistance **Cu brush** with high-resistance **Carbon brush**.

Additional advantage

- ✓ Self-lubricating to some degree.
- ✓ Should sparking occurs they damage commutator less

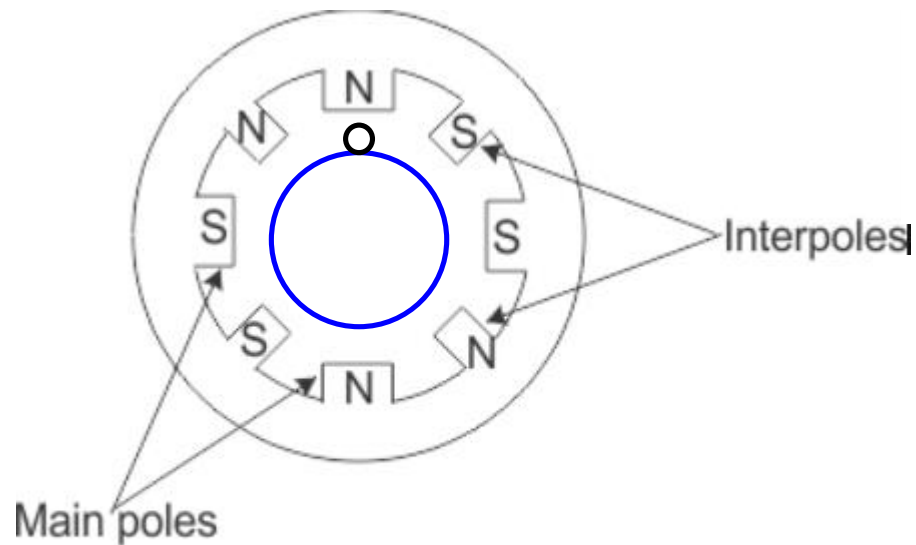
Disadvantage

- Due to high resistance they are not suitable for smaller machines.
- Commutator has be made somewhat larger.
- Need larger brush holder



EMF Commutation

- Involves inserting smaller poles (called **Interpoles**) in between the main poles.
- Their job is to start the current **reversal process a bit earlier**.
- Interpoles are also called **Compoles**.



Interpole Commutation

